

IOWA DEPARTMENT OF TRANSPORTATION

TO OFFICE: Bridges and Structures

DATE: January 19, 2012

ATTENTION: D. R. Claman

REF. NO. Woodbury County

FROM: Paul W. Flattery

Proj. No. NHSX-020-1(116)--3H-97

PIN: 98-97-020-010-01

OFFICE: Design

SUBJECT: Culvert Submittal (D3) – REVISED 2

This project involves grading of the westbound lanes on US 20 from east of Merville continued east to just west of Correctionville. Traffic will be maintained via staging. The reason for this revision was due to the change of the alignment from approximately Sta. 10750+00 to Sta. 10834+00 to eliminate the impact to the 4F on the south side and to improve constructability.

The Project Directory is W:\Projects2\97020050A98\Design\Section1. No printed plan sheets or cross sections are included with this submittal. Items included in the electronic files with this submittal are tabulated on the “D3 Check List.” The MicroStation and GEOPAK files, chains, and profiles are described in (“NHSX-020-1(116)--3H-97_Project Documentation.xls”).

By copy of this letter, the Office of Location and Environment is requested to make any necessary reviews.

The Bridge submittal (B1) is scheduled for 2/15/2012. The Right of Way submittal (D5) is scheduled for 3/15/2012. The current letting date is 07/15/2014.

You may indicate your acceptance or request additional information by e-mail.

PWF:mk

Attach.

cc: M. J. Kennerly	N. L. McDonald
D. E. Ohman	G. A. Novey
K. D. Nicholson	J. P. Rost
R. L. Stanley	L. C. Funnell
Judy Lensing	S. C. Marler
M. J. Sankey	T. Crouch
T. Gettings	E.C. Wright
D. A. Widick	B. Bradley
M. A. Swenson	J. W. Smith
J. McCollough	J. Vortherms
Tony Lazarowicz	Shane Tymkowicz
Doug Manley	

D3 Check List

Updated Field Exam Plans including:

Typicals reviewed for correct dimensions, and stationing.

- Main Line
- Side roads
- Accessways
- Interchange Ramps & Loops

D, E, F & K sheets updated for Field Exam changes.

- Horizontal and vertical alignments, including stationing and tic marks.
- Ditch bar graph and ditch grades
- Entrances and crossovers (future labeled as future)
- Auxiliary and turn lanes including tapers.
- Final Interchange layouts and details
- Staging or Detour Runarounds.

Cross Sections (Design files)

- Mainline
- Side road
- Accessways
- Ramps and loops
- Detour runarounds or staging details
- Draw sections, at box culvert locations
- Skewed culvert locations (3 cross sections minimum, 1 on skew and 1 at each end of skewed culvert, perpendicular to centerline)
- Estimate of Stability berm and backslope benching locations
- Auxiliary and turn lanes including tapers
- Entrances

Pipe culvert layouts with type, size and location of culvert from Field Exam; including station/elevations for centerline, hinge point, flow lines and length of the culverts.

- A copy of the PDF of the plans has been created, printed and checked to make sure the plans print appropriately.

WOODBURY CO.

LETTING DATE **7/15/2014**
NHSX-020-1(116)--3H-97

INDEX OF SHEETS	
No.	DESCRIPTION
A Sheets	Title Sheets
A.1	Title Sheet
A.2	Location Map
B Sheets	Typical Cross Sections and Details
B.1 - 6	Typical Cross Sections and Details
D Sheets	Mainline Plan and Profile Sheets
* D.1	Legend and Symbol Information Sheet
* D.2 - 49	Mainline - US 20
E Sheets	Side Road Plan and Profile Sheets
* E.1	Jasper Avenue
* E.2 - 3	Jewell Avenue
* E.4	Knox Avenue
* E.5	Kossuth Avenue
* E.6	Lee Avenue
* E.7 - 8	Lucas Avenue
* E.9	Lenox Avenue
* E.10	Minnesota Avenue
* E.11	Mason Avenue
J Sheets	Traffic Control and Staging Sheets
* J.1	Stage 1 & 2
* J.2	Stage 3 & 4
* J.3	Final Stage
* Color Plan Sheets	



Iowa Department of Transportation
Highway Division

PLANS OF PROPOSED IMPROVEMENT ON THE
PRIMARY ROAD SYSTEM
WOODBURY COUNTY
GRADING

US 20 From E. of Moville E. to W. of Correctionville

SCALES: As Noted

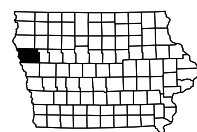
Refer to the Proposal Form for list of applicable specifications.

Value Engineering Saves. Refer to Article 1105.15 of the Specifications.



MILEAGE SUMMARY			
			105-1
			09-27-94
Div.	Location	Lin. Ft.	Miles
1	Sta. 10219+00.00 - Sta. 10820+00.00	60,100	11.38
Total		60,100	11.38

For Project Location Map
Refer to Sheet A.2



DESIGN DATA RURAL			
2019 AADT	4,700	V.P.D.	
2039 AADT	6,200	V.P.D.	
2039 DHV	640	V.P.H.	
TRUCKS	22	%	
Total			
Design ESALs	--		

INDEX OF SEALS		
SHEET NO.	NAME	TYPE
A.1	Paul Flattery	Primary Signature Block

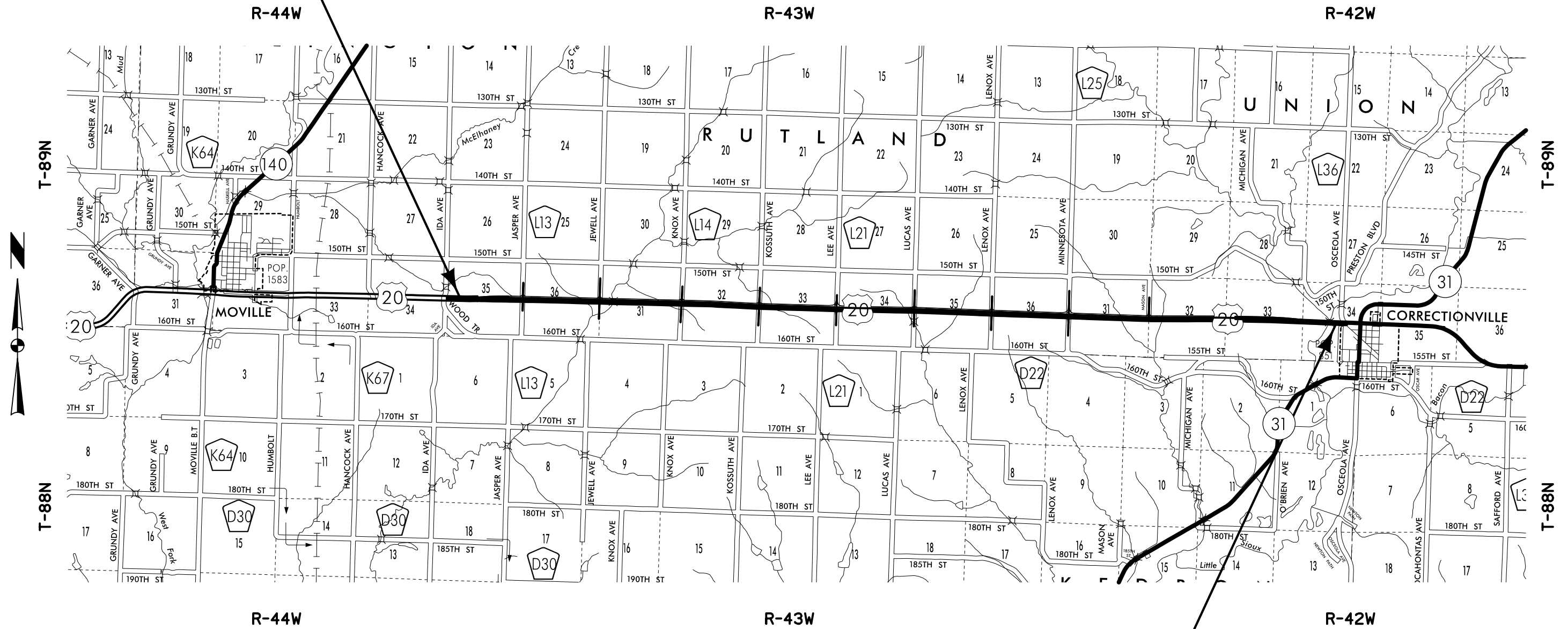
D3 Submittal 10-03-2011
D5 Submittal 02-10-2012
Letting Date 07-15-2014

PRELIMINARY PLANS
Subject to change by final design.
D3 PLAN - Date: 10/03/2011

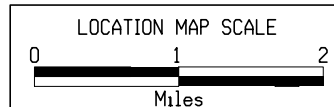
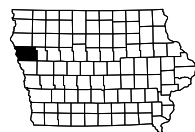
REVISIONS	TOTAL
	71

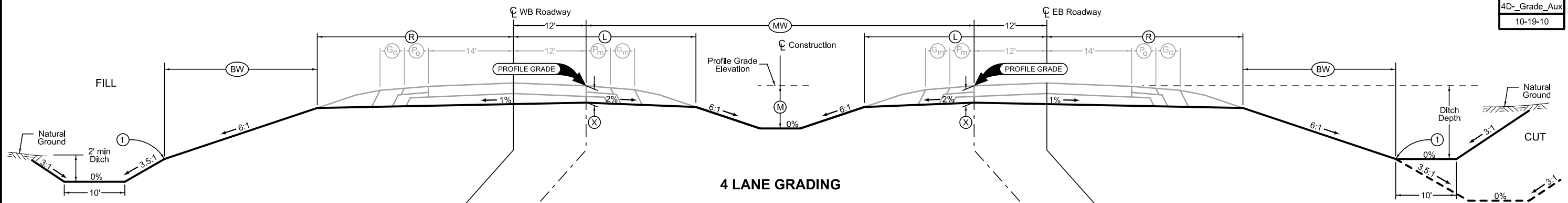
PROJECT IDENTIFICATION NUMBER	98-97-020-010-01
PROJECT NUMBER	NHSX-020-1(116)--3H-97
R.O.W. PROJECT NUMBER	NHSN-020-1(080)--2R-97

STA. 10219+00.00
BEGIN PROJECT
MP 21.50

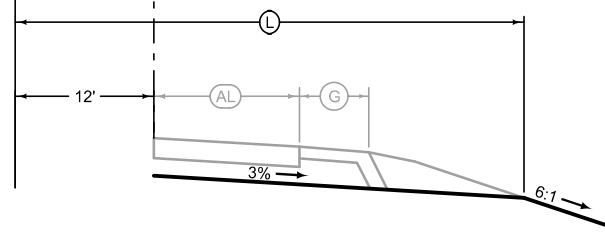


STA. 10820+00.00
END PROJECT
MP 32.50



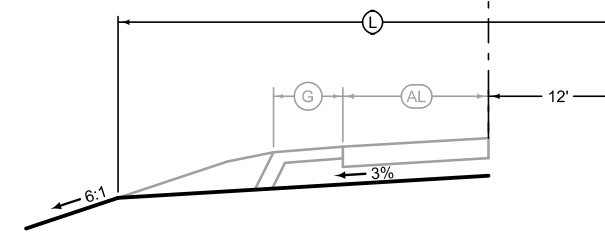


LOCATION		DIMENSIONS						
ROAD IDENTIFICATION	STATION TO STATION	L Feet	R Feet	X Inches	BW Feet	MW Feet	M Feet	
US 20	10253+00.00	28.09	32.09	16.00	19.59	82.00	4.00	
US 20	10769+00.00	28.09	32.09	16.00	19.59	82.00-16.00	4.00-0	



Auxiliary Lane Grading

LOCATION			L
ROAD IDENTIFICATION	STATION TO STATION		Feet
US 20	10263+96.00	10266+76.00	41.27
US 20	10316+80.00	10319+60.00	41.27
US 20	10372+45.00	10375+25.00	41.27
US 20	10425+40.00	10428+20.00	41.27
US 20	10478+38.00	10481+18.00	41.27
US 20	10531+18.00	10533+98.00	41.27
US 20	10584+00.00	10586+80.00	41.27
US 20	10636+60.00	10639+40.00	41.27



Auxiliary Lane Grading

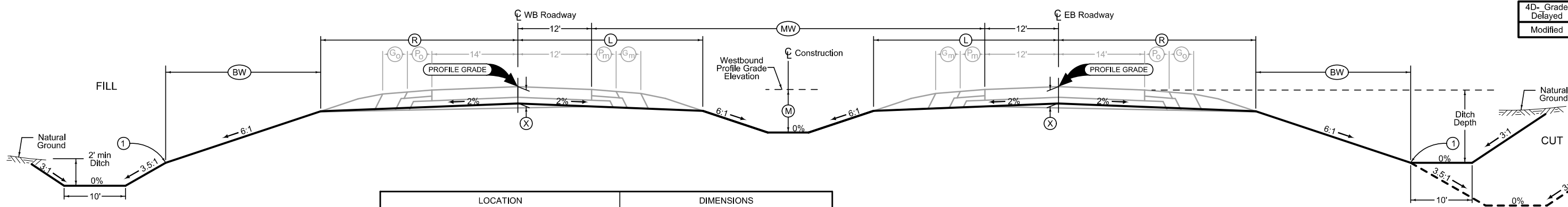
LOCATION			L
ROAD IDENTIFICATION	STATION TO STATION		Feet
US 20	10259+40.00	10262+20.00	41.27
US 20	10312+20.00	10315+00.00	41.27
US 20	10367+85.00	10370+65.00	41.27
US 20	10420+80.00	10423+60.00	41.27
US 20	10473+78.00	10476+58.00	41.27
US 20	10526+58.00	10529+38.00	41.27
US 20	10579+40.00	10582+20.00	41.27
US 20	10632+00.00	10634+80.00	41.27
US 20	10686+48.00	10689+28.00	41.27

Normal section shown may be modified appropriately in areas of superelevated curves or other locations specifically designated by the Engineer.

See Plan & Profile sheets and cross sections for additional details of ditches and backslopes.

① Refer to project plan and cross sections for specific location of foreslope change.

US 20
Mainline



4D- Grade Delayed Modified

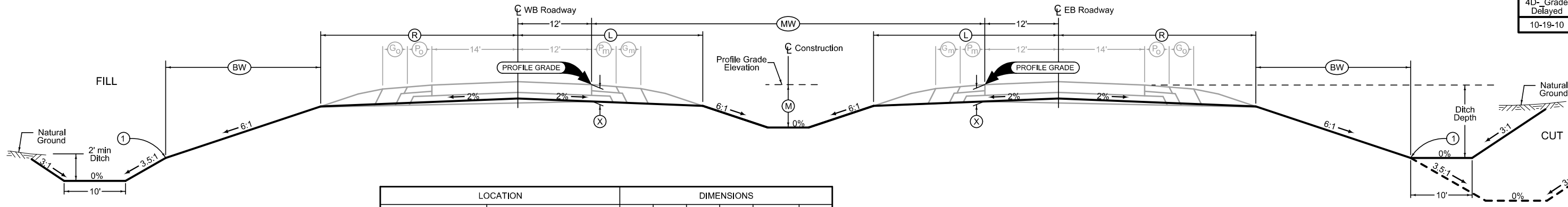
Normal section shown may be modified appropriately in areas of super-elevated curves or other locations specifically designated by the Engineer.

See Plan & Profiles sheets and cross sections for additional details of ditches and backslopes.

① Refer to project plan and cross sections for specific location of foreslope change.

ROAD IDENTIFICATION	LOCATION		DIMENSIONS						
	STATION TO STATION		L Feet	R Feet	X Inches	BW Feet	MW Feet	M Feet	
US 20 (WB)	20219+00.00	20253+00.32	28.09	31.82	16.00	19.86	60.00-82.00	4.00	
US 20 (EB)	30219+00.00	30252+99.70	28.09	31.82	16.00	19.86	60.00-82.00	4.00	

4 LANE GRADING (Delayed Paving)



4D- Grade Delayed 10-19-10

Normal section shown may be modified appropriately in areas of super-elevated curves or other locations specifically designated by the Engineer.

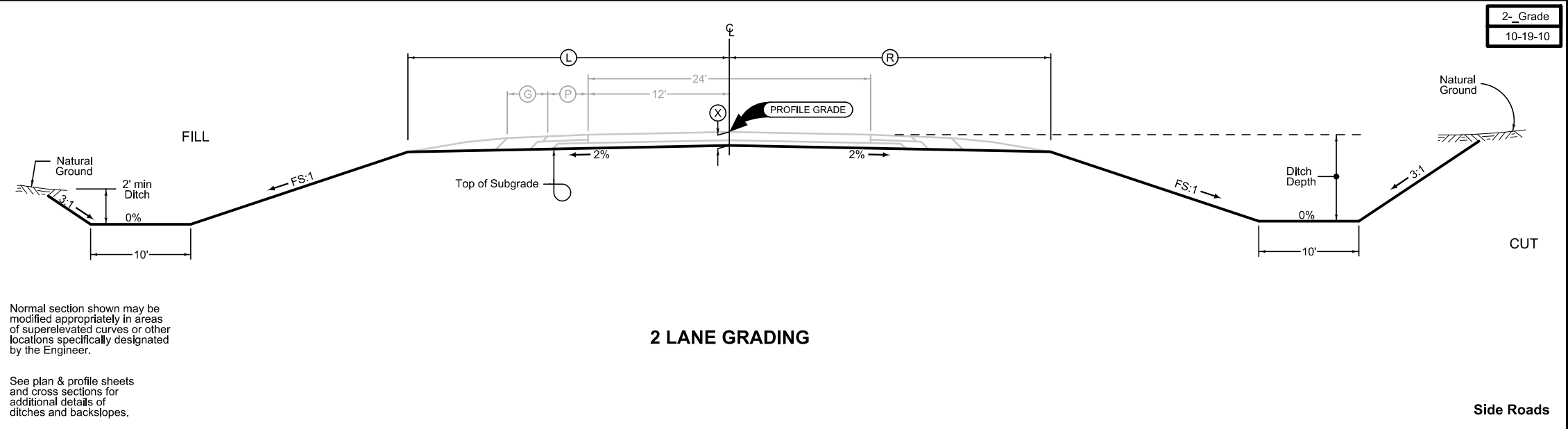
See Plan & Profiles sheets and cross sections for additional details of ditches and backslopes.

① Refer to project plan and cross sections for specific location of foreslope change.

ROAD IDENTIFICATION	LOCATION		DIMENSIONS						
	STATION TO STATION		L Feet	R Feet	X Inches	BW Feet	MW Feet	M Feet	
US 20	10253+00.00	10769+00.00	28.09	31.82	16.00	19.86	82.00	4.00	
US 20	10769+00.00	10820+00.00	28.09	31.82	16.00	19.86	82.00-16.00	4.00-0	

4 LANE GRADING (Delayed Paving)

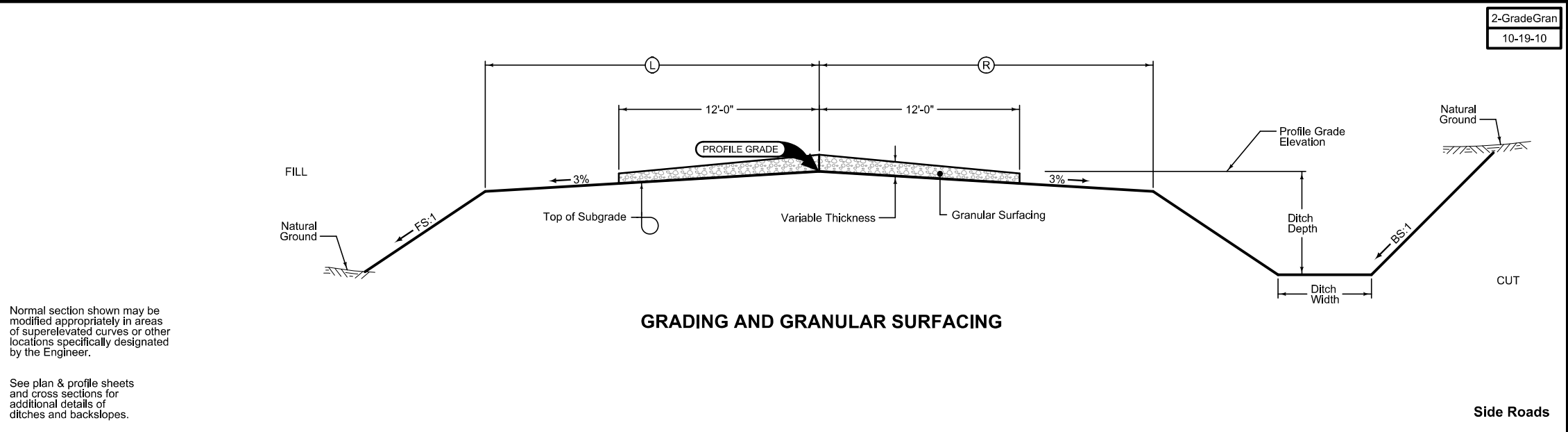
LOCATION		DIMENSIONS			
ROAD IDENTIFICATION	STATION TO STATION	(L) Feet	(R) Feet	(X) Inches	FS
Lee Avenue	507+00.00 515+50.00	24.85	24.85	16.00	3
Minnesota Avenue	804+00.00 824+25.00	24.85	24.85	16.00	3



2-Grade
10-19-10

Side Roads

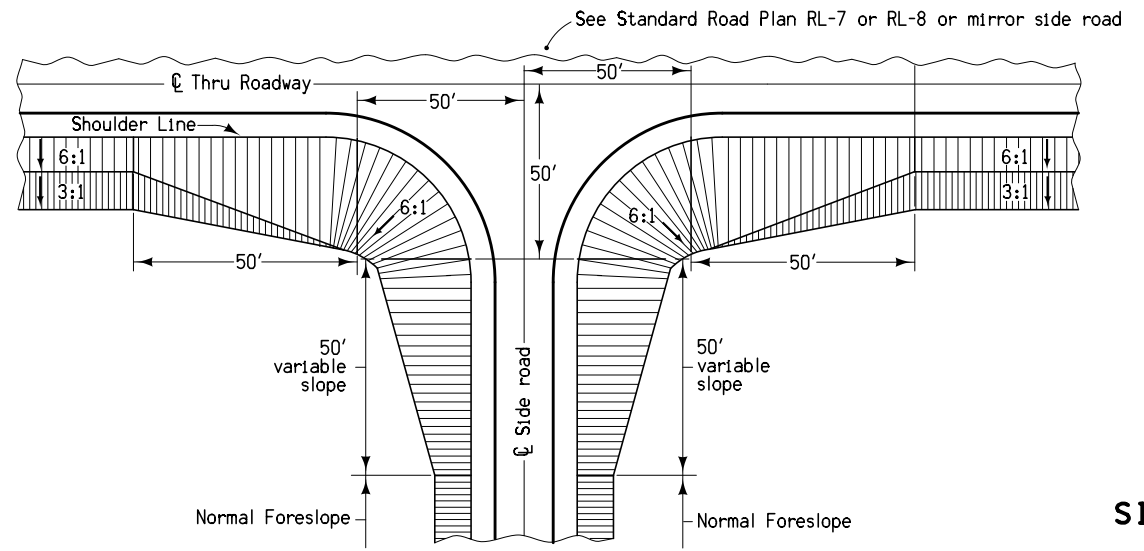
LOCATION		DIMENSIONS			
ROAD IDENTIFICATION	STATION TO STATION	(L) Feet	(R) Feet	FS	BS
Jasper Avenue	114+25.00 122+00.00	15.00	15.00	3	3
Jewell Avenue	208+00.00 220+25.00	15.00	15.00	3	3
Knox Avenue	305+50.00 318+00.00	15.00	15.00	3	3
Kossuth Avenue	404+50.00 419+00.00	15.00	15.00	3	3
Lucas Avenue	606+00.00 622+50.00	15.00	15.00	3	3
Lenox Avenue	707+50.00 718+25.00	15.00	15.00	3	3
Mason Avenue	900+34.39 913+75.00	15.00	15.00	3	3



2-GradeGran
10-19-10

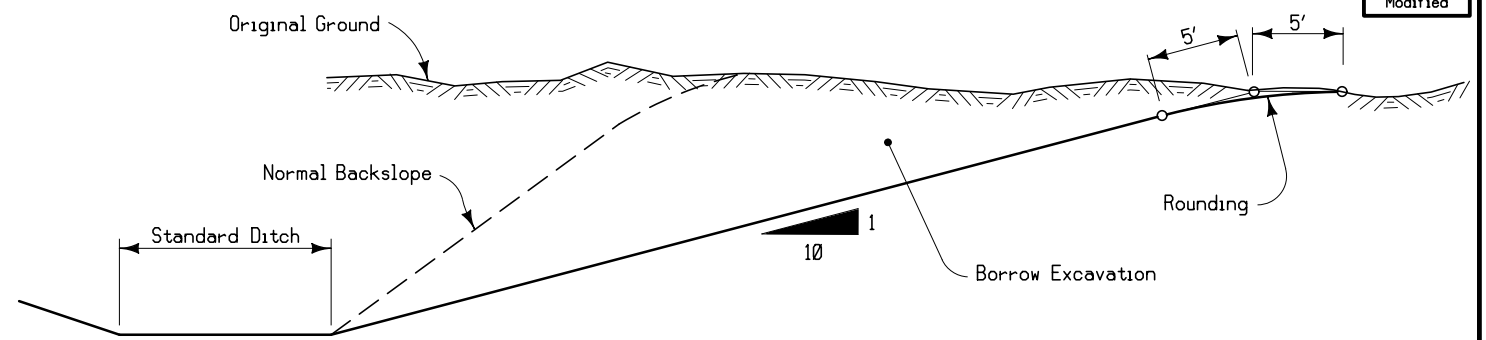
Side Roads

2117
04-15-08



SIDE ROAD GRADING (BARNROOF)

4109
Modified



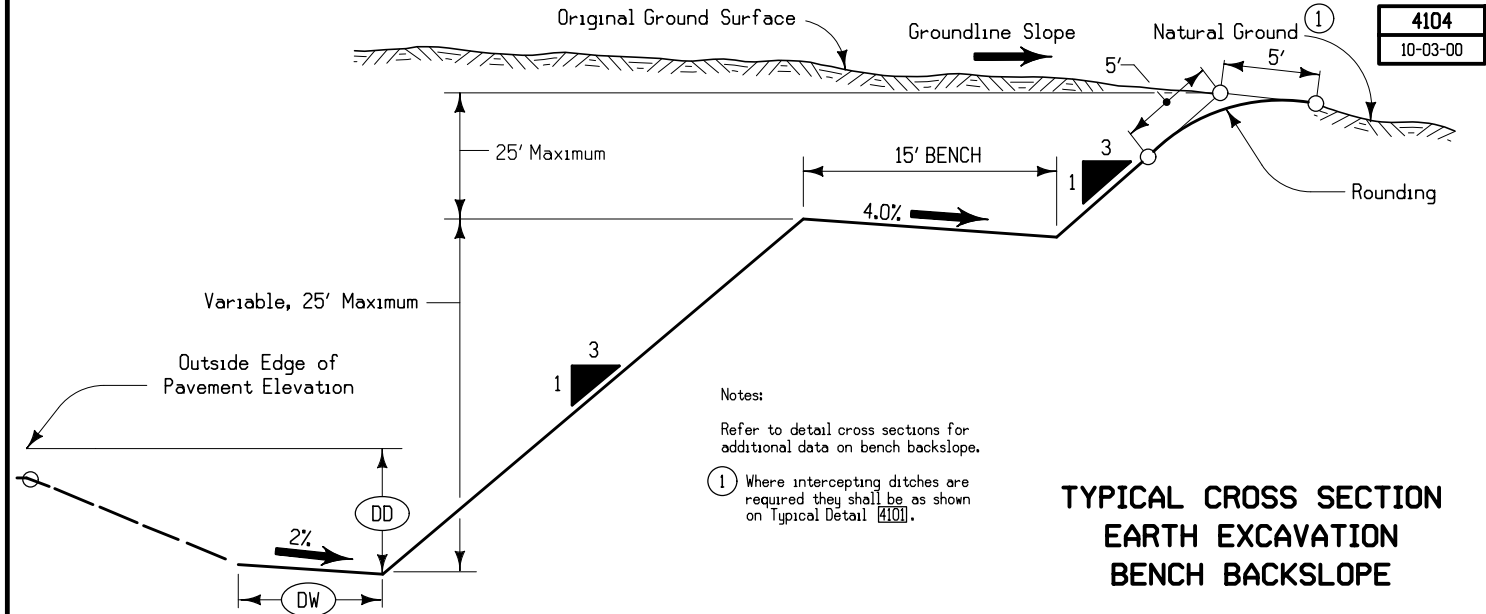
Notes:

Borrow backslope shall be used at those locations shown on plans or specifically required by the engineer.

Where intercepting ditches are required they shall be as shown on 4101.

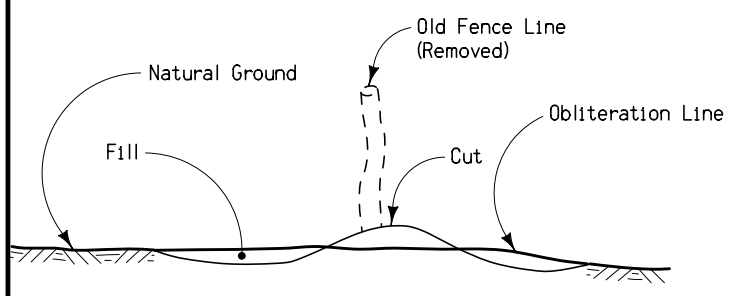
TYPICAL CROSS SECTION SNOW BORROW

4104
10-03-00



TYPICAL CROSS SECTION EARTH EXCAVATION BENCH BACKSLOPE

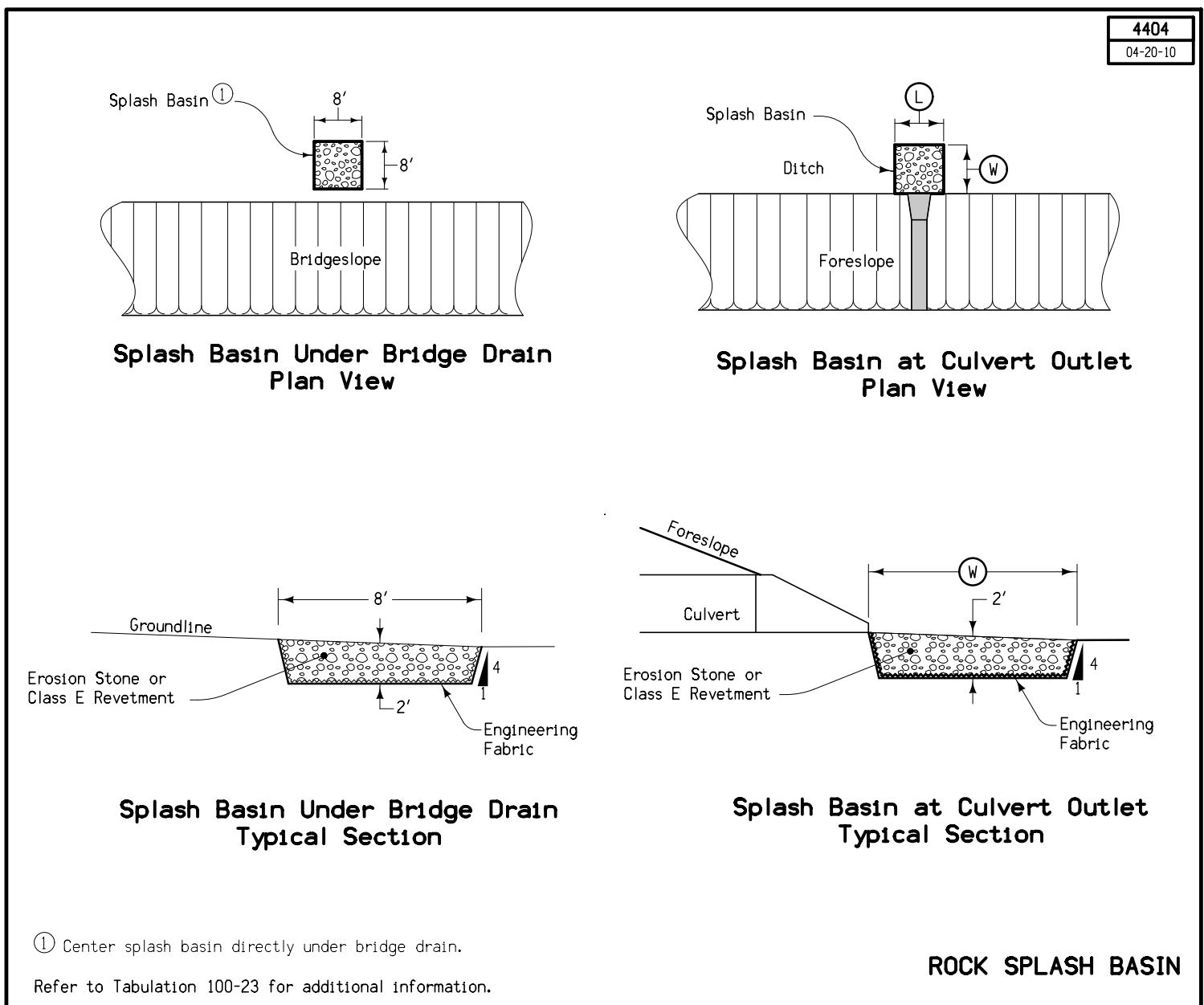
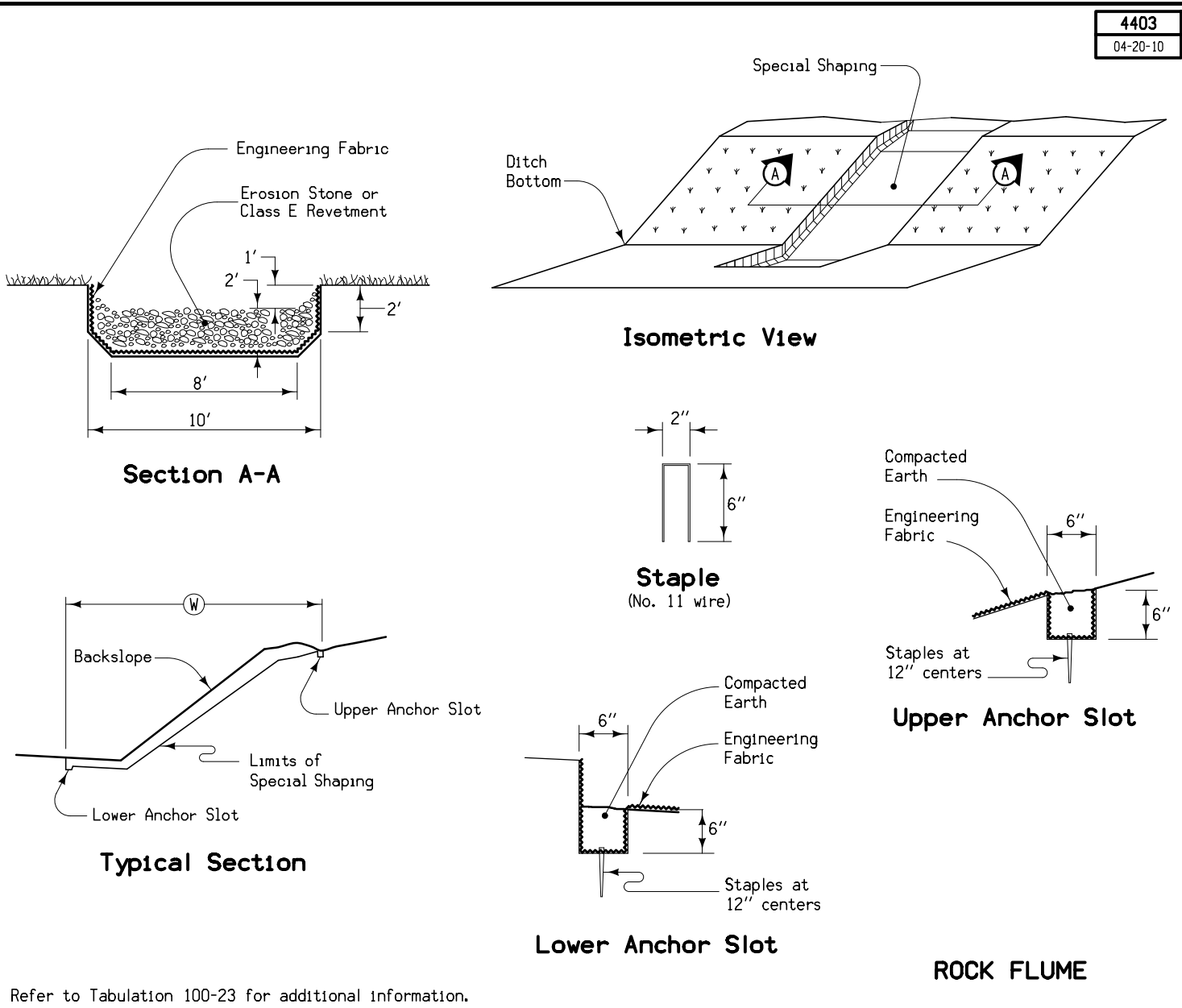
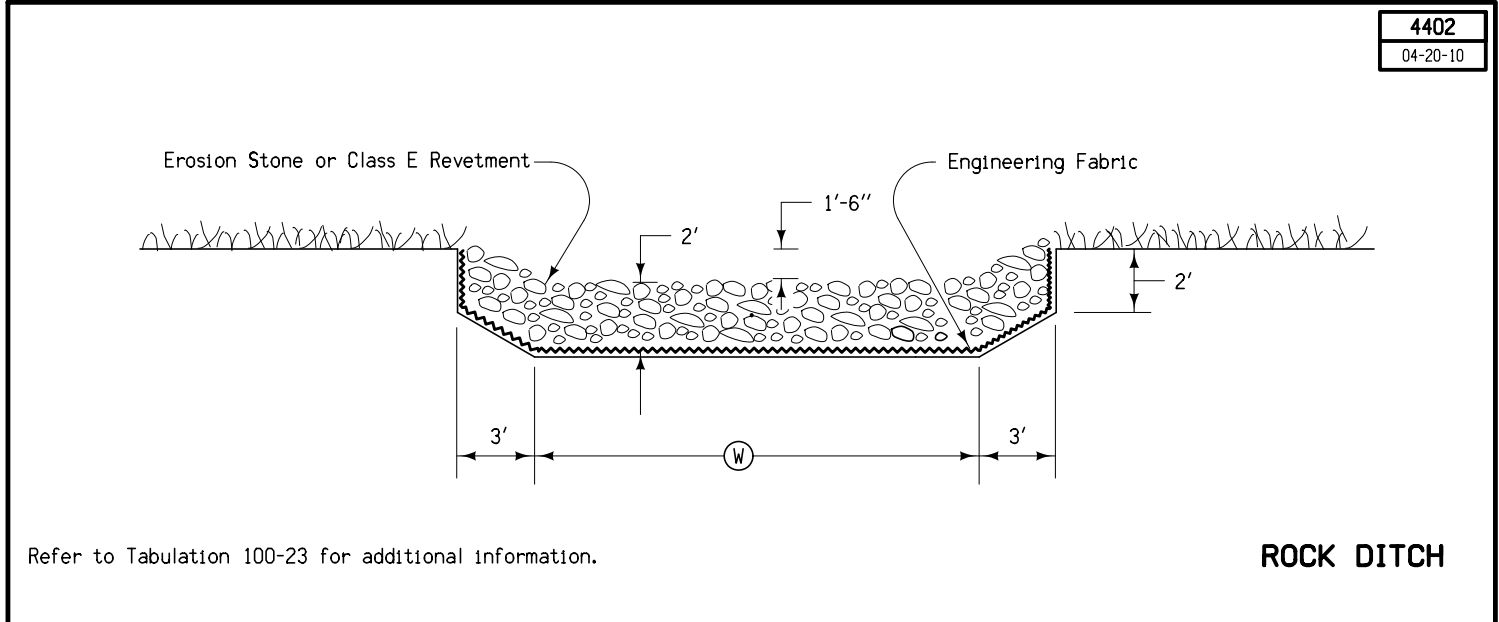
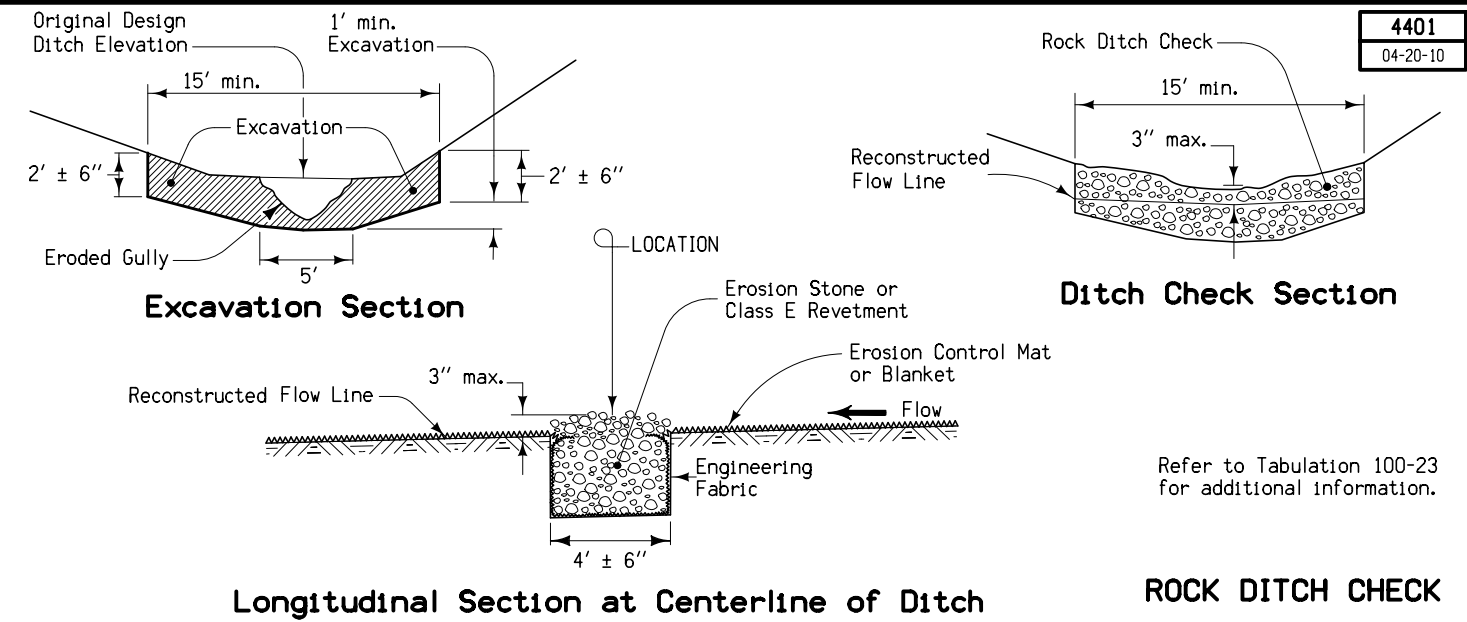
4301
08-20-96



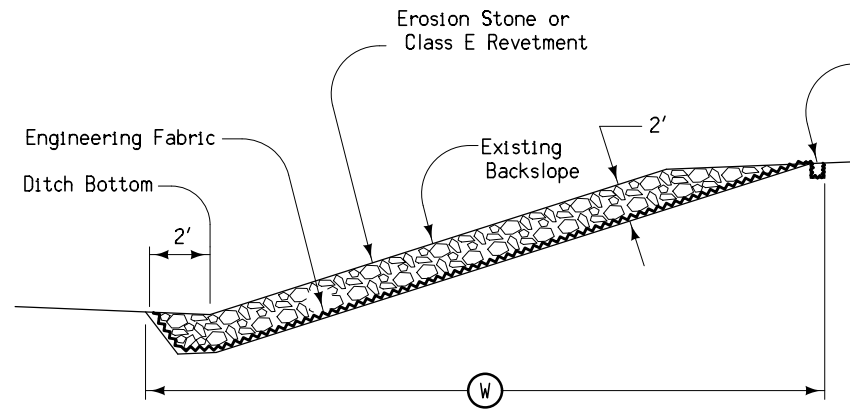
TYPICAL DETAILS FOR OBLITERATION OF OLD FENCE RIDGE

Notes:

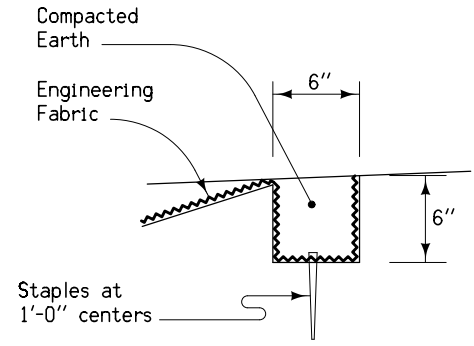
The work of obliterating or reshaping old fence ridges shall be done at the direction of the Engineer.



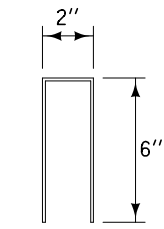
4405
04-20-10



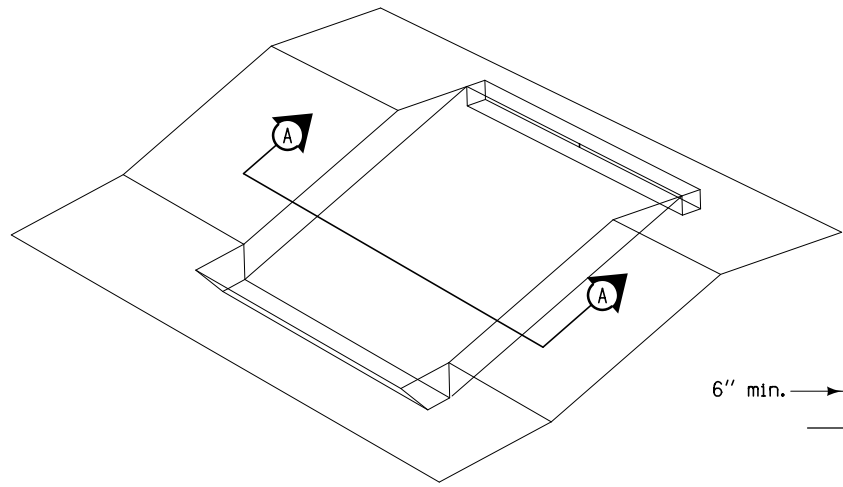
Typical Section



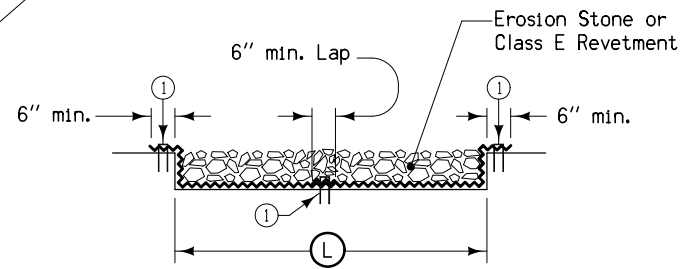
Anchor Slot



Staple
(No. 11 wire)



Isometric View



Section A-A

ROCK SLOPE PROTECTION

① Staples at 12" centers
Refer to Tabulation 100-23 for additional information.

SURVEY SYMBOLS

- x — FW Wire Fence
- TP TPD Telephone Pedestal
- UB UB Utility Box
- Tile — TIL Tile Line
- OUT Tile Outlet
- ⊙ BIN Grain Bin
- PPA Power Pole Co. 1
- GDL Guard Rail (Rail and Cable)
- MM MM Mile Marker Post
- PR Electric Riser Pole
- FWD Wood Fence
- RET Retaining Walls
- ⊕ MH Utility Access (Manhole)
- COR Round Bridge Pier Column
- COS Square Bridge Pier Column
- ⊕ INB Storm Sewer Beehive Intake
- EB EB Electrical Box
- ⊕ WEL Well
- ⊕ PPB Power Pole Co. 2
- WH WHD Water Hydrant
- ⊕ LP L.P. Tank
- ⊕ SEP Septic Tank
- ⊕ AST Above Ground Storage Tank
- SIGN SI Sign
- FLG FLG Flag Poles
- ⊕ TV Satellite TV Dish
- ⊕ CIS Cistern
- ⊕ UST Underground Tank
- GP GP Guard Post (Less Than 4 Posts)
- LUM Luminaire
- ENT Centerline BL of Entrance
- ← DU Centerline Draw or Stream (Up)
- D Centerline Draw or Stream (Down)
- EW Edge of Water
- BNK Stream Bank
- DIK Centerline of Dike or Dam
- ⊕ IN Storm Sewer Intake
- ▲ RIP Rip-Rap
- T3 — TLC Underground Telephone Line Co. 3
- F0 — FOA Underground Fiber Optic Co. 1
- F05 — FOE Underground Fiber Optic Co. 5
- F02 — FOB Underground Fiber Optic Co. 2
- T2 — TLB Underground Telephone Line Co. 2
- T1 — TLA Underground Telephone Line Co. 1
- E1 — ELA Underground Electric Line Co. 1
- ROW Right of Way Rail
- BB BB Billboard
- TDC Tree Deciduous
- SIGN SL Speed Limit Sign
- # — FCL Chain Link and Security Fence
- San.1 — SAA Sanitary Sewer Line Co. 1
- ✱ TEV Evergreen Tree
- FHD Fire Hydrants
- T4 — TLD Underground Telephone Line Co. 4
- F04 — FOD Underground Fiber Optic Co. 4
- F03 — FOC Underground Fiber Optic Co. 3
- E2 — ELB Underground Electric Line Co. 2
- ⊕ SHR Shrub
- ⊕ TFR Tree Fruit
- WV WV Water Valve
- W — WLA Underground Water Line Co. 1
- San.2 — SAB Sanitary Sewer Line Co. 2
- HDG Hedge Row
- ⊕ WM Wind Mill
- TLN Treeline
- T1 — TLA Qwest Local Network (B)
- T2 — TLB Frontier Communications (B)
- T3 — TLC Western Iowa Telephone (B)
- T4 — TLD Schaller Telephone Company
- F0 — FOA INS (B)
- F02 — FOB Qwest Communications (B)
- F03 — FOC Comserve (B)
- F04 — FOD McLeod (B)
- F05 — FOE Knology (B)
- E1 — ELA Woodbury Rural Electric (B)
- W — WLA Iowa DOT
- San. — SAA Iowa DOT
- San.2 — SAB City of Correctionville

UTILITY LEGEND

- PPA MidAmerican
- ⊕ PPB Private
- T1 — TLA Qwest Local Network (B)
- T2 — TLB Frontier Communications (B)
- T3 — TLC Western Iowa Telephone (B)
- T4 — TLD Schaller Telephone Company
- F0 — FOA INS (B)
- F02 — FOB Qwest Communications (B)
- F03 — FOC Comserve (B)
- F04 — FOD McLeod (B)
- F05 — FOE Knology (B)
- E1 — ELA Woodbury Rural Electric (B)
- W — WLA Iowa DOT
- San. — SAA Iowa DOT
- San.2 — SAB City of Correctionville

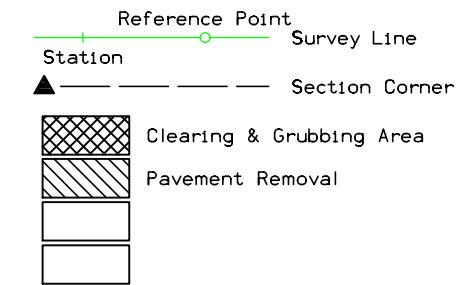
PLAN VIEW COLOR LEGEND OF PLAN AND PROFILE SHEETS

- Green (2) Existing Topographic Features and Labels
- Blue (1) Proposed Alignment, Stationing, Tic Marks, and Alignment Annotation
- Purple (5) Existing Utilities
- Yellow (4) Highlight for Critical Notes or Features
- Red (3) Delineates Restricted Areas
- Lavender (9) Temporary Pavement Shading
- Gray, Light (48) Proposed Pavement Shading
- Gray, Med (80) Proposed Granular Shading
- Gray, Dark (112) Proposed Grade and Pave Shading
- Brown, Light (237) Grading Shading

PROFILE VIEW COLOR LEGEND OF PLAN AND PROFILE SHEETS

- Green (2) Existing Ground Line Profile
- Blue (1) Proposed Profile and Annotation
- Purple (5) Existing Utilities
- Blue, Light (230) Proposed Ditch Grades, Left
- Black (0) Proposed Ditch Grades, Median
- Rust (14) Proposed Ditch Grades, Right

CONVENTIONAL SIGNS



RIGHT-OF-WAY LEGEND

- ▲ Proposed Right-of-Way
- △ Existing Right-of-Way
- ▲ Existing and Proposed Right-of-Way
- ▲ Easement and Existing Right-of-Way
- Borrow
- Easement (Temporary)
- Easement
- X Excess
- |—|—| Property Line
- A/C Access Control

PLAN AND PROFILE LEGEND AND SYMBOL INFORMATION SHEET

(COVERS SHEET SERIES D, E, F, & K)

PROPOSED CULVERT CONCEPTS

- SAME LOCATION AND LEAVE MEDIAN OPEN
- OR
- NEW LOCATION AND LEAVE MEDIAN OPEN
- OR
- SAME LOCATION AND TIE TO OLD
- OR
- NEW LOCATION AND TEMP PIPE EXTENSION
- OR
- JACK AND LAY

Curve Data
 $\Delta = 0^\circ 16' 21.82''$ (LT)
 $T = 300.00$
 $R = 600.00$
 $E = 126,050.48$
 $F = 0.36$

Arlington TWP.
 T-89N R-44
 SEC. 35

Sta. 221+97.88, 42.68 Rt.
 18" X 10.7 Conc Pipe
 D.A. = 2 Ac

Curve Data WB
 $\Delta = 5^\circ 49' 25.13''$ (LT)
 $T = 813.84$
 $R = 1,626.27$
 $E = 16,000.00$
 $F = 20.68$

STA. 20219+00.00 (WB)
 BEGIN PROJECT

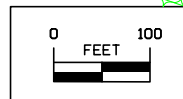
OUTLET FLOW RAISED

Sta. 221+60.58
 24" X 205.2 Conc Pipe
 D.A. = 3 Ac

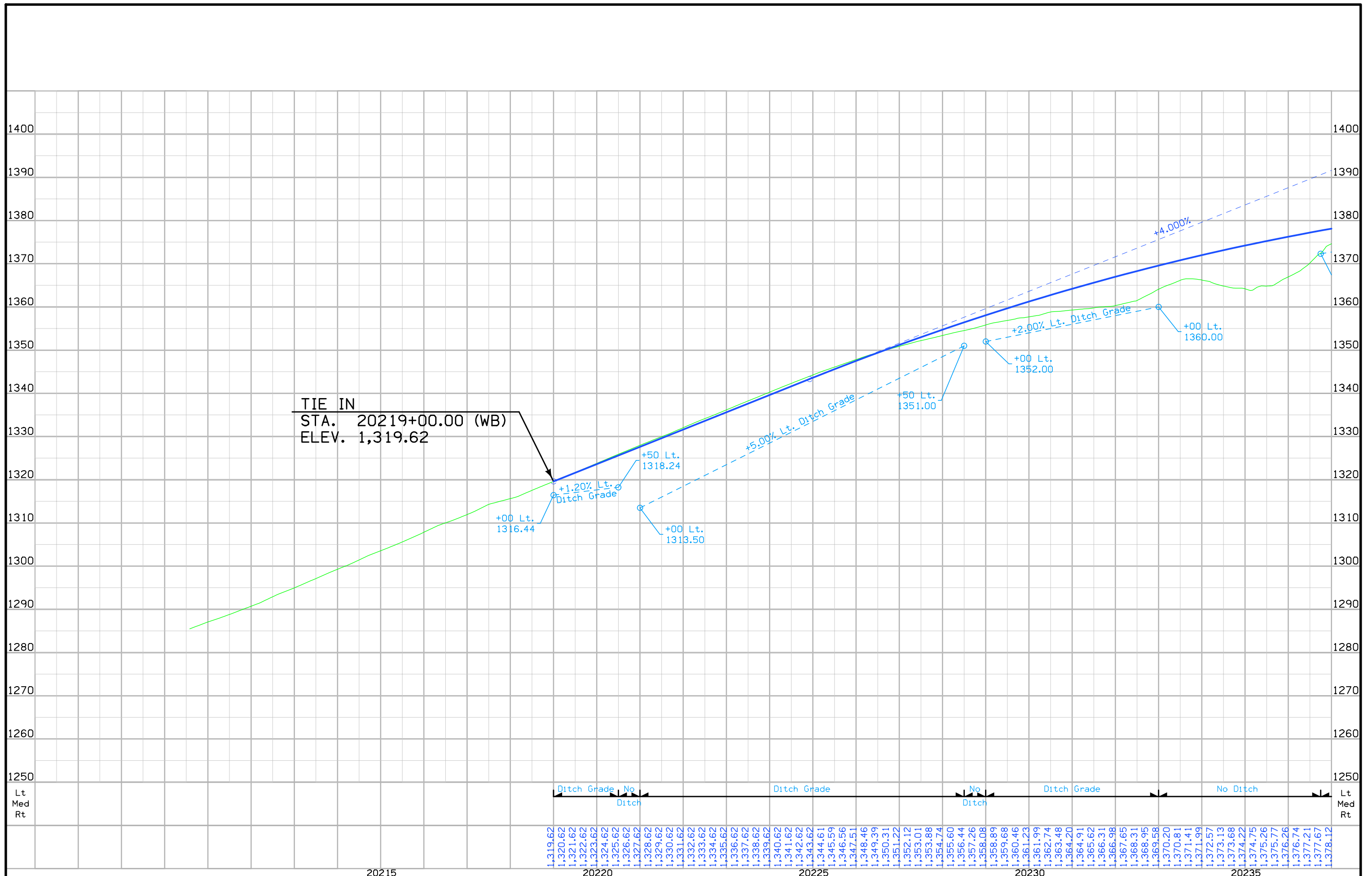
20221+60.12 WBL
 24" RCP
 STAGE 1 REMOVE 116' OF OUTLET
 AND REPLACE WITH 134' + AP
 STAGE 2 EXTEND RT 106' + AP

D.3 SHEET DOESN'T SHOW RIGHT DG

IDA AVE



WESTBOUND



TIE IN
 STA. 20219+00.00 (WB)
 ELEV. 1,319.62

+00 Lt.
1316.44

+1.20% Lt.
Ditch Grade

+50 Lt.
1318.24

+00 Lt.
1313.50

+5.00% Lt.
Ditch Grade

+50 Lt.
1351.00

+00 Lt.
1352.00

+2.00% Lt.
Ditch Grade

+00 Lt.
1360.00

+4.00%

Ditch Grade No
Ditch

Ditch Grade

No
Ditch

Ditch Grade

No Ditch

1,319.62	1,320.62	1,321.62	1,322.62	1,323.62	1,324.62	1,325.62	1,326.62	1,327.62	1,328.62	1,329.62	1,330.62	1,331.62	1,332.62	1,333.62	1,334.62	1,335.62	1,336.62	1,337.62	1,338.62	1,339.62	1,340.62	1,341.62	1,342.62	1,343.62	1,344.61	1,345.59	1,346.56	1,347.51	1,348.46	1,349.39	1,350.31	1,351.22	1,352.12	1,353.01	1,353.88	1,354.74	1,355.60	1,356.44	1,357.26	1,358.08	1,358.89	1,359.68	1,360.46	1,361.23	1,361.99	1,362.74	1,363.48	1,364.20	1,365.62	1,366.31	1,366.98	1,367.65	1,368.31	1,368.95	1,369.58	1,370.20	1,370.81	1,371.41	1,371.99	1,372.57	1,373.13	1,373.68	1,374.22	1,374.75	1,375.26	1,375.77	1,376.26	1,376.74	1,377.21	1,377.67	1,378.12
----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------

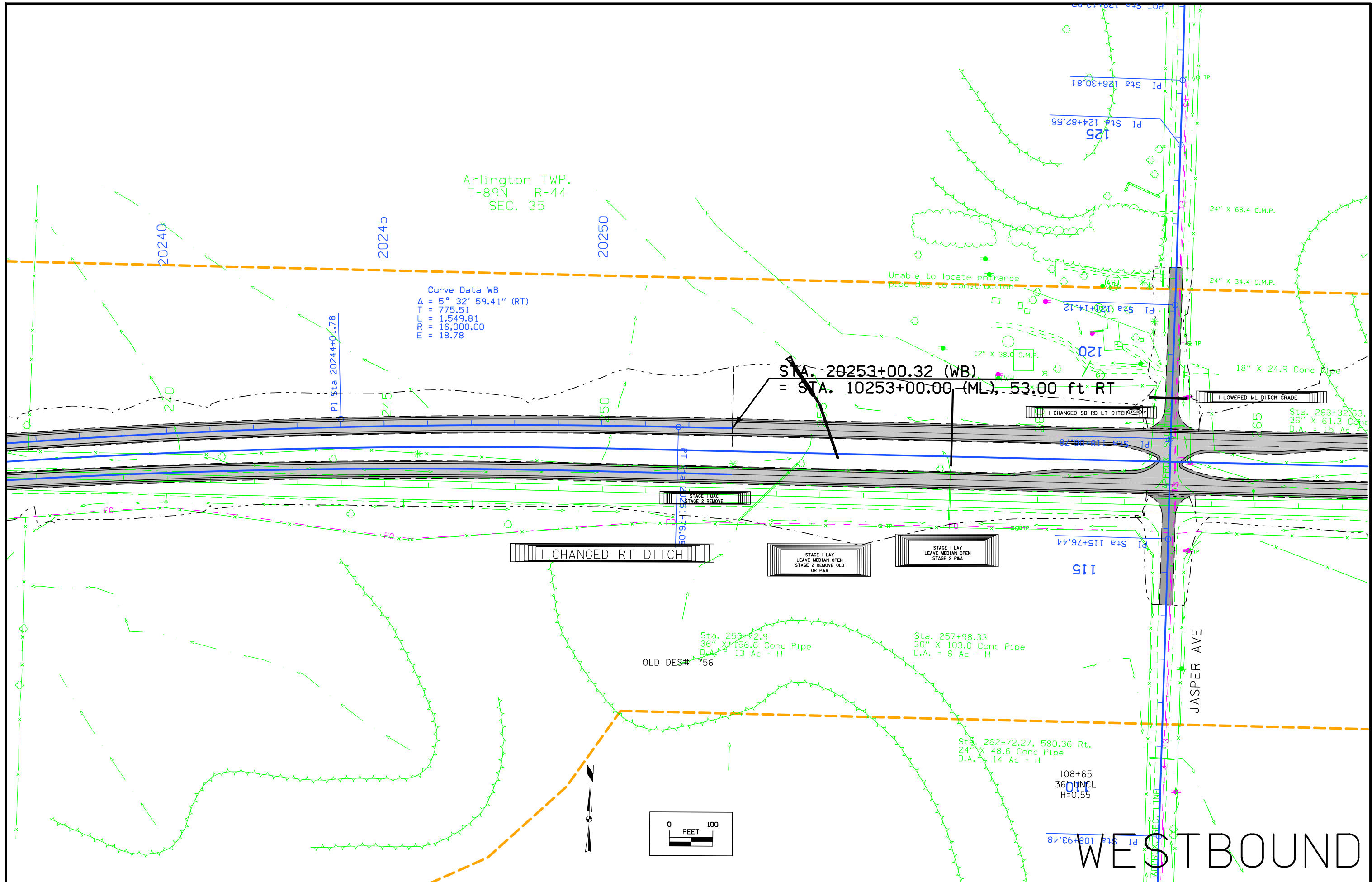
20215

20220

20225

20230

20235



Arlington TWP.
T-89N R-44
SEC. 35

Curve Data WB
 $\Delta = 5^\circ 32' 59.41''$ (RT)
 $T = 775.51$
 $L = 1,549.81$
 $R = 16,000.00$
 $E = 18.78$

STA. 20253+00.32 (WB)
 = STA. 10253+00.00 (ML), 53.00 ft RT

CHANGED RT DITCH

STAGE 1 LAY
LEAVE MEDIAN OPEN
STAGE 2 REMOVE OLD
OR P&A

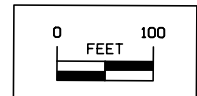
STAGE 1 LAY
LEAVE MEDIAN OPEN
STAGE 2 P&A

Sta. 253+72.9
36" X 156.6 Conc Pipe
D.A. = 13 Ac - H
OLD DES# 756

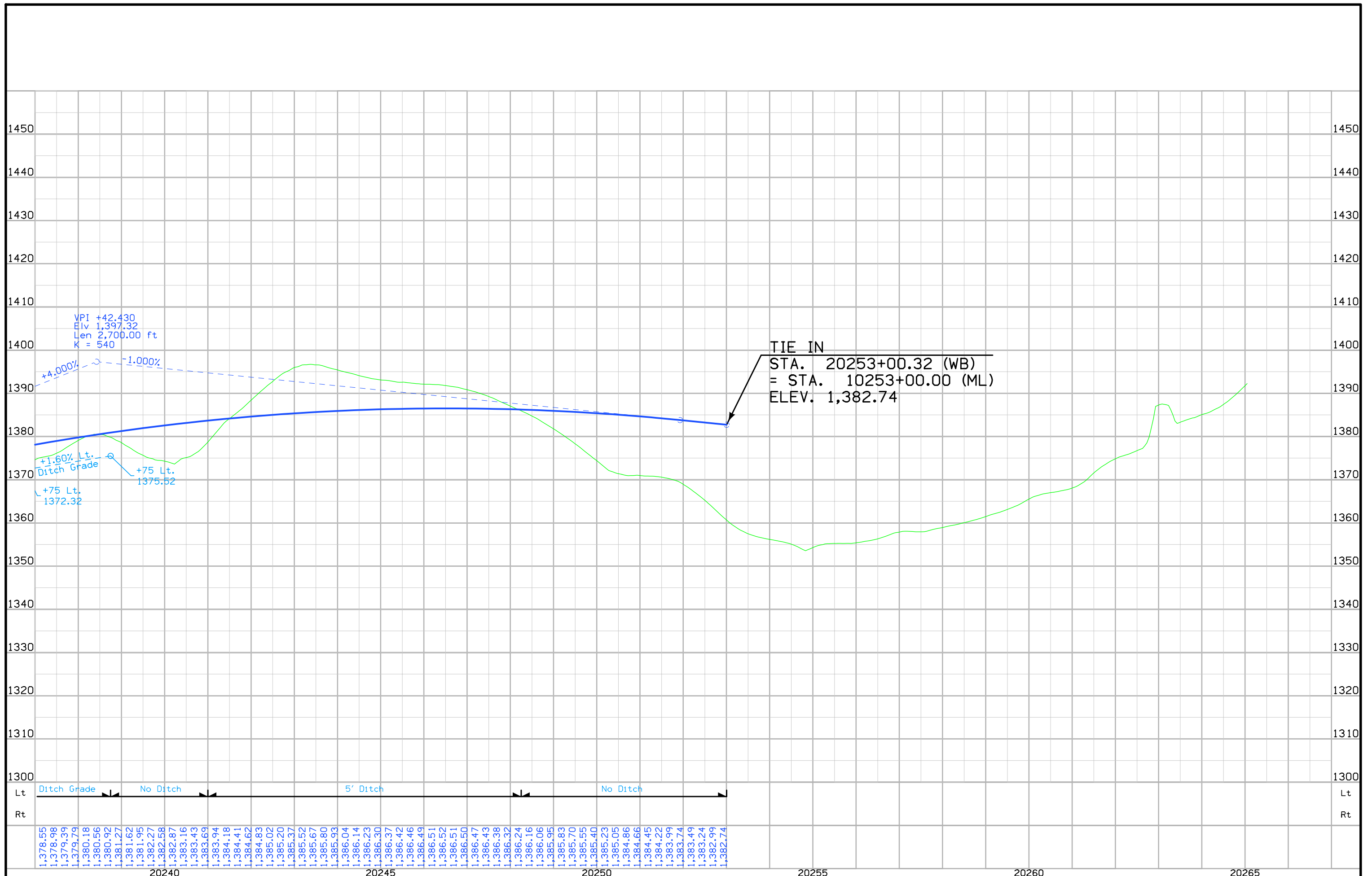
Sta. 257+98.33
30" X 103.0 Conc Pipe
D.A. = 6 Ac - H

Sta. 262+72.27, 580.36 Rt.
24" X 48.6 Conc Pipe
D.A. = 14 Ac - H

108+65
36" UNCL
H=0.55



WESTBOUND



PROPOSED CULVERT CONCEPTS

- SAME LOCATION AND LEAVE MEDIAN OPEN
- OR
- NEW LOCATION AND LEAVE MEDIAN OPEN
- OR
- SAME LOCATION AND TIE TO OLD
- OR
- NEW LOCATION AND TEMP PIPE EXTENSION
- OR
- JACK AND LAY

Curve Data
 $\Delta = 0^\circ 16' 21.82''$ (LT)
 $T = 300.00$
 $R = 600.00$
 $PR = 126,050.48$
 $E = 0.36$

Arlington TWP.
 T-89N R-44
 SEC. 35

Sta. 221+97.88, 42.68 Rt.
 18" X 10.7 Conc Pipe
 D.A. = 2 Ac - P

STA. 30219+00.00 (EB)
 BEGIN PROJECT

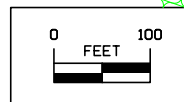
OUTLET FLOW RAISED

Sta. 221+60.58
 24" X 205.2 Conc Pipe
 D.A. = 3 Ac - P

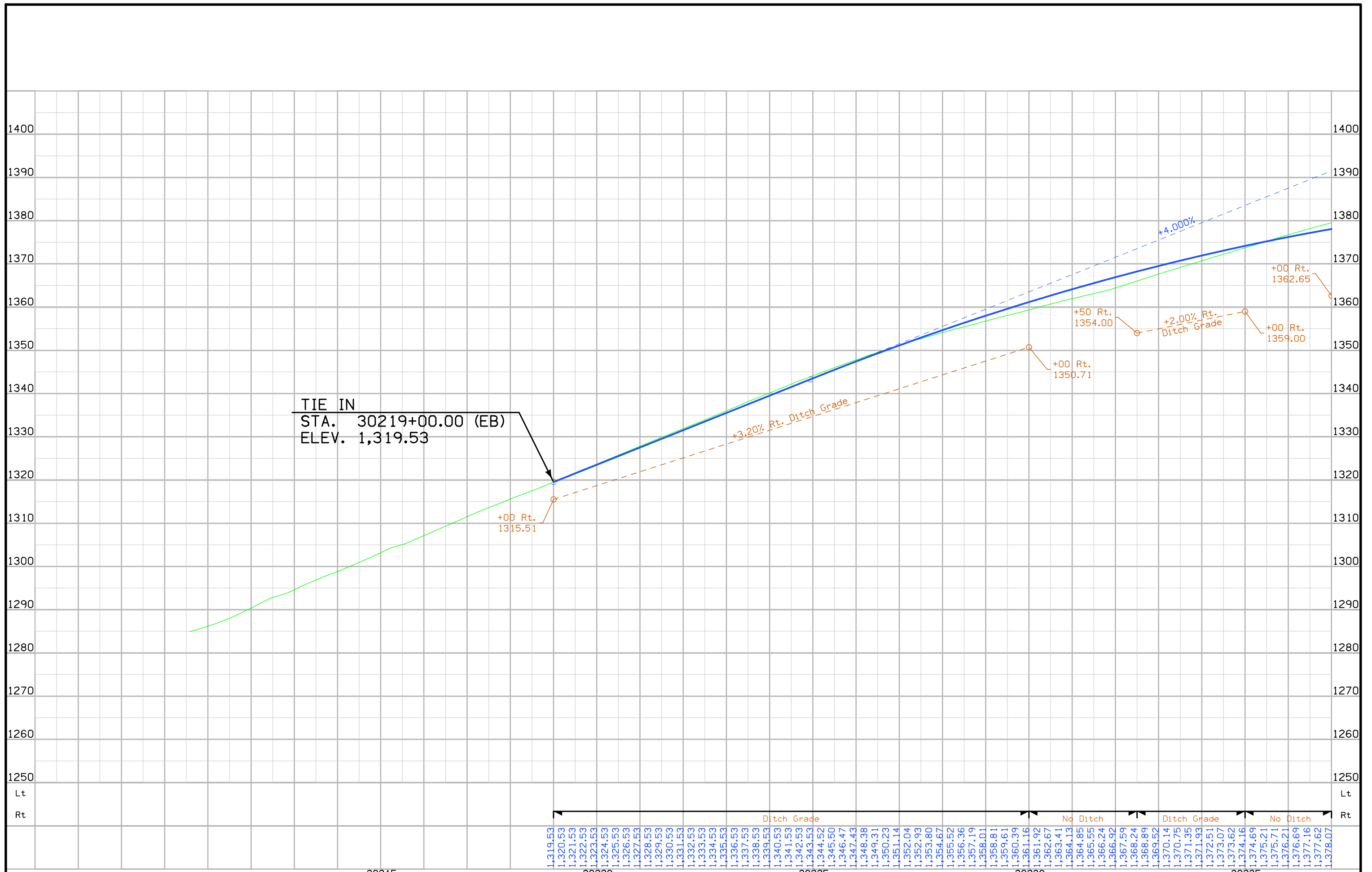
20221+60.12 WBL
 24" RCP
 STAGE 1 REMOVE 116' OF OUTLET
 AND REPLACE WITH 134' + AP
 STAGE 2 EXTEND RT 106' + AP

D.3 SHEET DOESN'T SHOW RIGHT DG

Curve Data EB
 $\Delta = 5^\circ 24' 00.79''$ (LT)
 $T = 754.57$
 $R = 1,508.03$
 $PR = 16,000.00$
 $E = 17.78$

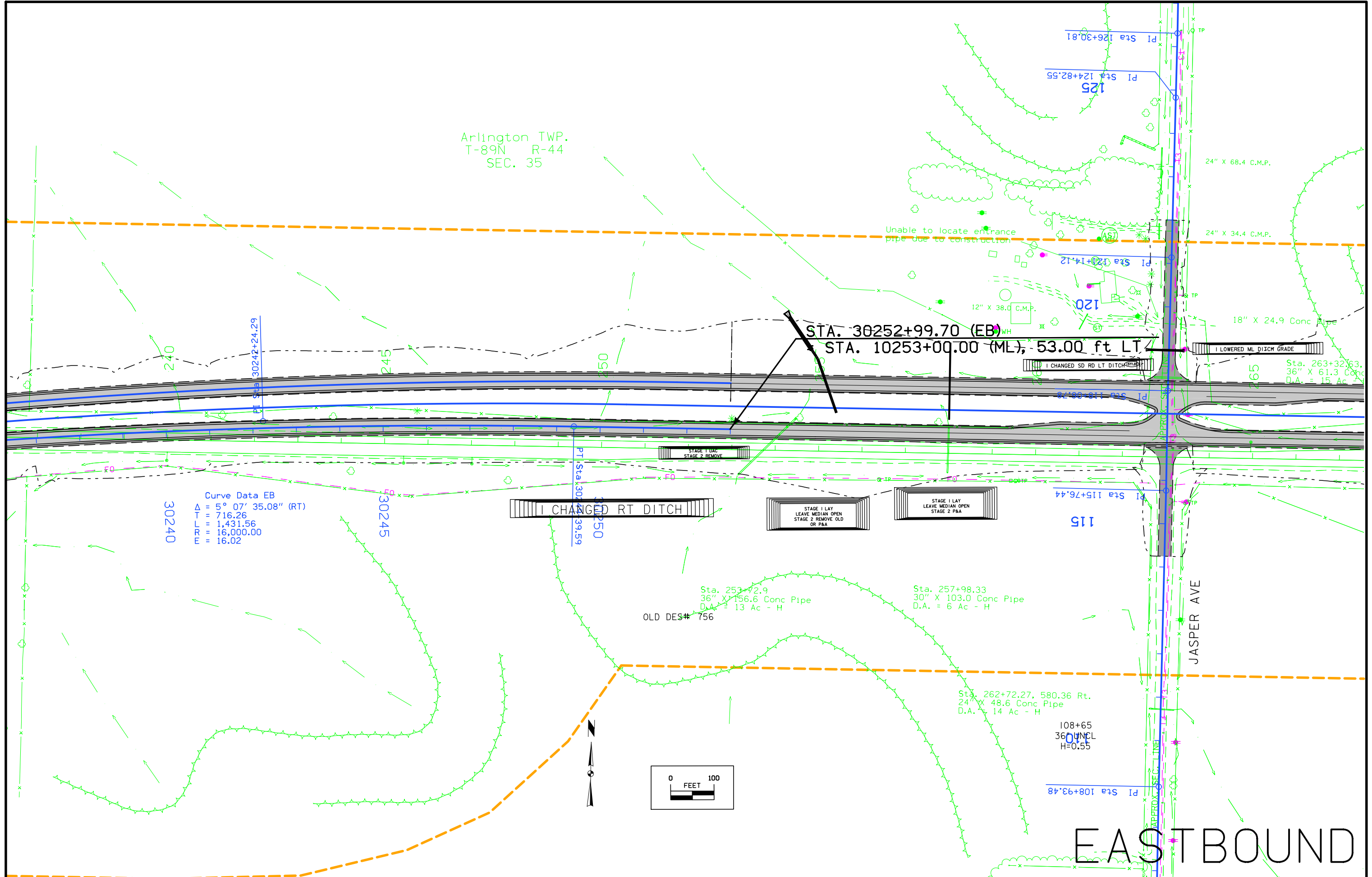


EASTBOUND

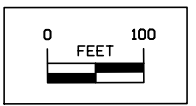


30215										30220										30225										30230										30235																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																	
										Ditch Grade										No Ditch										Ditch Grade										No Ditch																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																	
1,319.53										1,320.53										1,321.53										1,322.53										1,323.53										1,324.53										1,325.53										1,326.53										1,327.53										1,328.53										1,329.53										1,330.53										1,331.53										1,332.53										1,333.53										1,334.53										1,335.53										1,336.53										1,337.53										1,338.53										1,339.53										1,340.53										1,341.53										1,342.53										1,343.53										1,344.52										1,345.50										1,346.47										1,347.43										1,348.38										1,349.31										1,350.23										1,351.14										1,352.04										1,352.93										1,353.80										1,354.67										1,355.52										1,356.36										1,357.19										1,358.01										1,358.81										1,359.61										1,360.39										1,361.16										1,361.92										1,362.67										1,363.41										1,364.13										1,364.85										1,365.55										1,366.24										1,366.92										1,367.59										1,368.24										1,368.89										1,369.52										1,370.14										1,370.75										1,371.35										1,371.93										1,372.51										1,373.07										1,373.62										1,374.16										1,374.69										1,375.21										1,375.71										1,376.21										1,376.69										1,377.16										1,377.62										1,378.07									

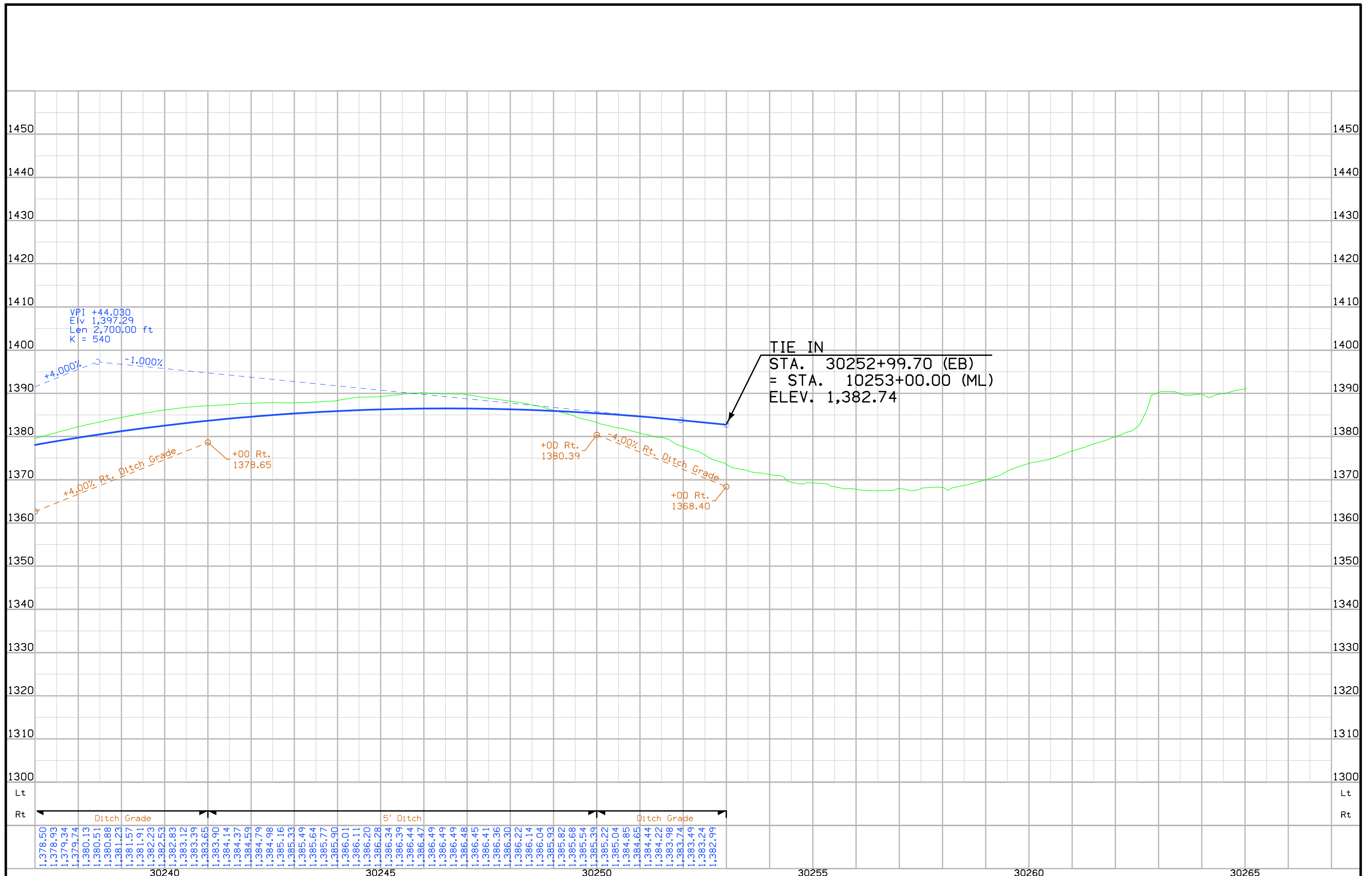
Arlington TWP.
T-89N R-44
SEC. 35



Curve Data EB
Δ = 5° 07' 35.08" (RT)
T = 716.26
L = 1,431.56
R = 16,000.00
E = 16.02



EASTBOUND



Arlington TWP.
T-89N R-44
SEC. 35

STA. 10253+00.00 (ML)
= STA. 20253+00.32 (WB), 53.00 ft LT
= STA. 30252+99.70 (EB), 53.00 ft RT

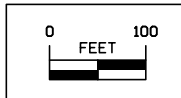
Curve Data
 $\Delta = 5^\circ 20' 32.31''$ (RT)
T = 746.47
L = 1,491.85
R = 16,000.00
E = 17.40

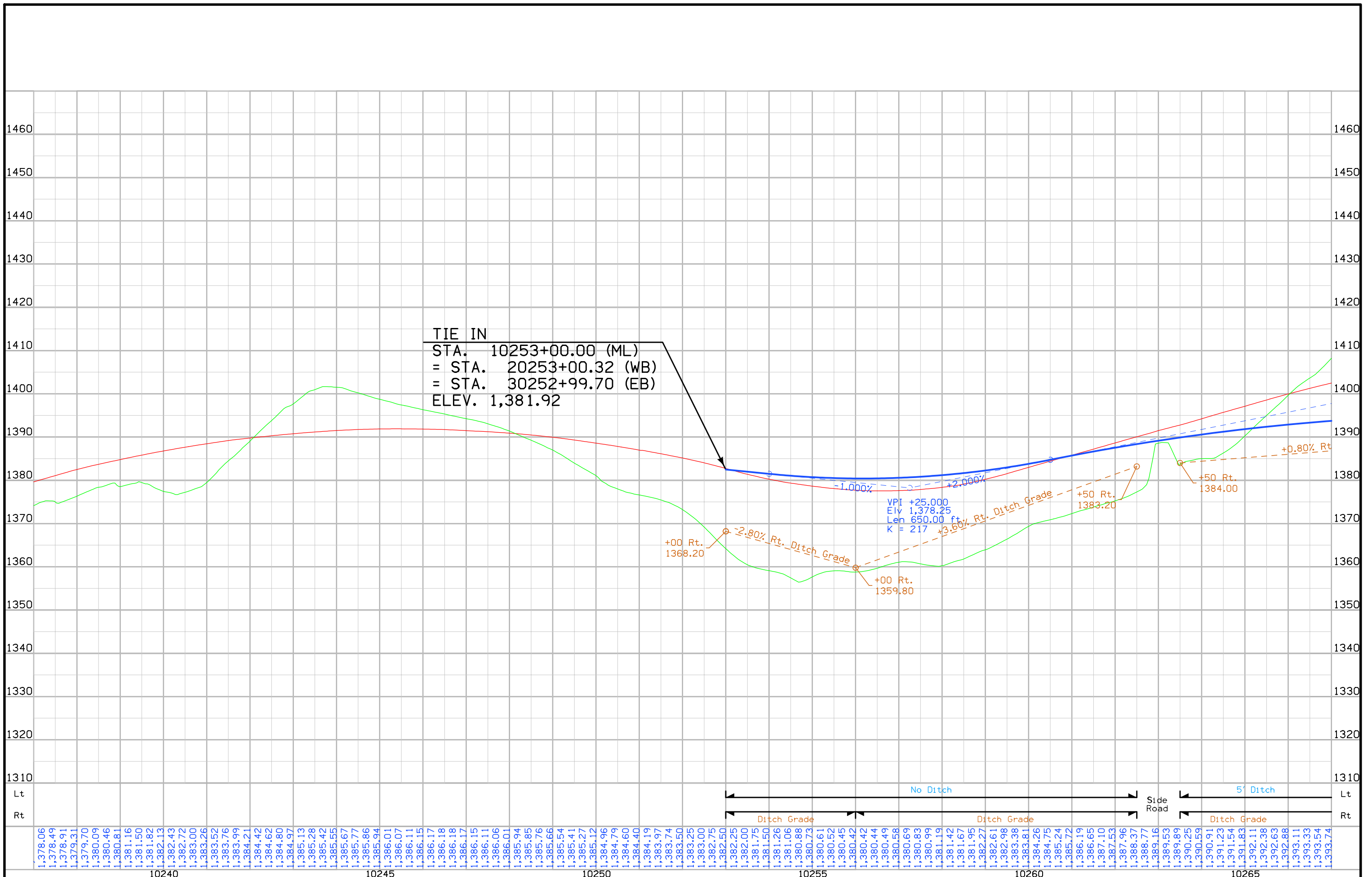
Sta. 253+72.9
36" X 156.6 Conc Pipe
D.A. = 13 Ac - H
OLD DES# 756

Sta. 257+98.33
30" X 103.0 Conc Pipe
D.A. = 6 Ac - H

Sta. 262+72.27, 580.36 Rt.
24" X 48.6 Conc Pipe
D.A. = 14 Ac - H

108+65
36" UNCL
H=0.55



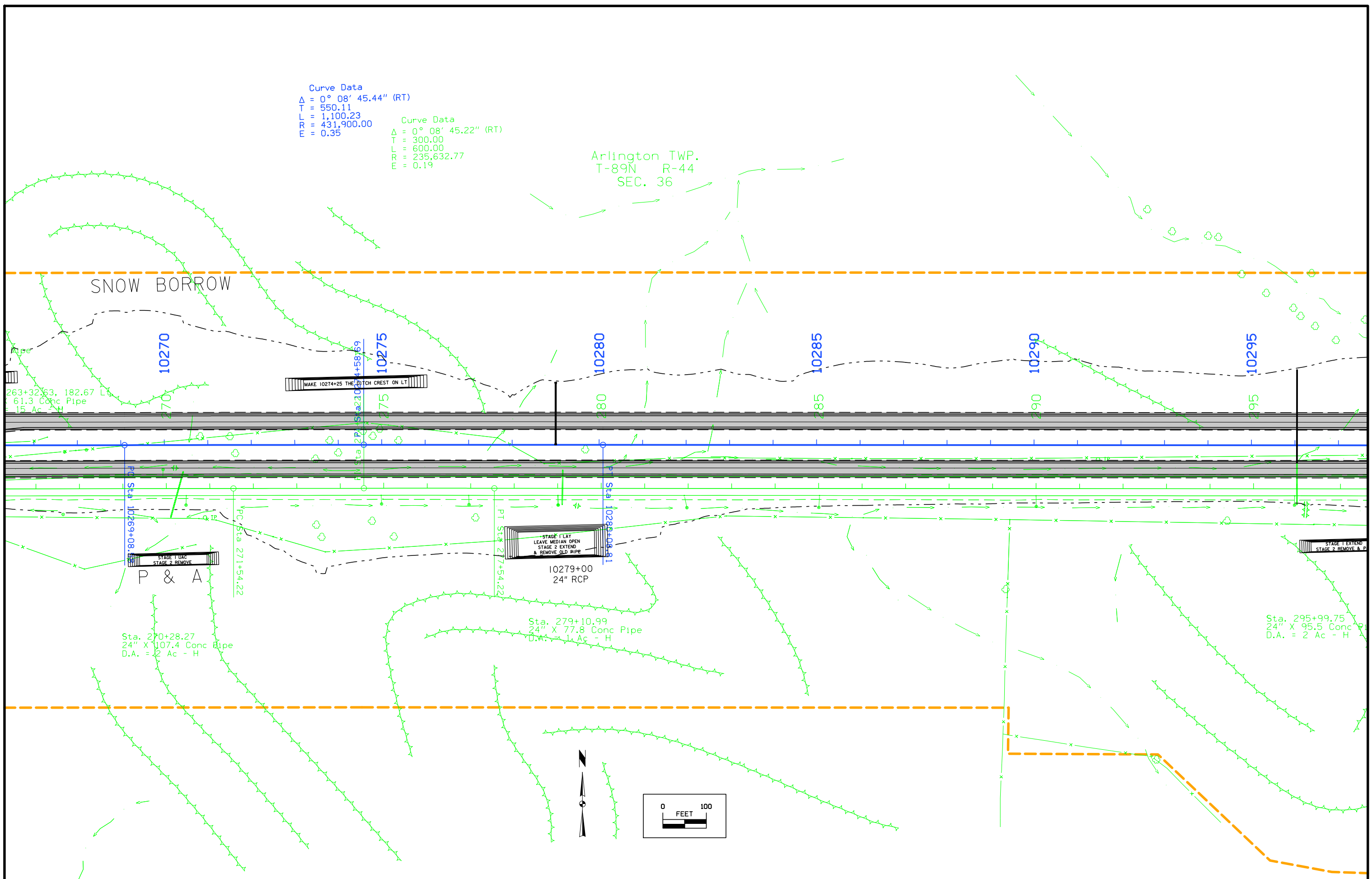


1,378.06	1,378.49	1,378.91	1,379.31	1,379.70	1,380.09	1,380.46	1,380.81	1,381.16	1,381.50	1,381.82	1,382.13	1,382.43	1,382.72	1,383.00	1,383.26	1,383.52	1,383.76	1,383.99	1,384.21	1,384.42	1,384.62	1,384.80	1,384.97	1,385.13	1,385.28	1,385.42	1,385.55	1,385.67	1,385.77	1,385.86	1,385.94	1,386.01	1,386.07	1,386.11	1,386.15	1,386.17	1,386.18	1,386.18	1,386.17	1,386.15	1,386.11	1,386.06	1,386.01	1,385.94	1,385.85	1,385.76	1,385.66	1,385.54	1,385.41	1,385.27	1,385.12	1,384.96	1,384.79	1,384.60	1,384.40	1,384.19	1,383.97	1,383.74	1,383.50	1,383.25	1,383.00	1,382.75	1,382.50	1,382.25	1,382.00	1,381.75	1,381.50	1,381.26	1,381.06	1,380.88	1,380.73	1,380.61	1,380.52	1,380.45	1,380.42	1,380.42	1,380.44	1,380.49	1,380.58	1,380.69	1,380.83	1,380.99	1,381.19	1,381.42	1,381.67	1,381.95	1,382.27	1,382.61	1,382.98	1,383.38	1,383.81	1,384.26	1,384.75	1,385.24	1,385.72	1,386.19	1,386.65	1,387.10	1,387.53	1,387.96	1,388.37	1,388.77	1,389.16	1,389.53	1,389.89	1,390.25	1,390.59	1,390.91	1,391.23	1,391.54	1,391.83	1,392.11	1,392.38	1,392.63	1,392.88	1,393.11	1,393.33	1,393.54	1,393.74
----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------

Curve Data
 $\Delta = 0^\circ 08' 45.44''$ (RT)
 T = 550.11
 L = 1,100.23
 RR = 431,900.00
 E = 0.35

Curve Data
 $\Delta = 0^\circ 08' 45.22''$ (RT)
 T = 300.00
 L = 600.00
 RR = 235,632.77
 E = 0.19

Arlington TWP.
 T-89N R-44
 SEC. 36



STAGE 1 LAY
 STAGE 2 REMOVE
 P & A

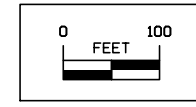
STAGE 1 LAY
 LEAVE MEDIAN OPEN
 STAGE 2 EXTEND
 & REMOVE OLD PIPE
 10279+00
 24" RCP

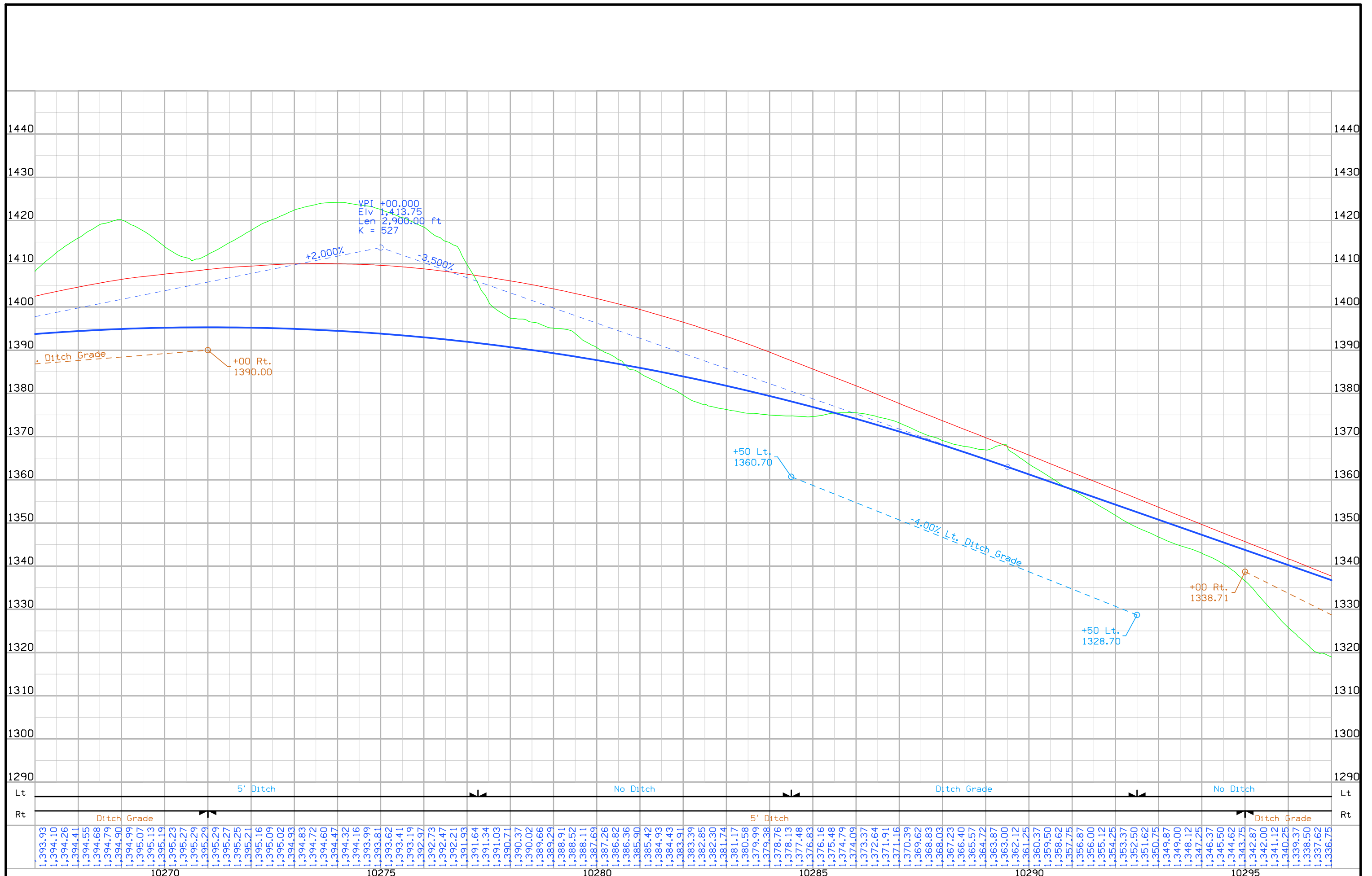
STAGE 1 EXTEND
 STAGE 2 REMOVE & P

Sta. 270+28.27
 24" X 107.4 Conc Pipe
 D.A. = 2 Ac - H

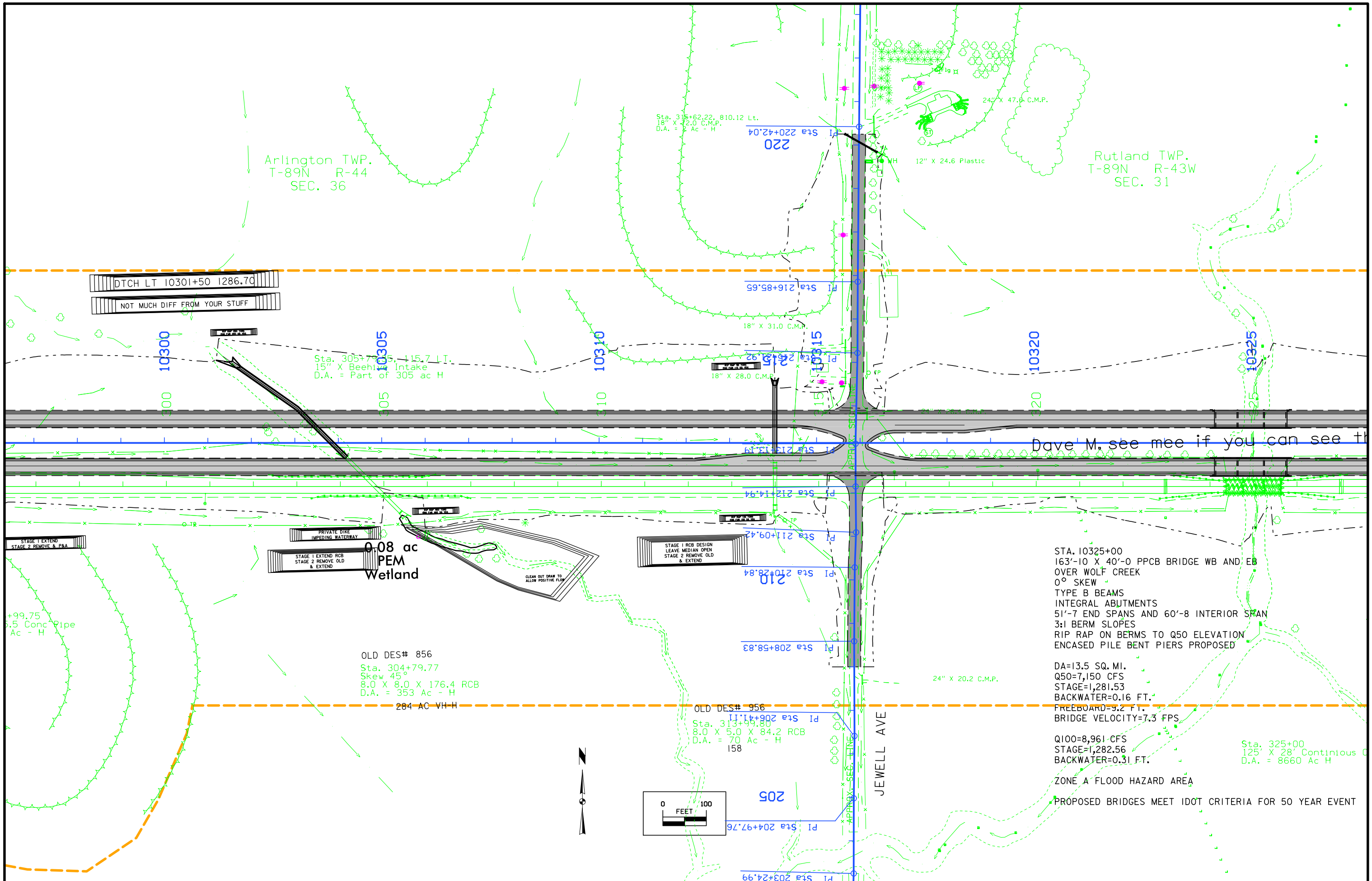
Sta. 279+10.99
 24" X 77.8 Conc Pipe
 D.A. = 1 Ac - H

Sta. 295+99.75
 24" X 95.5 Conc Pipe
 D.A. = 2 Ac - H





1,393.93	1,394.10	1,394.26	1,394.41	1,394.55	1,394.68	1,394.79	1,394.90	1,394.99	1,395.07	1,395.13	1,395.19	1,395.23	1,395.27	1,395.29	1,395.29	1,395.27	1,395.25	1,395.21	1,395.16	1,395.09	1,395.02	1,394.93	1,394.83	1,394.72	1,394.60	1,394.47	1,394.32	1,394.16	1,393.99	1,393.81	1,393.62	1,393.41	1,393.19	1,392.97	1,392.73	1,392.47	1,392.21	1,391.93	1,391.64	1,391.34	1,391.03	1,390.71	1,390.37	1,390.02	1,389.66	1,389.29	1,388.91	1,388.52	1,388.11	1,387.69	1,387.26	1,386.82	1,386.36	1,385.90	1,385.42	1,384.93	1,384.43	1,383.91	1,383.39	1,382.85	1,382.30	1,381.74	1,381.17	1,380.58	1,379.99	1,379.38	1,378.76	1,378.13	1,377.48	1,376.83	1,376.16	1,375.48	1,374.79	1,374.09	1,373.37	1,372.64	1,371.91	1,371.16	1,370.39	1,369.62	1,368.83	1,368.03	1,367.23	1,366.40	1,365.57	1,364.72	1,363.87	1,363.00	1,362.12	1,361.25	1,360.37	1,359.50	1,358.62	1,357.75	1,356.87	1,356.00	1,355.12	1,354.25	1,353.37	1,352.50	1,351.62	1,350.75	1,349.87	1,349.00	1,348.12	1,347.25	1,346.37	1,345.50	1,344.62	1,343.75	1,342.87	1,342.00	1,341.12	1,340.25	1,339.37	1,338.50	1,337.62	1,336.75
----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------



Arlington TWP.
T-89N R-44
SEC. 36

Rutland TWP.
T-89N R-43W
SEC. 31

DTCH LT 10301+50 1286.70
NOT MUCH DIFF FROM YOUR STUFF

Sta. 305+79.55, 115.7 LT.
15" X Beehive Intake
D.A. = Part of 305 ac H

Sta. 313+62.22, 810.12 Lt.
18" X 22.0 C.M.P.
D.A. = 172 Ac - H

24" X 47.6 C.M.P.

12" X 24.6 Plastic

18" X 31.0 C.M.P.

18" X 28.0 C.M.P.

PI Sta 212+14.94

PI Sta 211+09.42

PI Sta 210+28.84

PI Sta 208+58.83

PI Sta 206+41.11

Sta. 313+66.80
8.0 X 5.0 X 84.2 RCB
D.A. = 70 Ac - H
158

24" X 20.2 C.M.P.

Dave M. see mee if you can see th

STAGE 1 EXTEND
STAGE 2 REMOVE & PAA

PRIVATE DITCH
IMPEDING WATERWAY
0.08 ac
PEM
Wetland

STAGE 1 RCB DESIGN
LEAVE MEDIAN OPEN
STAGE 2 REMOVE OLD
& EXTEND

CLEAN OUT DRAIN TO
ALLOW POSITIVE FLOW

+99.75
3.5 Conc Pipe
Ac - H

OLD DES# 856
Sta. 304+79.77
Skew 45°
8.0 X 8.0 X 176.4 RCB
D.A. = 353 Ac - H

284 AC VH-H

STA. 10325+00
163'-10 X 40'-0 PPCB BRIDGE WB AND EB
OVER WOLF CREEK
0° SKEW
TYPE B BEAMS
INTEGRAL ABUTMENTS
51'-7 END SPANS AND 60'-8 INTERIOR SPAN
3:1 BERM SLOPES
RIP RAP ON BERMS TO Q50 ELEVATION
ENCASED PILE BENT PIERS PROPOSED

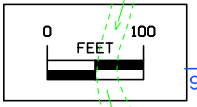
DA=13.5 SQ. MI.
Q50=7,150 CFS
STAGE=1,281.53
BACKWATER=0.16 FT.
FREEBOARD=3.2 FT.
BRIDGE VELOCITY=7.3 FPS

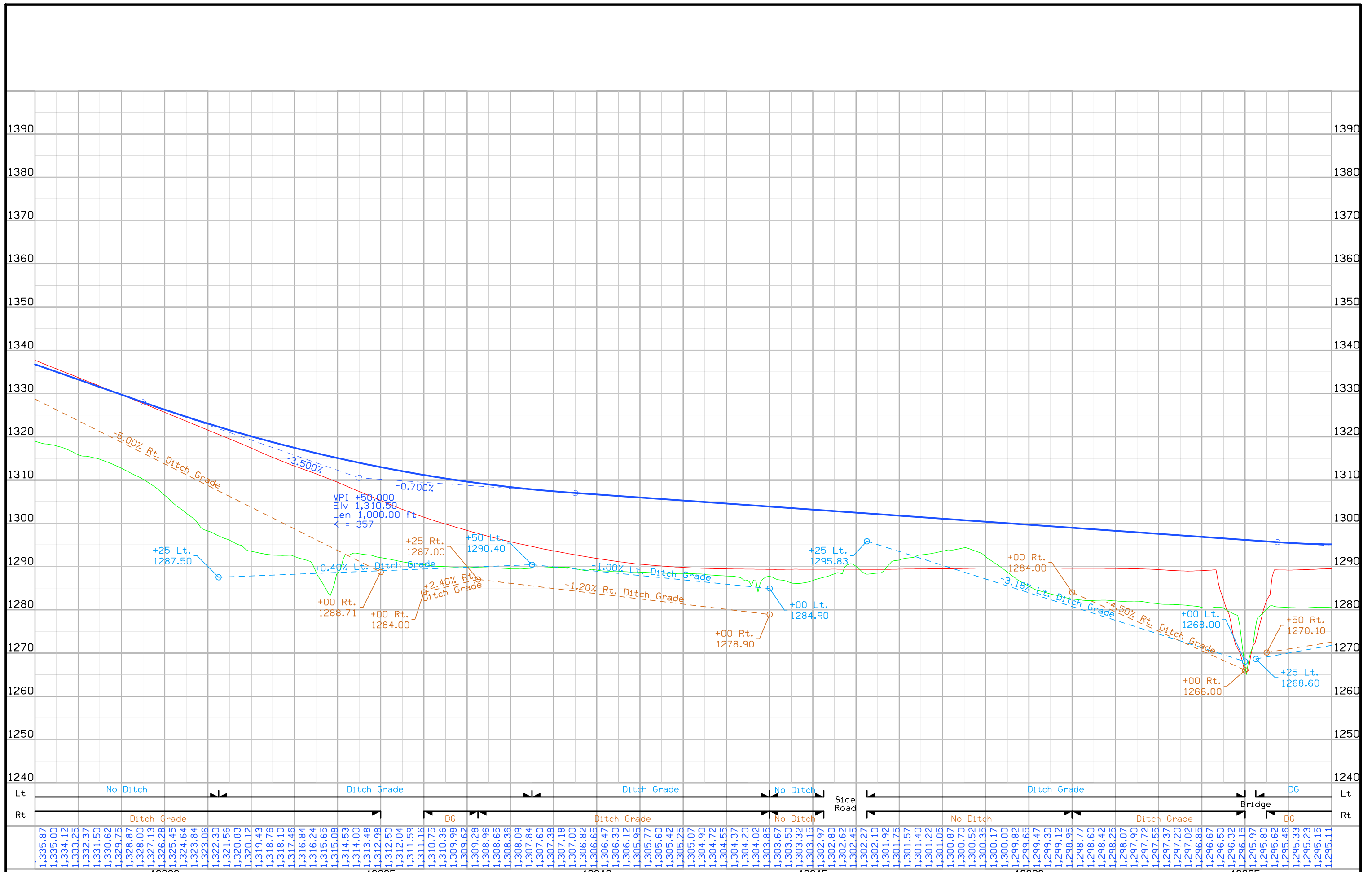
Q100=8,961 CFS
STAGE=1,282.56
BACKWATER=0.31 FT.

ZONE A FLOOD HAZARD AREA

PROPOSED BRIDGES MEET IDOT CRITERIA FOR 50 YEAR EVENT

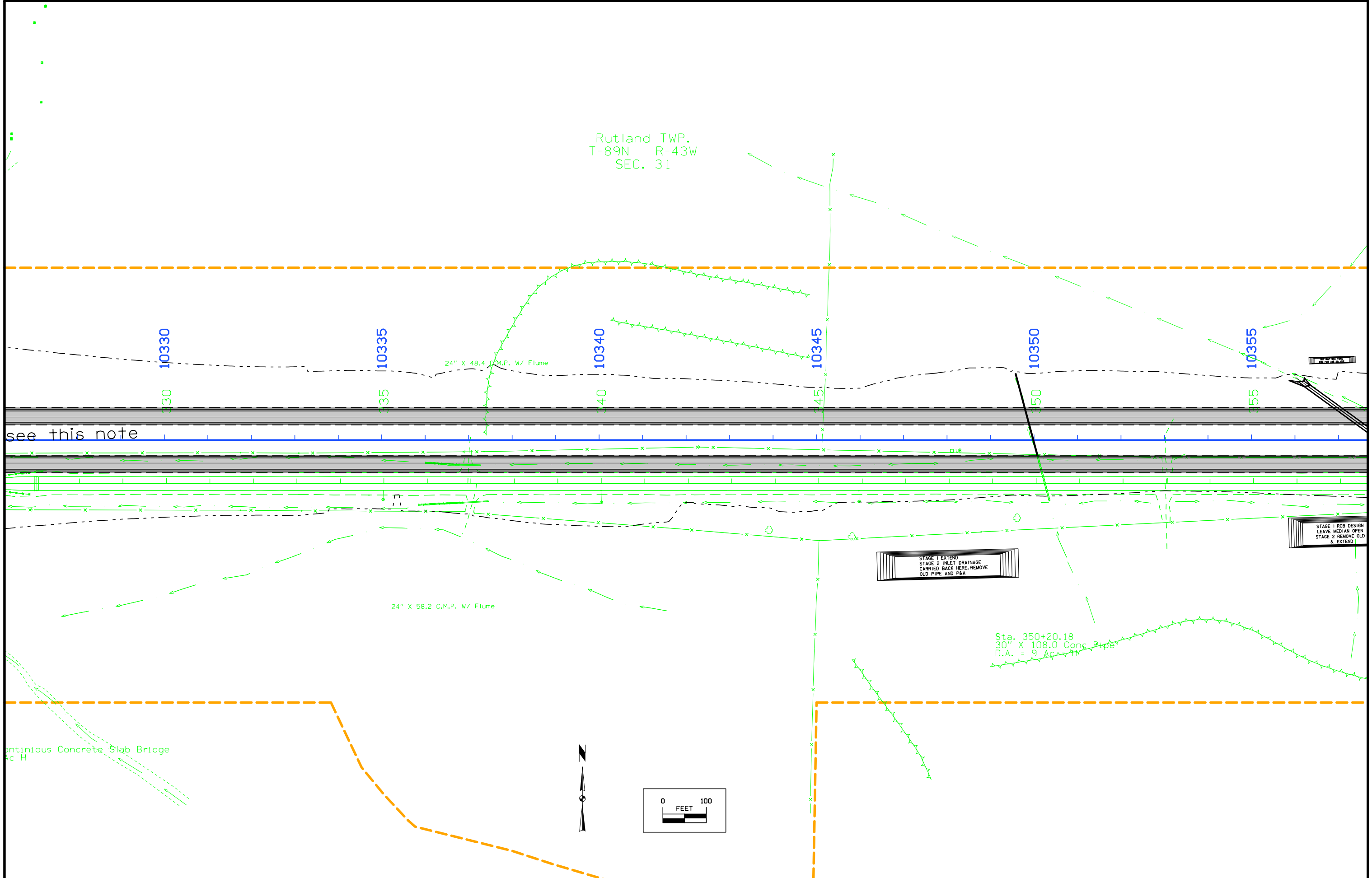
Sta. 325+00
125" X 28" Continuous
D.A. = 8660 Ac H





English		IOWA DOT	DESIGN TEAM Flattery\Johnson	WOODBURY COUNTY	PROJECT NUMBER NHSX-020-1(116)--3H-97	SHEET NUMBER D.15
---------	--	----------	------------------------------	-----------------	---------------------------------------	-------------------

Rutland TWP.
T-89N R-43W
SEC. 31

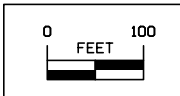


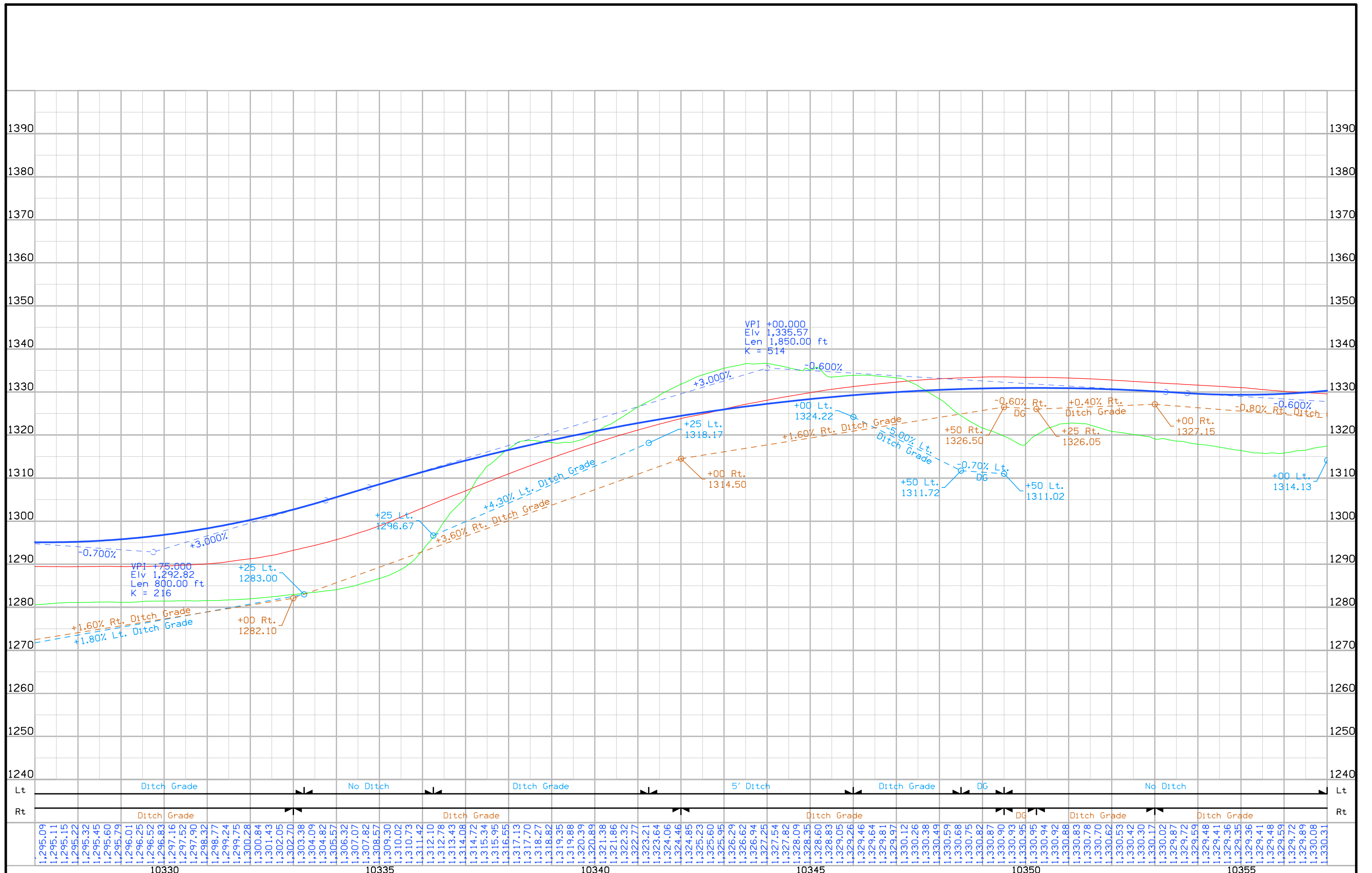
see this note

STAGE 1 EXTEND
STAGE 2 INLET DRAINAGE
CARRIED BACK HERE, REMOVE
OLD PIPE AND P&A

STAGE 1 RCB DESIGN
LEAVE MEDIAN OPEN
STAGE 2 REMOVE OLD
& EXTEND

Sta. 350+20.18
30" X 108.0 Conc Pipe
D.A. = 9' Ac





Rutland TWP.
T-89N R-43W
SEC. 31

Rutland TWP.
T-89N R-43W
SEC. 32

Sta. 359+10.79, 96.56 Lt.
18" Beehive Intake
D.A. = Part of 236 Ac - GR - H

Sta. 371+01.31
24" X 96.0 Conc Pipe
D.A. = 2 Ac - H

Sta. 372+01.88
42" X 115.5 Conc Pipe
D.A. = 18 Ac - H

IF WE CAN KEEP THE WATER IN OUR LEFT DITCH ALL THE WAY TO THE SIDE
CULVERT BACK AND KEEP IN OUR DITCH TO STA 10356 (+OR-) THESE 2 PIPES
BE UAC STAGE 1 AND REMOVED IN STAGE 2

ELIMINATED 2 PIPES AND CHANGED
YOUR DITCH & NEW PIPE UNDER SD RD

0.05 ac
PEM
Wetland

4.31 ac
PEM
Wetland

OLD DES# 1056
Sta. 359+59.11
10.0 X 6.0 X 54.5 RCB
D.A. = 235 Ac - GR - H
OK DA

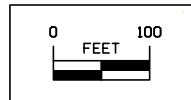
OLD DES# 7556
Sta. 364+00.97
4.0 X 5.5 X 54.5 RCB STOCK PASS
D.A. = 1 Ac - H

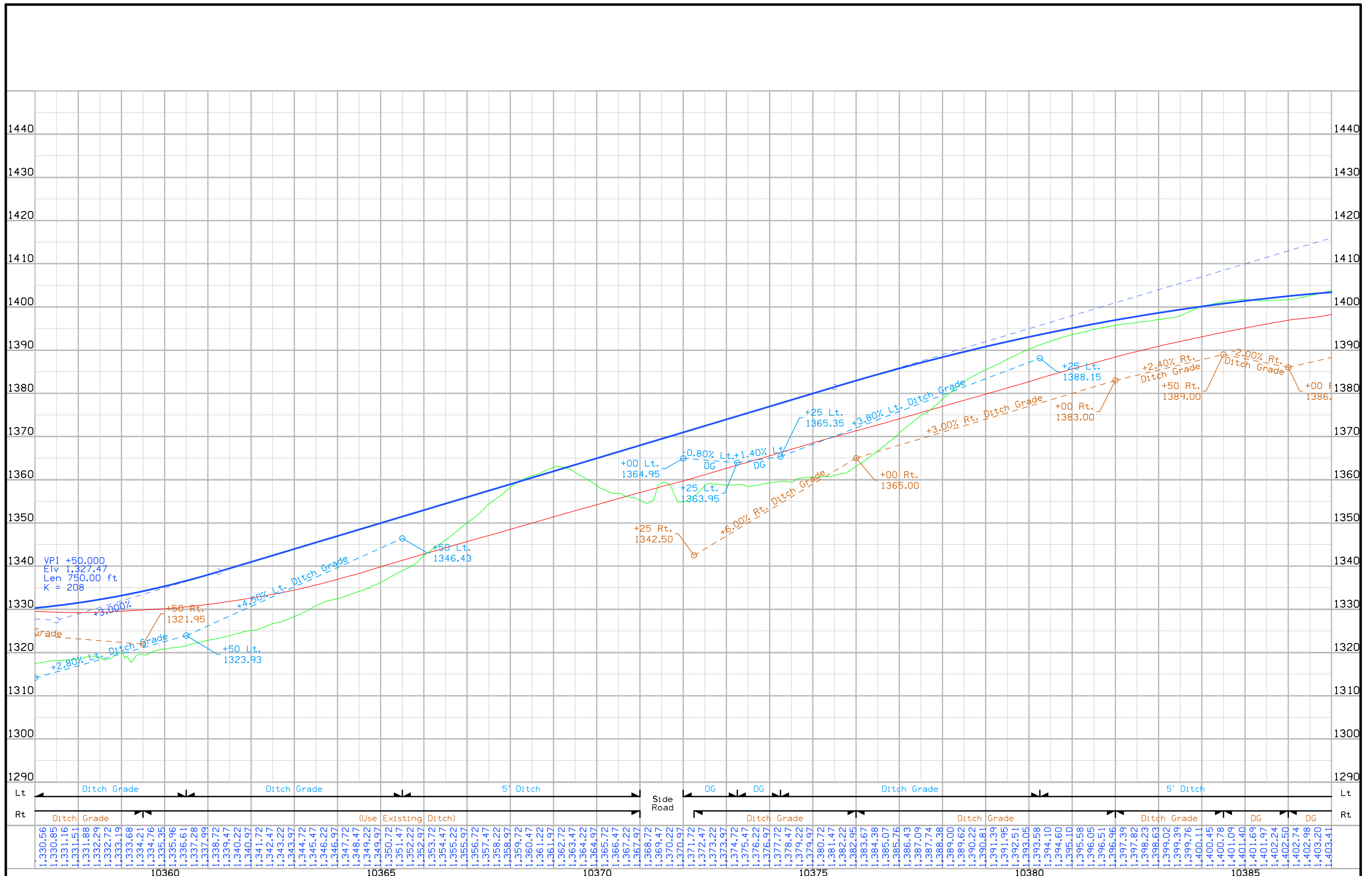
WE WILL ELIMINATE THESE TWO PIPES WHEN MOVE TRAFFIC TO WBL'S BUT
BE USED FOR TEMP MEDIAN DRAINAGE AND REMOVE DITCH GRADE
AT 10386 RT AND DITCH BRING WATER TO WEST AND AROUND RADI11 SD RD
SOUTH OR LEAVE YOUR DTCH GRADE THERE AND THE WATER FROM THE EAST
CONTINUE WHERE IT USED TO GO (10385+50 TO SOUTH) AND WE WOULD BE
PERPETUATING THE DRAINAGE WHICH MAY BE THE BEST RECOURSE

SIDE ROAD
Sta. 371+48.83 389.14' RT
8.0 X 4.0 X 50.0 RCB
D.A. = 142 Ac - H

Sta. 382+60.28
24" X 78.5 Conc Pipe
D.A. = 2 Ac - R

Sta. 385+61.49
24" X 71.7 Conc Pipe
D.A. = 3 Ac - H



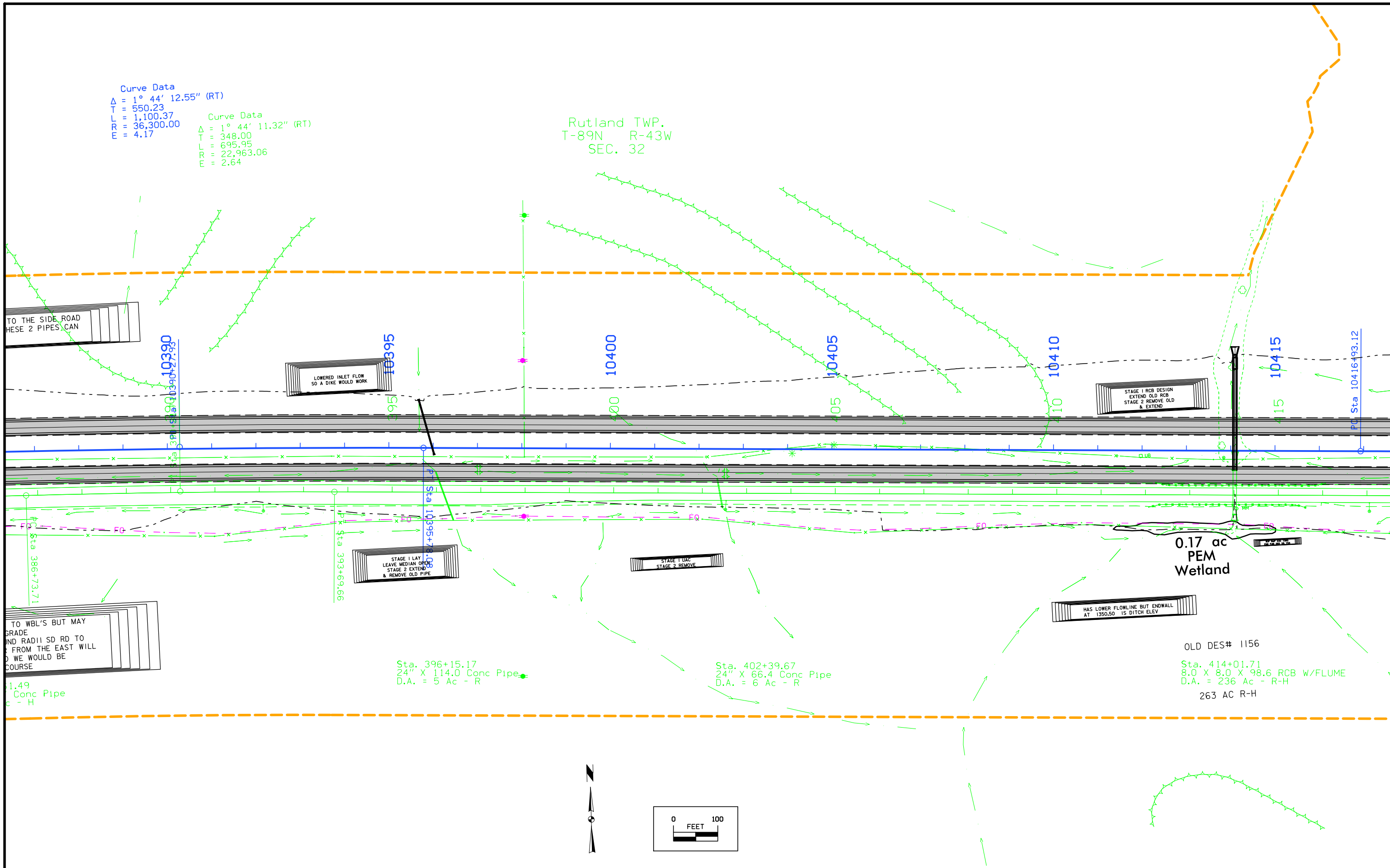


1,330.56		1,330.85		1,331.16		1,331.51		1,331.88		1,332.29		1,332.72		1,333.19		1,333.68		1,334.21		1,334.76		1,335.35		1,335.96		1,336.61		1,337.28		1,337.99		1,338.72		1,339.47		1,340.22		1,340.97		1,341.72		1,342.47		1,343.22		1,343.97		1,344.72		1,345.47		1,346.22		1,346.97		1,347.72		1,348.47		1,349.22		1,349.97		1,350.72		1,351.47		1,352.22		1,352.97		1,353.72		1,354.47		1,355.22		1,355.97		1,356.72		1,357.47		1,358.22		1,358.97		1,359.72		1,360.47		1,361.22		1,361.97		1,362.72		1,363.47		1,364.22		1,364.97		1,365.72		1,366.47		1,367.22		1,367.97		1,368.72		1,369.47		1,370.22		1,370.97		1,371.72		1,372.47		1,373.22		1,373.97		1,374.72		1,375.47		1,376.22		1,376.97		1,377.72		1,378.47		1,379.22		1,379.97		1,380.72		1,381.47		1,382.22		1,382.97		1,383.72		1,384.47		1,385.22		1,385.97		1,386.72		1,387.47		1,388.22		1,388.97		1,389.72		1,389.47		1,390.22		1,390.97		1,391.72		1,391.47		1,392.22		1,392.97		1,393.72		1,393.47		1,394.22		1,394.97		1,395.72		1,395.47		1,396.22		1,396.97		1,397.72		1,397.47		1,398.22		1,398.97		1,399.72		1,399.47		1,400.22		1,400.97		1,401.72		1,401.47		1,402.22		1,402.97		1,403.72		1,403.47	
----------	--	----------	--	----------	--	----------	--	----------	--	----------	--	----------	--	----------	--	----------	--	----------	--	----------	--	----------	--	----------	--	----------	--	----------	--	----------	--	----------	--	----------	--	----------	--	----------	--	----------	--	----------	--	----------	--	----------	--	----------	--	----------	--	----------	--	----------	--	----------	--	----------	--	----------	--	----------	--	----------	--	----------	--	----------	--	----------	--	----------	--	----------	--	----------	--	----------	--	----------	--	----------	--	----------	--	----------	--	----------	--	----------	--	----------	--	----------	--	----------	--	----------	--	----------	--	----------	--	----------	--	----------	--	----------	--	----------	--	----------	--	----------	--	----------	--	----------	--	----------	--	----------	--	----------	--	----------	--	----------	--	----------	--	----------	--	----------	--	----------	--	----------	--	----------	--	----------	--	----------	--	----------	--	----------	--	----------	--	----------	--	----------	--	----------	--	----------	--	----------	--	----------	--	----------	--	----------	--	----------	--	----------	--	----------	--	----------	--	----------	--	----------	--	----------	--	----------	--	----------	--	----------	--	----------	--	----------	--	----------	--	----------	--	----------	--	----------	--	----------	--	----------	--	----------	--	----------	--	----------	--	----------	--	----------	--	----------	--	----------	--	----------	--	----------	--	----------	--	----------	--	----------	--

Curve Data
 $\Delta = 1^\circ 44' 12.55''$ (RT)
 T = 550.23
 L = 1,100.37
 R = 36,300.00
 E = 4.17

Curve Data
 $\Delta = 1^\circ 44' 11.32''$ (RT)
 T = 348.00
 L = 695.95
 R = 22,963.06
 E = 2.64

Rutland TWP.
 T-89N R-43W
 SEC. 32



TO WBL'S BUT MAY GRADE AND RADI11 SD RD TO FROM THE EAST WILL WE WOULD BE COURSE

LOWERED INLET FLOW SO A DIKE WOULD WORK

STAGE 1 RCB DESIGN EXTEND OLD RCB STAGE 2 REMOVE OLD & EXTEND

STAGE 1 LAY LEAVE MEDIAN OPEN STAGE 2 EXTEND & REMOVE OLD PIPE

STAGE 1 UAC STAGE 2 REMOVE

HAS LOWER FLOWLINE BUT ENDWALL AT 1350.50 IS DITCH ELEV

0.17 ac PEM Wetland
 OLD DES# 1156
 Sta. 414+01.71
 8.0 X 8.0 X 98.6 RCB W/FLUME
 D.A. = 236 Ac - R-H
 263 AC R-H

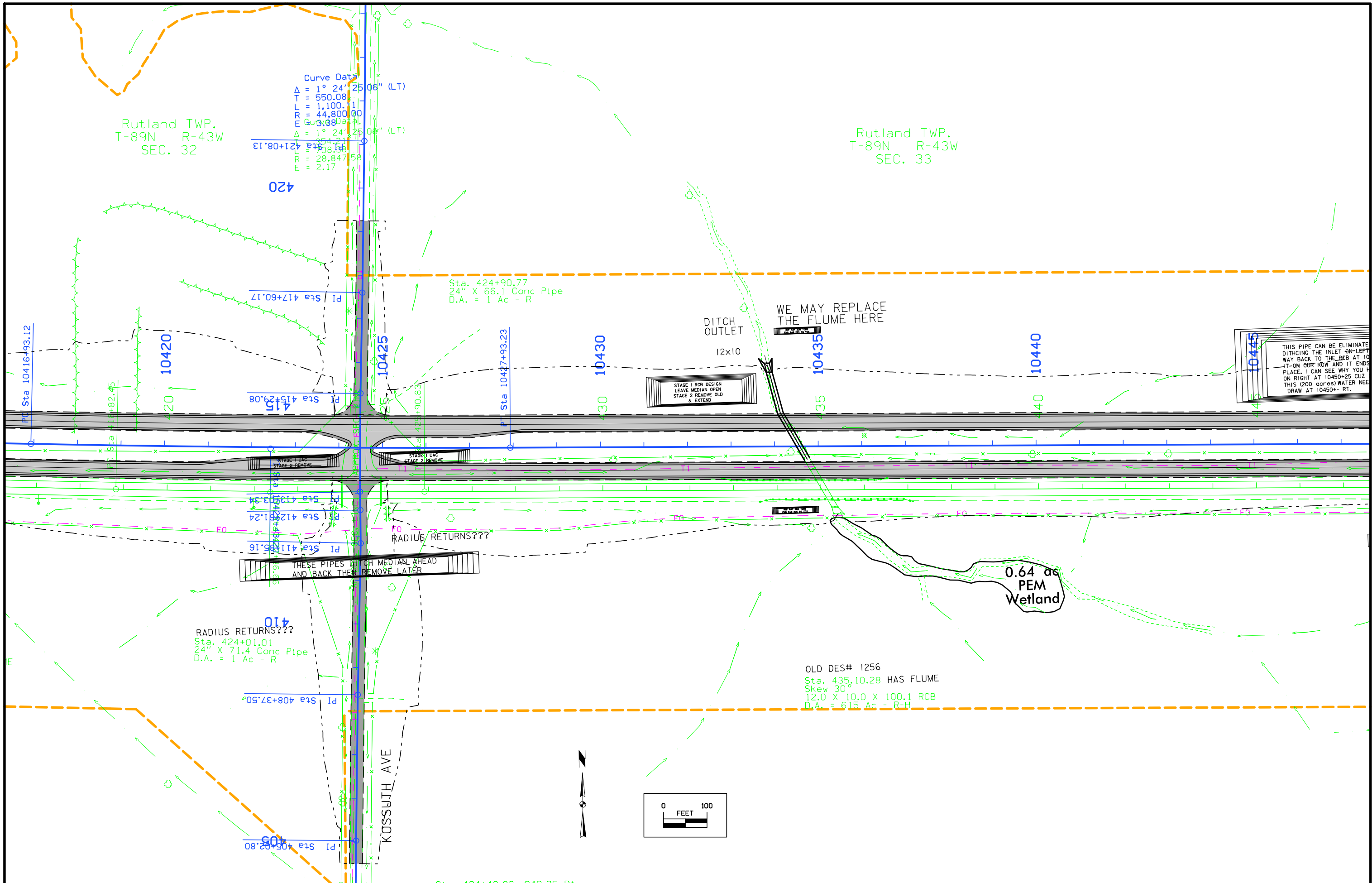
Sta. 396+15.17
 24" X 114.0 Conc Pipe
 D.A. = 5 Ac - R

Sta. 402+39.67
 24" X 66.4 Conc Pipe
 D.A. = 6 Ac - R

1.49 Conc Pipe



1,403.61	1,403.79	1,403.97	1,404.13	1,404.28	1,404.42	1,404.54	1,404.66	1,404.76	1,404.85	1,404.93	1,405.00	1,405.05	1,405.10	1,405.13	1,405.15	1,405.16	1,405.15	1,405.14	1,405.11	1,405.07	1,405.02	1,404.95	1,404.88	1,404.79	1,404.69	1,404.58	1,404.46	1,404.32	1,404.18	1,404.02	1,403.85	1,403.67	1,403.47	1,403.27	1,403.05	1,402.82	1,402.58	1,402.32	1,402.06	1,401.78	1,401.49	1,401.19	1,400.88	1,400.55	1,400.22	1,399.87	1,399.51	1,399.14	1,398.75	1,398.36	1,397.95	1,397.53	1,397.10	1,396.65	1,396.20	1,395.73	1,395.25	1,394.76	1,394.26	1,393.74	1,393.22	1,392.68	1,392.13	1,391.57	1,390.99	1,390.41	1,389.81	1,389.20	1,388.58	1,387.94	1,387.30	1,386.64	1,385.97	1,385.30	1,384.62	1,383.95	1,383.27	1,382.60	1,381.92	1,381.25	1,380.57	1,379.91	1,379.28	1,378.67	1,378.10	1,377.55	1,377.02	1,376.53	1,376.06	1,375.62	1,375.21	1,374.83	1,374.47	1,374.15	1,373.85	1,373.57	1,373.33	1,373.11	1,372.92	1,372.76	1,372.63	1,372.63	1,372.52	1,372.45	1,372.40	1,372.37	1,372.38	1,372.38	1,372.41	1,372.47	1,372.56	1,372.68	1,372.82	1,373.00	1,373.20	1,373.42	1,373.68	1,373.96	1,374.27	1,374.59	1,374.90
----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------



Curve Data
 $\Delta = 1^\circ 24' 25.06''$ (LT)
 $T = 550.08$
 $L = 1,100.11$
 $R = 44,800.00$
 $E = 3.68$
 $D.A. = 1.17$

Rutland TWP.
 T-89N R-43W
 SEC. 32

Rutland TWP.
 T-89N R-43W
 SEC. 33

Sta. 424+90.77
 24" X 66.1 Conc Pipe
 D.A. = 1 Ac - R

WE MAY REPLACE
 THE FLUME HERE

DITCH
 OUTLET
 12x10

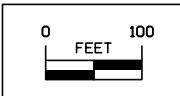
THIS PIPE CAN BE ELIMINATED
 DITCHING THE INLET ON-LEFT
 WAY BACK TO THE BEB AT 10445
 IT-ON OUR ROW AND IT ENDS
 PLACE. I CAN SEE WHY YOU H
 ON RIGHT AT 10450+25 CUZ
 THIS (200 acres) WATER NEED
 DRAW AT 10450+- RT.

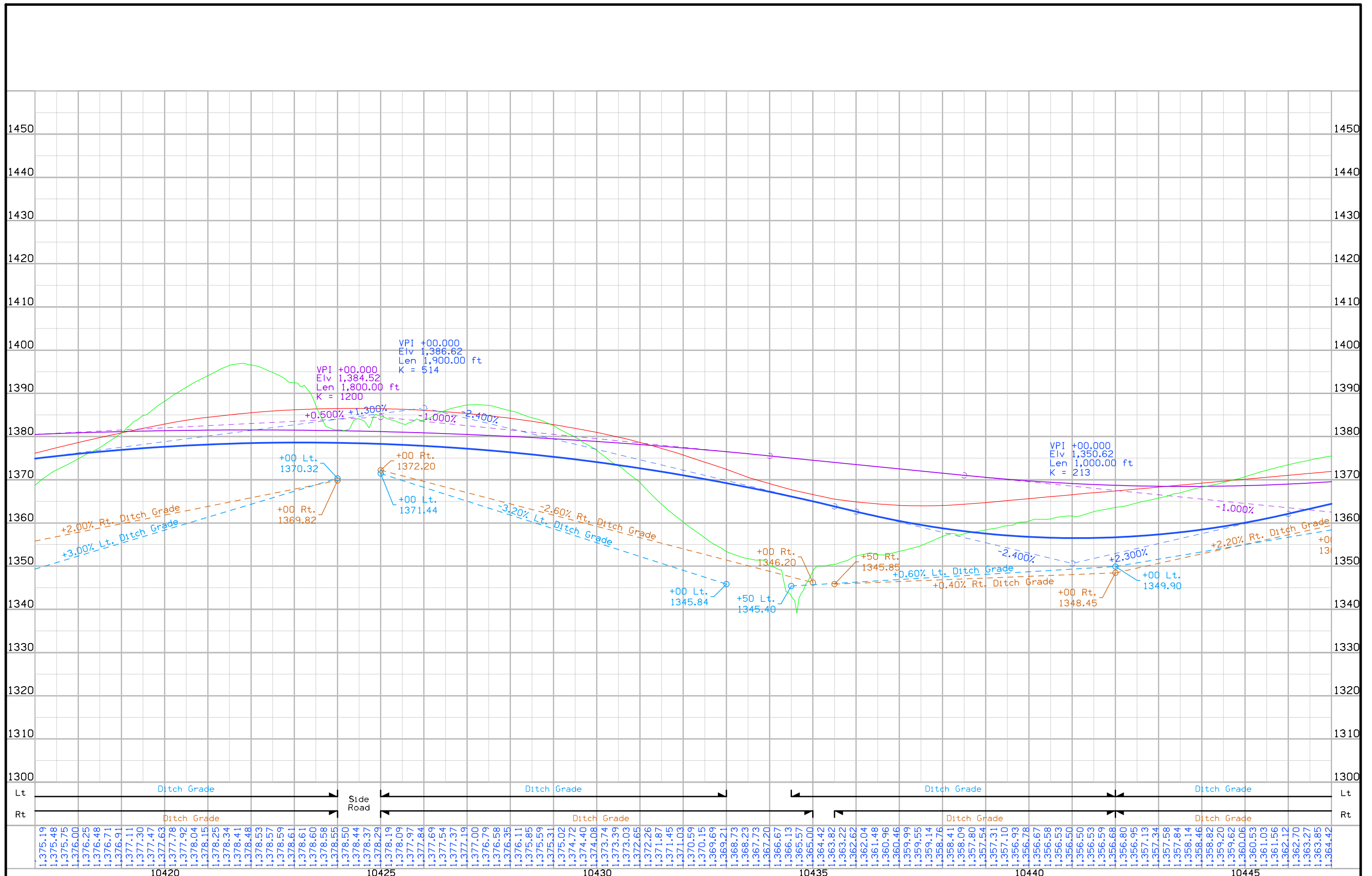
THESE PIPES BLIND MEDIAN AHEAD
 AND BACK THEN REMOVE LATER

0.64 ac
 PEM
 Wetland

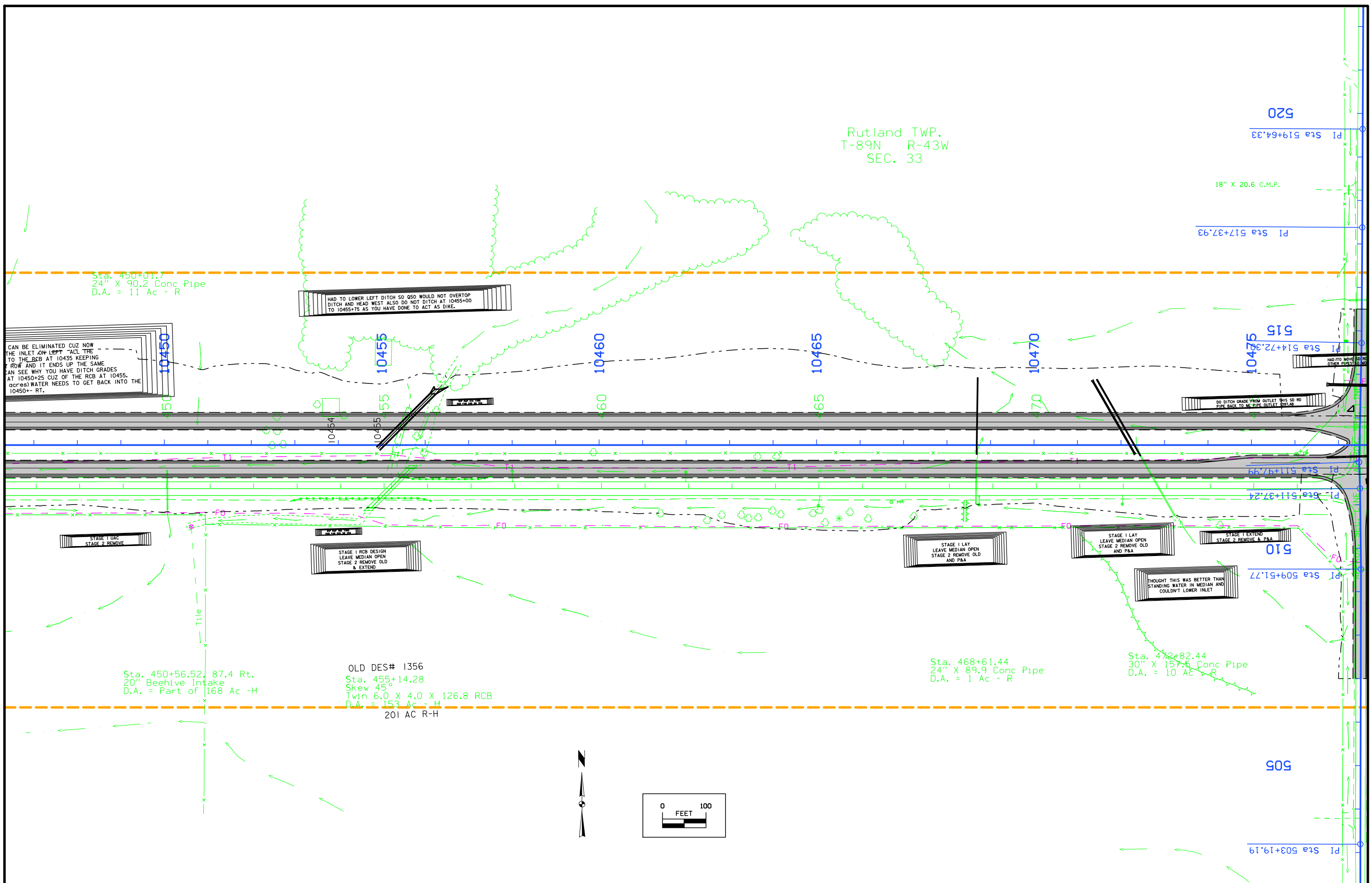
RADIUS RETURNS???
 Sta. 424+01.01
 24" X 71.4 Conc Pipe
 D.A. = 1 Ac - R

OLD DES# 1256
 Sta. 435.10.28 HAS FLUME
 Skew 30°
 12.0 X 10.0 X 100.1 RCB
 D.A. = 615 Ac - R-H





Rutland TWP.
T-89N R-43W
SEC. 33



Sta. 450+01.7
24" X 90.2' Conc Pipe
D.A. = 11 Ac - R

HAD TO LOWER LEFT DITCH SO QSO WOULD NOT OVERTOP
DITCH AND HEAD WEST ALSO DO NOT DITCH AT 10455+00
TO 10455+75 AS YOU HAVE DONE TO ACT AS DIKE.

CAN BE ELIMINATED CUZ NOW
THE INLET ON LEFT - ALL THE
TO THE RCB AT 10435 KEEPING
ROW AND IT ENDS UP THE SAME
CAN SEE WHY YOU HAVE DITCH GRADES
AT 10450+25 CUZ OF THE RCB AT 10455.
(acres) WATER NEEDS TO GET BACK INTO THE
10450+ RT.

STAGE 1 RCB DESIGN
LEAVE MEDIAN OPEN
STAGE 2 REMOVE OLD
& EXTEND

STAGE 1 LAY
LEAVE MEDIAN OPEN
STAGE 2 REMOVE OLD
AND P&A

STAGE 1 LAY
LEAVE MEDIAN OPEN
STAGE 2 REMOVE OLD
AND P&A

STAGE 1 EXTEND
STAGE 2 REMOVE & P&A

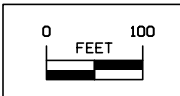
THOUGHT THIS WAS BETTER THAN
STANDING WATER IN MEDIAN AND
COULDN'T LOWER INLET

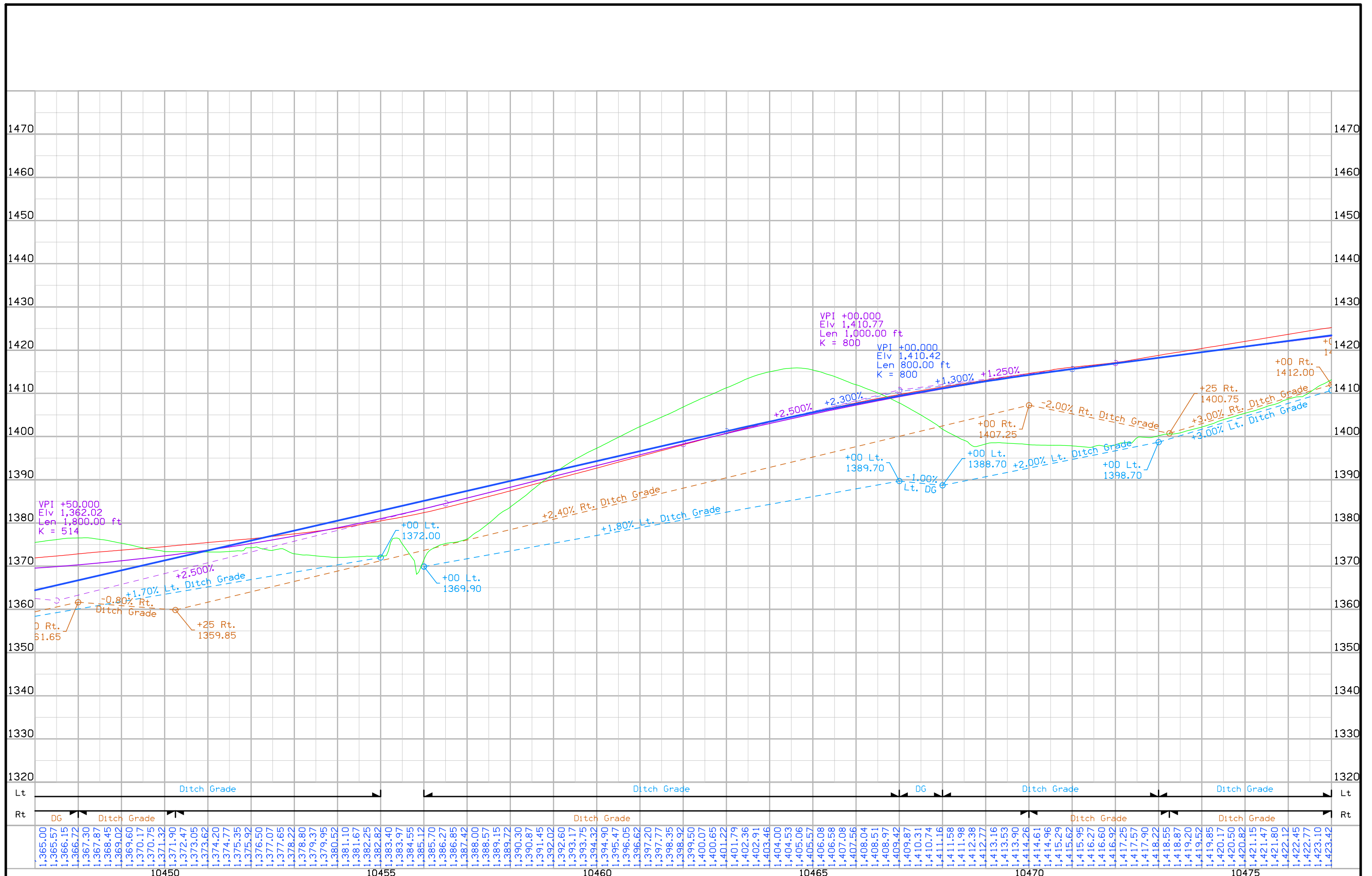
Sta. 450+56.52, 87.4 Rt.
20" Beehive Intake
D.A. = Part of 168 Ac -H

OLD DES# 1356
Sta. 455+14.28
Skew 45°
Twin 6.0 X 4.0 X 126.8 RCB
D.A. = 153 Ac -H
201 AC R-H

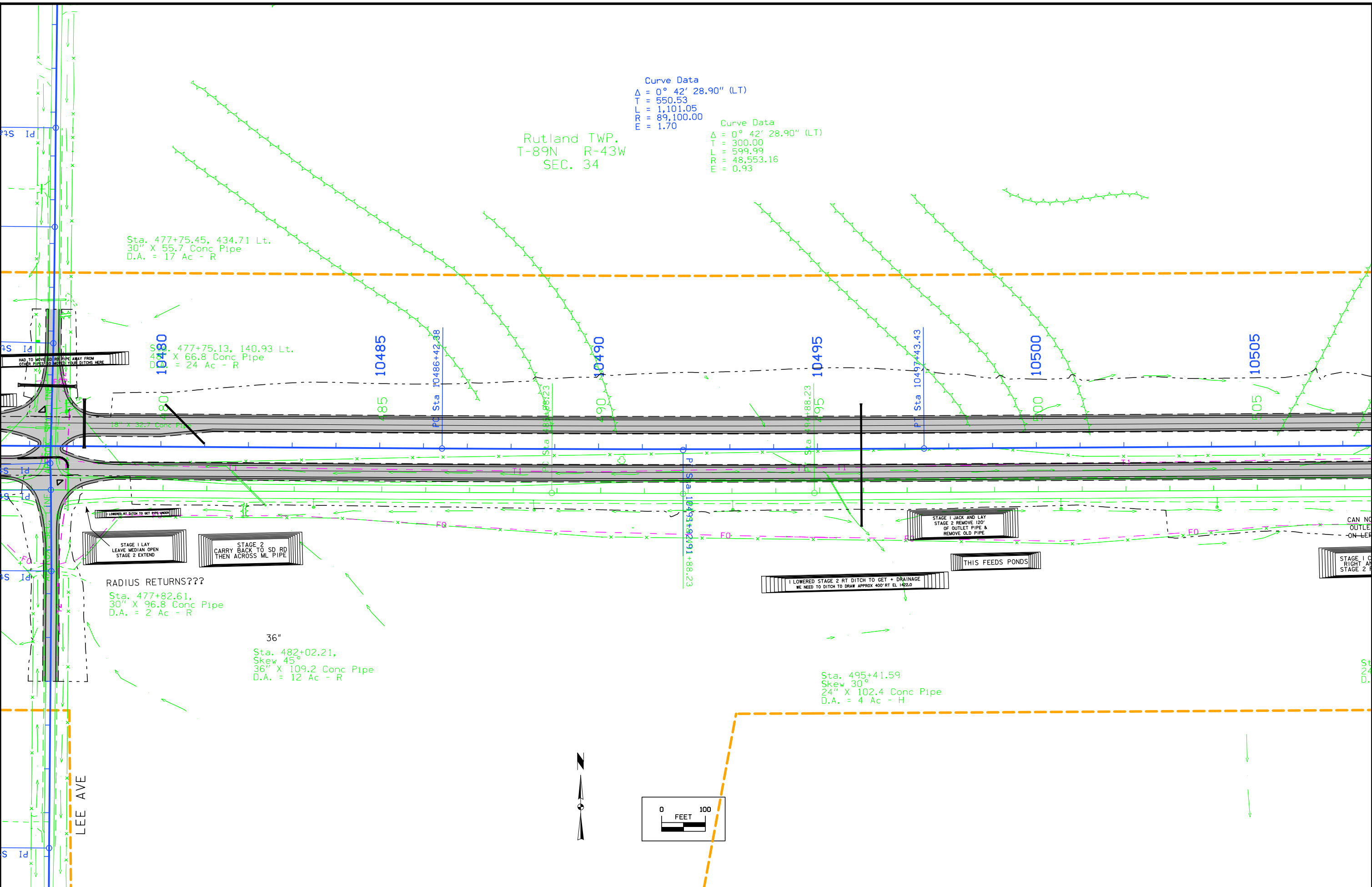
Sta. 468+61.44
24" X 89.9' Conc Pipe
D.A. = 1 Ac - R

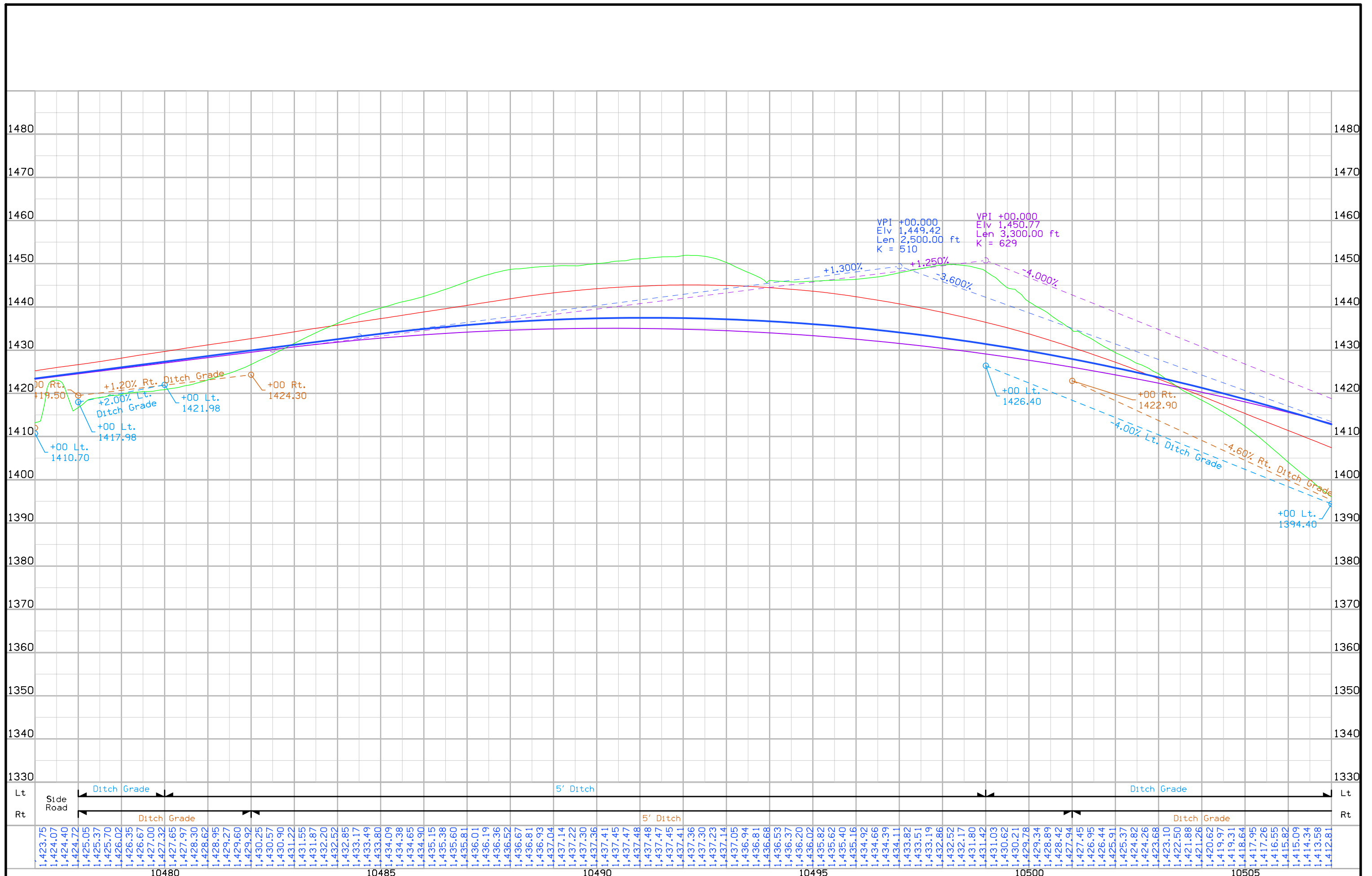
Sta. 472+82.44
30" X 157.5' Conc Pipe
D.A. = 10 Ac - R



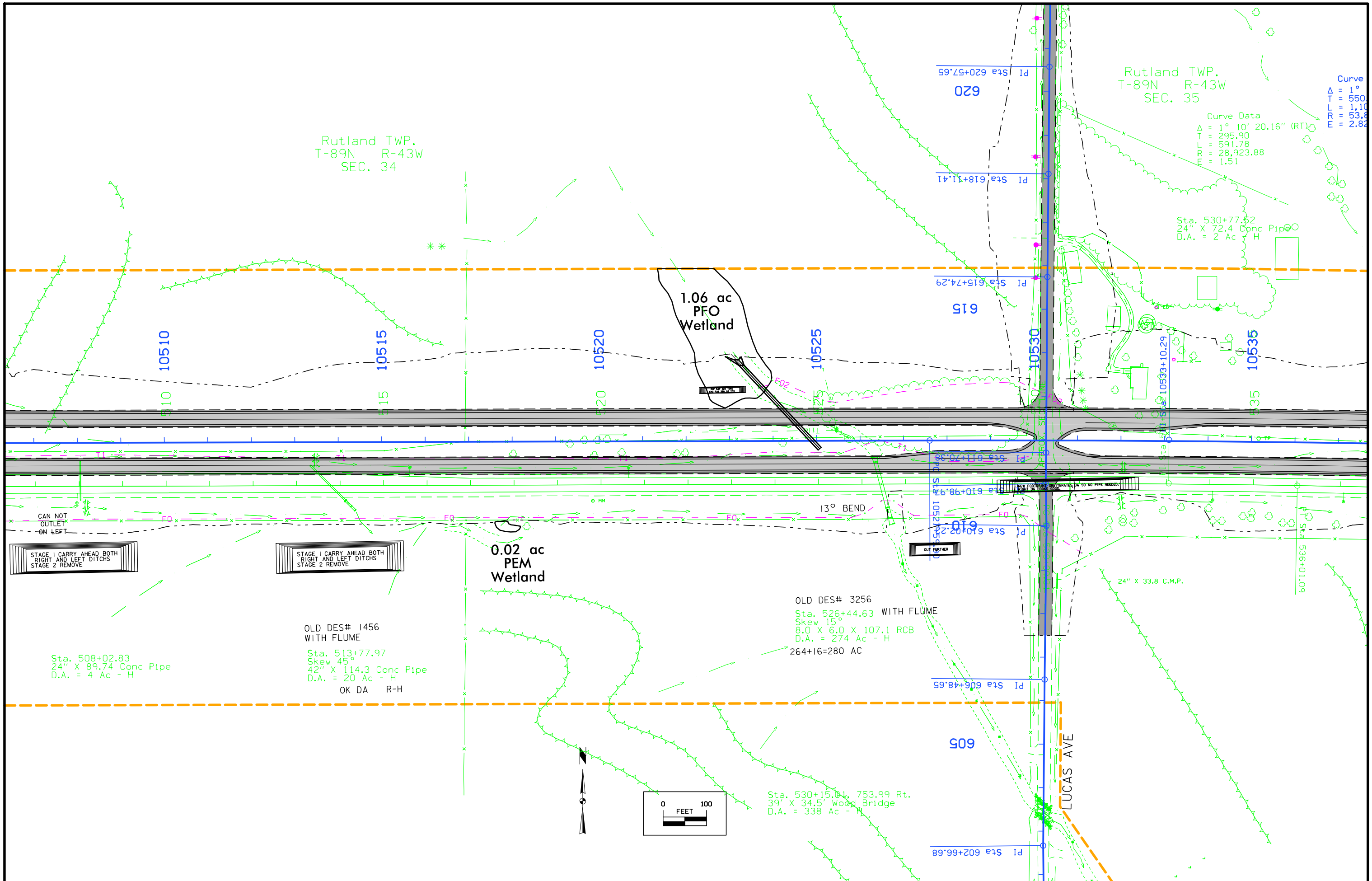


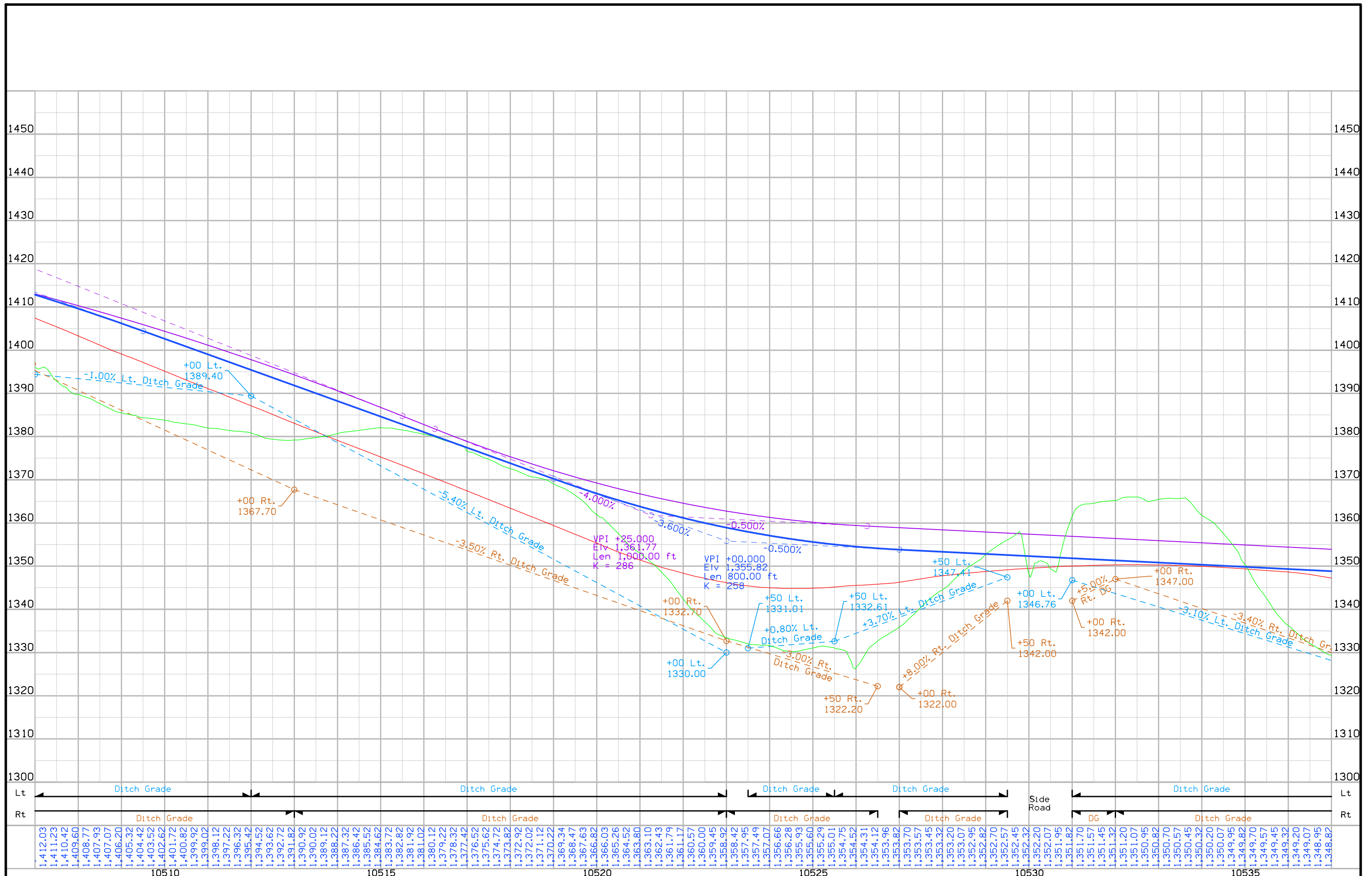
1,365.00	1,365.57	1,366.15	1,366.72	1,367.30	1,367.87	1,368.45	1,369.02	1,369.60	1,370.17	1,370.75	1,371.32	1,371.90	1,372.47	1,373.05	1,373.62	1,374.20	1,374.77	1,375.35	1,375.92	1,376.50	1,377.07	1,377.65	1,378.22	1,378.80	1,379.37	1,379.95	1,380.52	1,381.10	1,381.67	1,382.25	1,382.82	1,383.40	1,383.97	1,384.55	1,385.12	1,385.70	1,386.27	1,386.85	1,387.42	1,388.00	1,388.57	1,389.15	1,389.72	1,390.30	1,390.87	1,391.45	1,392.02	1,392.60	1,393.17	1,393.75	1,394.32	1,394.90	1,395.47	1,396.05	1,396.62	1,397.20	1,397.77	1,398.35	1,398.92	1,399.50	1,400.07	1,400.65	1,401.22	1,401.79	1,402.36	1,402.91	1,403.46	1,404.00	1,404.53	1,405.06	1,405.57	1,406.08	1,406.58	1,407.08	1,407.56	1,408.04	1,408.51	1,408.97	1,409.42	1,409.87	1,410.31	1,410.74	1,411.16	1,411.58	1,411.98	1,412.38	1,412.77	1,413.16	1,413.53	1,413.90	1,414.26	1,414.61	1,414.96	1,415.29	1,415.62	1,415.95	1,416.27	1,416.60	1,416.92	1,417.25	1,417.57	1,417.90	1,418.22	1,418.55	1,418.87	1,419.20	1,419.52	1,419.85	1,420.17	1,420.50	1,420.82	1,421.15	1,421.47	1,421.80	1,422.12	1,422.45	1,422.77	1,423.10	1,423.42
----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------





1,423.75	1,424.07	1,424.40	1,425.05	1,425.37	1,425.70	1,426.02	1,426.35	1,426.67	1,427.00	1,427.32	1,427.65	1,427.97	1,428.30	1,428.62	1,428.95	1,429.27	1,429.60	1,429.92	1,430.25	1,430.57	1,430.90	1,431.22	1,431.55	1,431.87	1,432.20	1,432.52	1,432.85	1,433.17	1,433.49	1,433.80	1,434.09	1,434.38	1,434.65	1,434.90	1,435.15	1,435.38	1,435.60	1,435.81	1,436.01	1,436.19	1,436.36	1,436.52	1,436.67	1,436.81	1,436.93	1,437.04	1,437.14	1,437.22	1,437.30	1,437.36	1,437.41	1,437.45	1,437.47	1,437.48	1,437.48	1,437.47	1,437.45	1,437.41	1,437.36	1,437.30	1,437.23	1,437.14	1,437.05	1,436.94	1,436.81	1,436.68	1,436.53	1,436.37	1,436.20	1,436.02	1,435.82	1,435.62	1,435.40	1,435.16	1,434.92	1,434.66	1,434.39	1,434.11	1,433.82	1,433.51	1,433.19	1,432.86	1,432.52	1,432.17	1,431.80	1,431.42	1,431.03	1,430.62	1,430.21	1,429.78	1,429.34	1,428.89	1,428.42	1,427.94	1,427.45	1,426.95	1,426.44	1,425.91	1,425.37	1,424.82	1,424.26	1,423.68	1,423.10	1,422.50	1,421.88	1,421.26	1,420.62	1,419.97	1,419.31	1,418.64	1,417.95	1,417.26	1,416.55	1,415.82	1,415.09	1,414.34	1,413.58	1,412.81
----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------

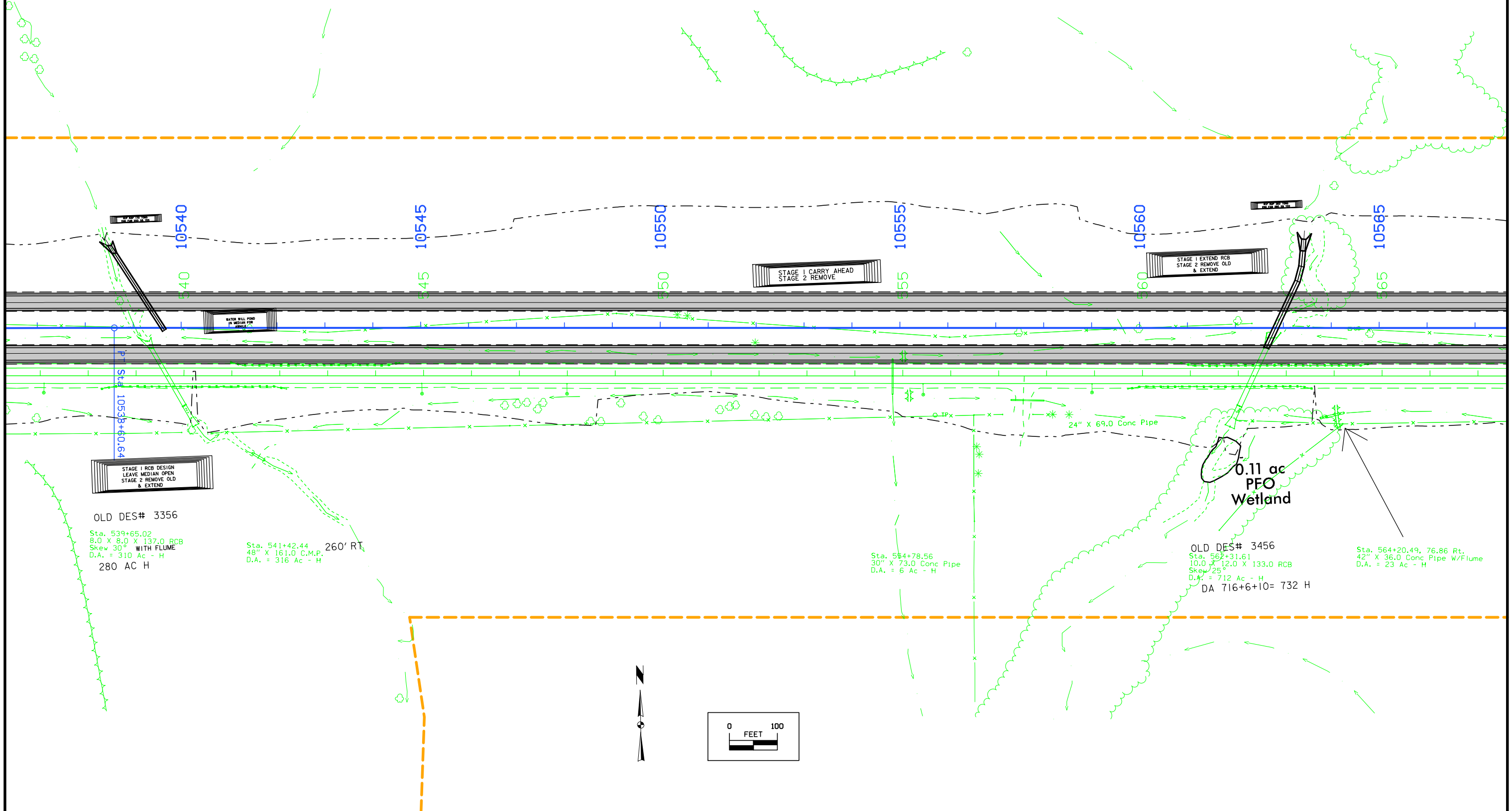




C		ENGLISH	IOWA DOT	DESIGN TEAM Flattery\Johnson	WOODBURY COUNTY	PROJECT NUMBER NHSX-020-1(116)--3H-97	SHEET NUMBER D.29
---	--	---------	----------	------------------------------	-----------------	---------------------------------------	-------------------

Curve Data
 $\Delta = 1^\circ 10' 20.16''$ (RT)
 $T = 550.39$
 $L = 1,100.74$
 $R = 53,800.00$
 $E = 2.82$

Rutland TWP.
 T-89N R-43W
 SEC. 35



OLD DES# 3356
 Sta. 539+65.02
 8.0' X 8.0' X 137.0 RCB
 Skew 30° WITH FLUME
 D.A. = 310 Ac - H
 280 AC H

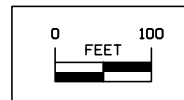
Sta. 541+42.44 260' RT
 48" X 161.0 C.M.P.
 D.A. = 316 Ac - H

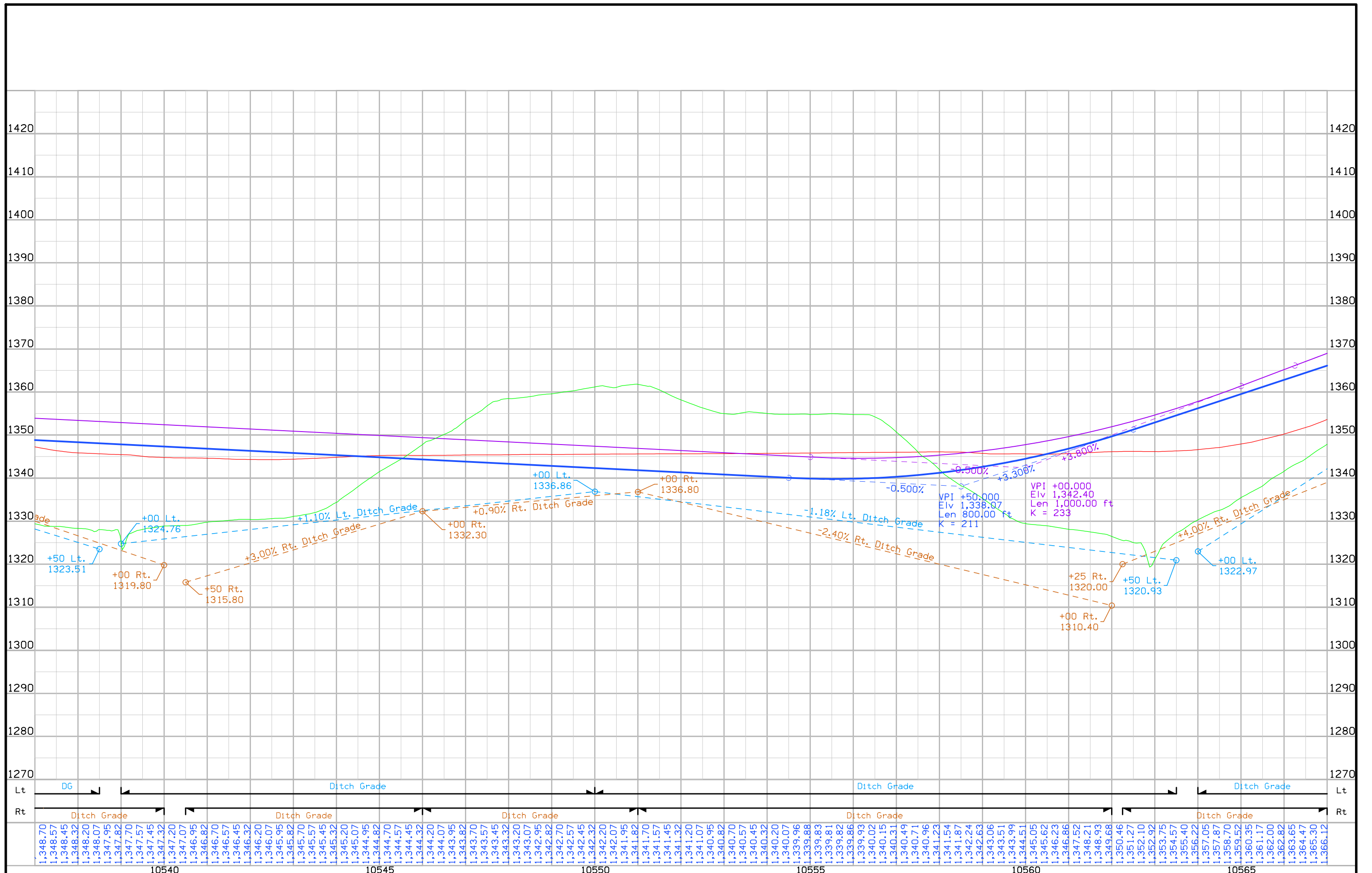
Sta. 554+78.56
 30" X 73.0 Conc Pipe
 D.A. = 6 Ac - H

OLD DES# 3456
 Sta. 562+31.61
 10.0' X 12.0' X 133.0 RCB
 Skew 25°
 D.A. = 712 Ac - H
 DA 716+6+10= 732 H

Sta. 564+20.49, 76.86 Rt.
 42" X 36.0 Conc Pipe W/Flume
 D.A. = 23 Ac - H

0.11 ac
 PFO
 Wetland



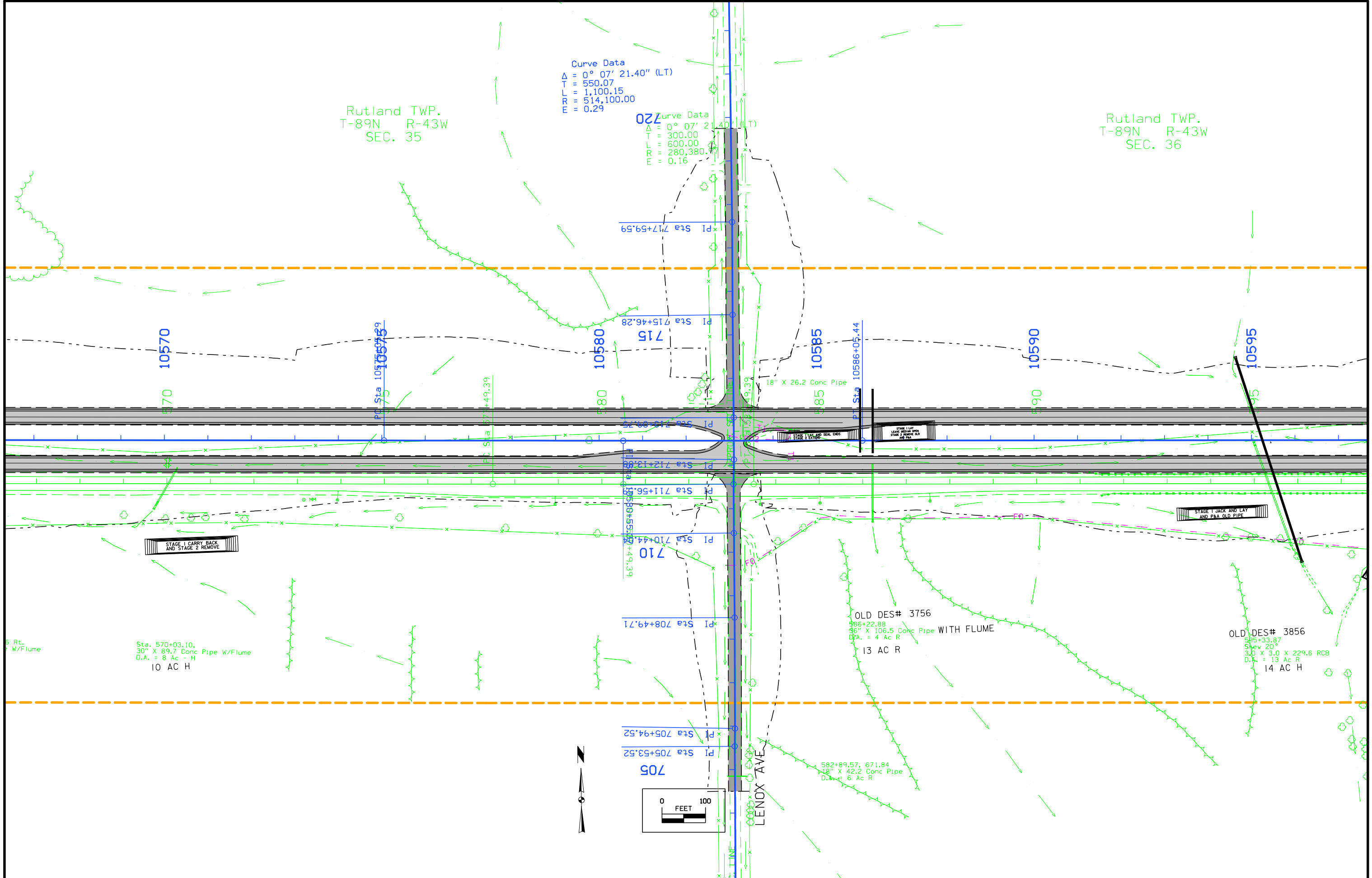


Rutland TWP.
T-89N R-43W
SEC. 35

Rutland TWP.
T-89N R-43W
SEC. 36

Curve Data
 $\Delta = 0^\circ 07' 21.40''$ (LT)
T = 550.07
L = 1,100.15
R = 514,100.00
E = 0.29

Curve Data
 $\Delta = 0^\circ 07' 21.40''$ (LT)
T = 300.00
L = 600.00
R = 280,380.00
E = 0.16



STAGE 1 CARRY BACK
AND STAGE 2 REMOVE

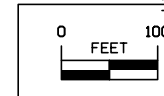
STAGE 1 JACK AND LAY
AND P&A OLD PIPE

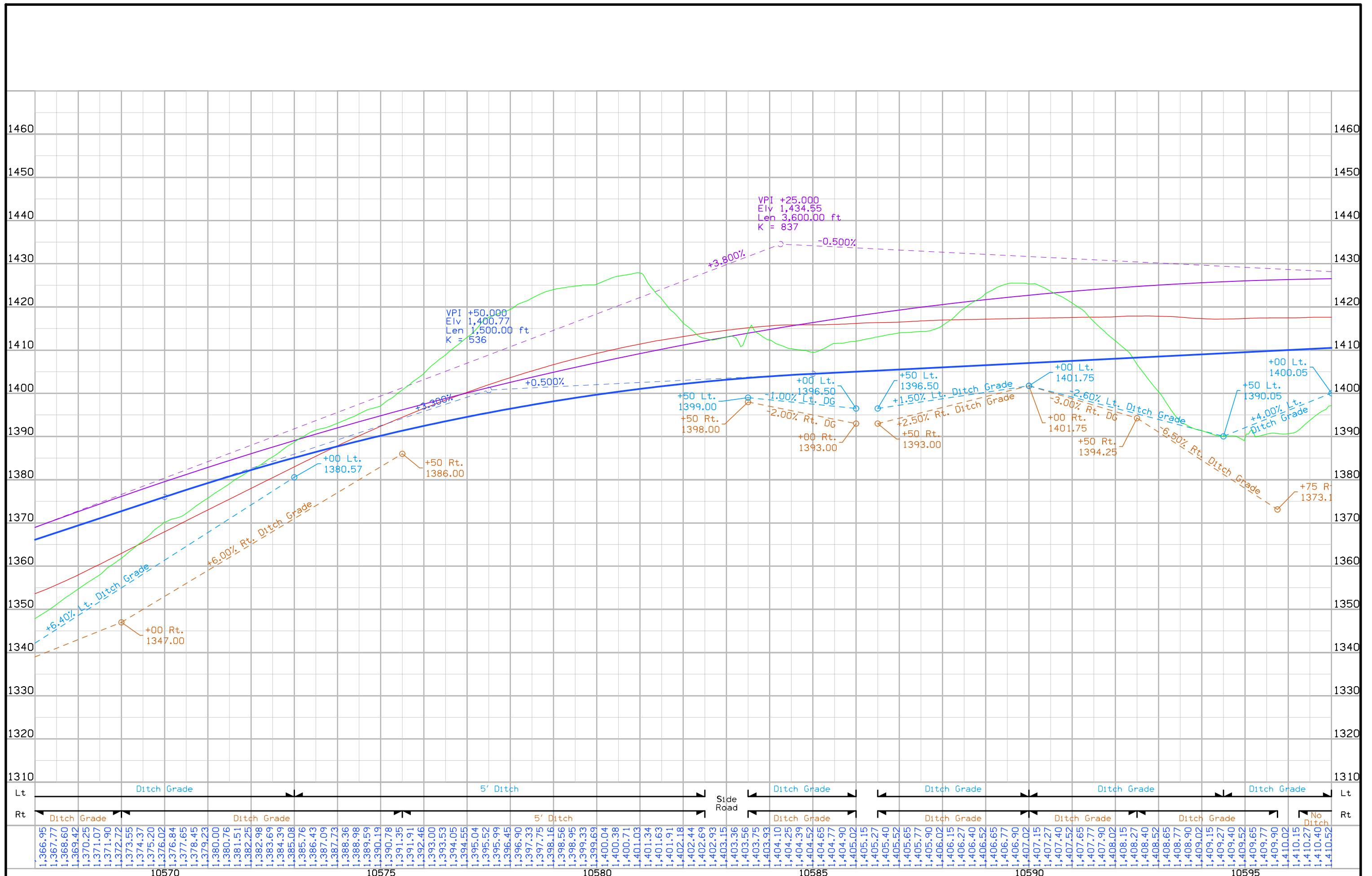
OLD DES# 3756
386+22.88
36" X 106.5 Conc Pipe WITH FLUME
D.A. = 4 Ac R
13 AC R

OLD DES# 3856
585+33.87
Slew 20°
3.0 X 3.0 X 229.6 RCB
D.A. = 13 Ac R
14 AC H

Sta. 570+03.10,
30" X 89.7 Conc Pipe W/Flume
D.A. = 8 Ac = H
10 AC H

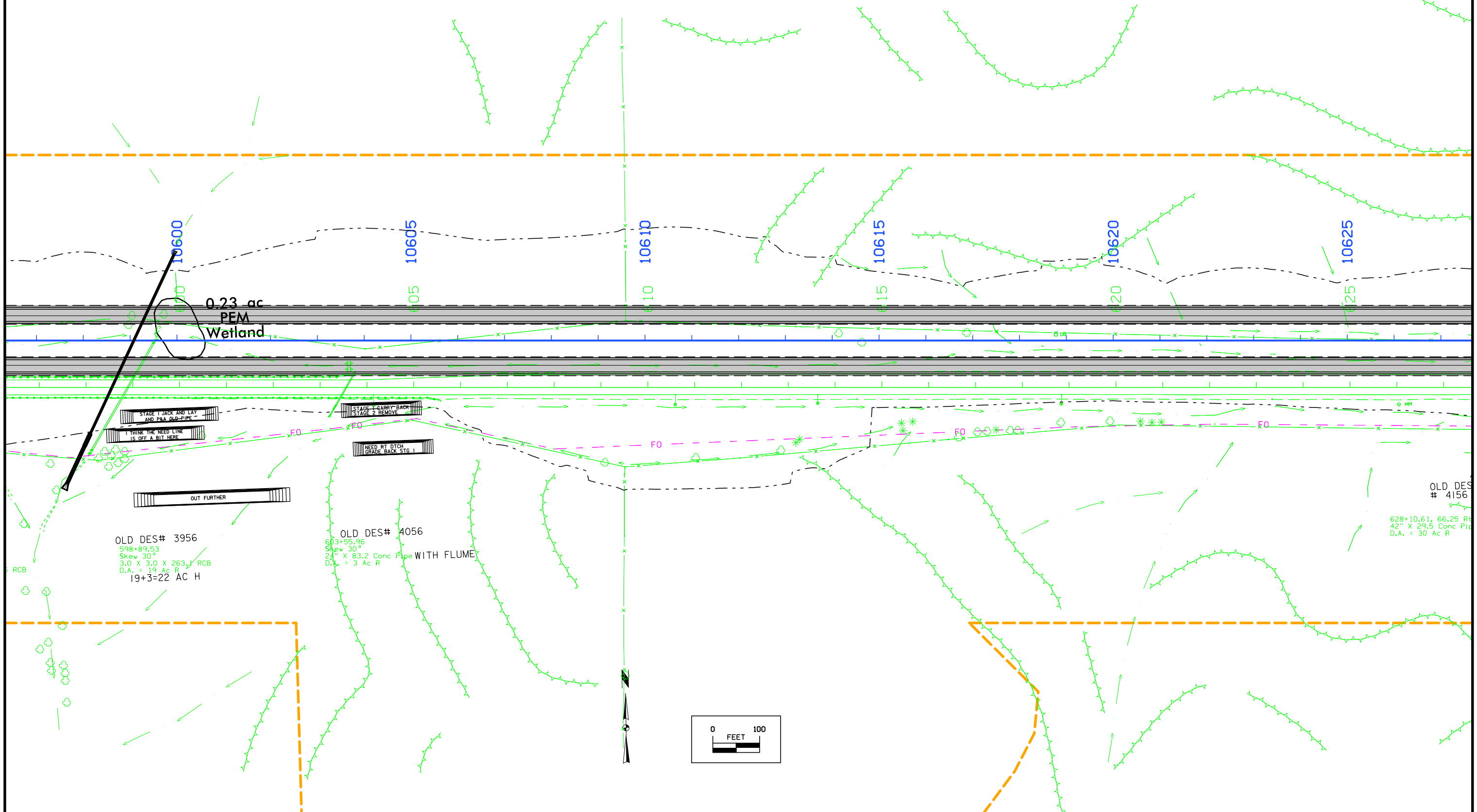
582+89.57, 671.84
18" X 42.2 Conc Pipe
D.A. = 6 Ac R

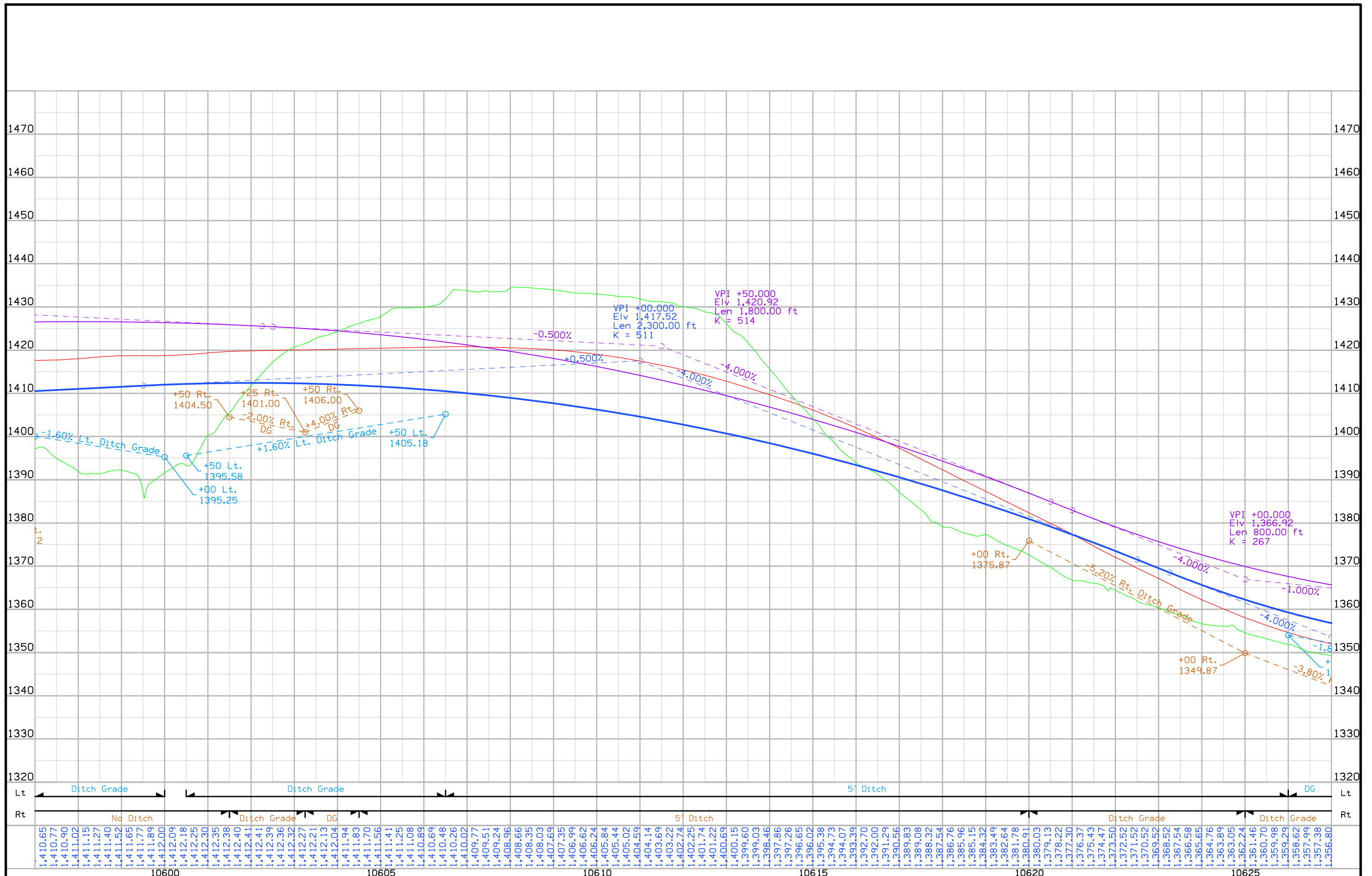


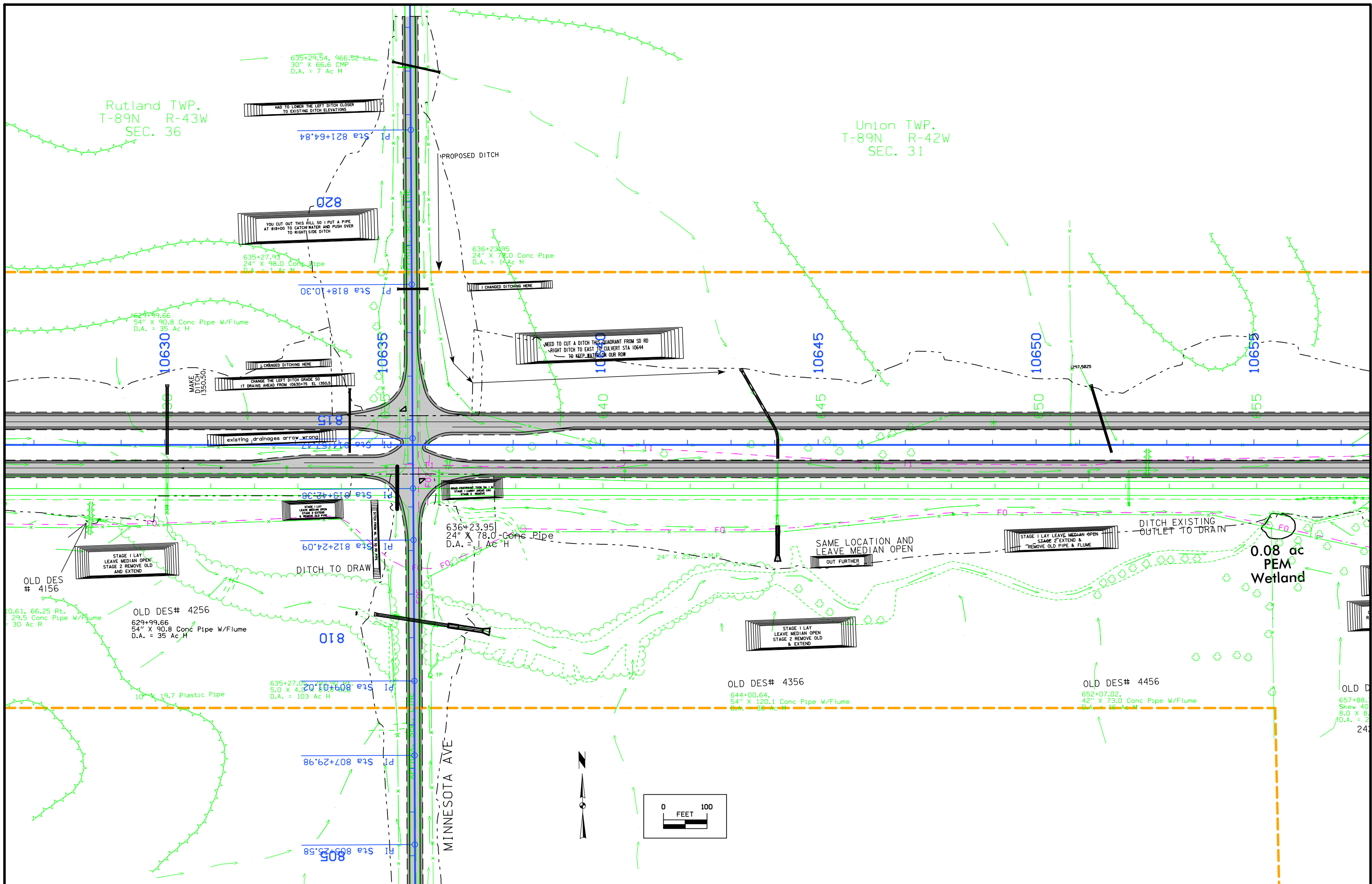


1,366.95	1,367.77	1,368.60	1,369.42	1,370.25	1,371.07	1,371.90	1,372.72	1,373.55	1,374.37	1,375.20	1,376.02	1,376.84	1,377.65	1,378.45	1,379.23	1,380.00	1,380.76	1,381.51	1,382.25	1,382.98	1,383.69	1,384.39	1,385.08	1,385.76	1,386.43	1,387.09	1,387.73	1,388.36	1,388.98	1,389.59	1,390.19	1,390.78	1,391.35	1,391.91	1,392.46	1,393.00	1,393.53	1,394.05	1,394.55	1,395.04	1,395.52	1,395.99	1,396.45	1,396.90	1,397.33	1,397.75	1,398.16	1,398.56	1,398.95	1,399.33	1,399.69	1,400.04	1,400.38	1,400.71	1,401.03	1,401.34	1,401.63	1,401.91	1,402.18	1,402.44	1,402.69	1,402.93	1,403.15	1,403.36	1,403.56	1,403.75	1,403.93	1,404.10	1,404.25	1,404.39	1,404.52	1,404.65	1,404.77	1,404.90	1,405.02	1,405.15	1,405.27	1,405.40	1,405.52	1,405.65	1,405.77	1,405.90	1,406.02	1,406.15	1,406.27	1,406.40	1,406.52	1,406.65	1,406.77	1,406.90	1,407.02	1,407.15	1,407.27	1,407.40	1,407.52	1,407.65	1,407.77	1,407.90	1,408.02	1,408.15	1,408.27	1,408.40	1,408.52	1,408.65	1,408.77	1,408.90	1,409.02	1,409.15	1,409.27	1,409.40	1,409.52	1,409.65	1,409.77	1,409.90	1,410.02	1,410.15	1,410.27	1,410.40	1,410.52
----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------

Rutland TWP.
T-89N R-43W
SEC. 36



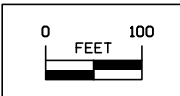




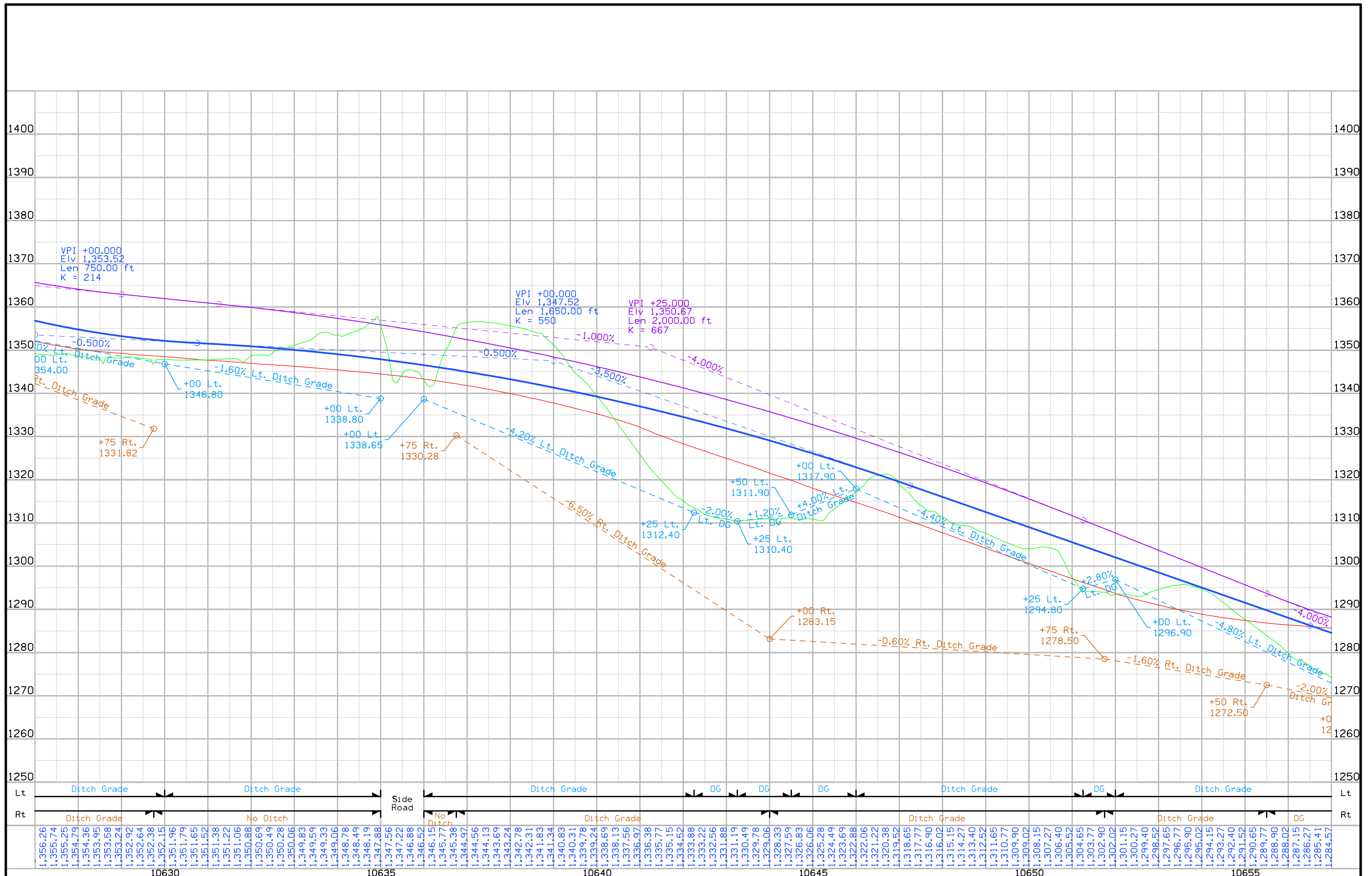
Rutland TWP.
T-89N R-43W
SEC. 36

Union TWP.
T-89N R-42W
SEC. 31

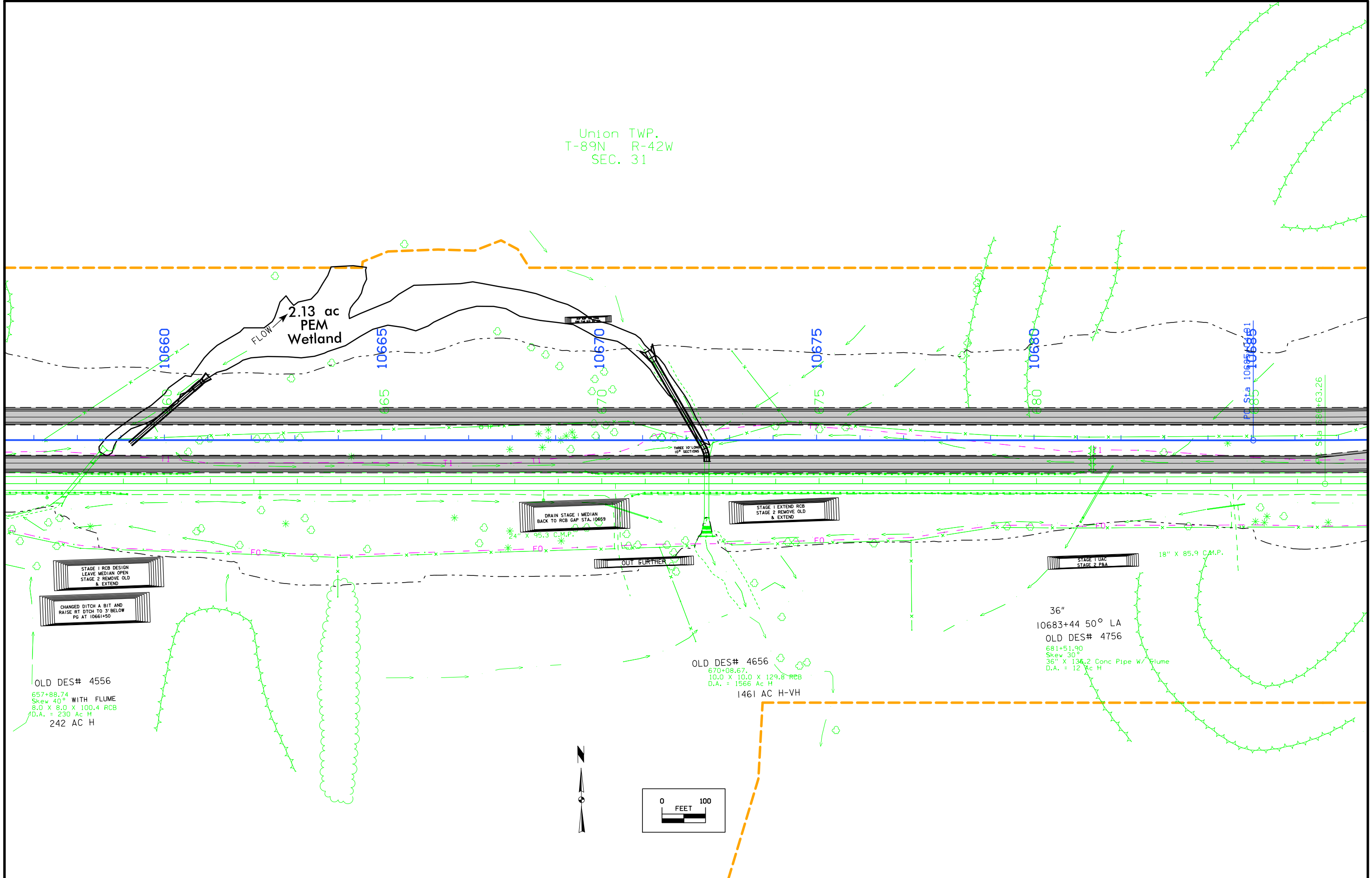
MINNESOTA AVE

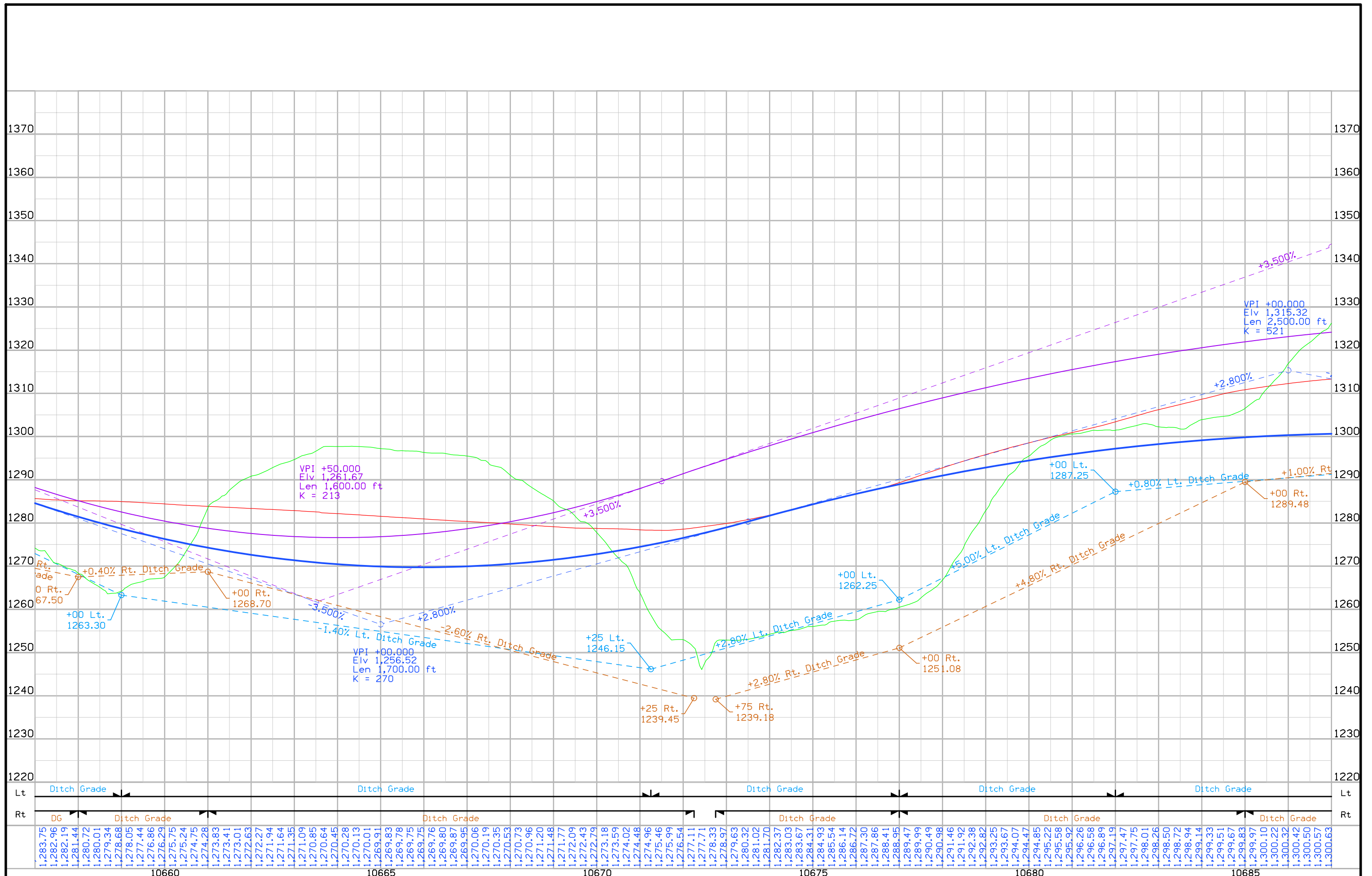


0.08 ac
PEM
Wetland



Union TWP.
T-89N R-42W
SEC. 31





Union TWP.
T-89N R-42W
SEC. 32

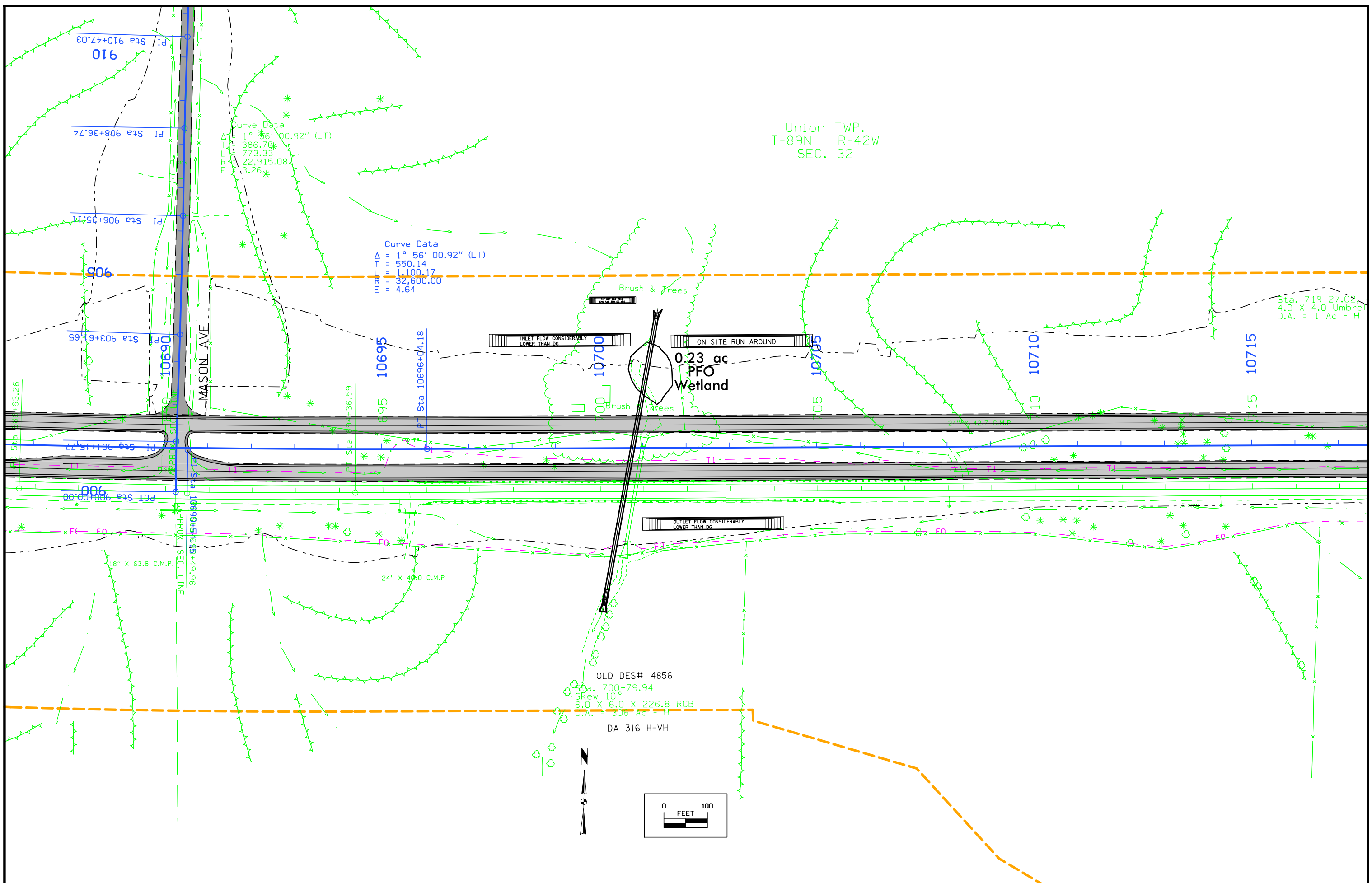
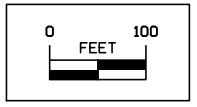
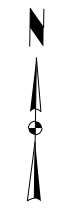
Curve Data
 $\Delta = 1^\circ 56' 00.92''$ (LT)
 T = 550.14
 L = 1,100.17
 R = 32,600.00
 E = 4.64

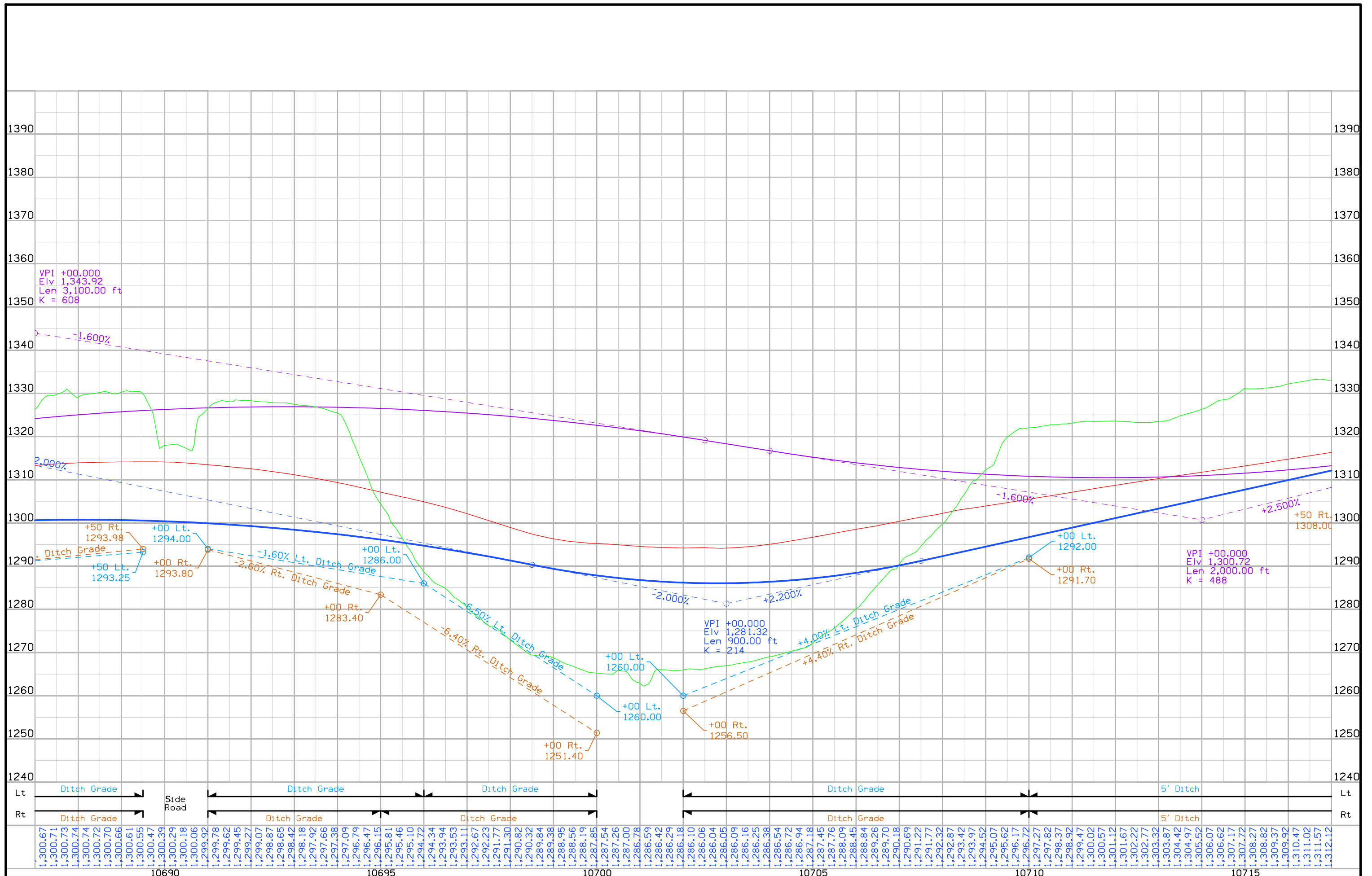
Curve Data
 $\Delta = 1^\circ 56' 00.92''$ (LT)
 T = 386.79
 L = 773.33
 R = 22,915.08
 E = 3.26

0.23 ac
PFO
Wetland

OLD DES# 4856
 Sta. 700+79.94
 Skew 10°
 6.0 X 6.0 X 226.8 RCB
 D.A. = 306 Ac - H
 DA 316 H-VH

Sta. 719+27.02
 4.0 X 4.0 Umbrel
 D.A. = 1 Ac - H

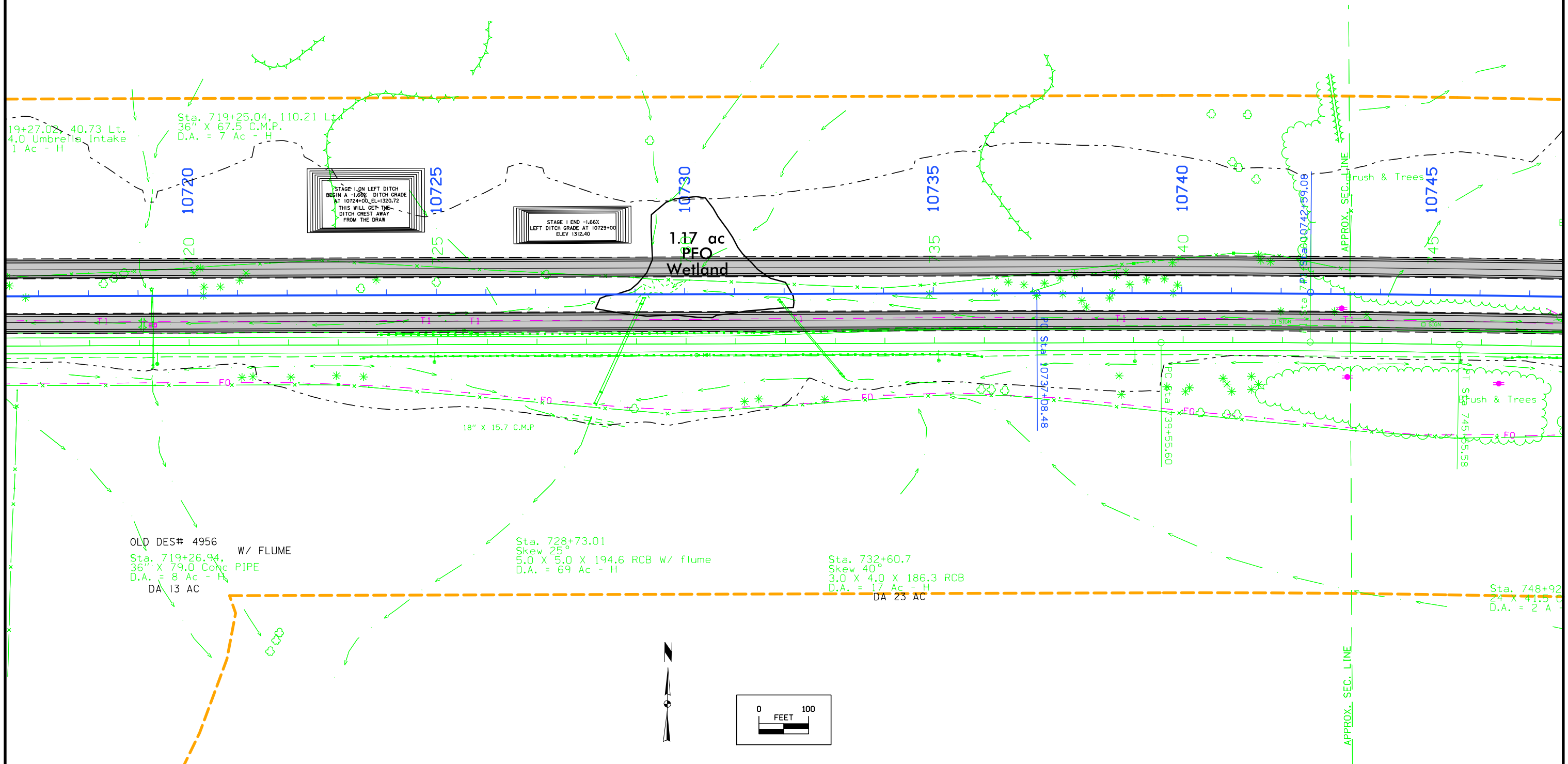


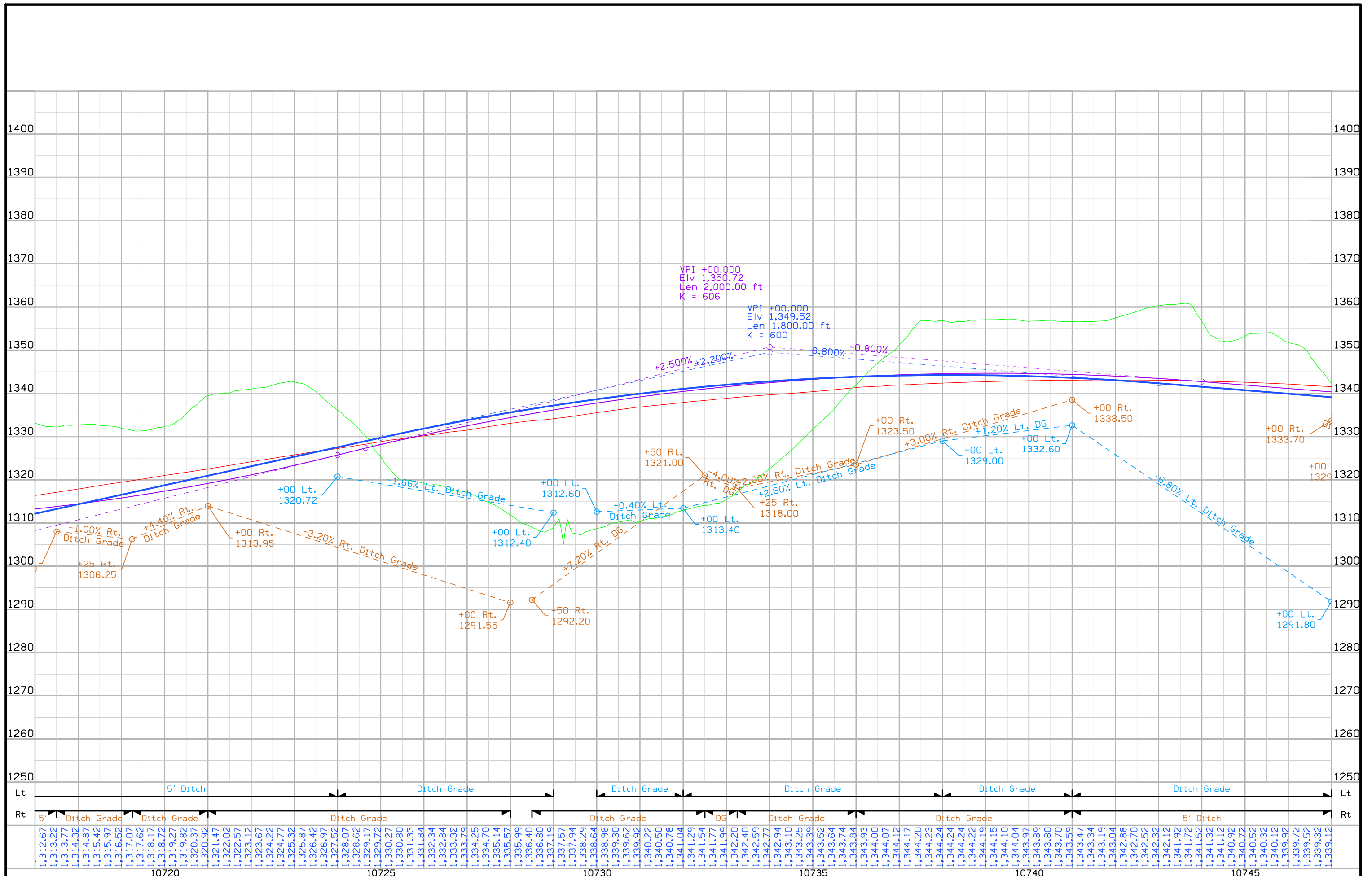


Union TWP.
T-89N R-42W
SEC. 32

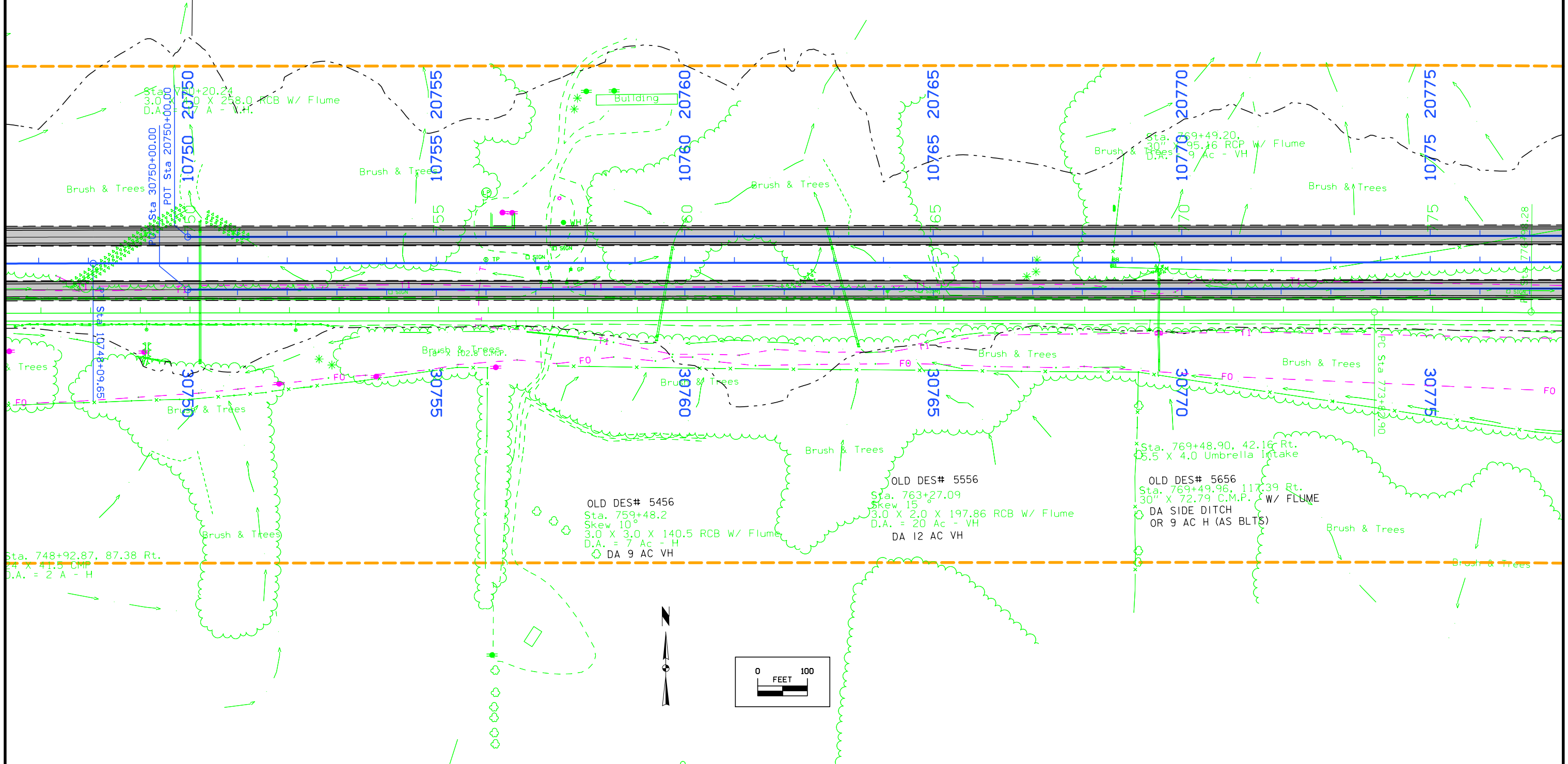
Curve Data
 $\Delta = 1^\circ 09' 58.39''$ (RT)
 $T = 550.60$
 $L = 1,101.17$
 $R = 54,100.00$
 $E = 2.88$

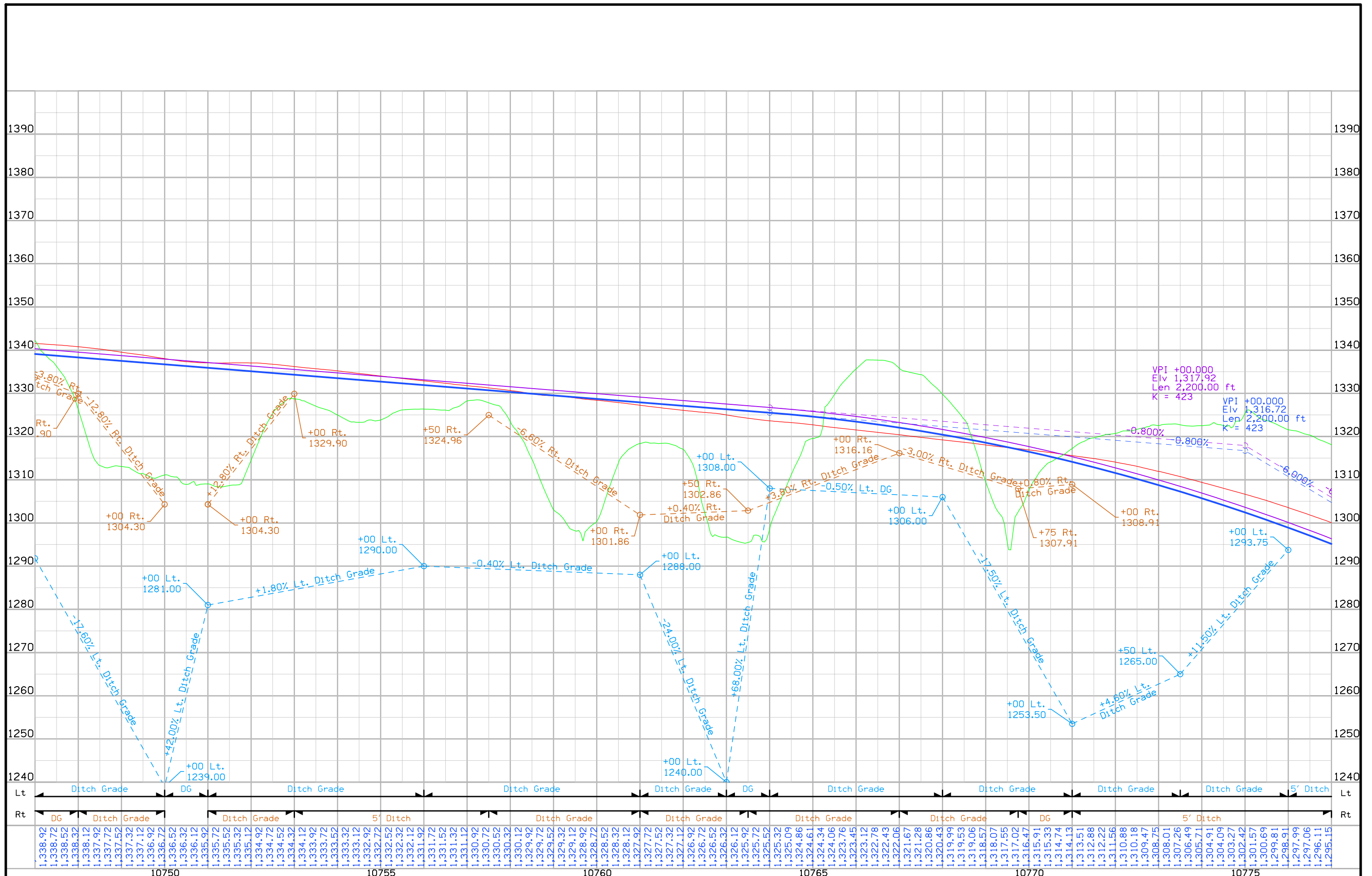
Curve Data
 $\Delta = 1^\circ 09' 58.39''$ (RT)
 $T = 300.00$
 $L = 599.98$
 $R = 29,476.70$
 $E = 1.53$





Union TWP.
T-89N R-42W
SEC. 33





C	ENGLISH	IOWA DOT	DESIGN TEAM Flattery\Johnson	WOODBURY COUNTY	PROJECT NUMBER NHSX-020-1(116)--3H-97	SHEET NUMBER D.45
---	---------	----------	------------------------------	-----------------	---------------------------------------	-------------------

Curve Data
 $\Delta = 1^\circ 03' 04.25''$ (RT)
 T = 315.39
 L = 630.75
 R = 34,380.00
 E = 1.45

Union TWP.
 T-89N R-42W
 SEC. 33

Curve Data
 $\Delta = 3^\circ 45' 58.23''$ (RT)
 T = 821.95
 L = 1,643.30
 R = 25,000.00
 E = 13.51

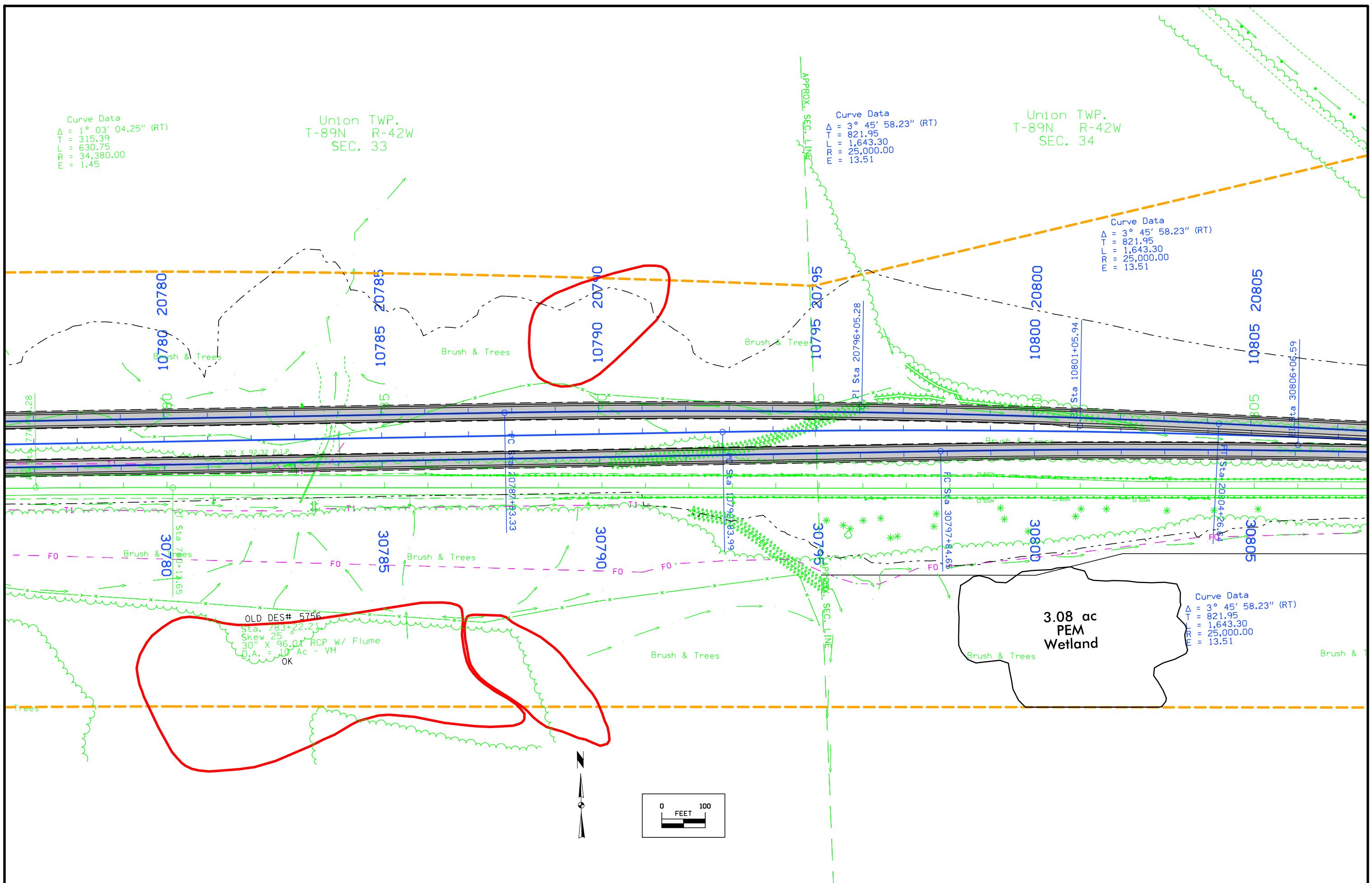
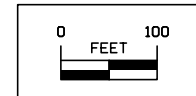
Union TWP.
 T-89N R-42W
 SEC. 34

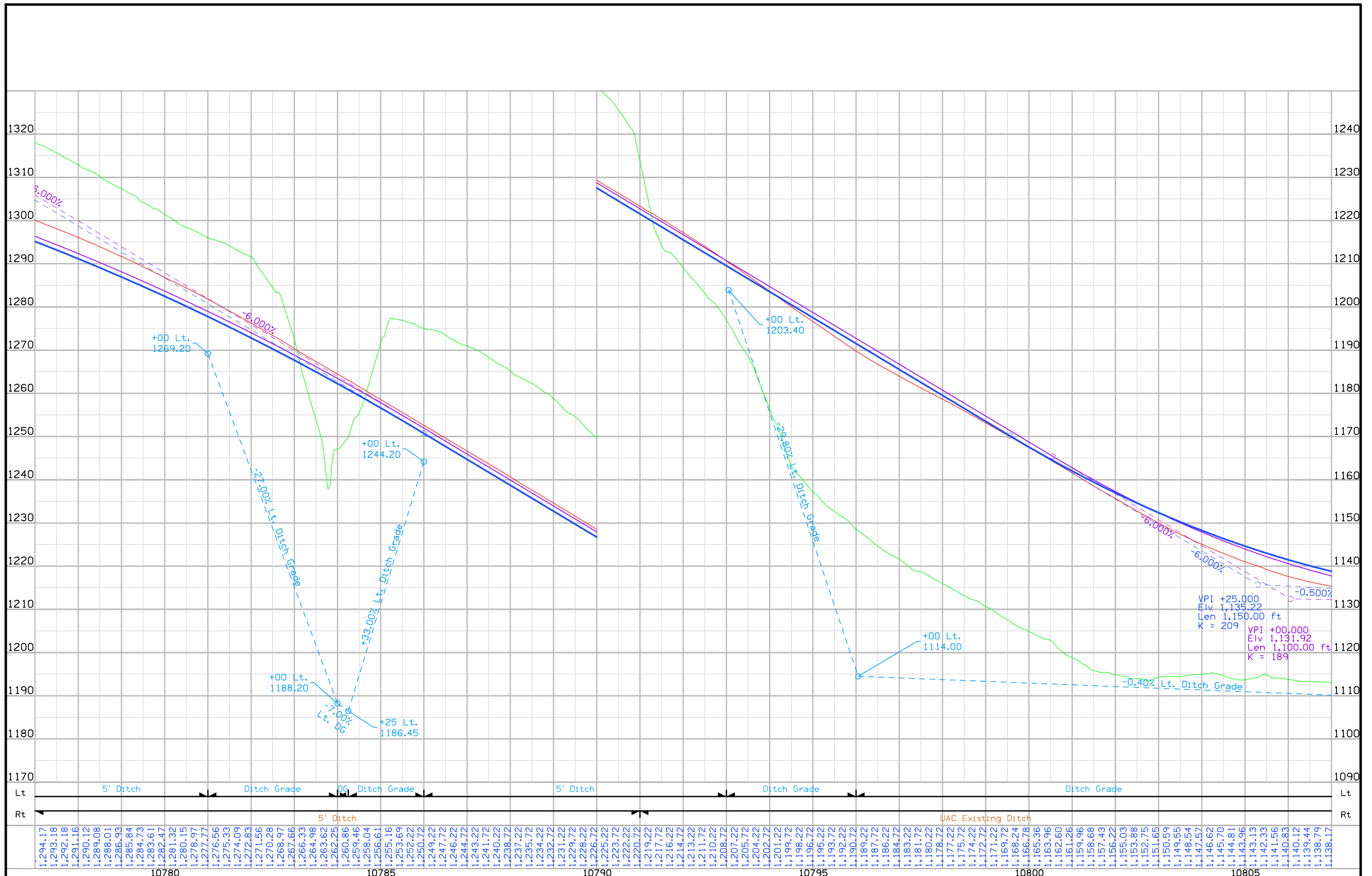
Curve Data
 $\Delta = 3^\circ 45' 58.23''$ (RT)
 T = 821.95
 L = 1,643.30
 R = 25,000.00
 E = 13.51

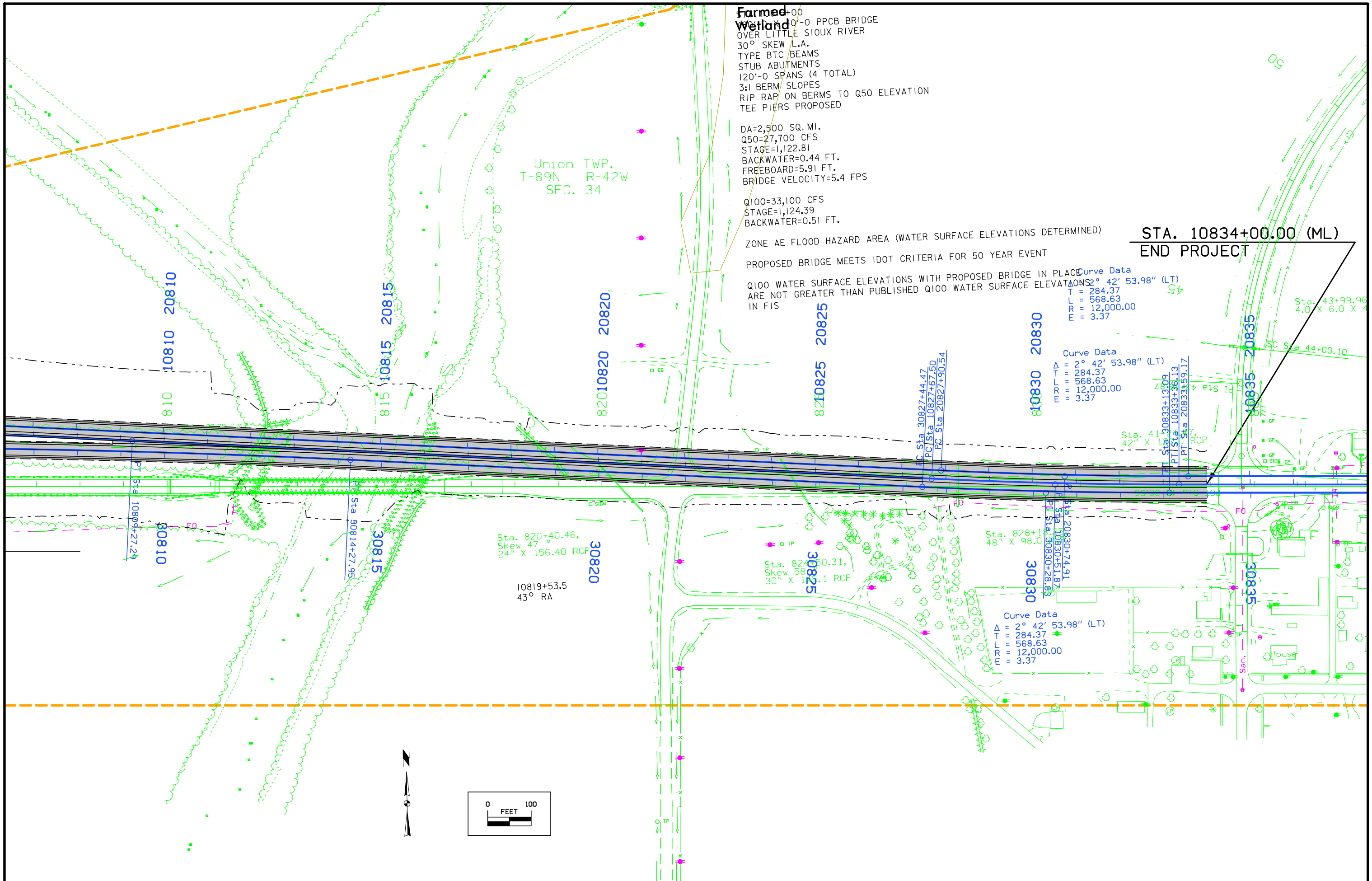
Curve Data
 $\Delta = 3^\circ 45' 58.23''$ (RT)
 T = 821.95
 L = 1,643.30
 R = 25,000.00
 E = 13.51

OLD DES# 5756
 Sta. 783+22.21
 Skew 25°
 30" X 96.01" RCP W/ Flume
 D.A. = 10' Ac - VH
 OK

3.08 ac
 PEM
 Wetland







Farmed Wetland
 120'-0" PPCB BRIDGE
 OVER LITTLE SIOUX RIVER
 30° SKEW L.A.
 TYPE BTC BEAMS
 STUB ABUTMENTS
 120'-0" SPANS (4 TOTAL)
 3:1 BERM SLOPES
 RIP RAP ON BERMS TO Q50 ELEVATION
 TEE PIERS PROPOSED

DA=2,500 SQ. MI.
 Q50=27,700 CFS
 STAGE=1,122.81
 BACKWATER=0.44 FT.
 FREEBOARD=5.91 FT.
 BRIDGE VELOCITY=5.4 FPS

Q100=33,100 CFS
 STAGE=1,124.39
 BACKWATER=0.51 FT.

ZONE AE FLOOD HAZARD AREA (WATER SURFACE ELEVATIONS DETERMINED)
 PROPOSED BRIDGE MEETS IDOT CRITERIA FOR 50 YEAR EVENT

Q100 WATER SURFACE ELEVATIONS WITH PROPOSED BRIDGE IN PLACE ARE NOT GREATER THAN PUBLISHED Q100 WATER SURFACE ELEVATIONS IN FIS

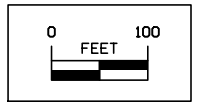
**STA. 10834+00.00 (ML)
 END PROJECT**

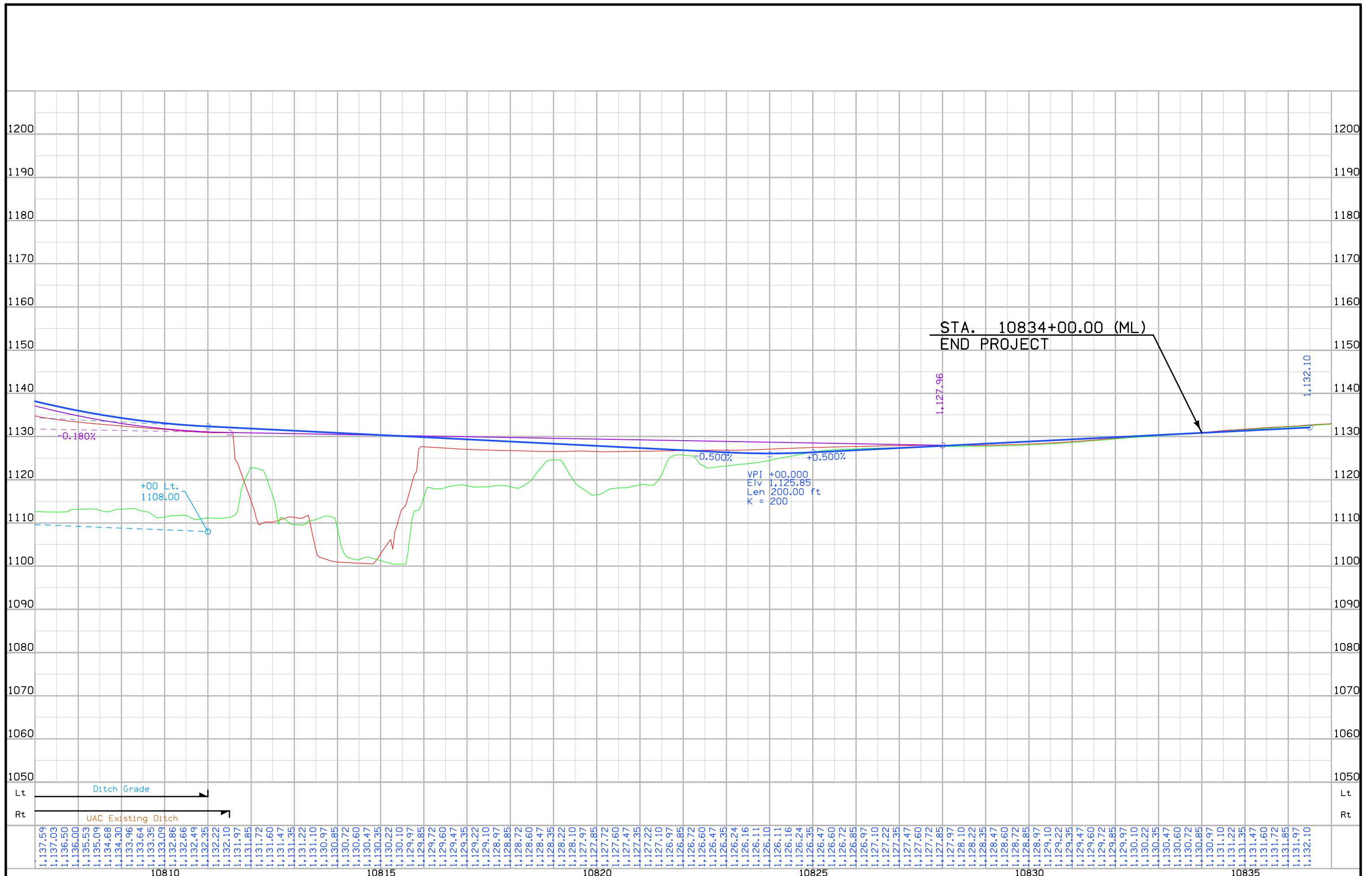
Curve Data
 $\Delta = 2^\circ 42' 53.98" (LT)$
 $T = 284.37$
 $R = 568.63$
 $M = 12,000.00$
 $E = 3.37$

Curve Data
 $\Delta = 2^\circ 42' 53.98" (LT)$
 $T = 284.37$
 $R = 568.63$
 $M = 12,000.00$
 $E = 3.37$

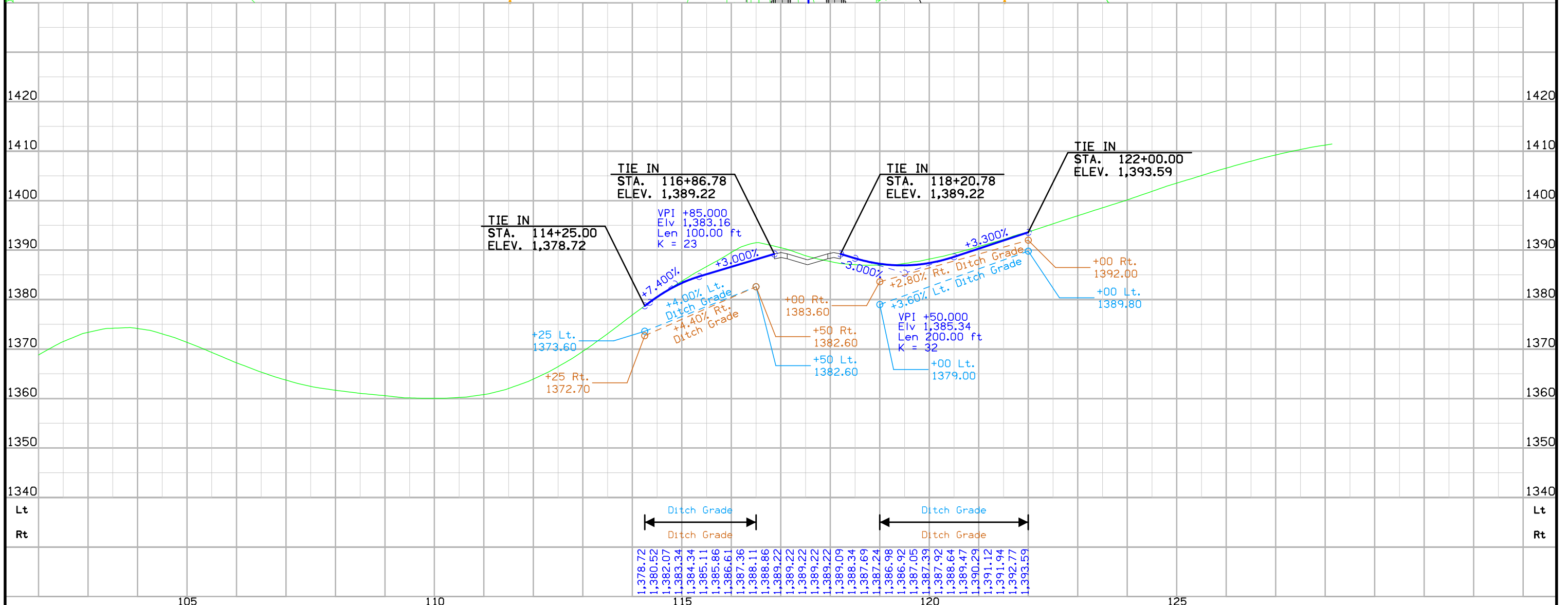
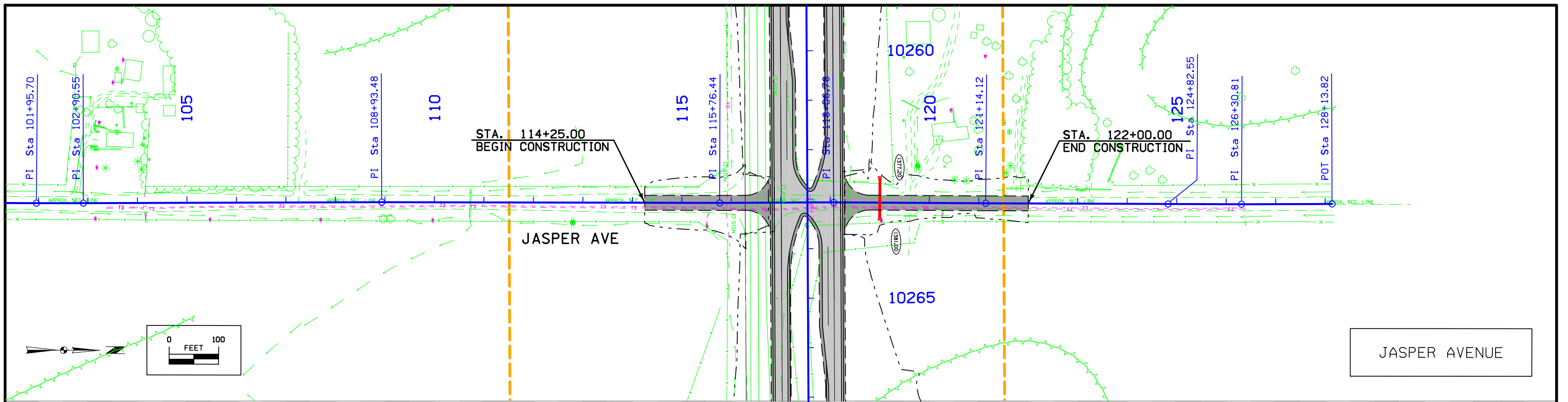
Curve Data
 $\Delta = 2^\circ 42' 53.98" (LT)$
 $T = 284.37$
 $R = 568.63$
 $M = 12,000.00$
 $E = 3.37$

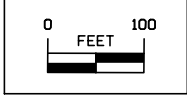
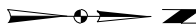
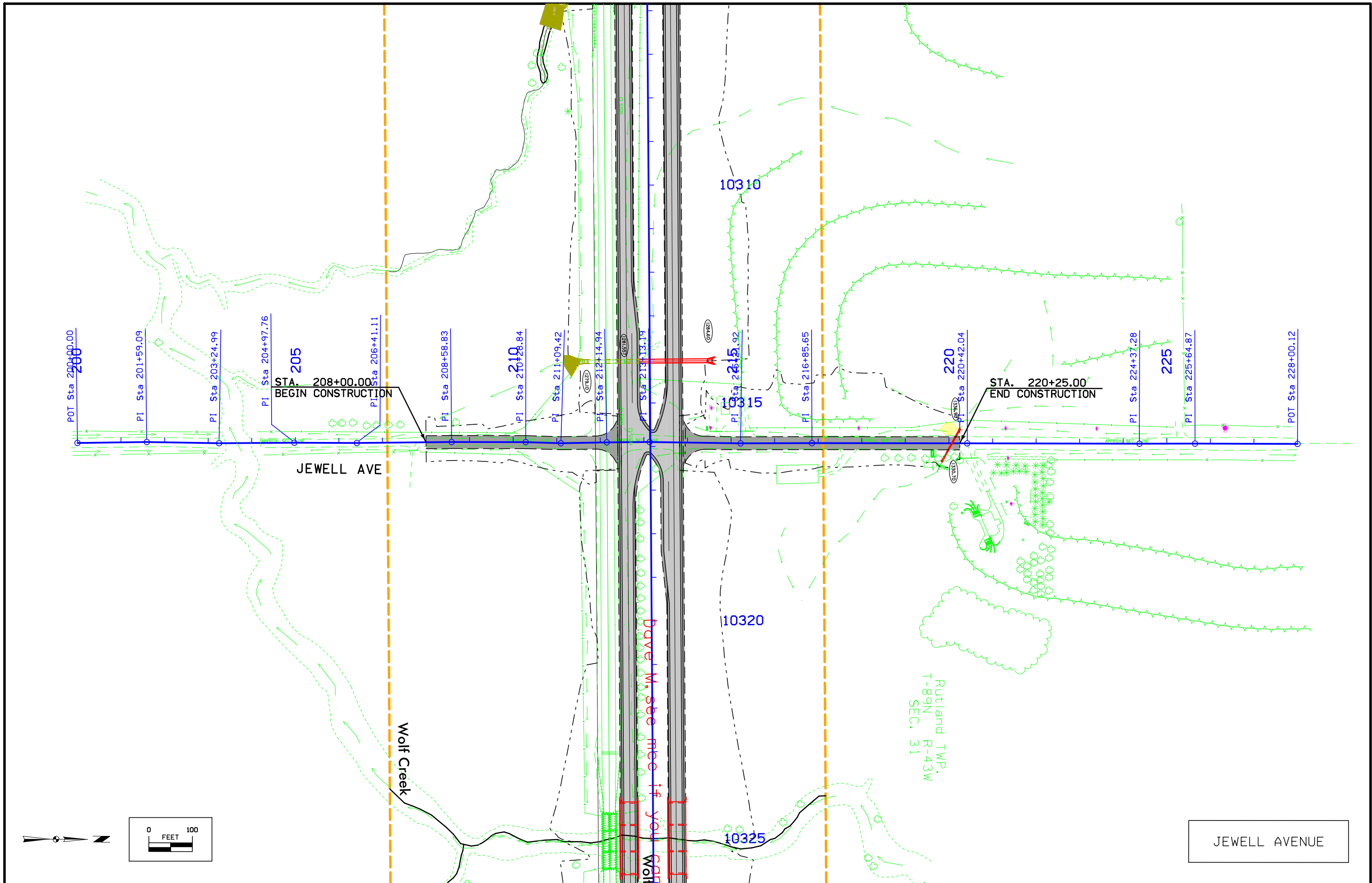
Union TWP.
 T-89N R-42W
 SEC. 34



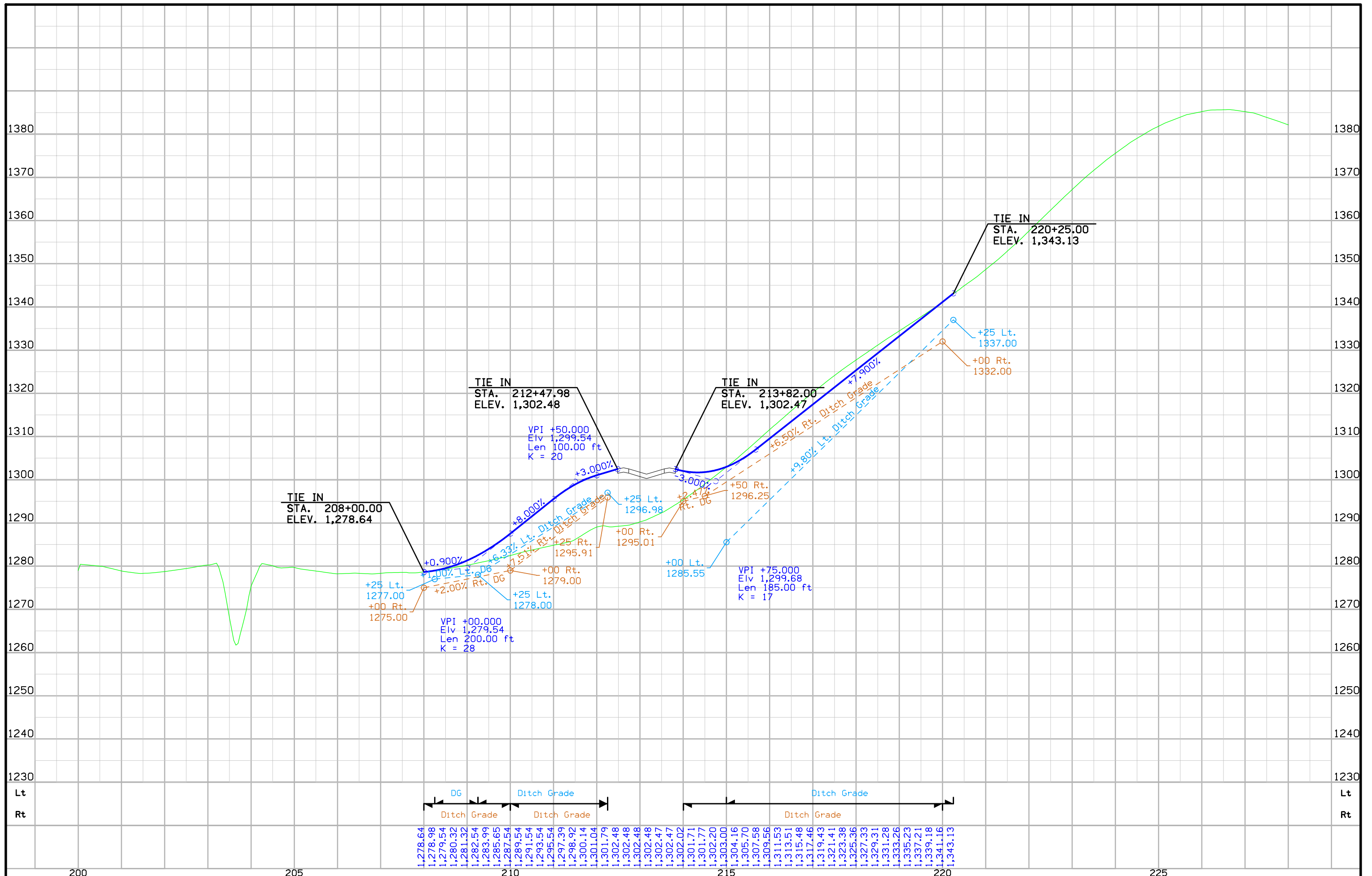


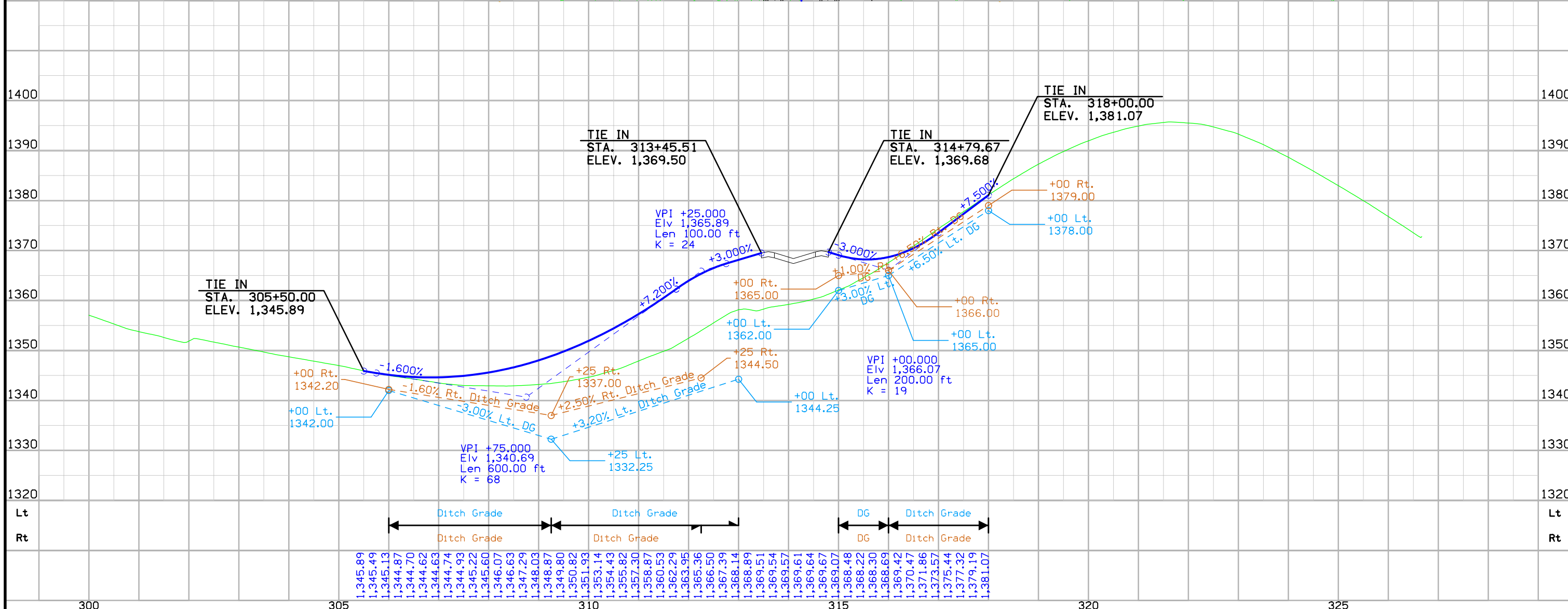
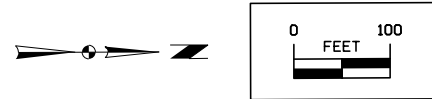
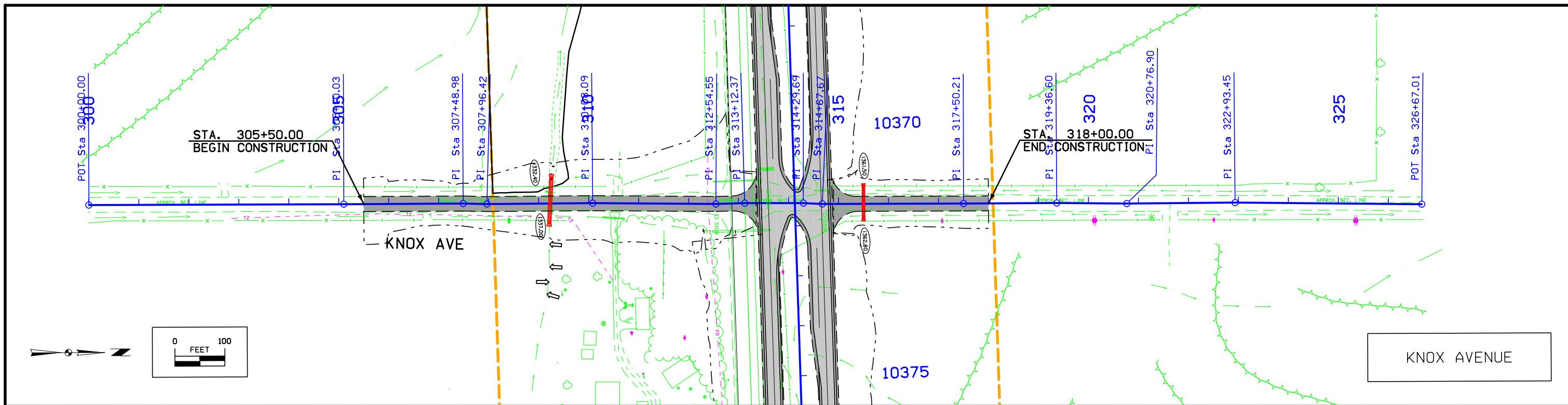
Lt	Ditch Grade		Rt
Rt	UAC Existing Ditch		Rt
1,137.59	10810	10815	1,132.10
1,137.03			1,131.85
1,136.50			1,131.72
1,136.00			1,131.60
1,135.53			1,131.47
1,135.09			1,131.35
1,134.68			1,131.22
1,134.30			1,131.10
1,133.96			1,130.97
1,133.64			1,130.85
1,133.35			1,130.72
1,133.09			1,130.60
1,132.86			1,130.47
1,132.66			1,130.35
1,132.49			1,130.22
1,132.35			1,130.10
1,132.22			1,129.97
1,132.10			1,129.85
1,131.97			1,129.72
1,131.85			1,129.60
1,131.72			1,129.47
1,131.60			1,129.35
1,131.47			1,129.22
1,131.35			1,129.10
1,131.22			1,128.97
1,131.10			1,128.85
1,130.97			1,128.72
1,130.85			1,128.60
1,130.72			1,128.47
1,130.60			1,128.35
1,130.47			1,128.22
1,130.35			1,128.10
1,130.22			1,127.97
1,130.10			1,127.85
1,129.97			1,127.72
1,129.85			1,127.60
1,129.72			1,127.47
1,129.60			1,127.35
1,129.47			1,127.22
1,129.35			1,127.10
1,129.22			1,126.97
1,129.10			1,126.85
1,128.97			1,126.72
1,128.85			1,126.60
1,128.72			1,126.47
1,128.60			1,126.35
1,128.47			1,126.24
1,128.35			1,126.16
1,128.22			1,126.11
1,128.10			1,126.10
1,127.97			1,126.11
1,127.85			1,126.16
1,127.72			1,126.24
1,127.60			1,126.35
1,127.47			1,126.47
1,127.35			1,126.60
1,127.22			1,126.72
1,127.10			1,126.85
1,126.97			1,126.97
1,126.85			1,127.10
1,126.72			1,127.22
1,126.60			1,127.35
1,126.47			1,127.47
1,126.35			1,127.60
1,126.24			1,127.72
1,126.16			1,127.85
1,126.11			1,127.97
1,126.10			1,128.10
1,126.11			1,128.22
1,126.16			1,128.35
1,126.24			1,128.47
1,126.35			1,128.60
1,126.47			1,128.72
1,126.60			1,128.85
1,126.72			1,128.97
1,126.85			1,129.10
1,126.97			1,129.22
1,127.10			1,129.35
1,127.22			1,129.47
1,127.35			1,129.60
1,127.47			1,129.72
1,127.60			1,129.85
1,127.72			1,129.97
1,127.85			1,130.10
1,127.97			1,130.22
1,128.10			1,130.35
1,128.22			1,130.47
1,128.35			1,130.60
1,128.47			1,130.72
1,128.60			1,130.85
1,128.72			1,130.97
1,128.85			1,131.10
1,128.97			1,131.22
1,129.10			1,131.35
1,129.22			1,131.47
1,129.35			1,131.60
1,129.47			1,131.72
1,129.60			1,131.85
1,129.72			1,131.97
1,129.85			1,132.10
1,129.97			
1,130.10			
1,130.22			
1,130.35			
1,130.47			
1,130.60			
1,130.72			
1,130.85			
1,130.97			
1,131.10			
1,131.22			
1,131.35			
1,131.47			
1,131.60			
1,131.72			
1,131.85			
1,131.97			
1,132.10			



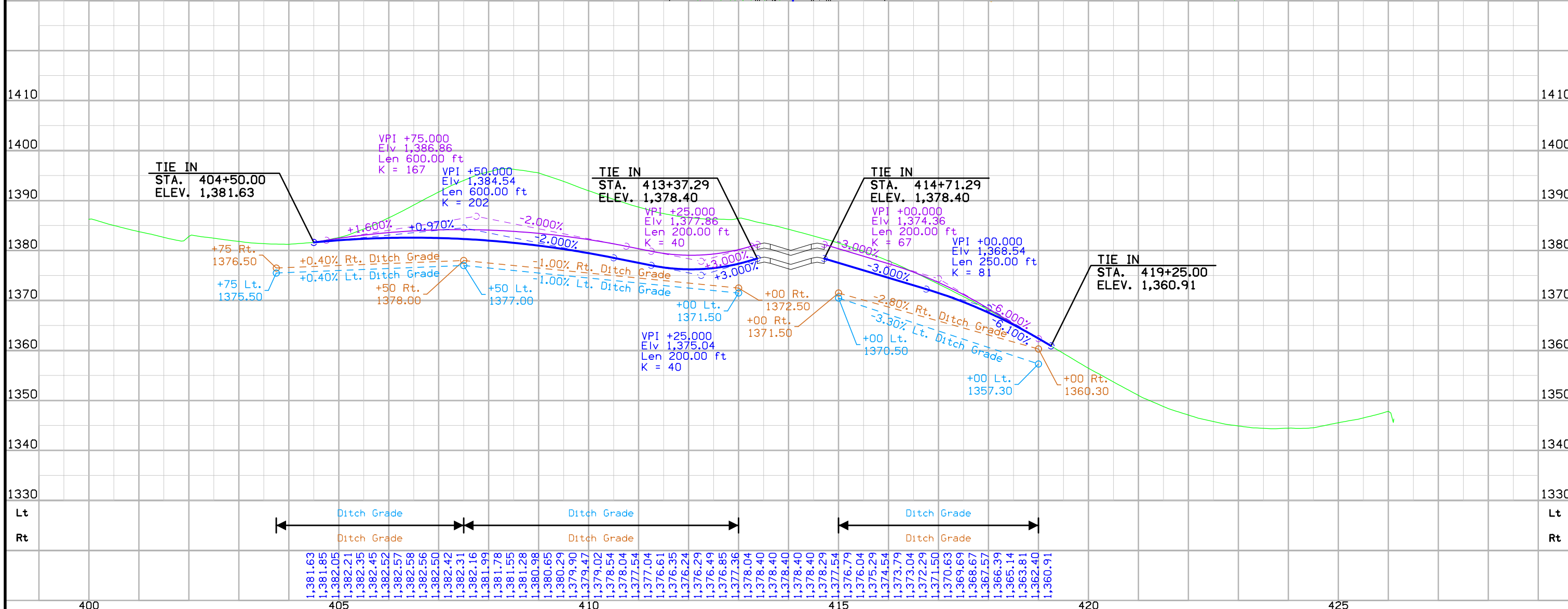
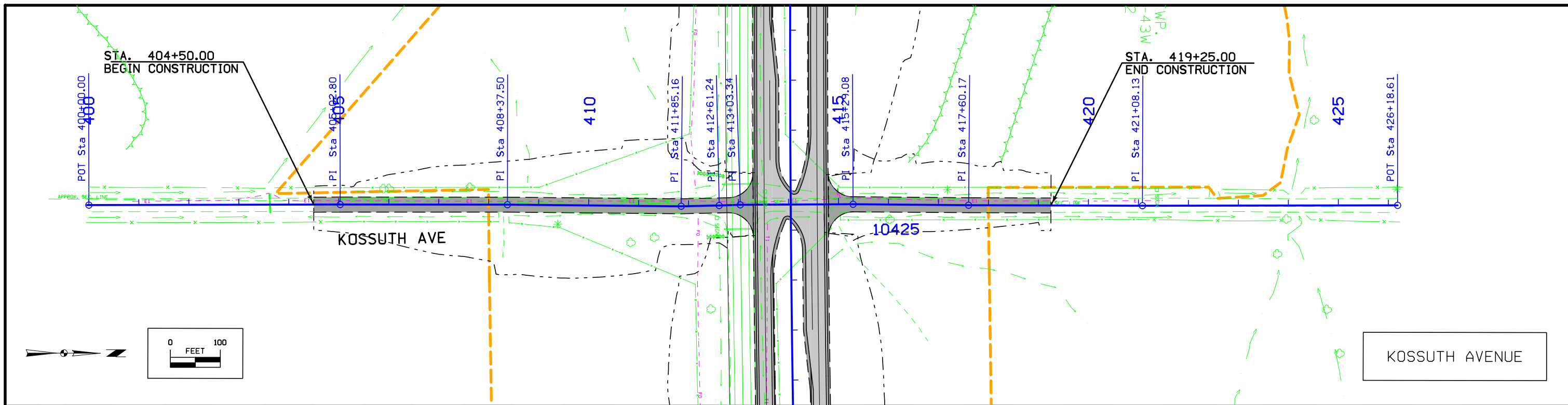


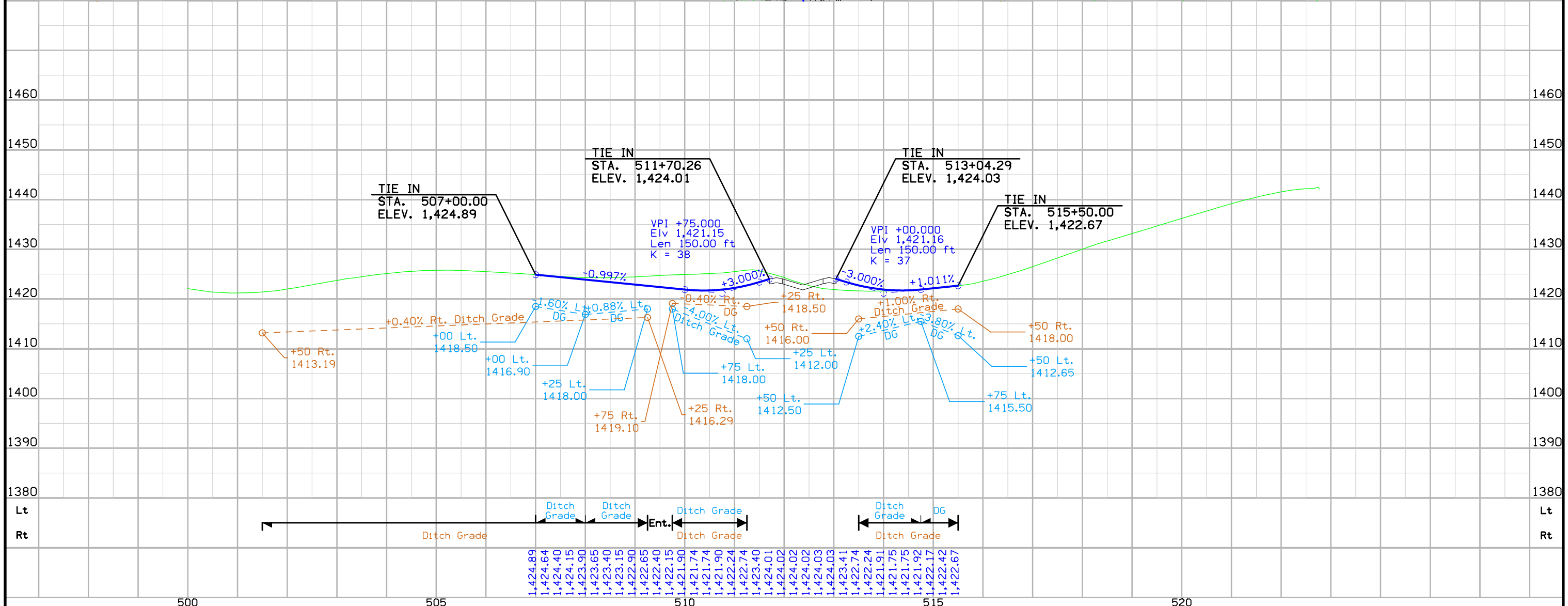
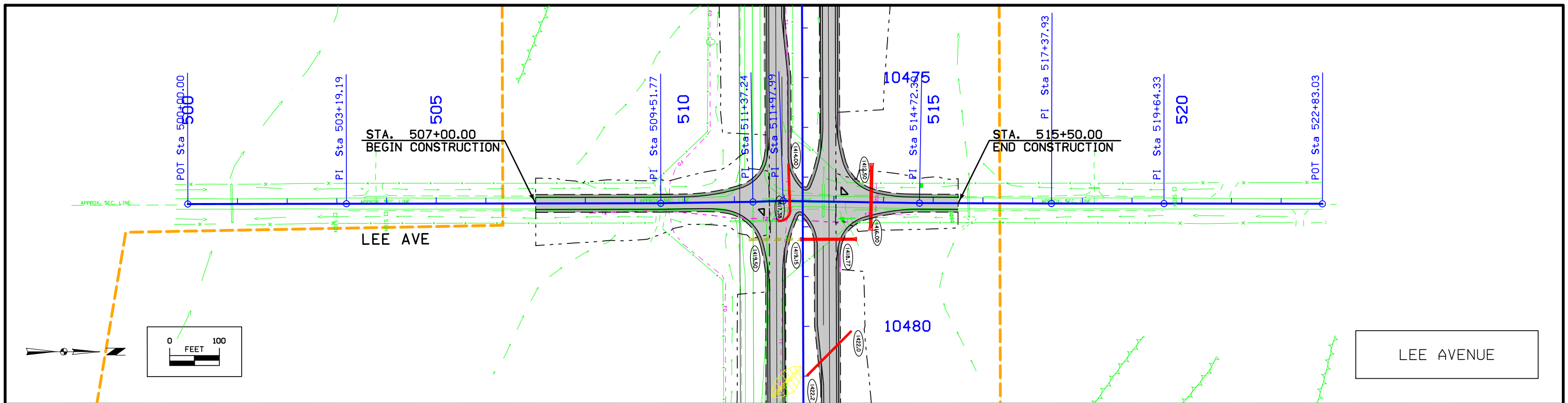
JEWELL AVENUE

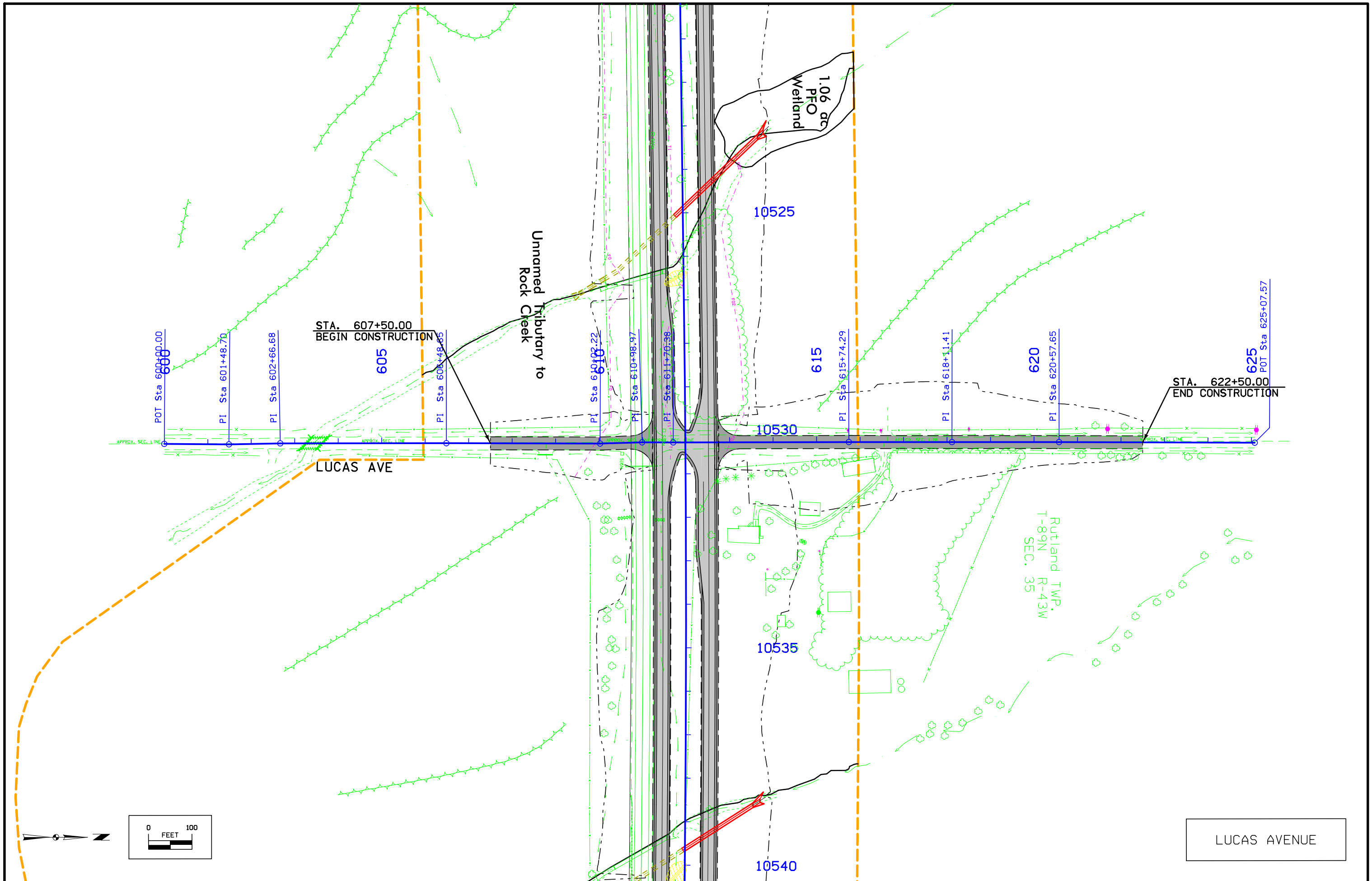




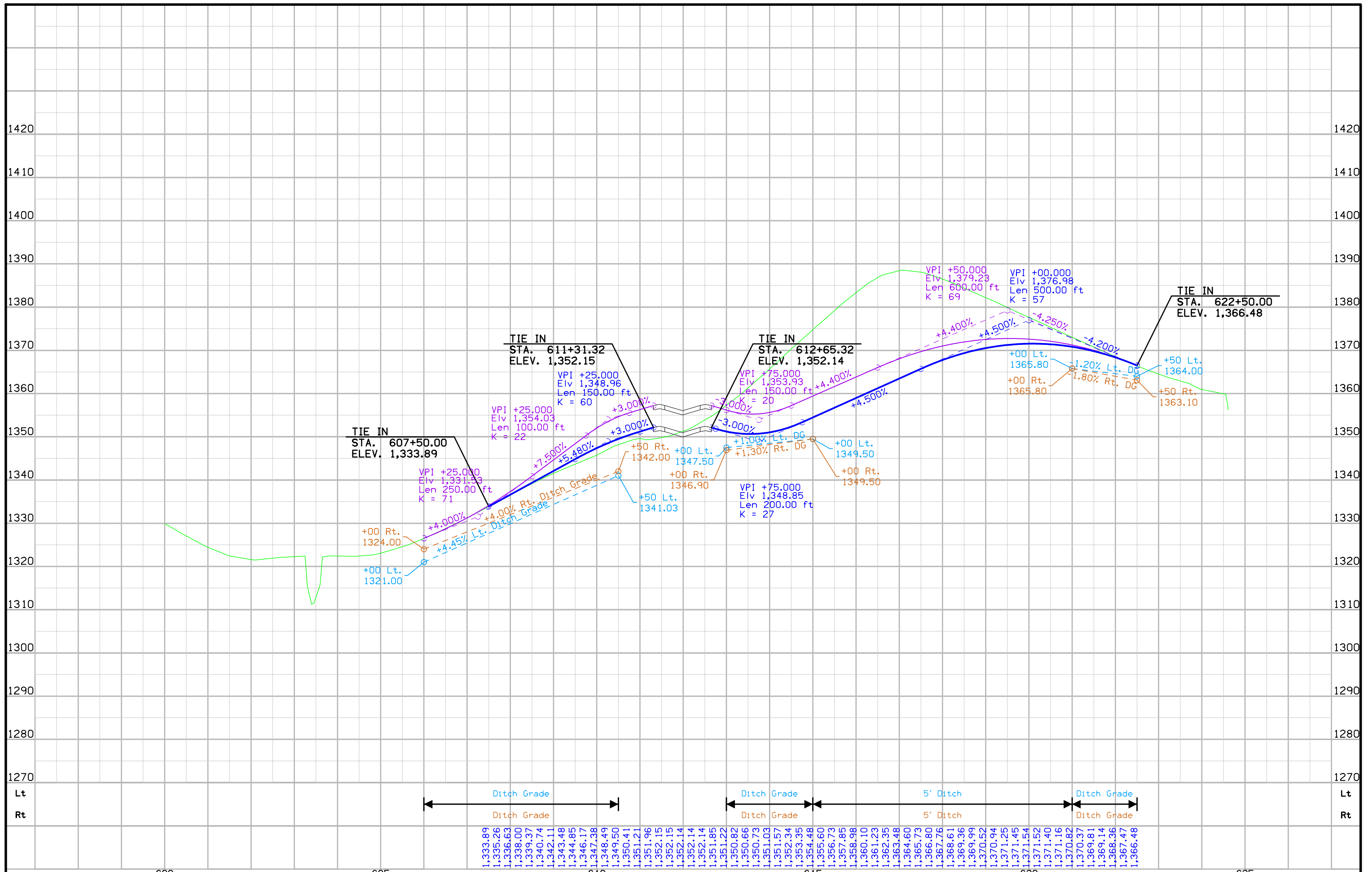
C	ENGLISH	IOWA DOT	DESIGN TEAM	Flattery\Johnson	WOODBURY COUNTY	PROJECT NUMBER	NHSX-020-1(116)--3H-97	SHEET NUMBER	E.4
---	---------	----------	-------------	------------------	-----------------	----------------	------------------------	--------------	-----



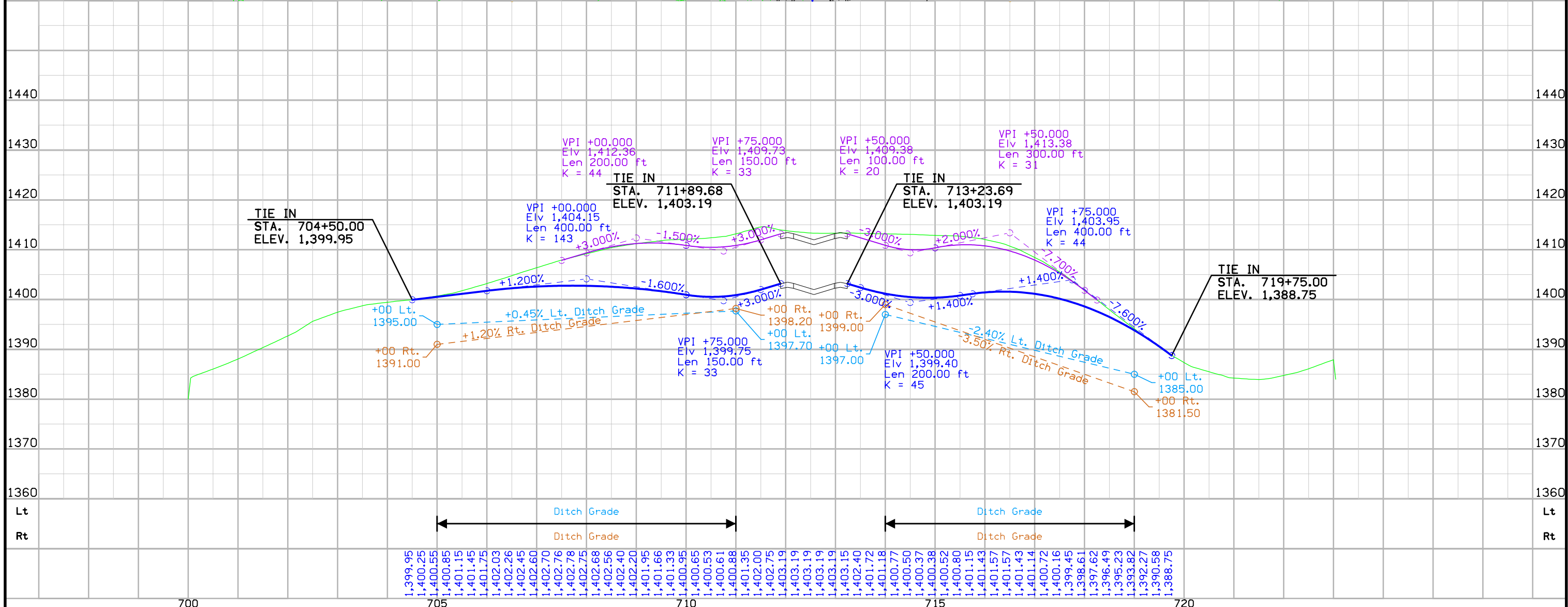
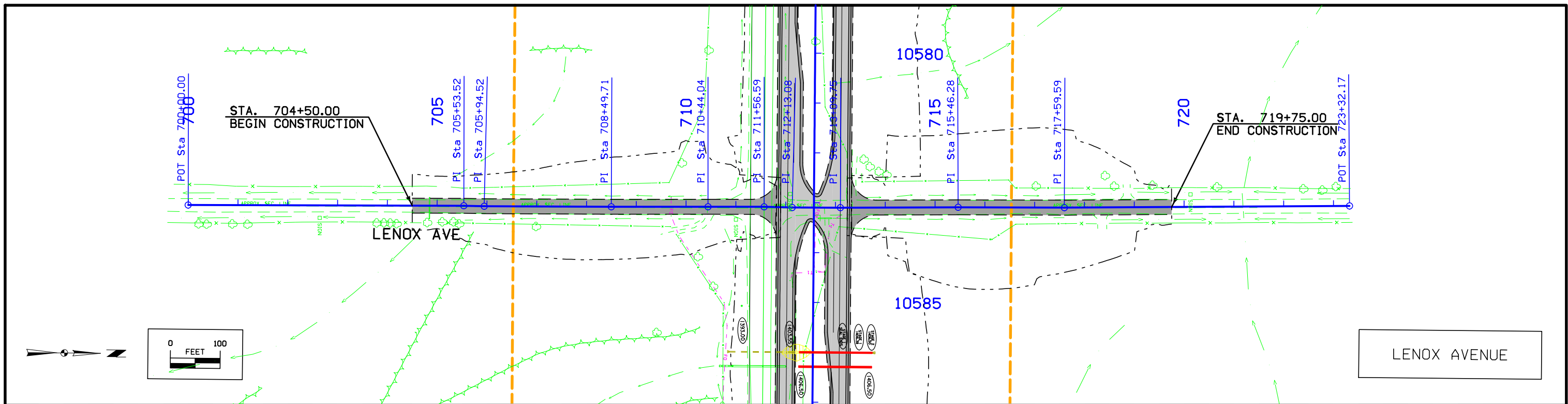




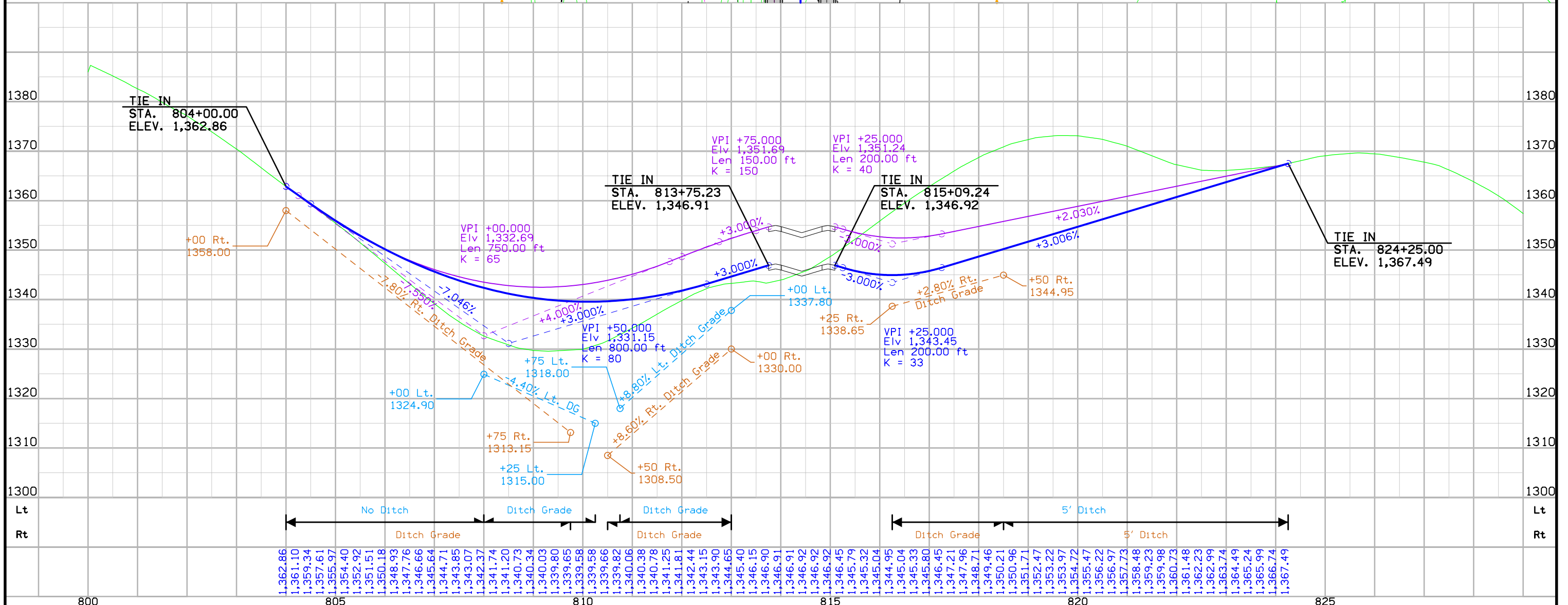
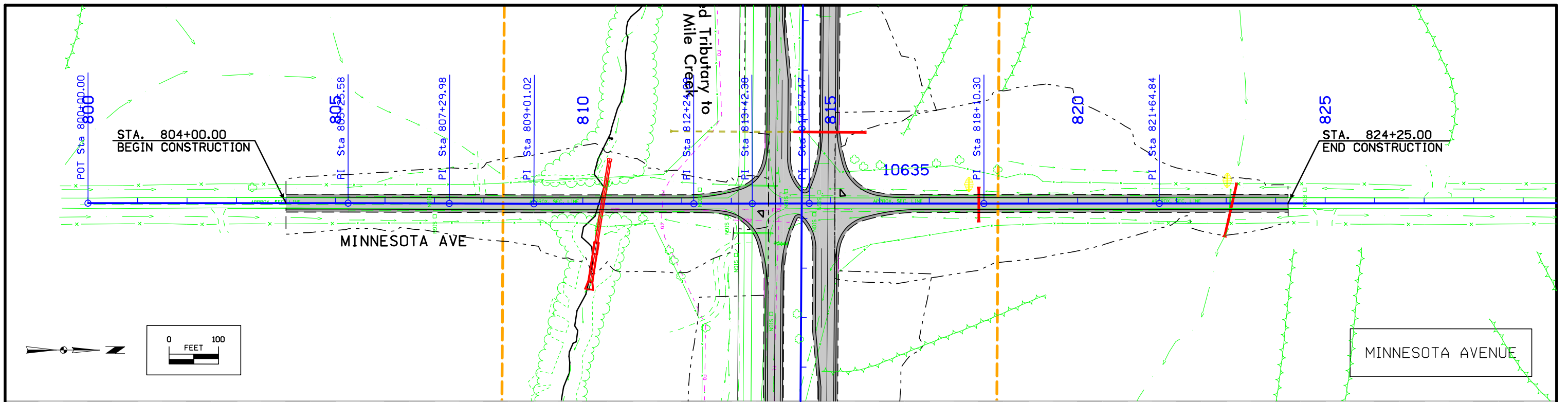
LUCAS AVENUE



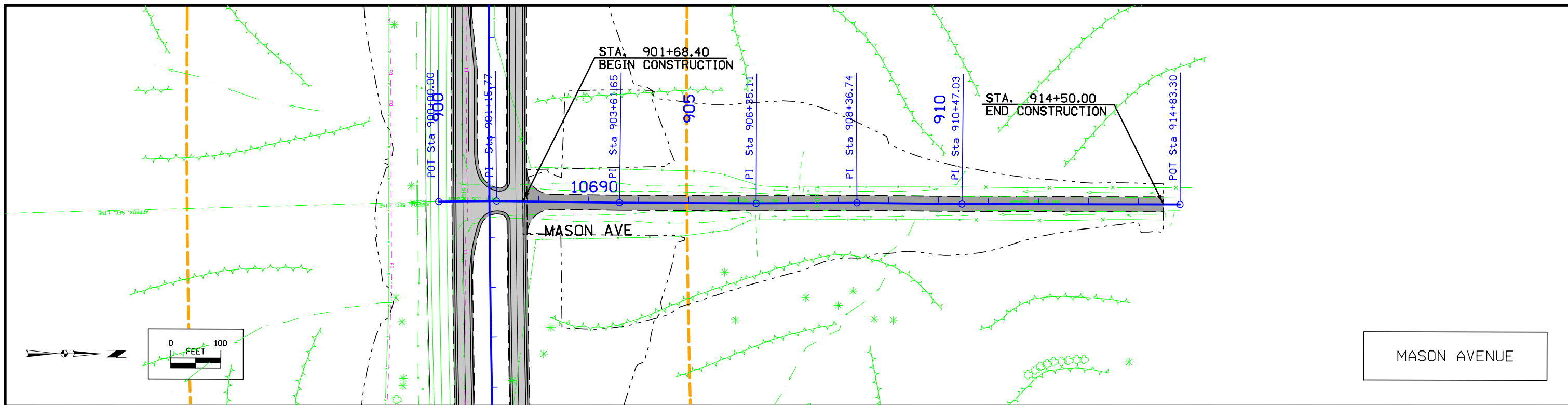
600	605	610	615	620	625
Ditch Grade			Ditch Grade	5' Ditch	Ditch Grade
Ditch Grade			Ditch Grade	5' Ditch	Ditch Grade
1,333.89	1,335.26	1,336.63	1,338.00	1,339.37	1,340.74
1,340.74	1,342.11	1,343.48	1,344.85	1,346.17	1,347.38
1,347.38	1,348.49	1,349.50	1,350.41	1,351.21	1,351.96
1,351.96	1,352.15	1,352.15	1,352.14	1,352.14	1,351.85
1,351.85	1,351.22	1,350.82	1,350.66	1,350.73	1,351.03
1,351.03	1,352.34	1,353.35	1,354.48	1,355.60	1,356.73
1,356.73	1,357.85	1,358.98	1,360.10	1,361.23	1,362.35
1,362.35	1,363.48	1,364.60	1,365.73	1,366.80	1,367.76
1,367.76	1,368.61	1,369.36	1,369.99	1,370.52	1,370.94
1,370.94	1,371.25	1,371.45	1,371.54	1,371.52	1,371.40
1,371.40	1,371.16	1,370.82	1,370.37	1,369.81	1,369.14
1,369.14	1,368.36	1,367.47	1,366.48		



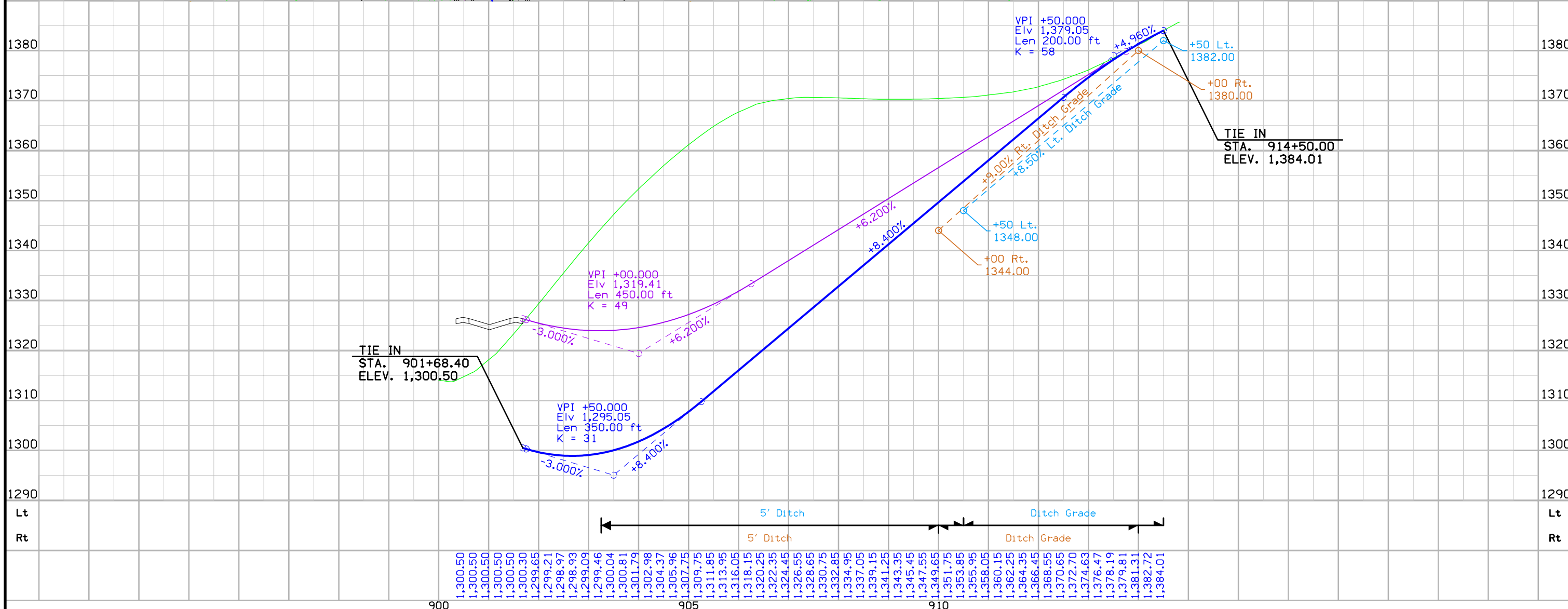
C	ENGLISH	IOWA DOT	DESIGN TEAM	Flattery\Johnson	WOODBURY COUNTY	PROJECT NUMBER	NHSX-020-1(116)--3H-97	SHEET NUMBER	E.9
---	---------	----------	-------------	------------------	-----------------	----------------	------------------------	--------------	-----



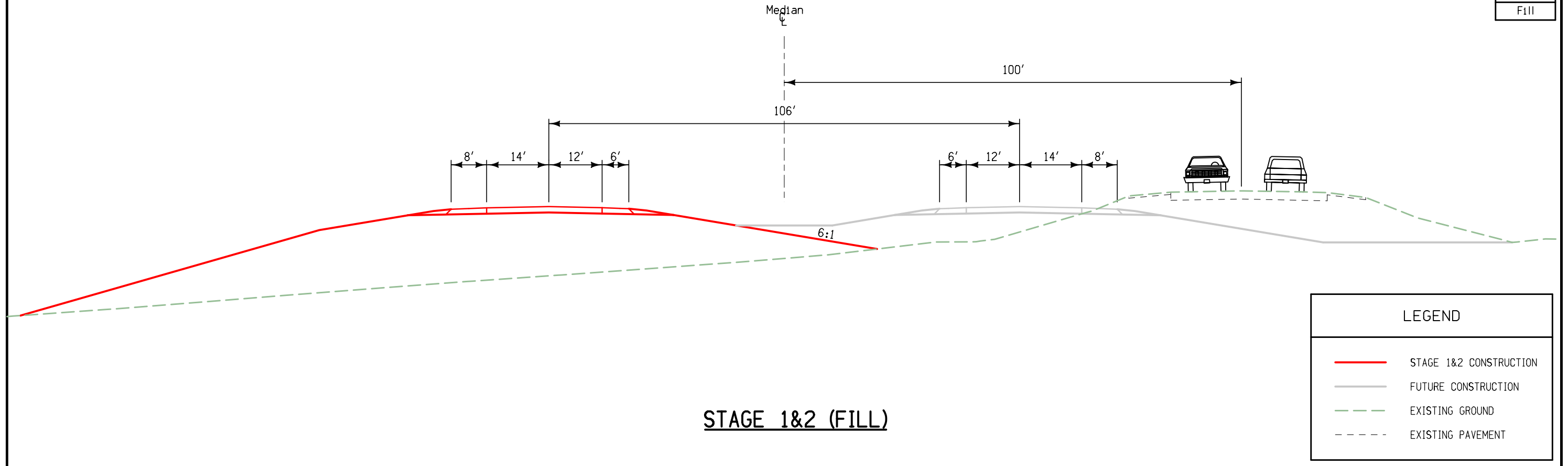
800	805	810	815	820	825
1,362.86	1,361.10	1,359.34	1,357.61	1,355.97	1,354.40
1,351.51	1,350.18	1,348.93	1,347.76	1,346.66	1,345.64
1,344.71	1,343.85	1,343.07	1,342.37	1,341.74	1,341.20
1,340.73	1,340.34	1,340.03	1,339.80	1,339.65	1,339.58
1,339.66	1,339.82	1,340.06	1,340.38	1,340.78	1,341.25
1,341.81	1,342.44	1,343.90	1,344.65	1,345.40	1,346.15
1,346.90	1,346.91	1,346.92	1,346.92	1,346.92	1,346.92
1,346.45	1,345.79	1,345.32	1,345.04	1,344.95	1,345.04
1,345.80	1,346.45	1,347.21	1,347.96	1,348.71	1,349.46
1,350.21	1,350.96	1,351.71	1,352.47	1,353.22	1,353.97
1,354.72	1,355.47	1,356.22	1,356.97	1,357.73	1,358.48
1,359.23	1,359.98	1,360.73	1,361.48	1,362.23	1,362.99
1,363.74	1,364.49	1,365.24	1,365.99	1,366.74	1,367.49



MASON AVENUE



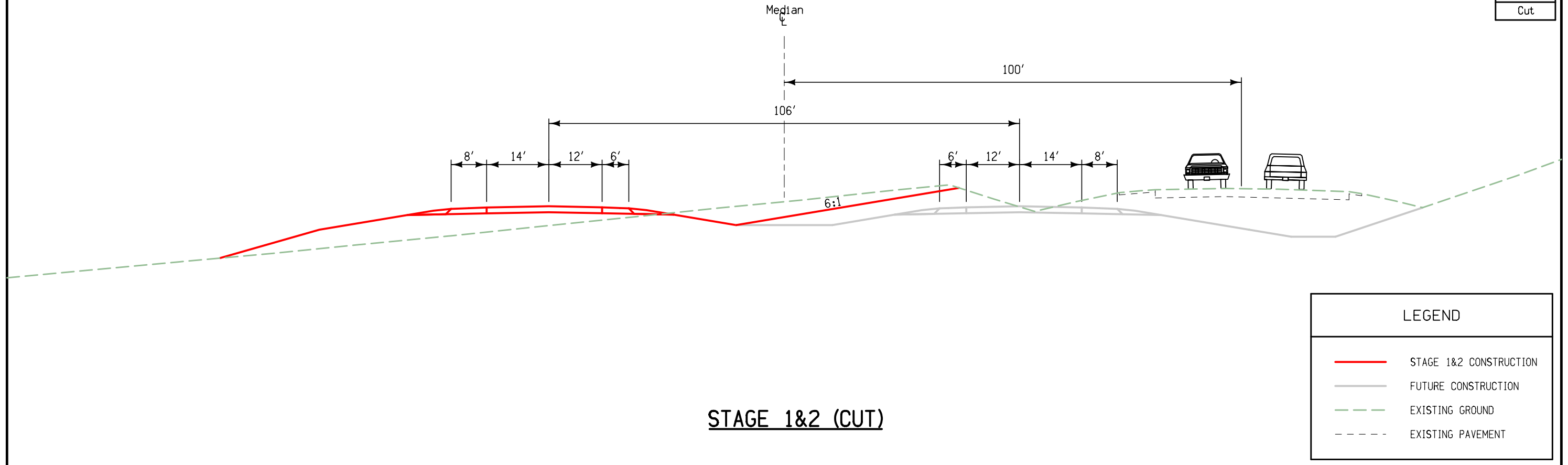
Stage 1&2
Fill



STAGE 1&2 (FILL)

LEGEND	
	STAGE 1&2 CONSTRUCTION
	FUTURE CONSTRUCTION
	EXISTING GROUND
	EXISTING PAVEMENT

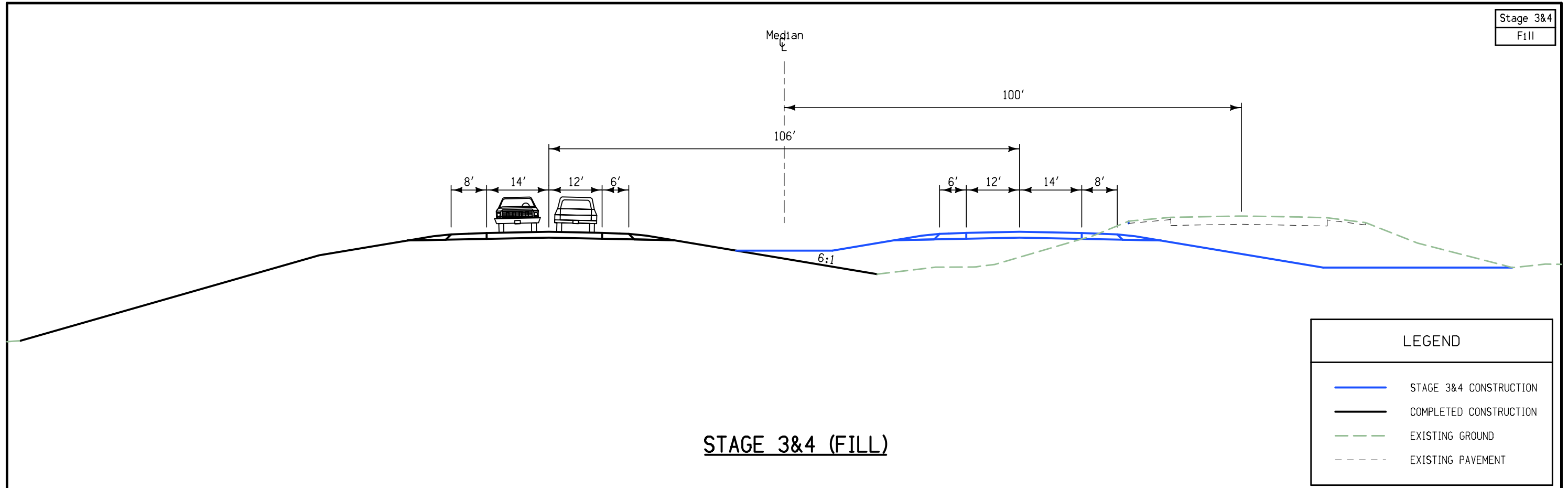
Stage 1&2
Cut



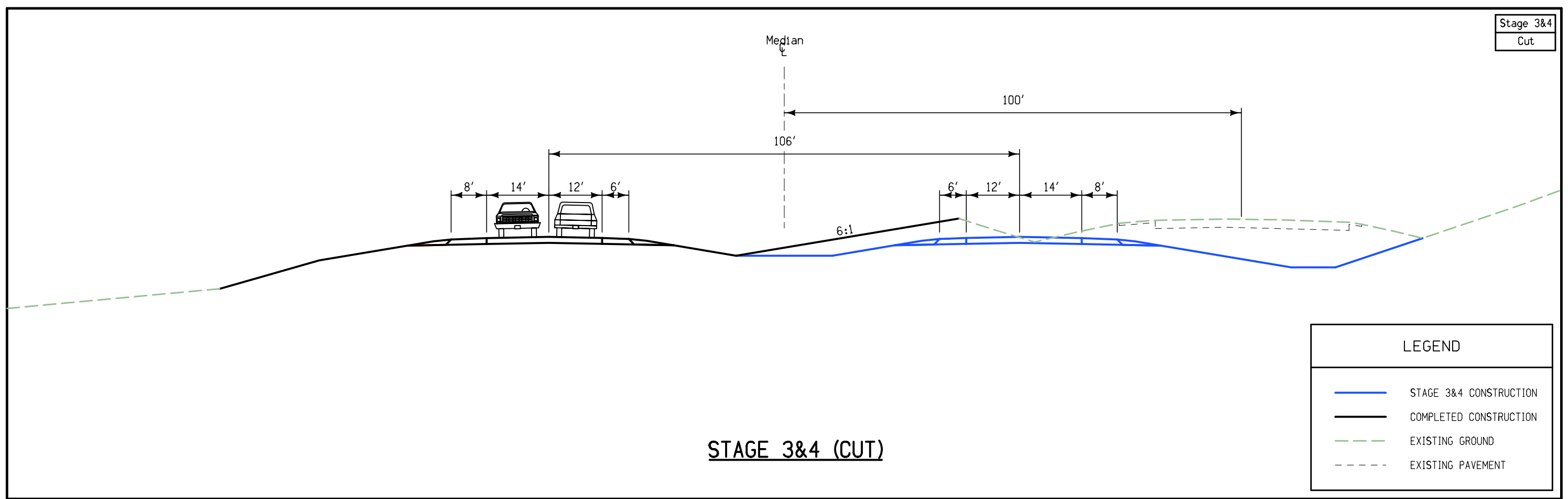
STAGE 1&2 (CUT)

LEGEND	
	STAGE 1&2 CONSTRUCTION
	FUTURE CONSTRUCTION
	EXISTING GROUND
	EXISTING PAVEMENT

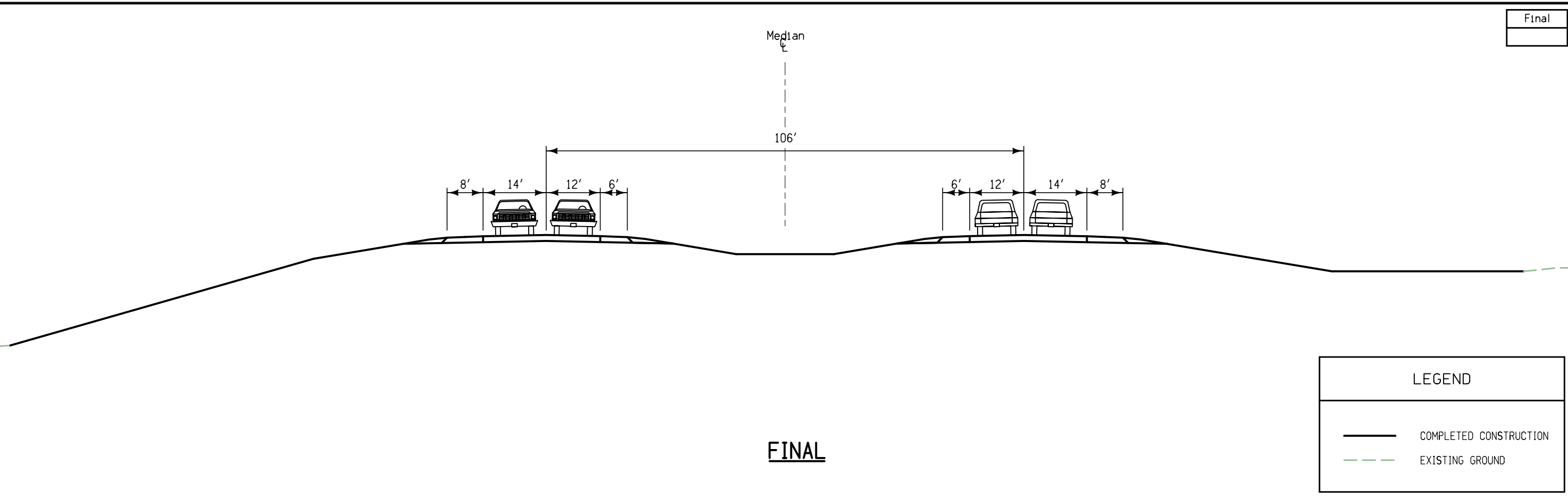
Stage 3&4
Fill



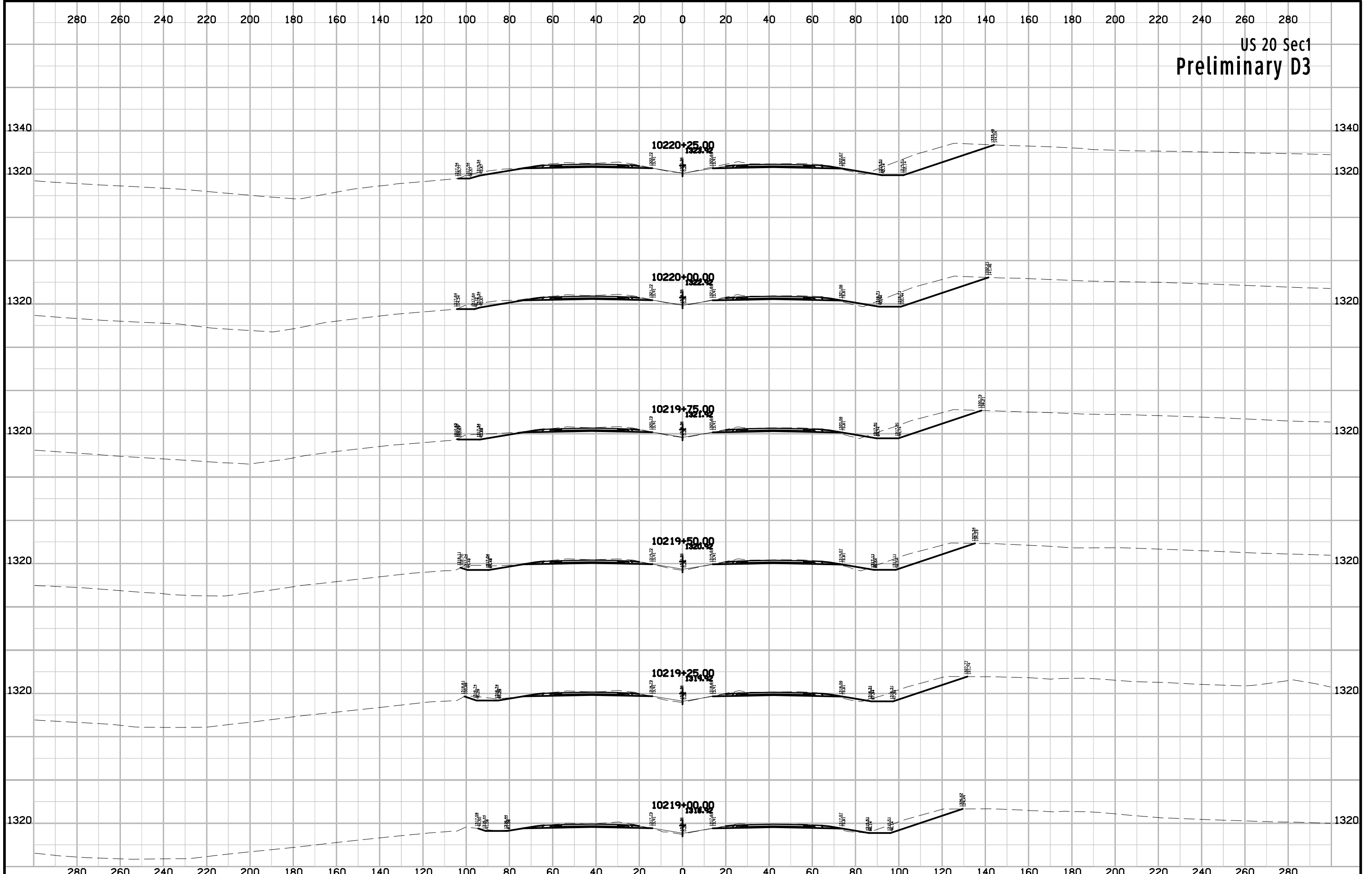
Stage 3&4
Cut



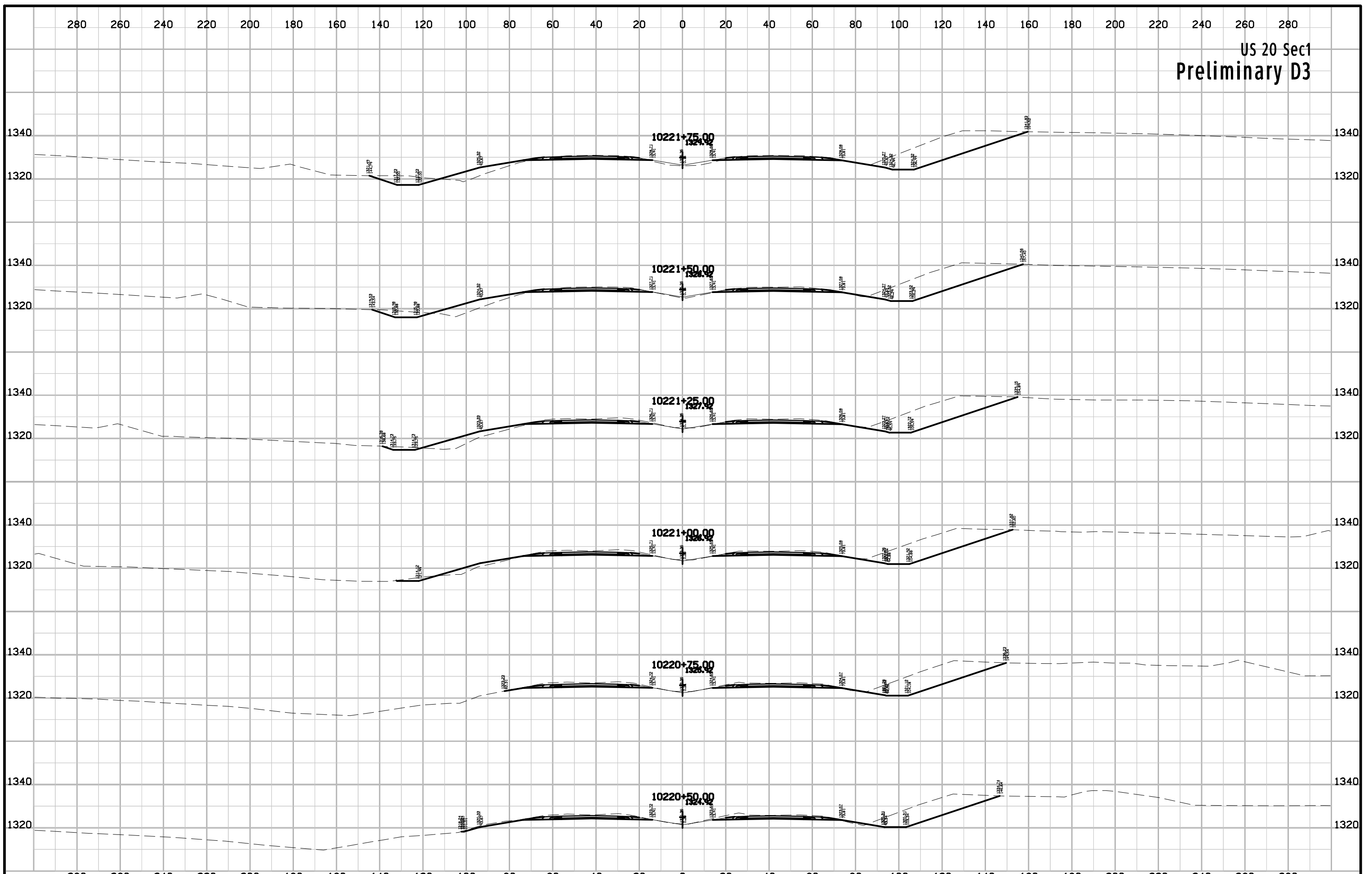
Final



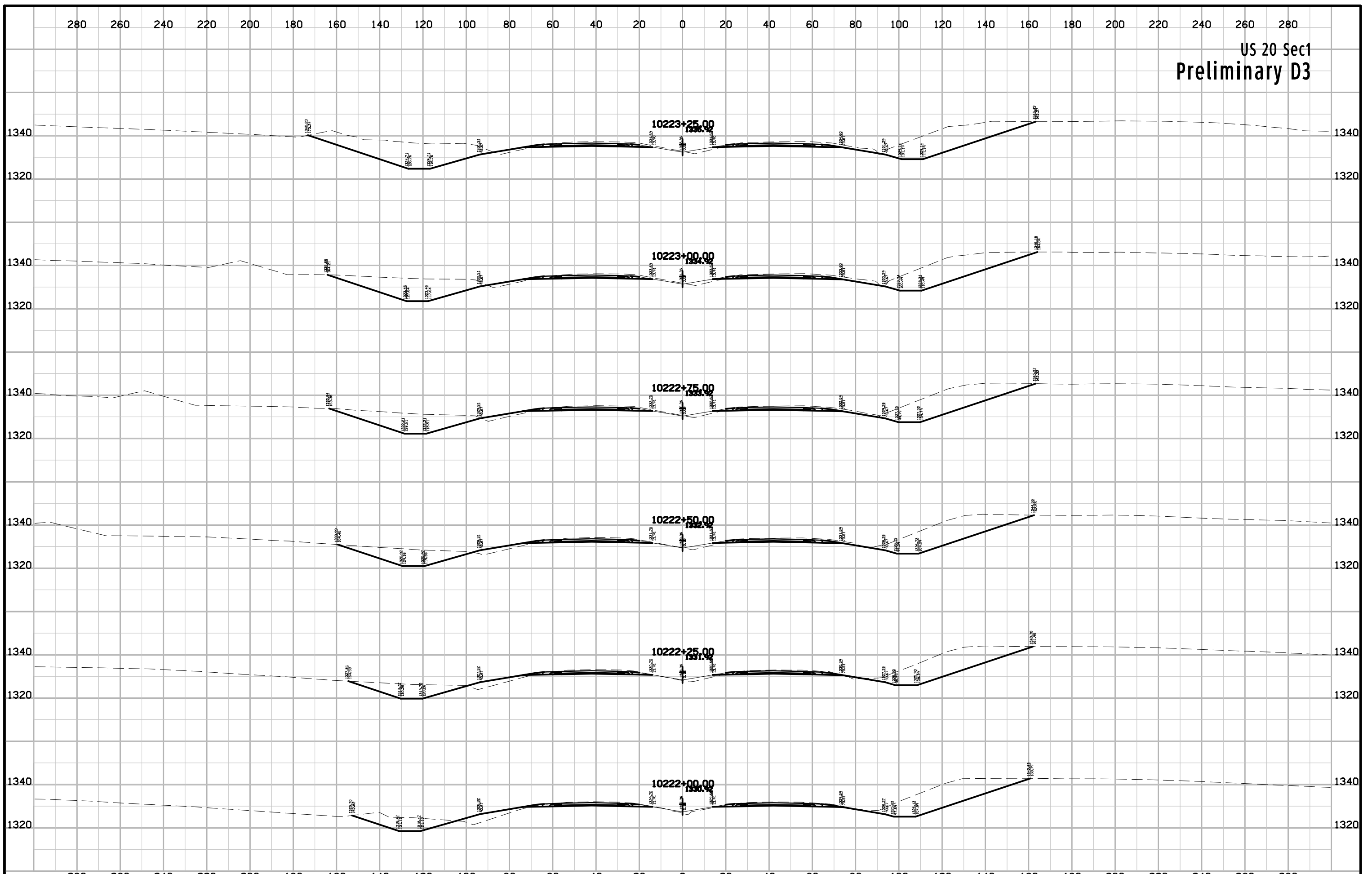
US 20 Sec1
Preliminary D3



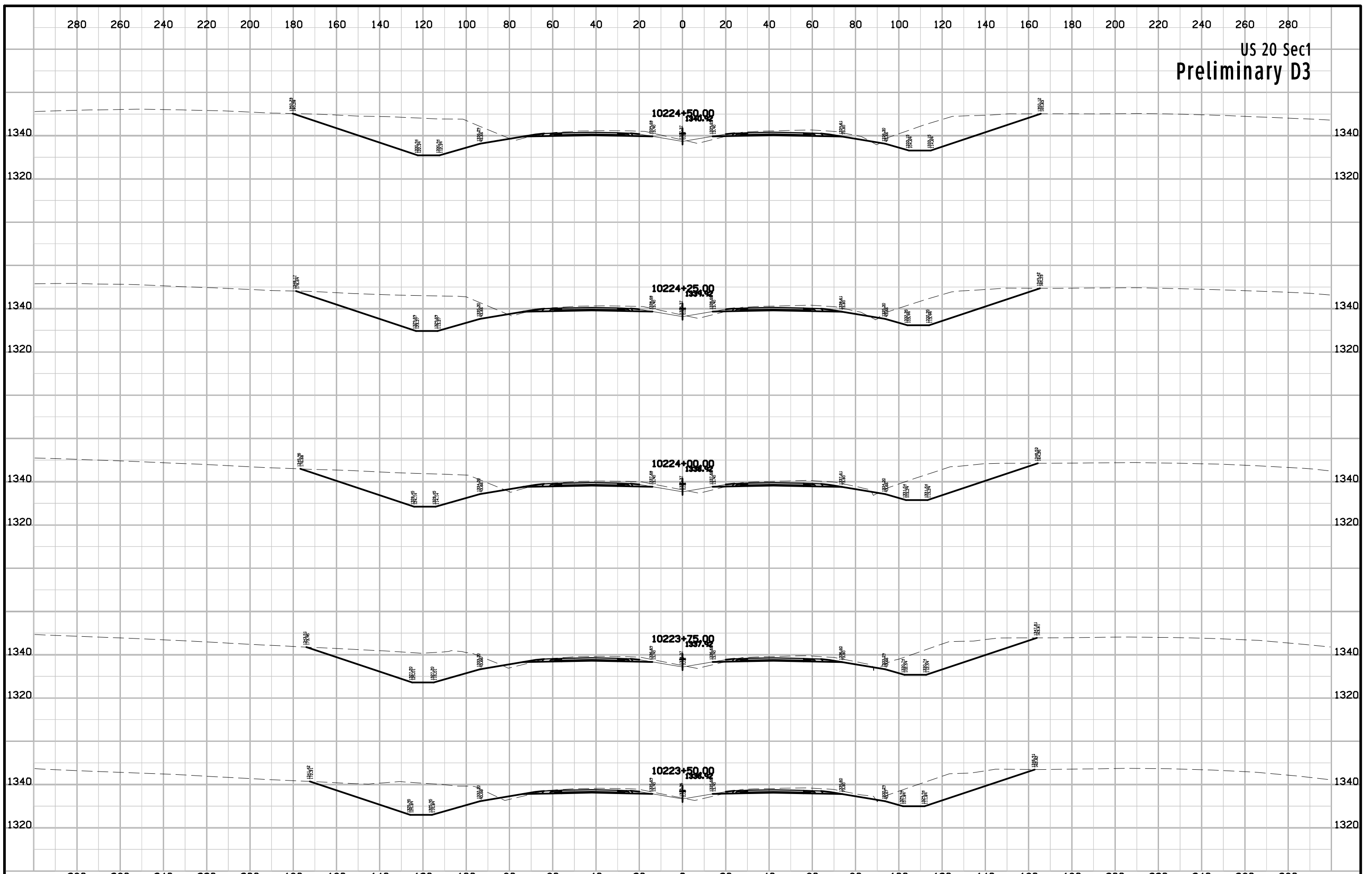
US 20 Sec1
Preliminary D3

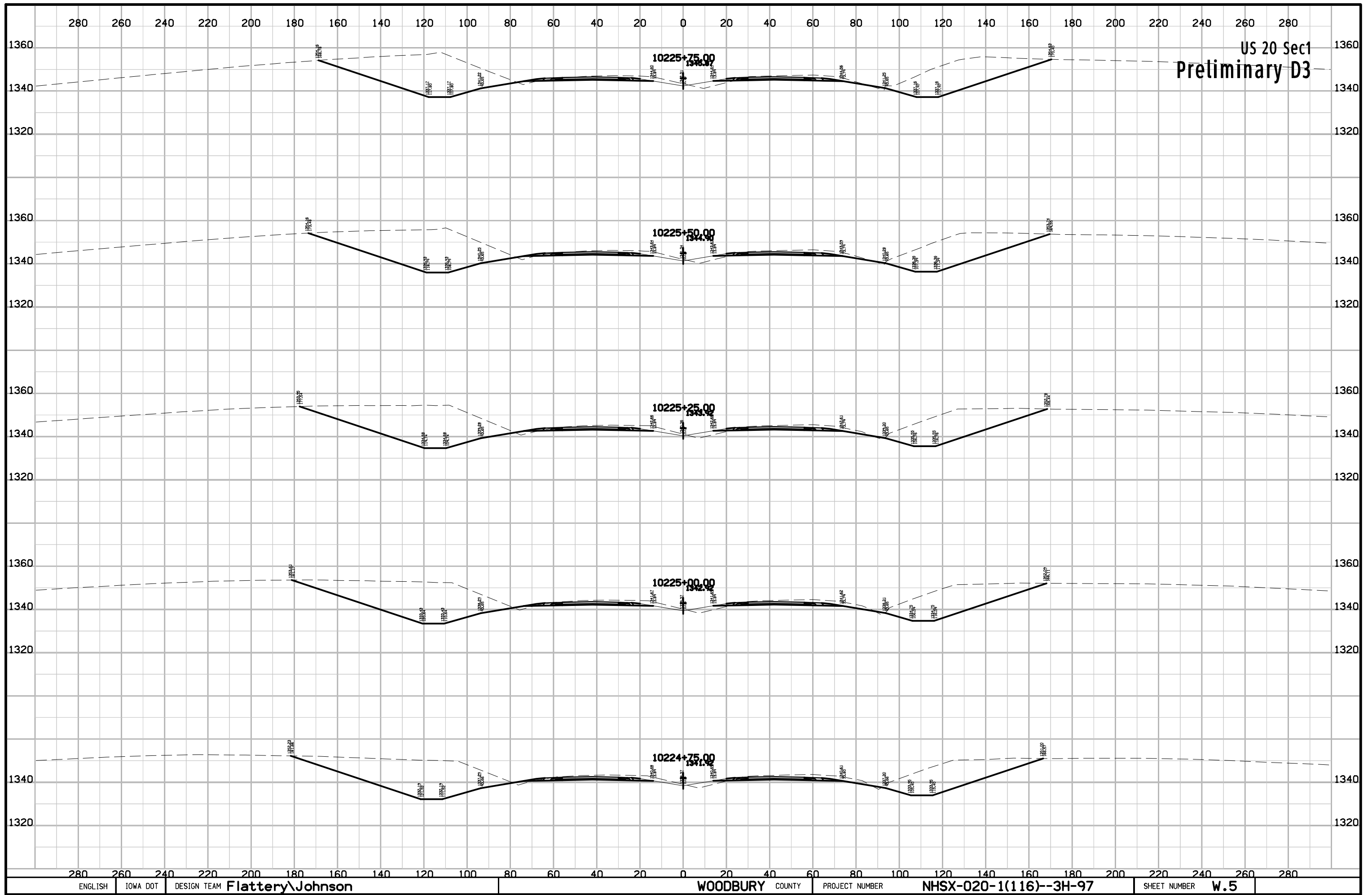


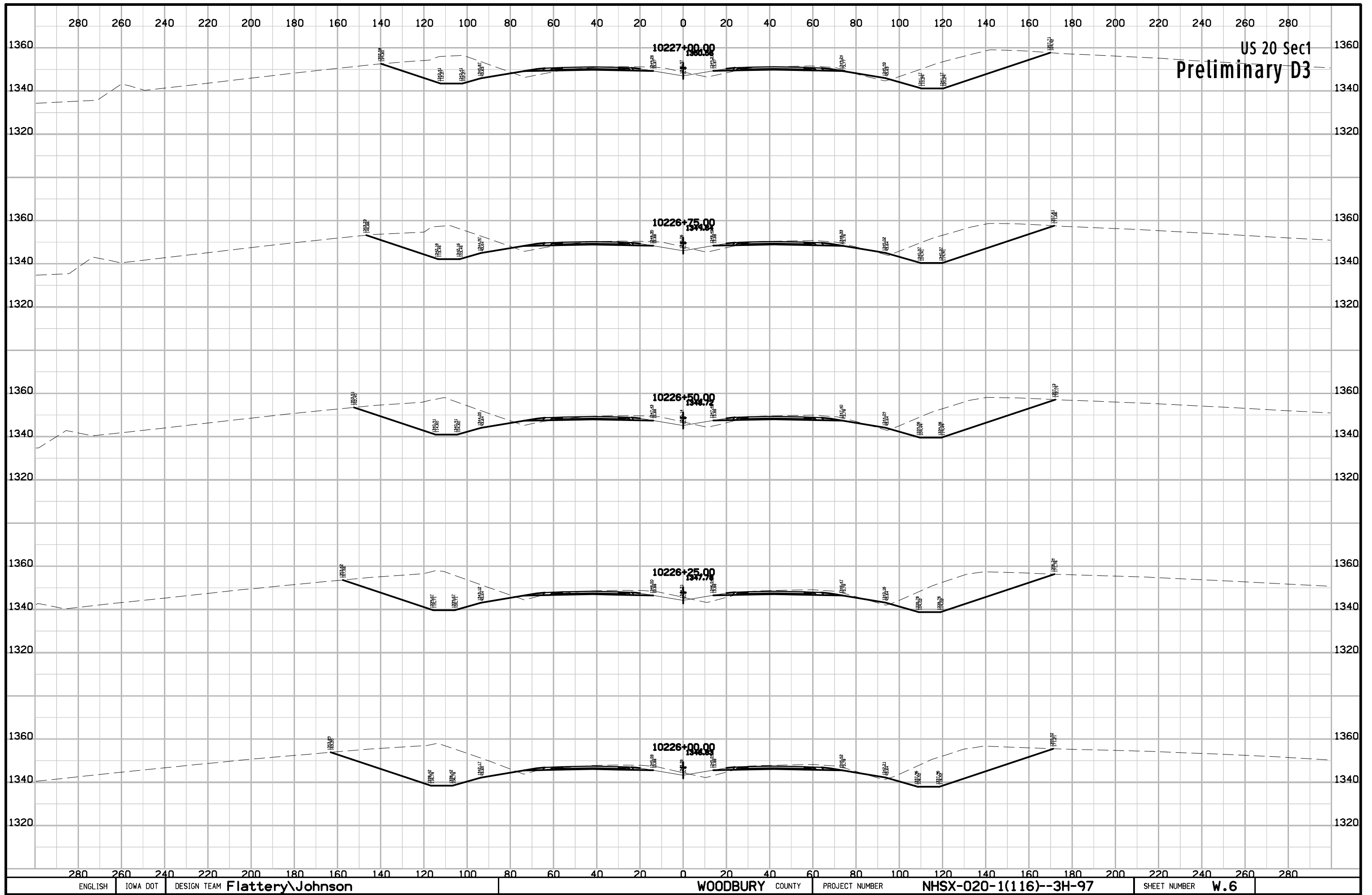
US 20 Sec1
Preliminary D3

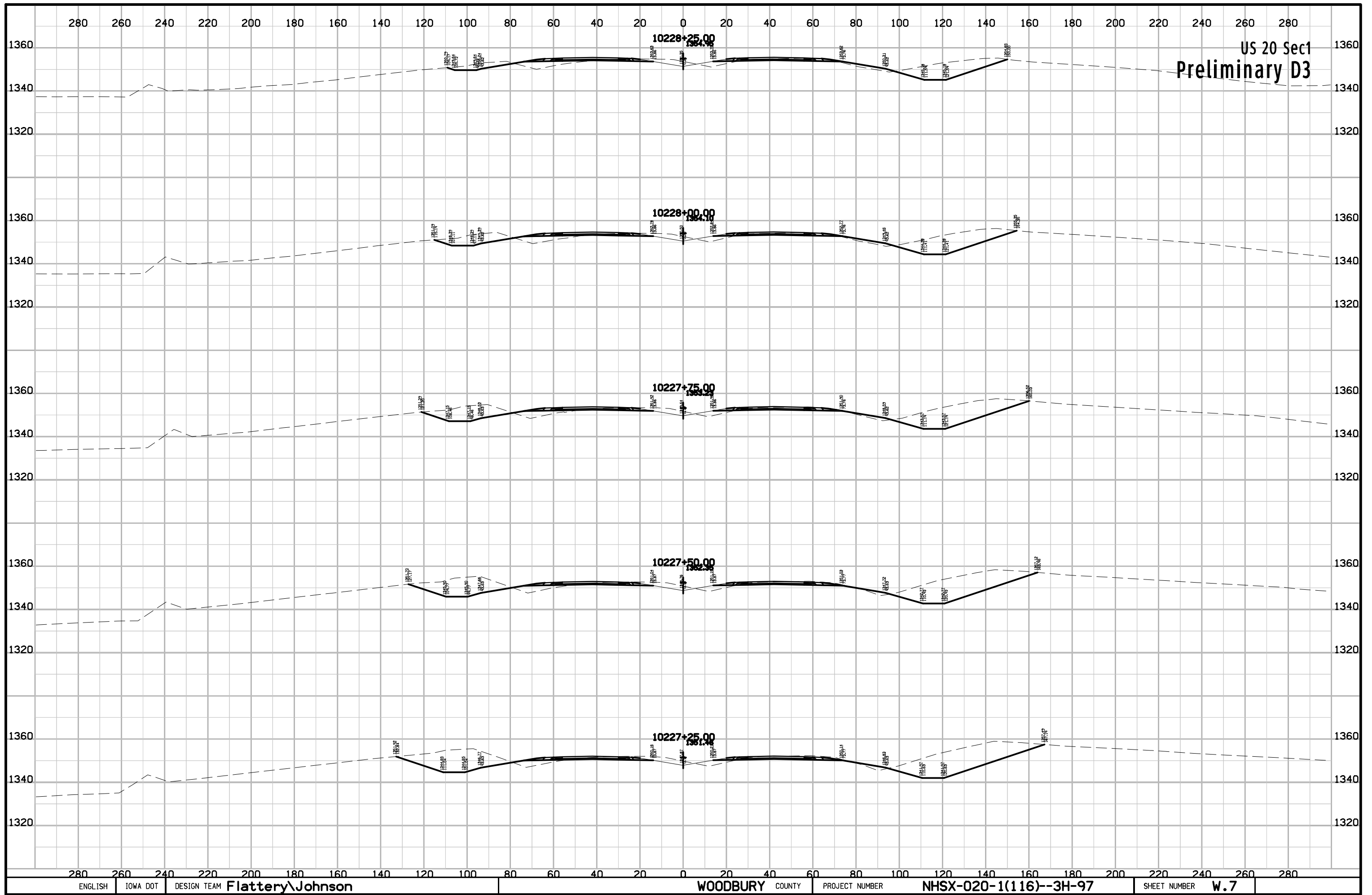


US 20 Sec1
Preliminary D3

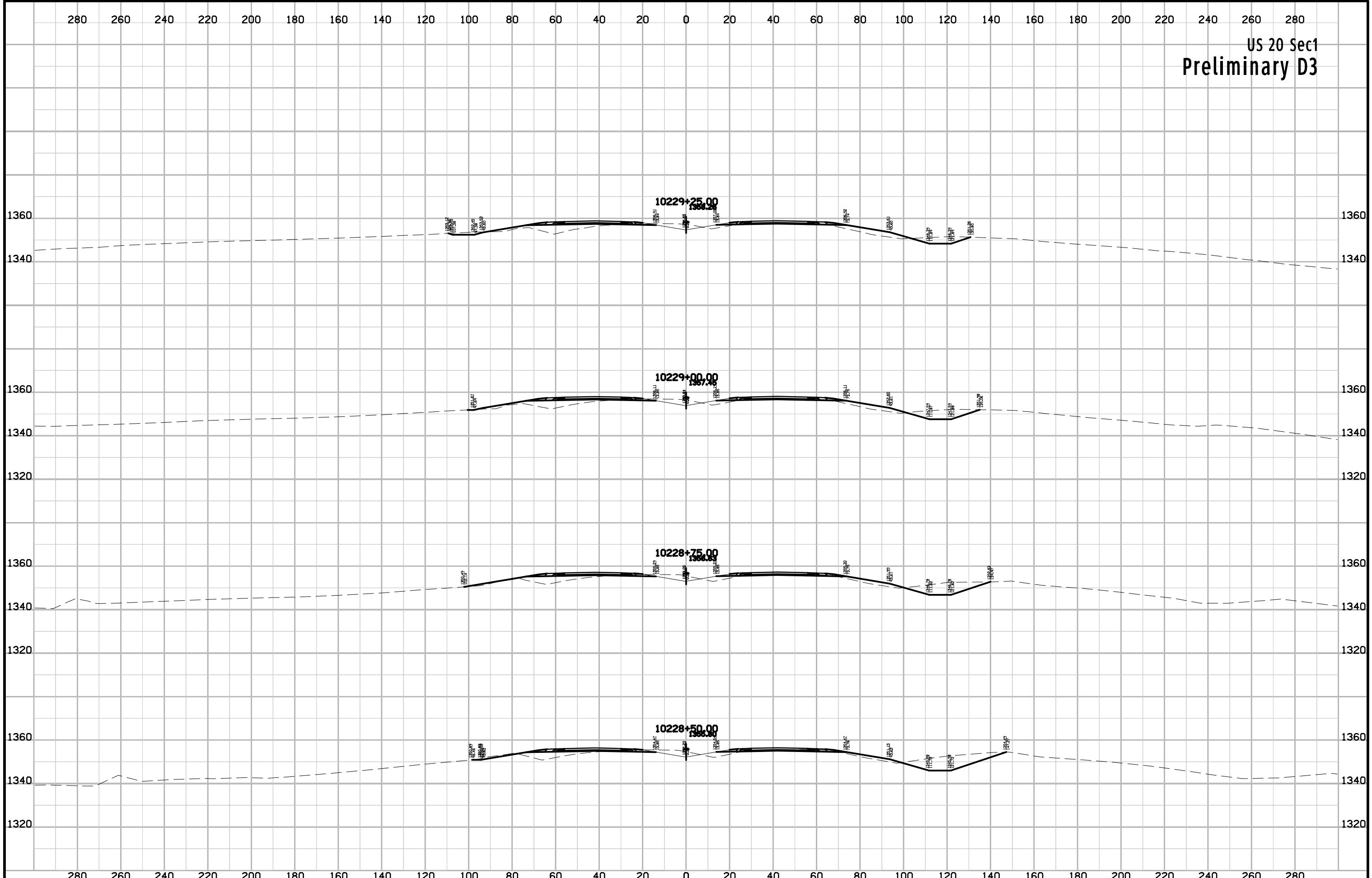




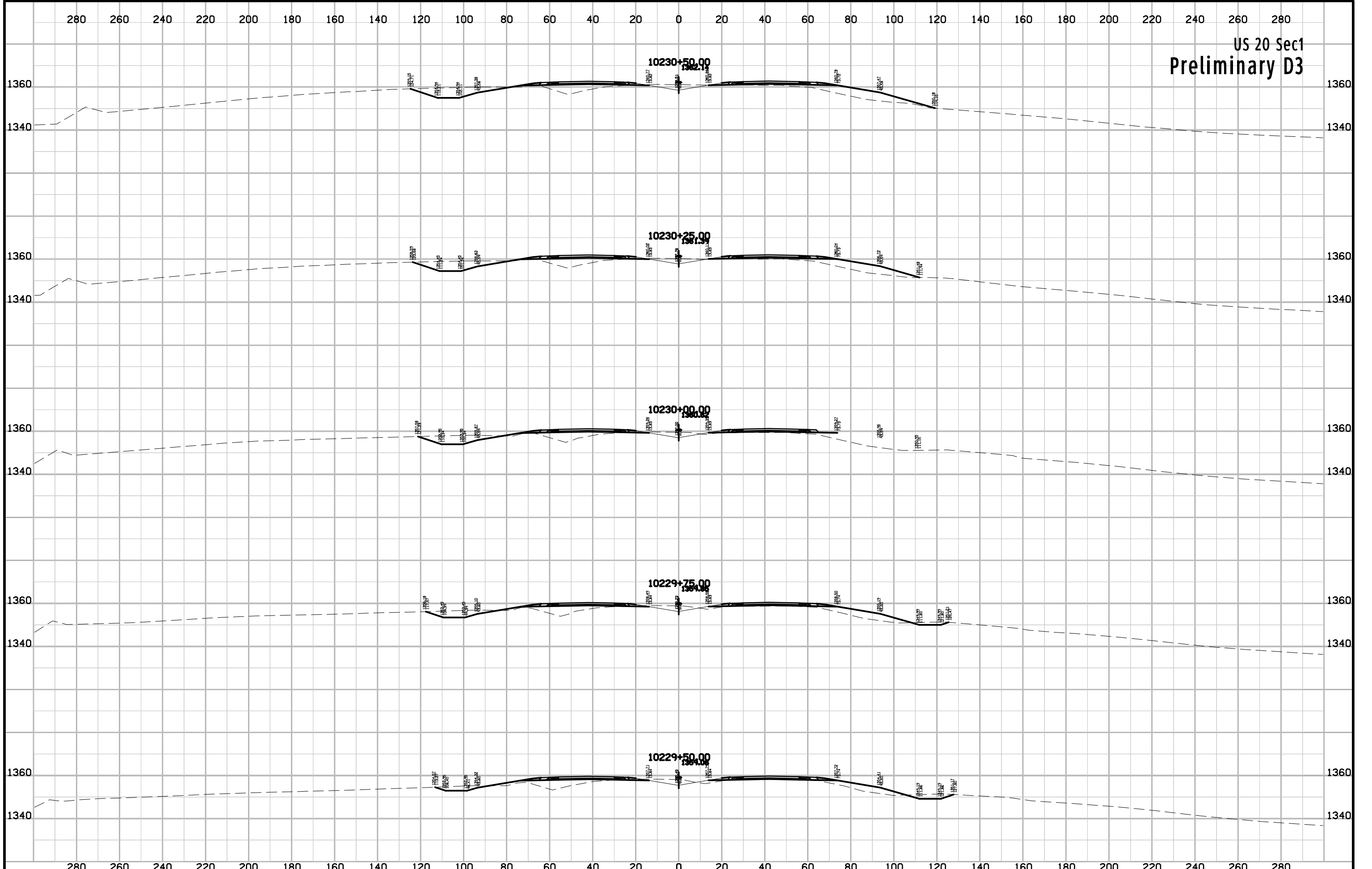




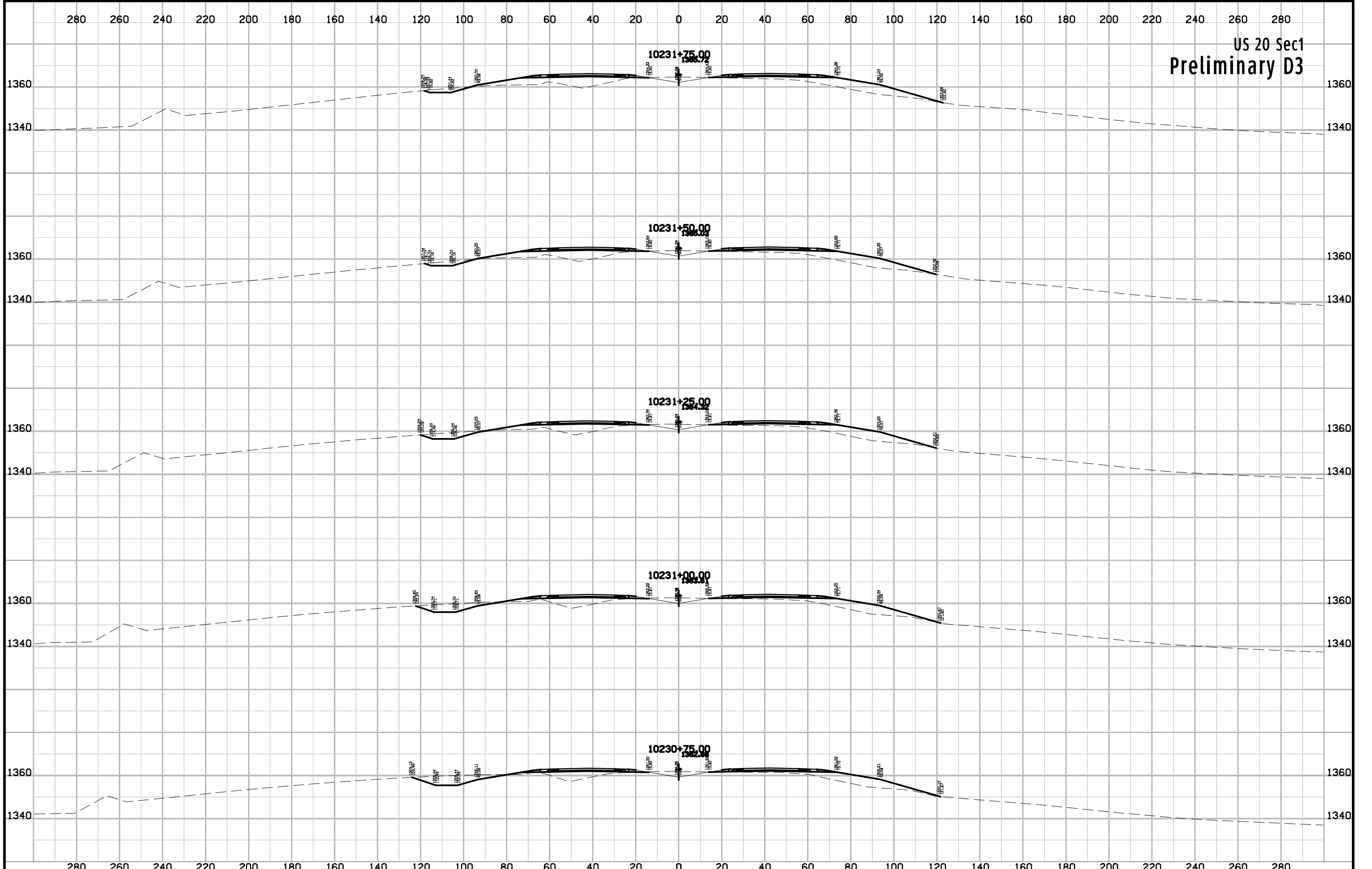
US 20 Sec1
Preliminary D3



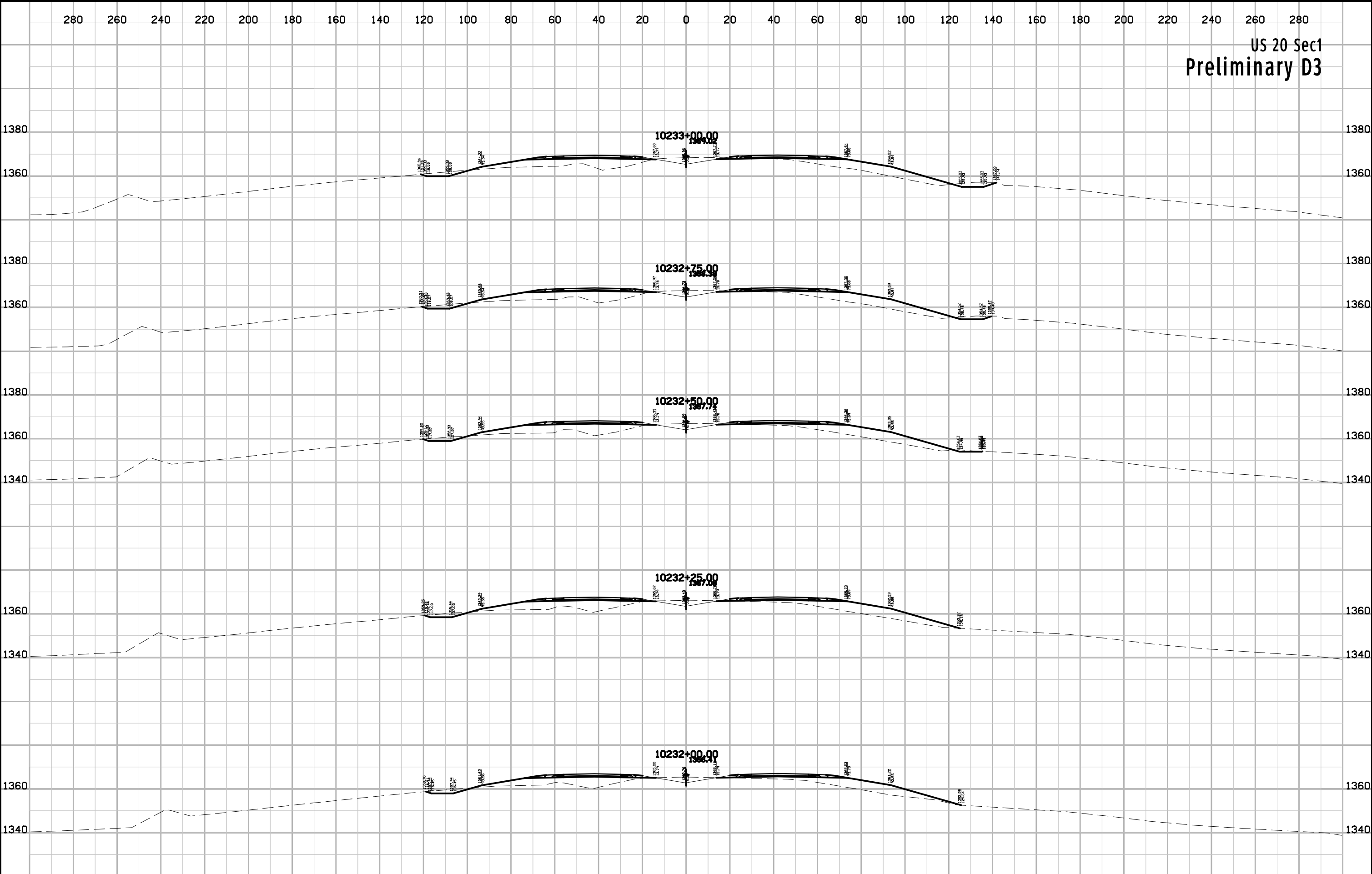
US 20 Sec1
Preliminary D3



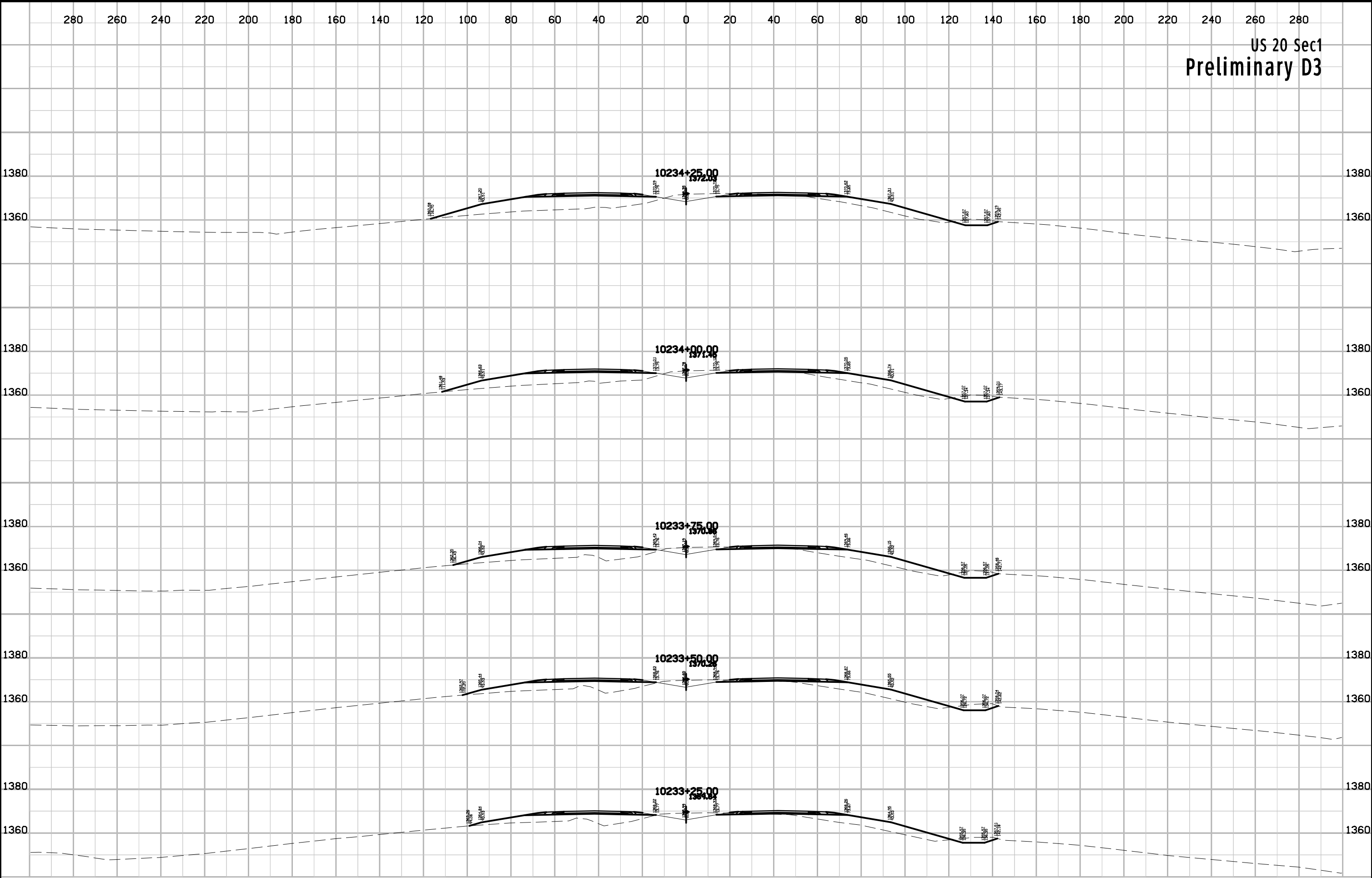
US 20 Sec1
Preliminary D3



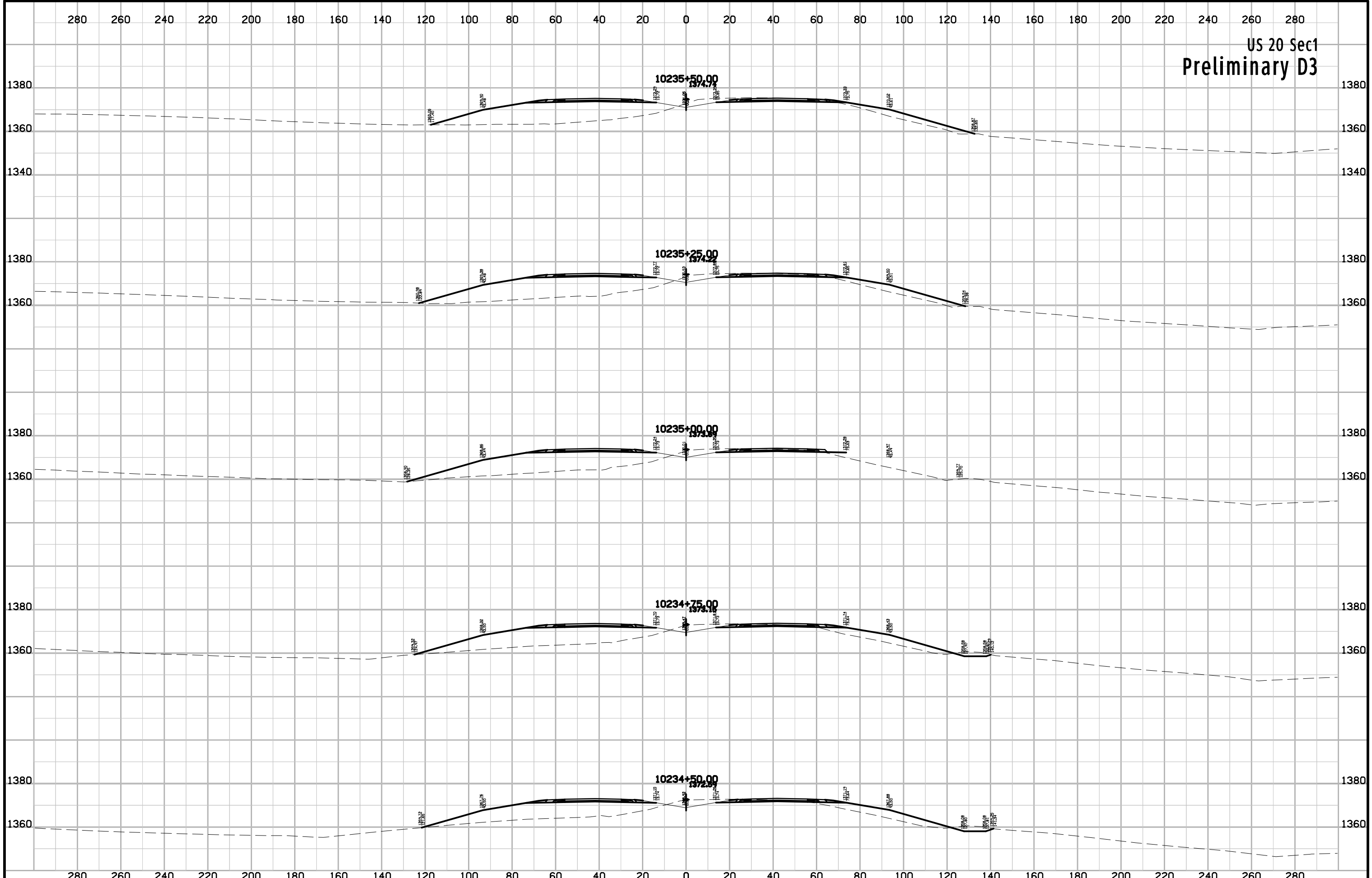
US 20 Sec1
Preliminary D3

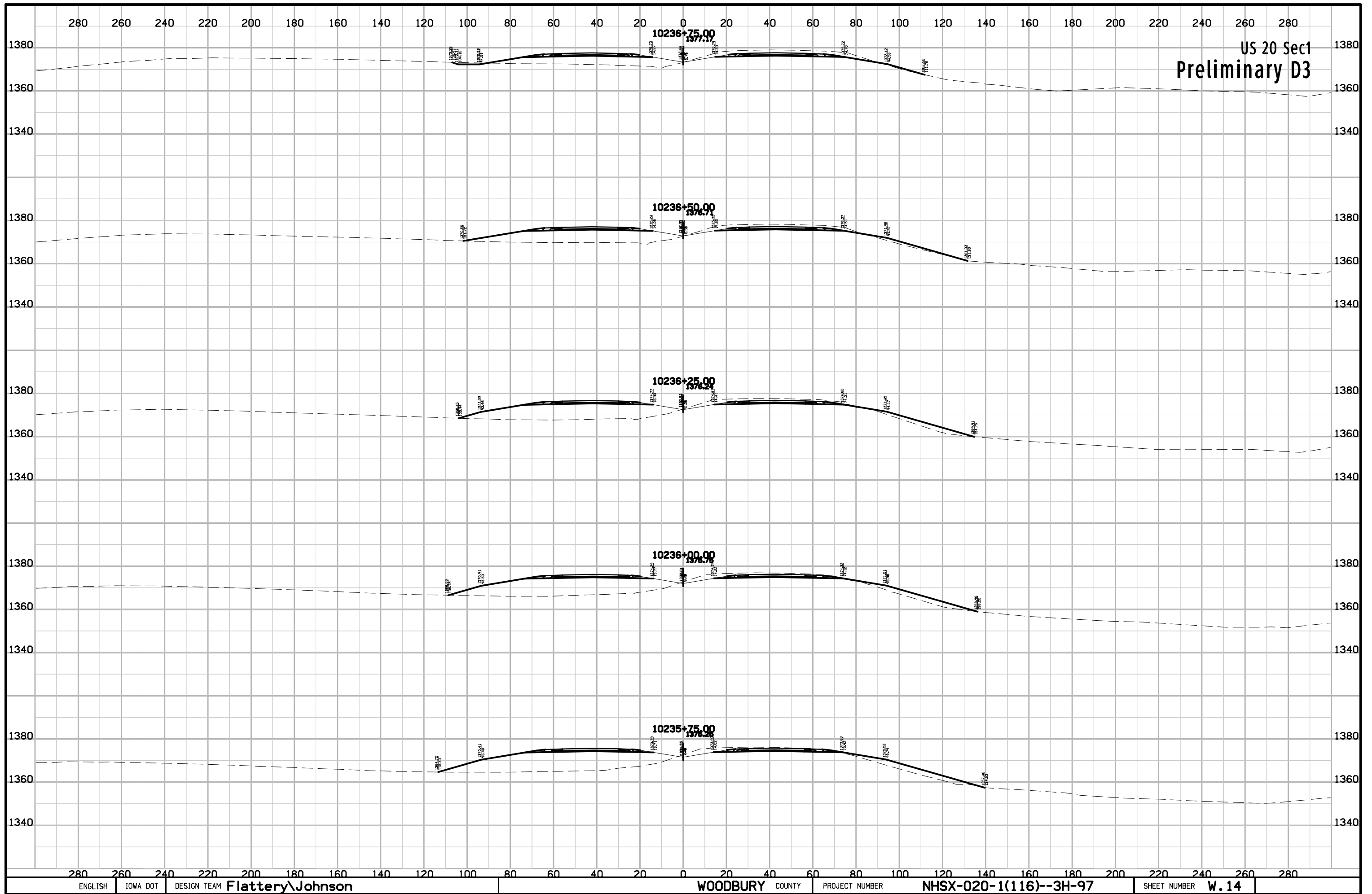


US 20 Sec1
Preliminary D3



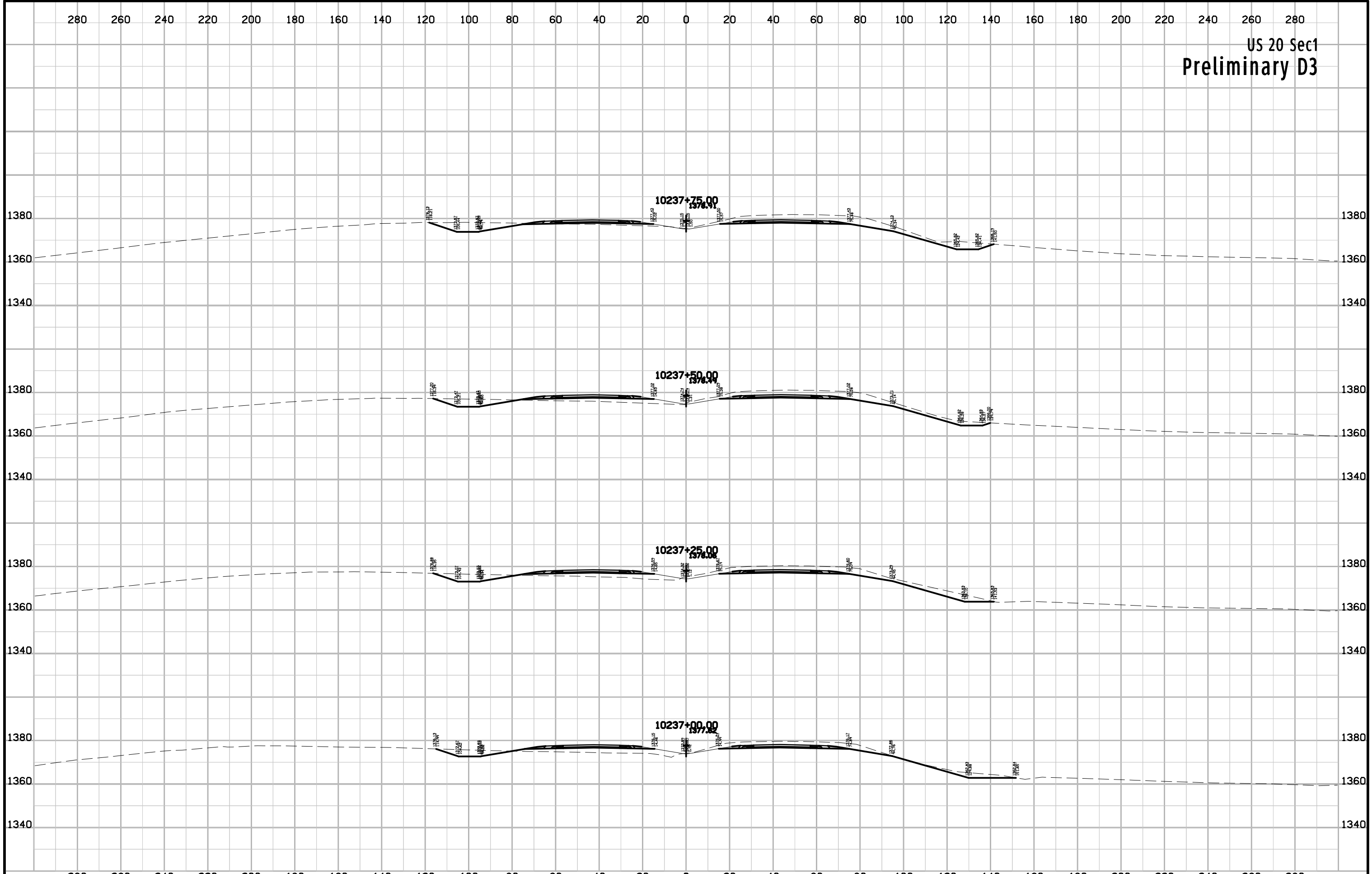
US 20 Sec1
Preliminary D3



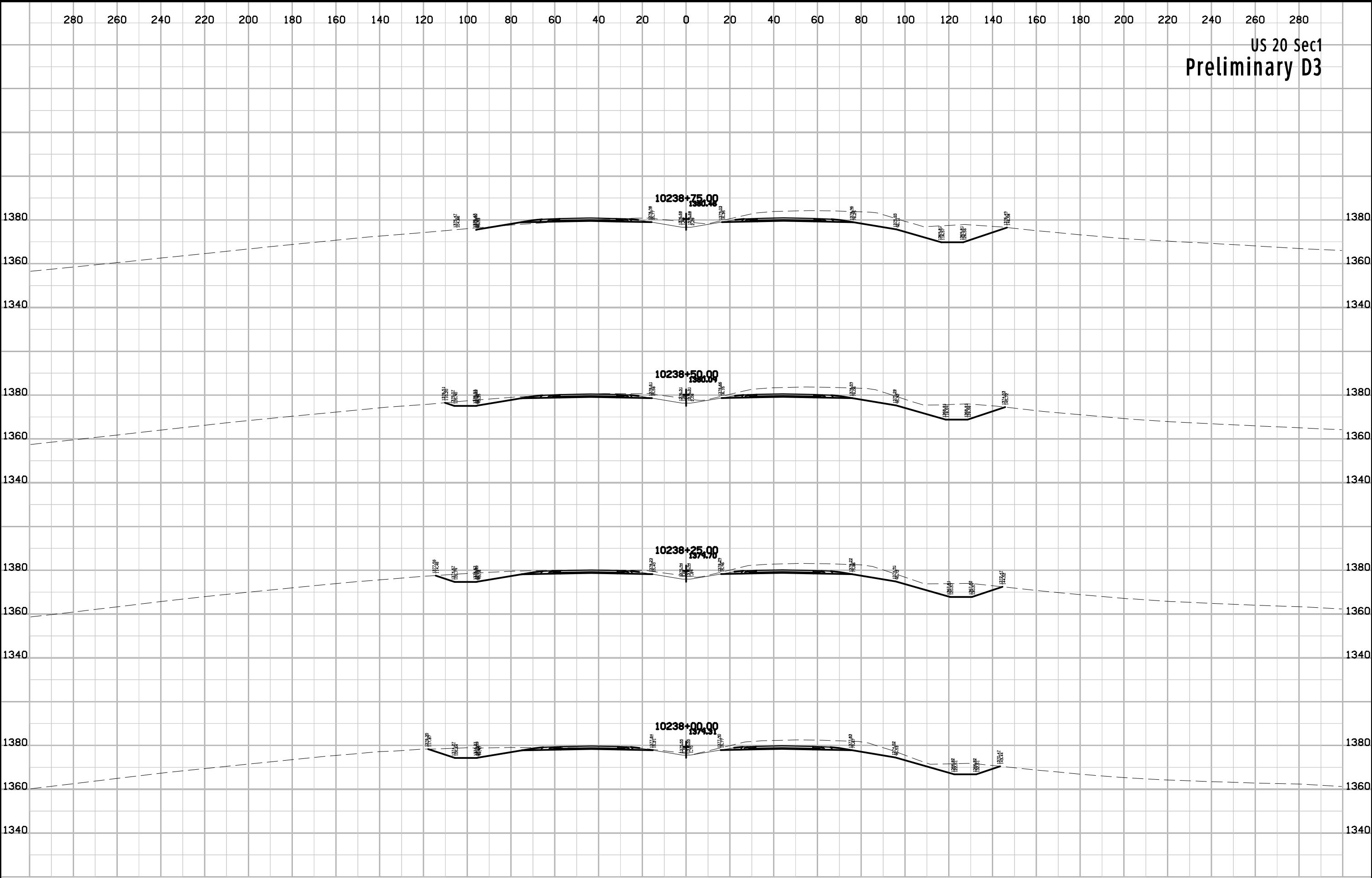


US 20 Sec1
Preliminary D3

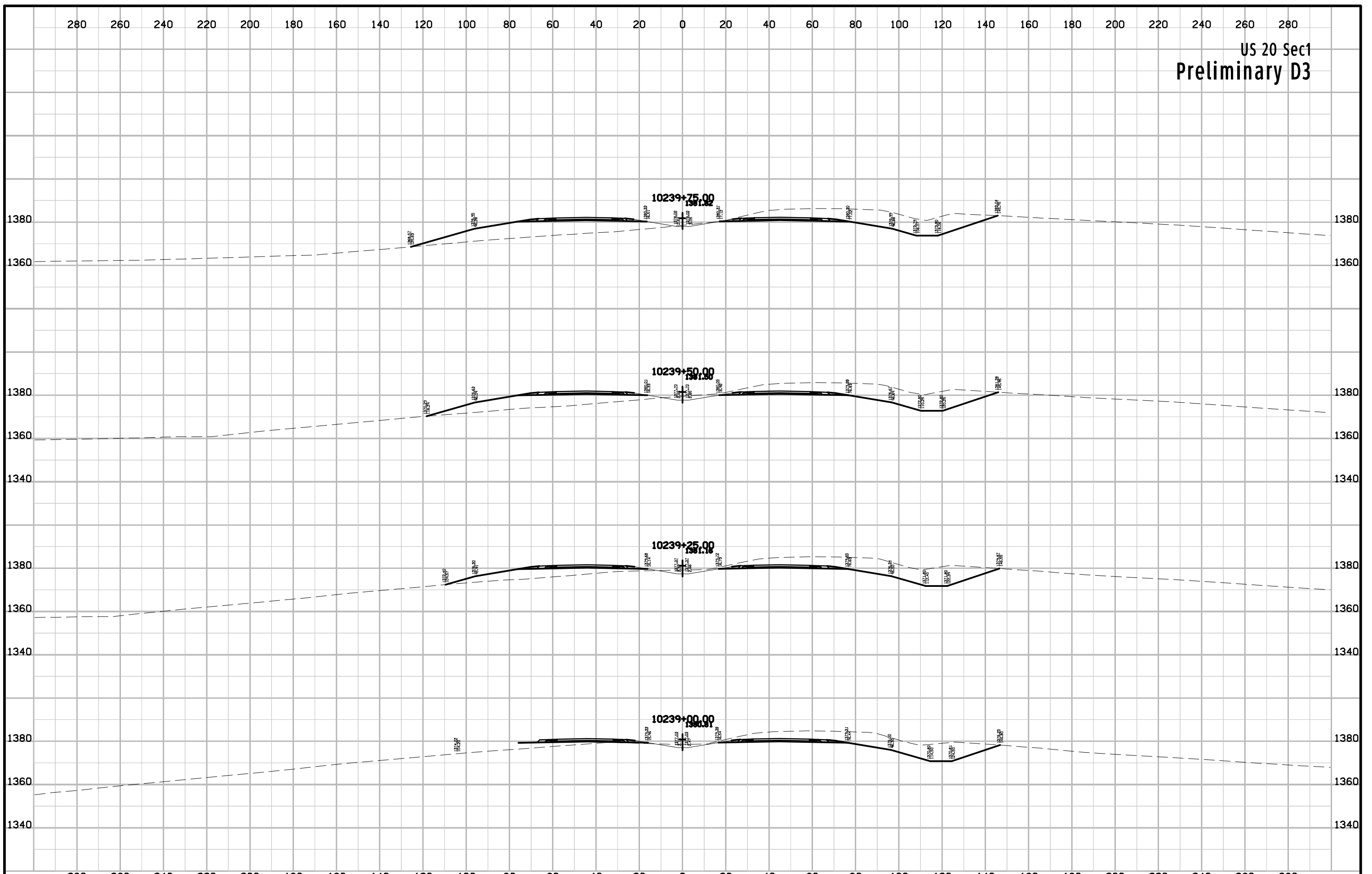
US 20 Sec1
Preliminary D3

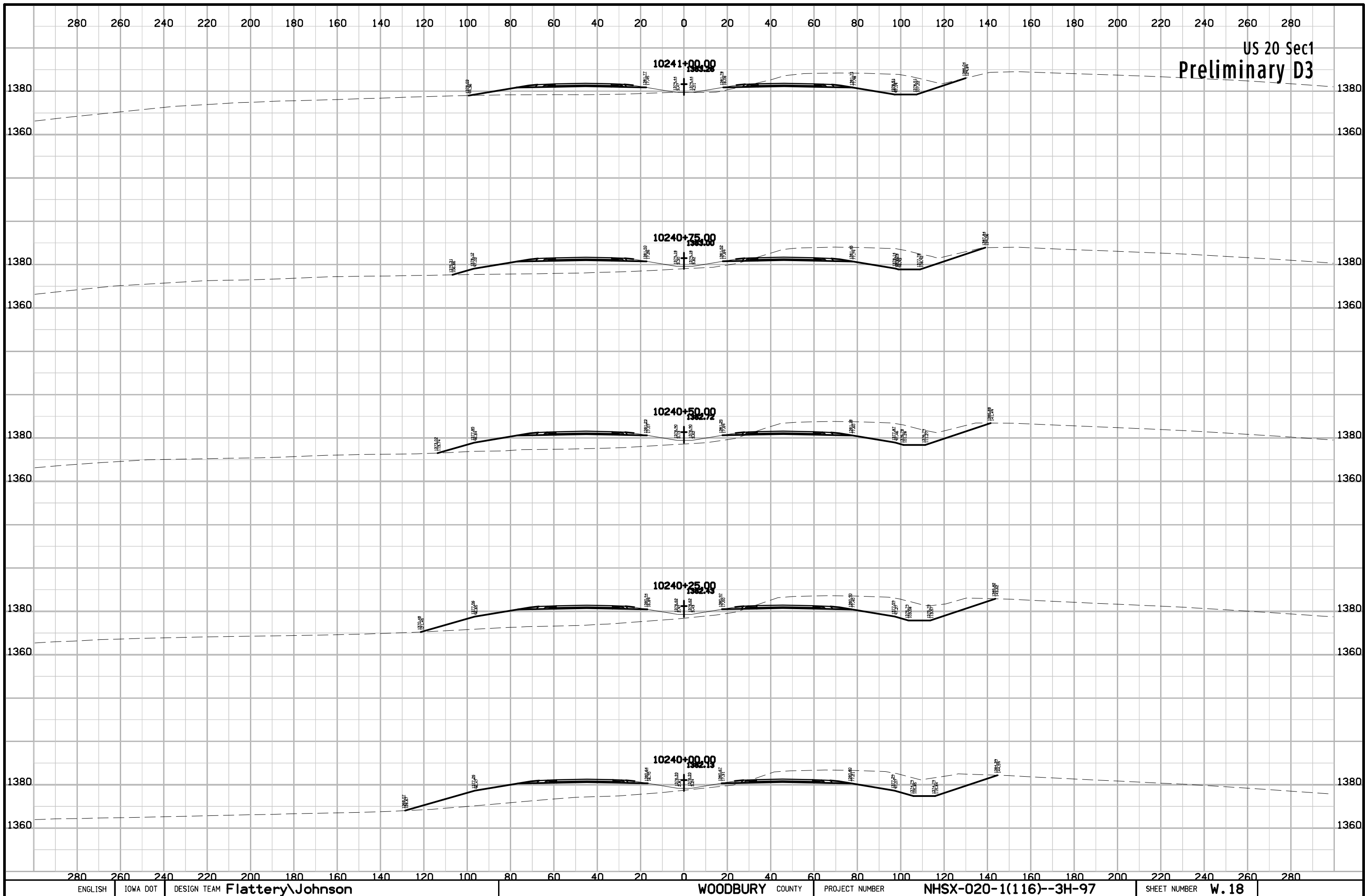


US 20 Sec1
Preliminary D3



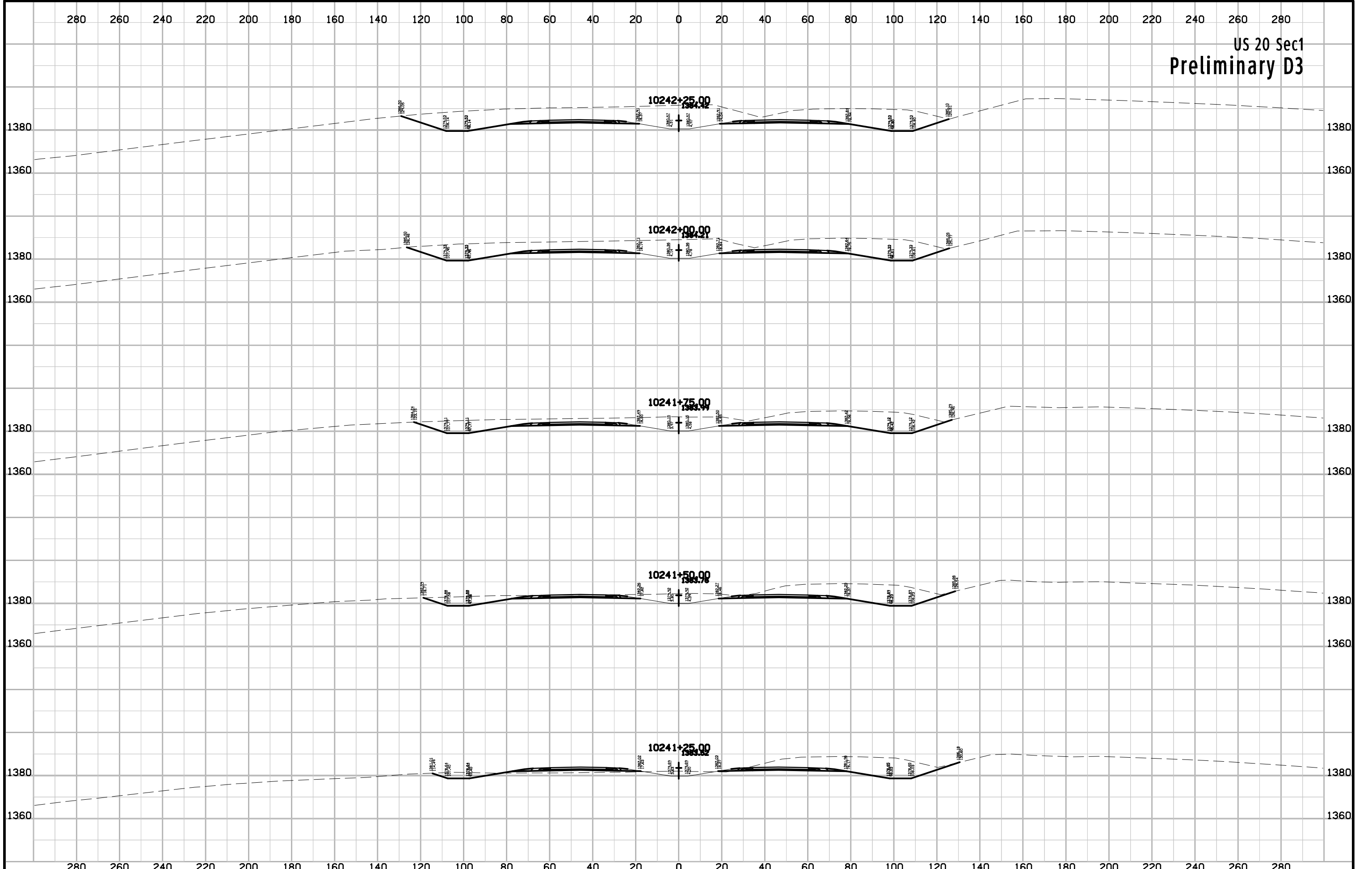
US 20 Sec1
Preliminary D3



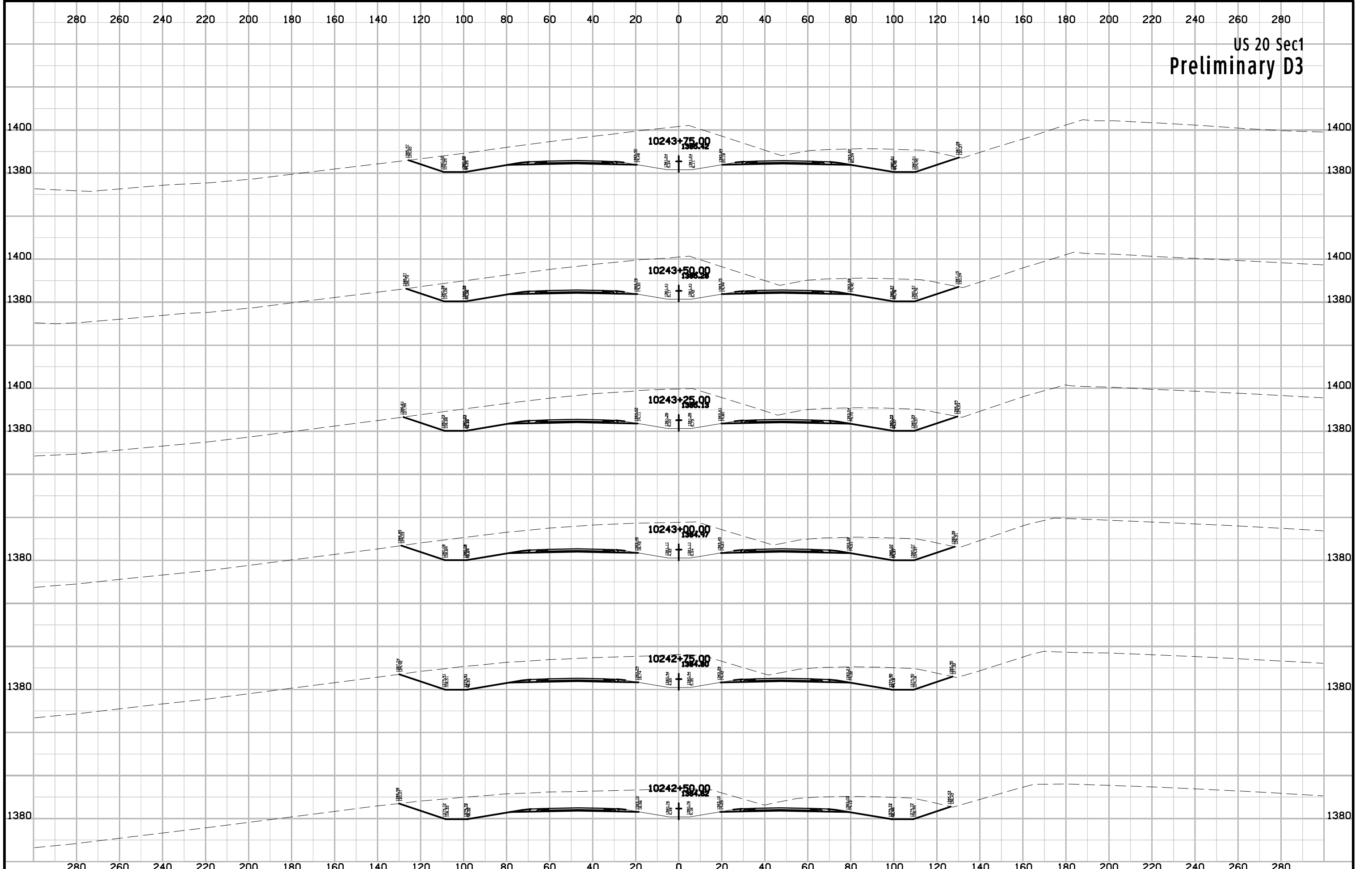


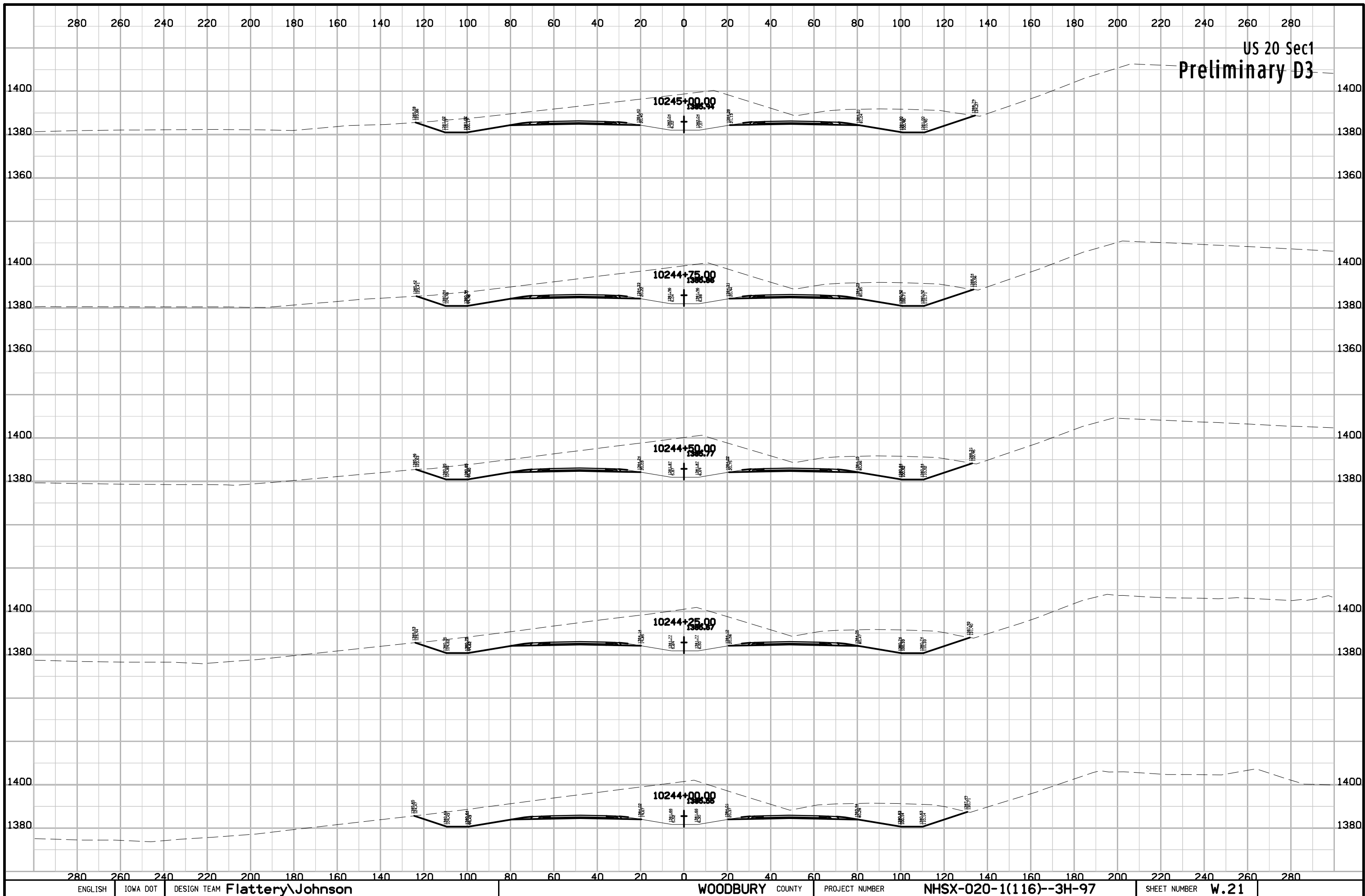
US 20 Sec1
Preliminary D3

US 20 Sec1
Preliminary D3



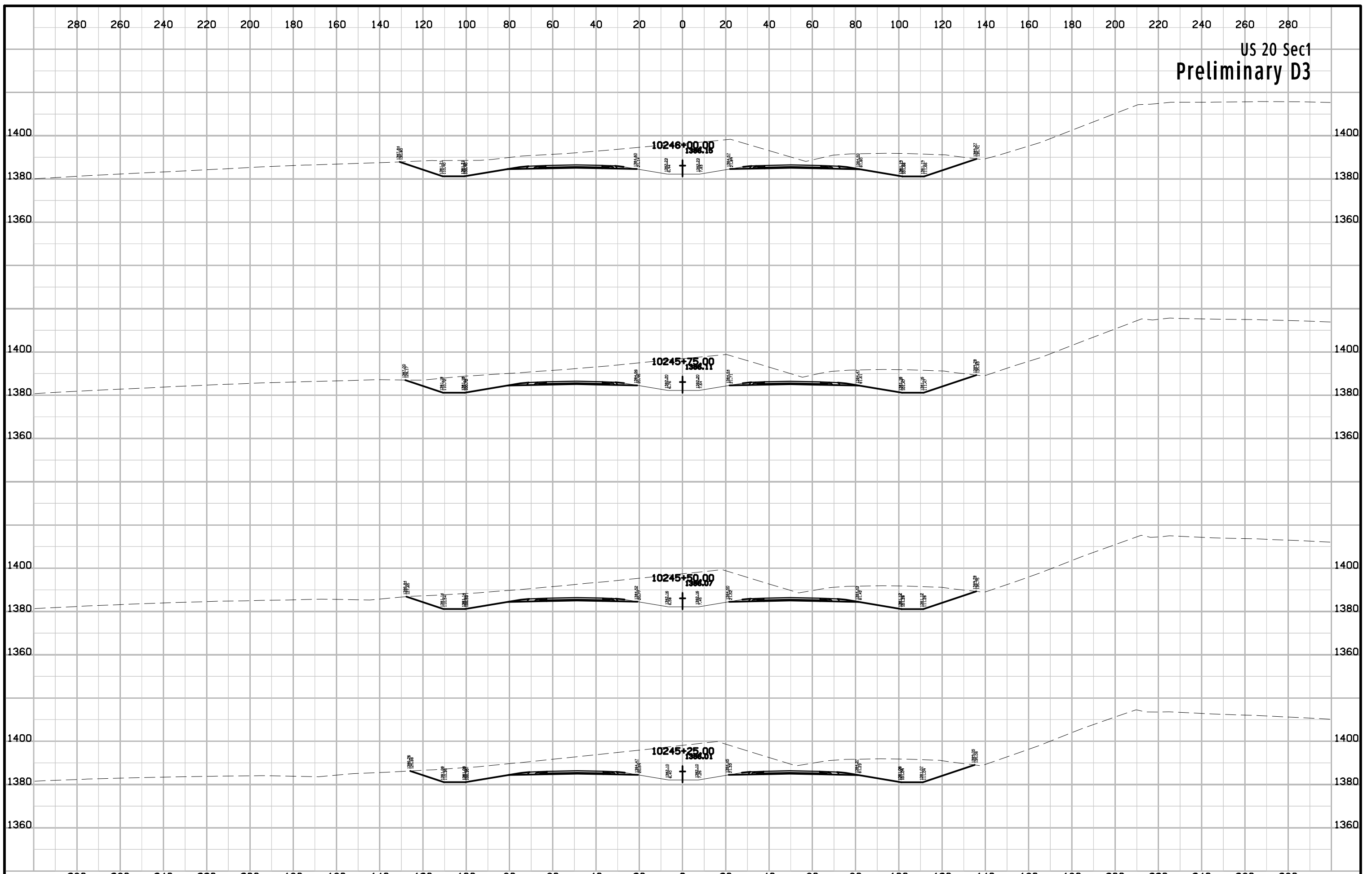
US 20 Sec1
Preliminary D3

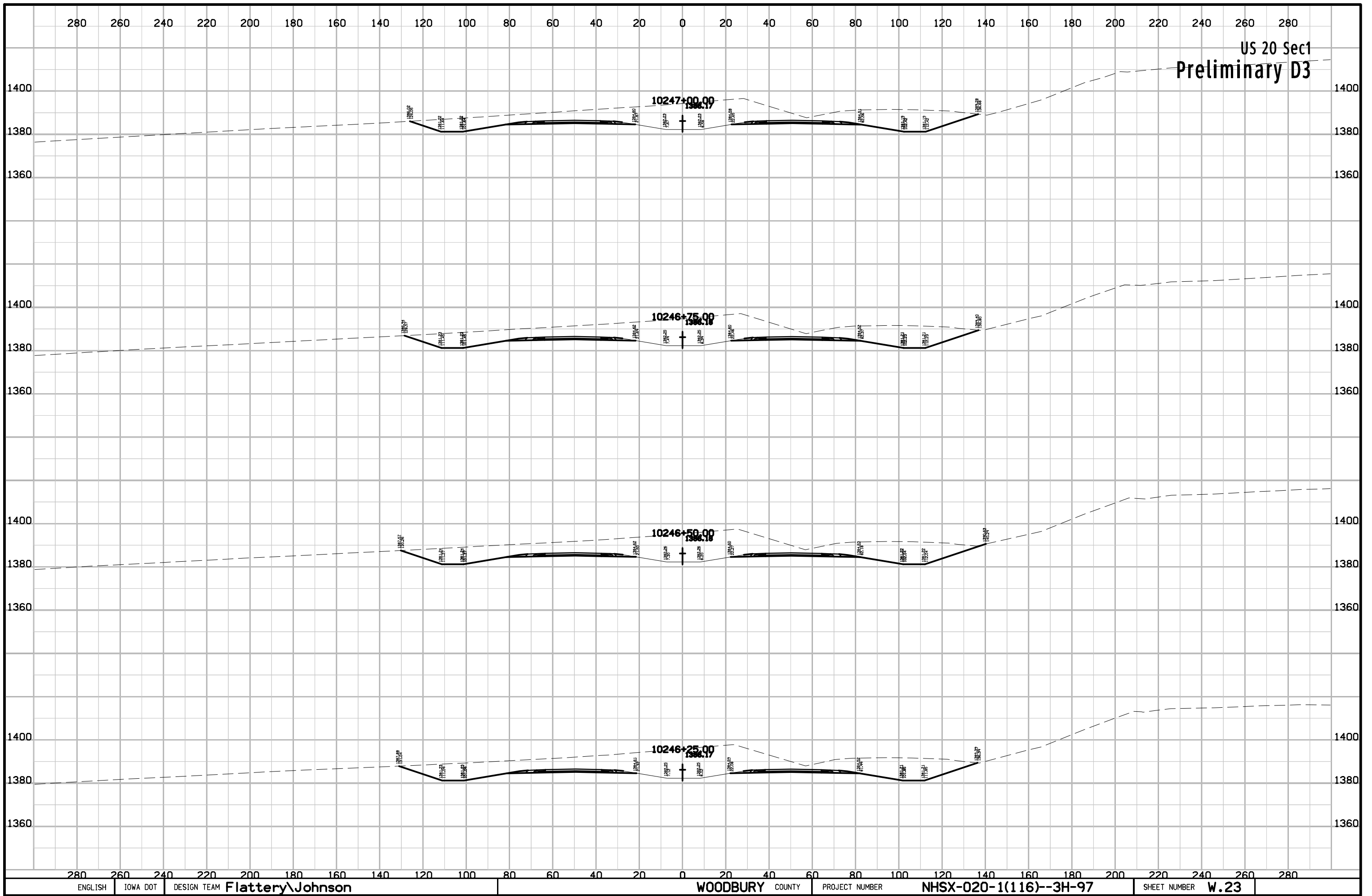




US 20 Sec1
Preliminary D3

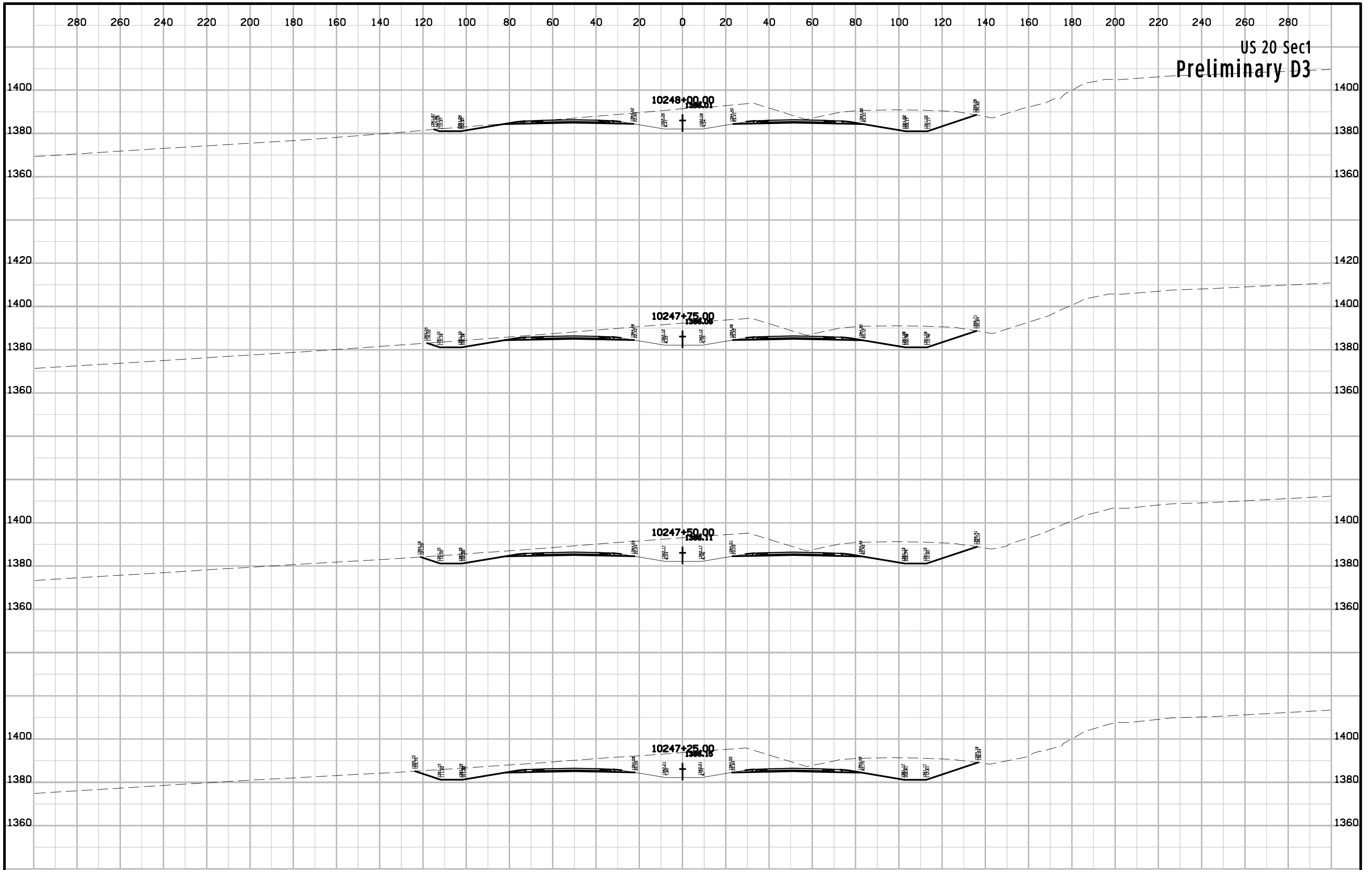
US 20 Sec1
Preliminary D3



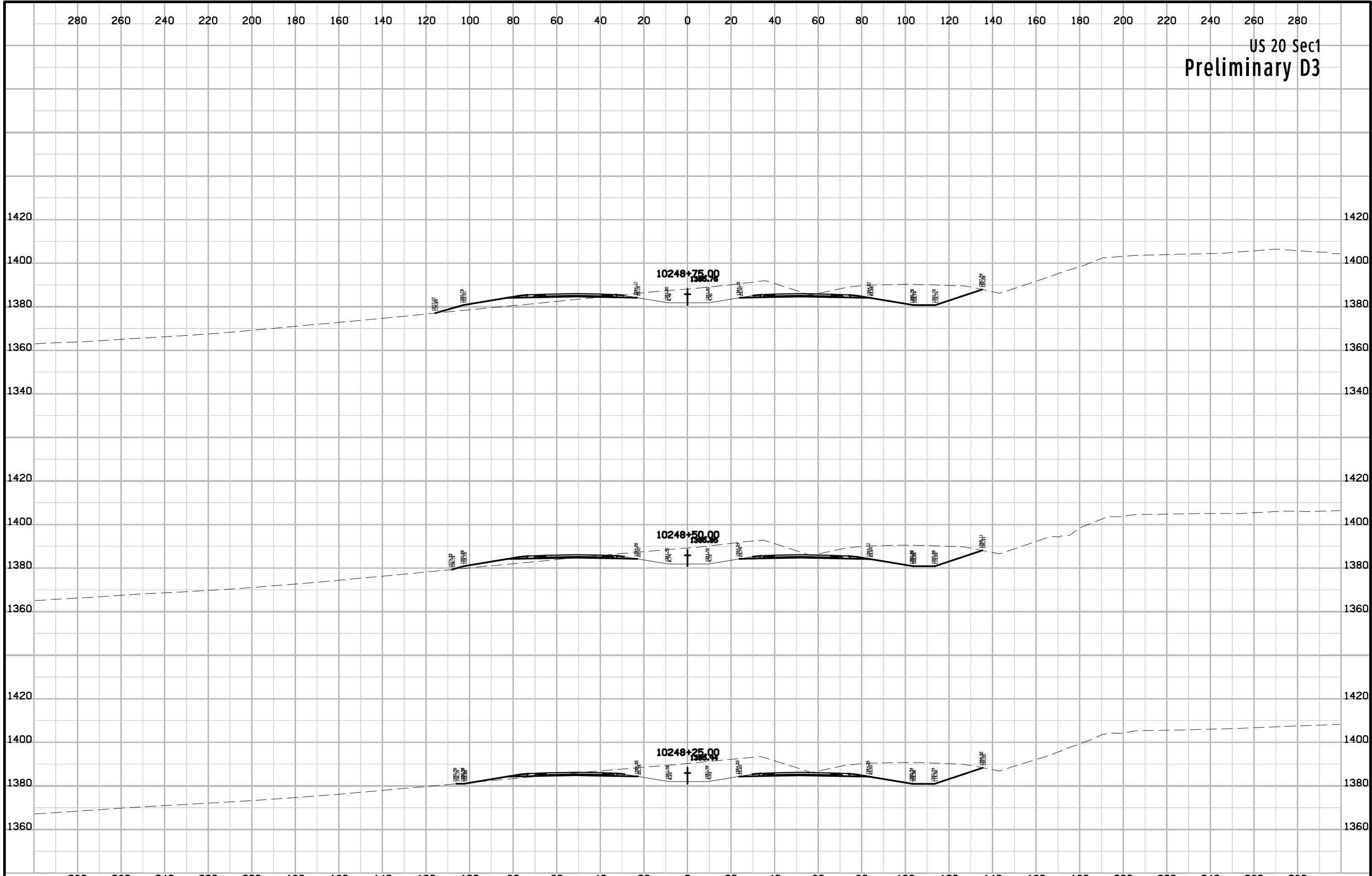


US 20 Sec1
Preliminary D3

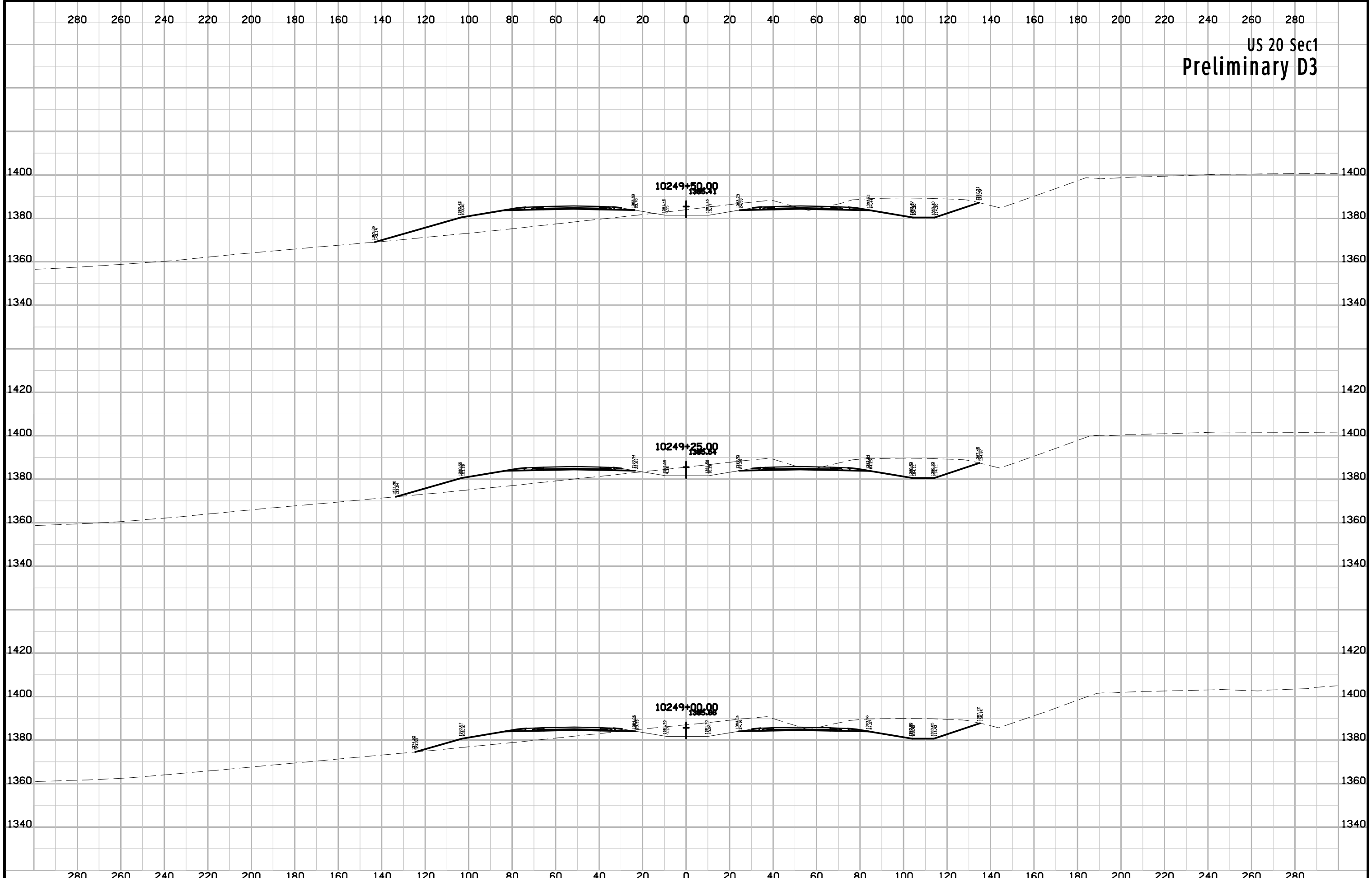
US 20 Sec1
Preliminary D3



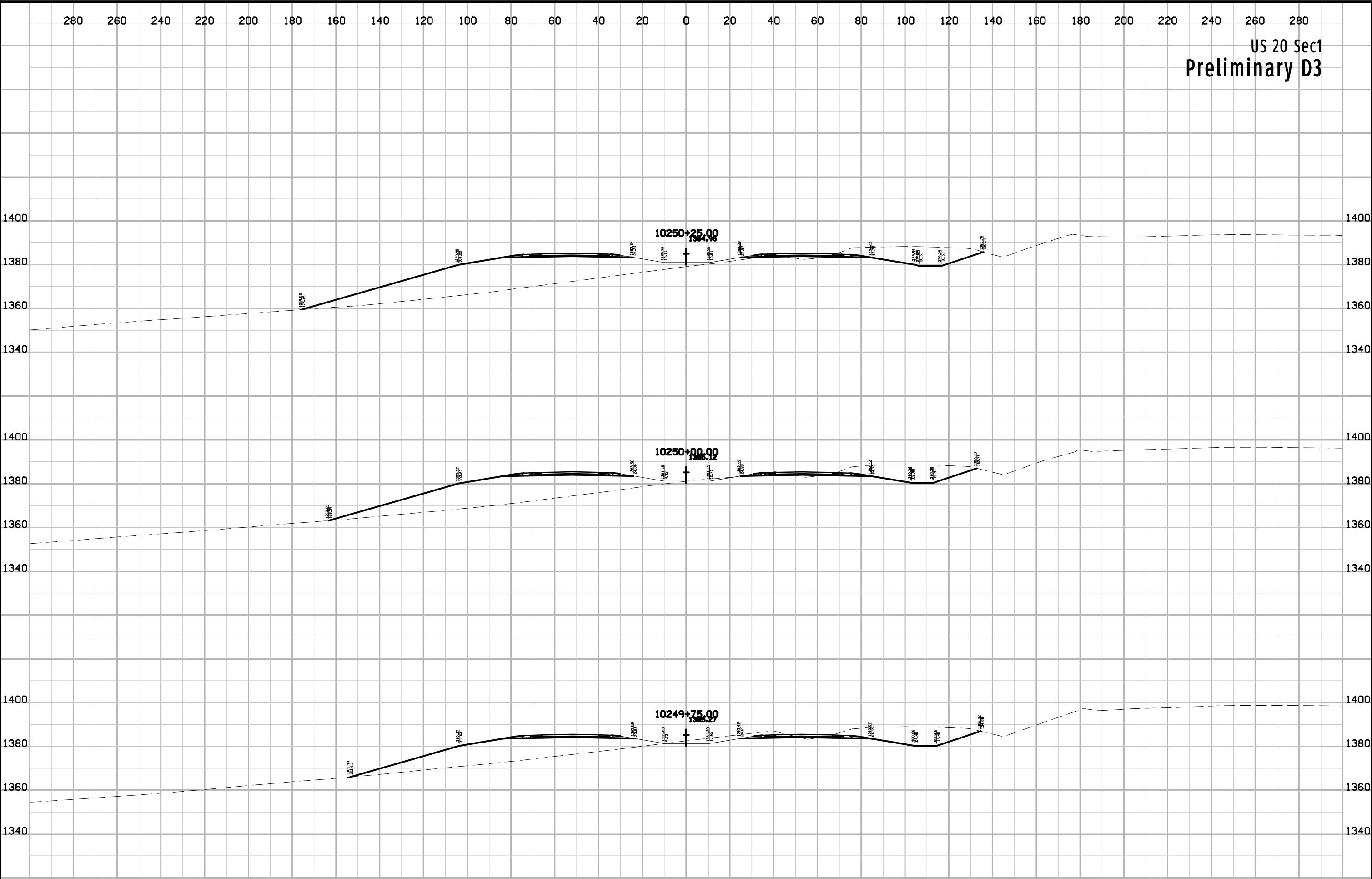
US 20 Sec1
Preliminary D3

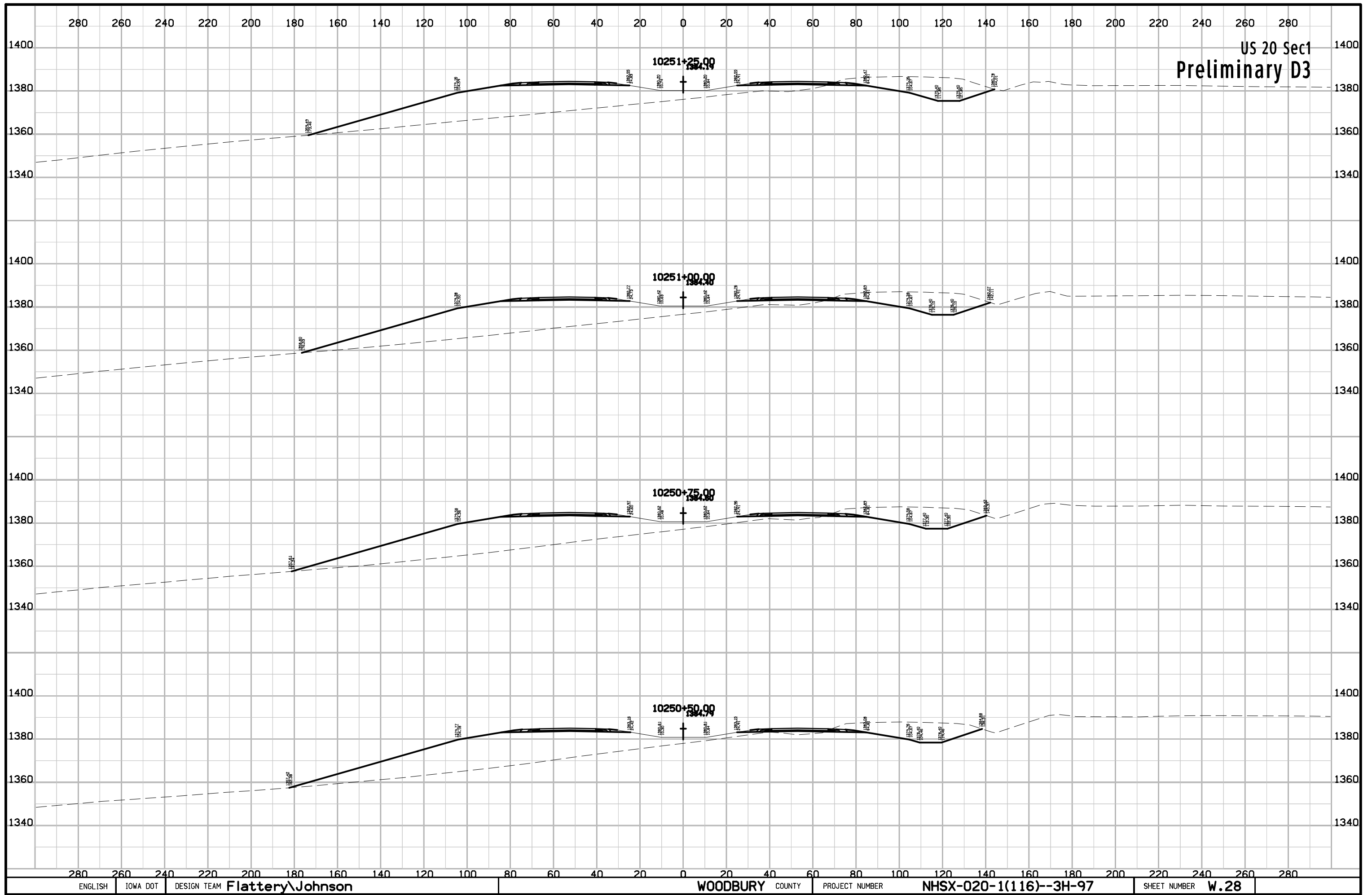


US 20 Sec1
Preliminary D3



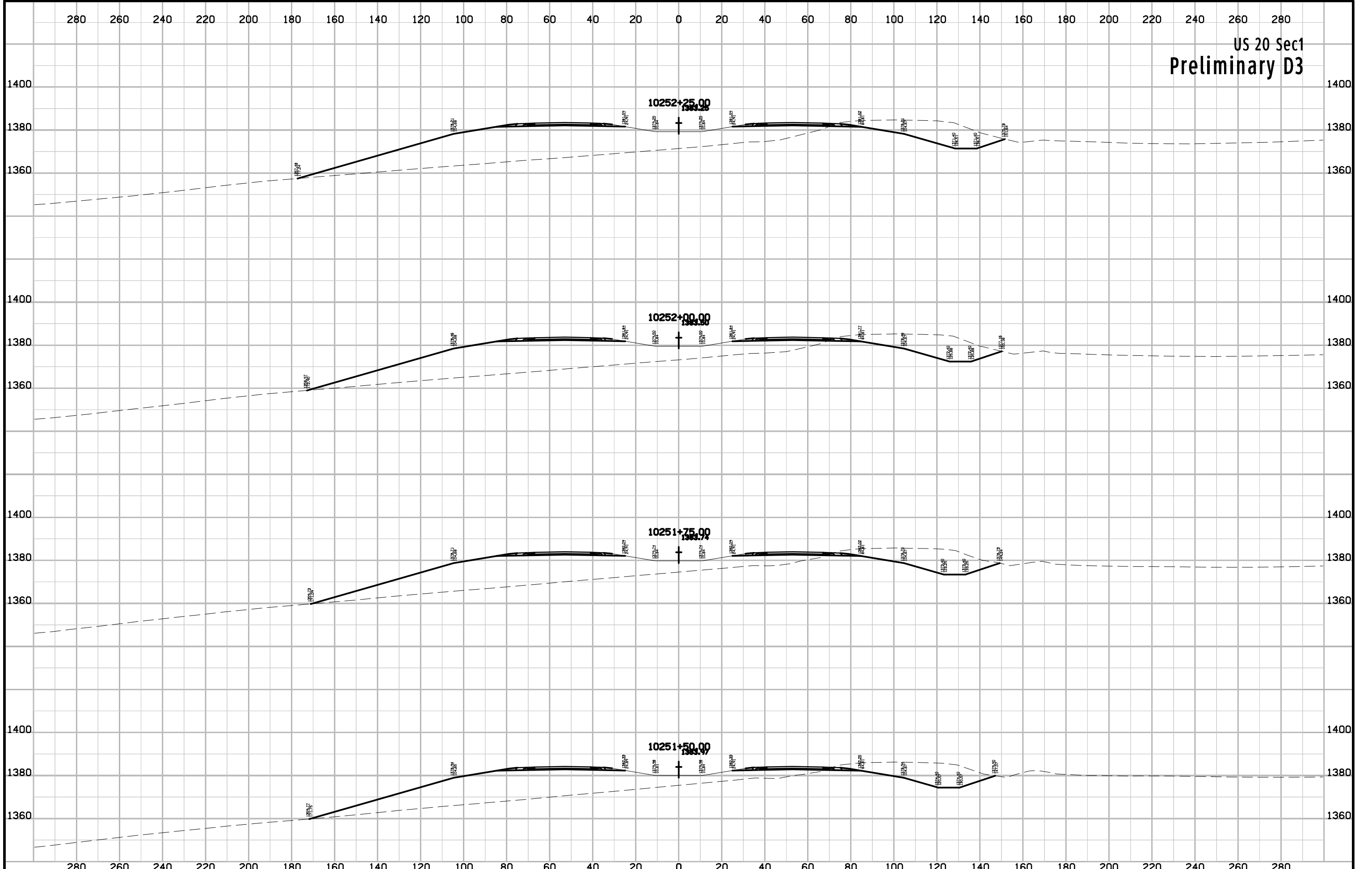
US 20 Sec1
Preliminary D3



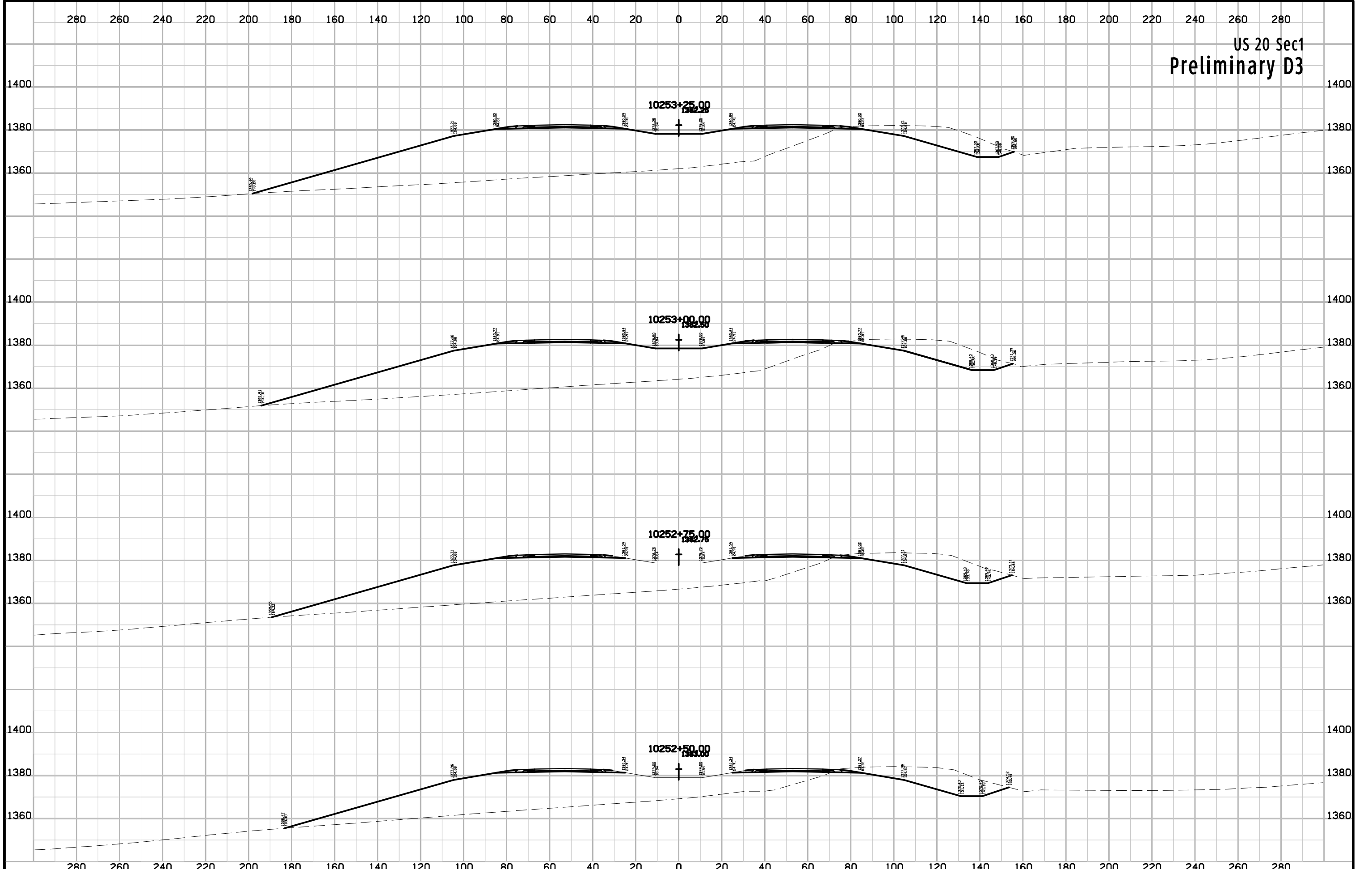


US 20 Sec1
Preliminary D3

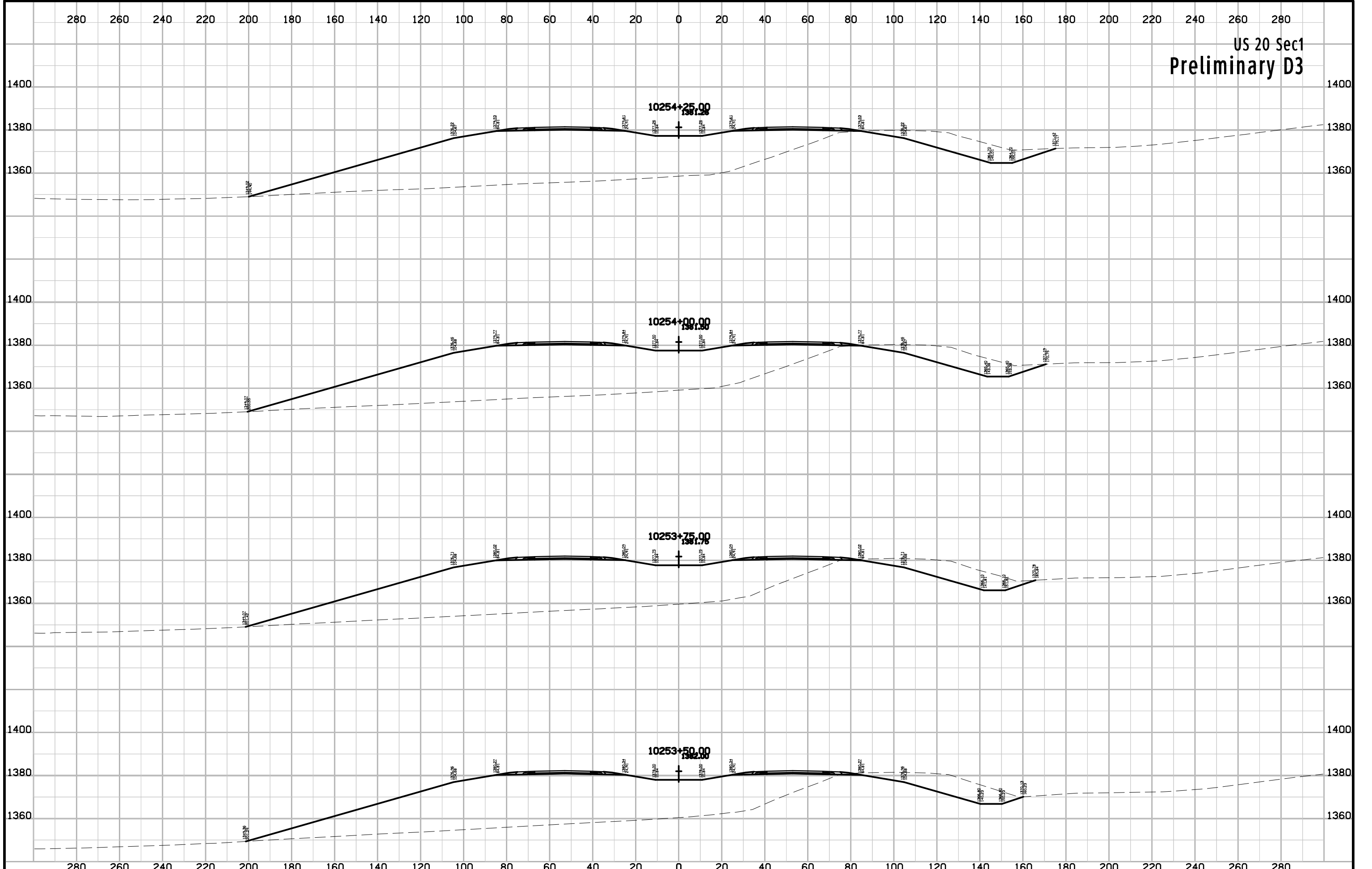
US 20 Sec1
Preliminary D3



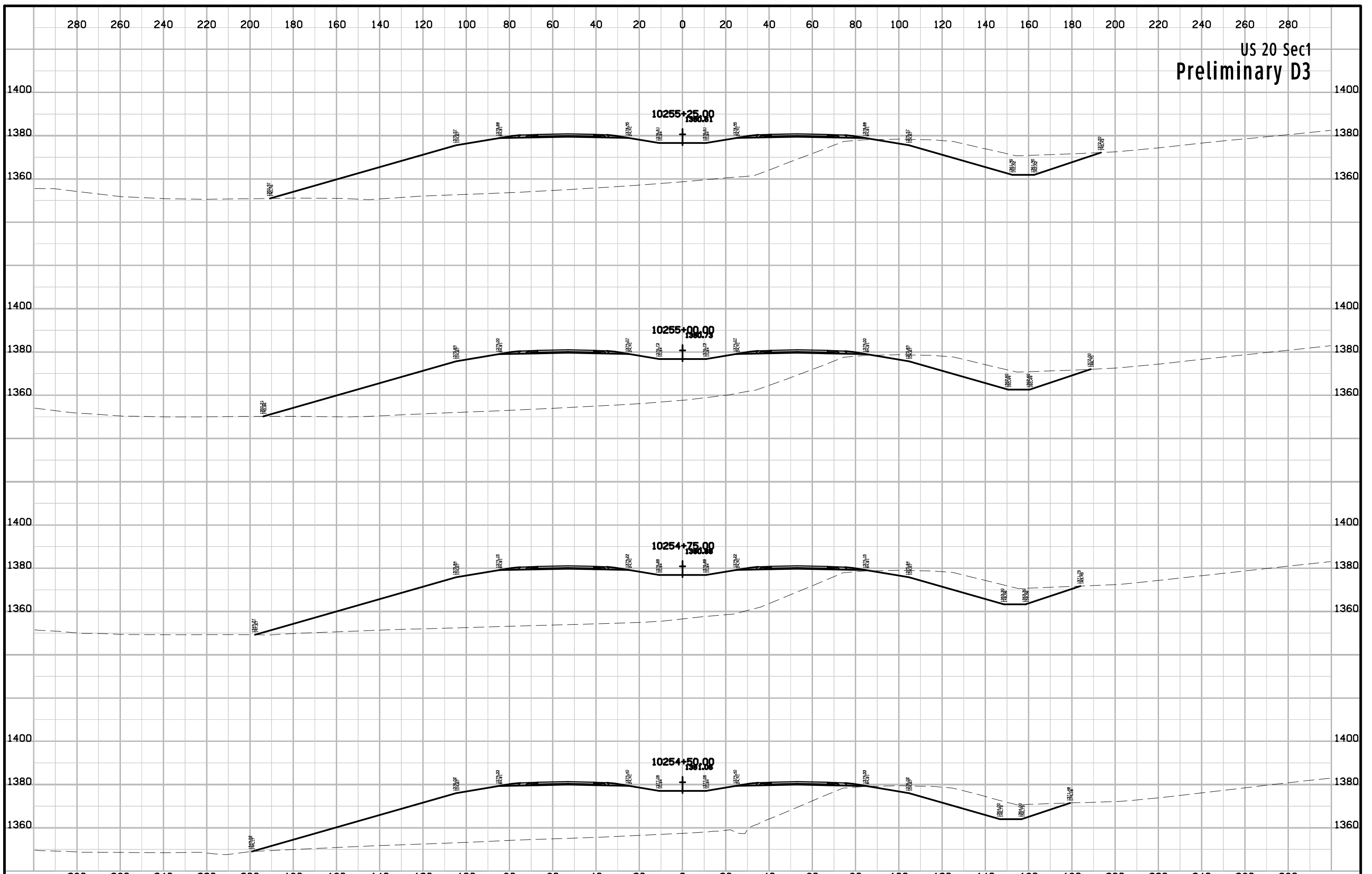
US 20 Sec1
Preliminary D3



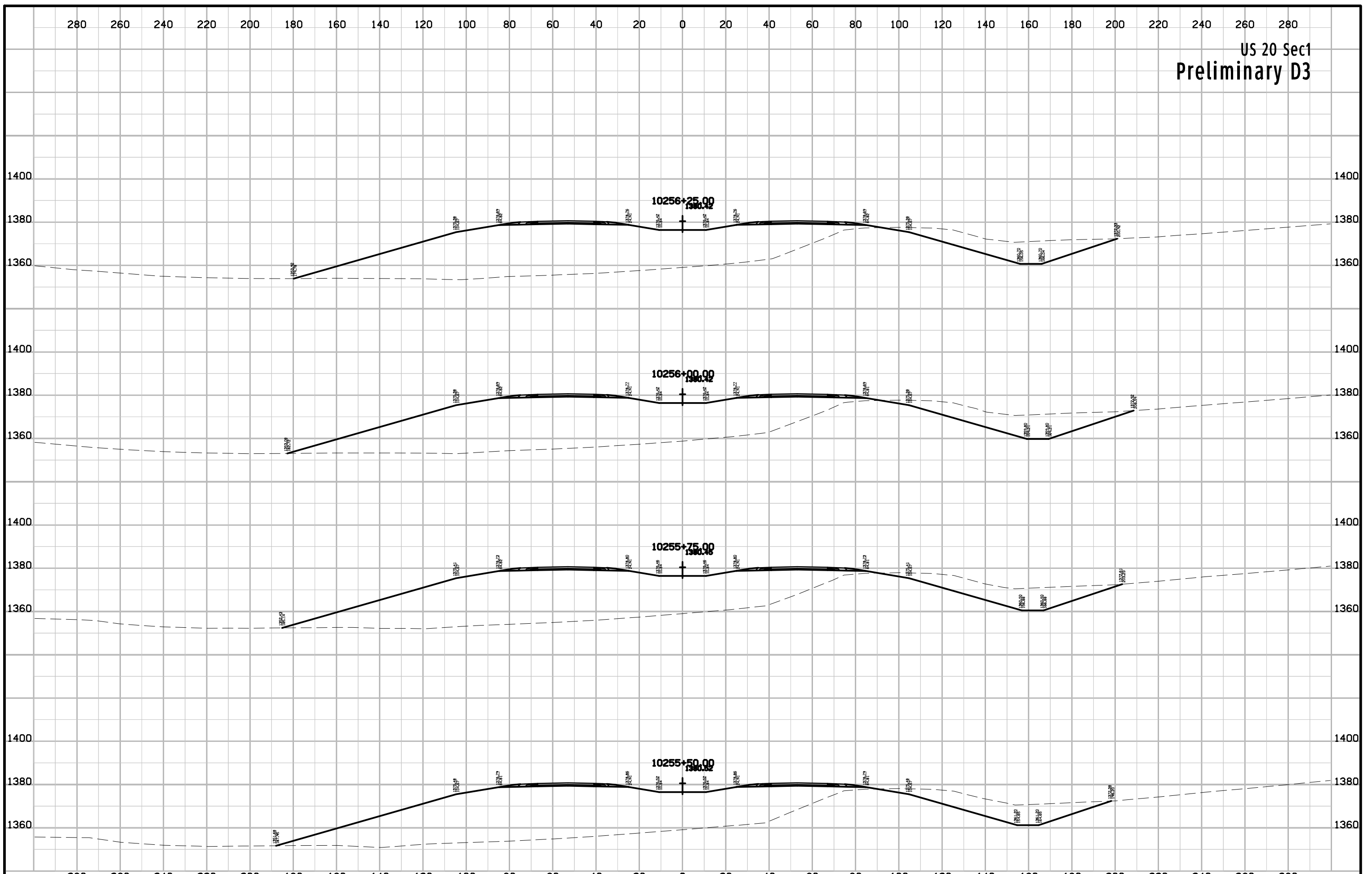
US 20 Sec1
Preliminary D3



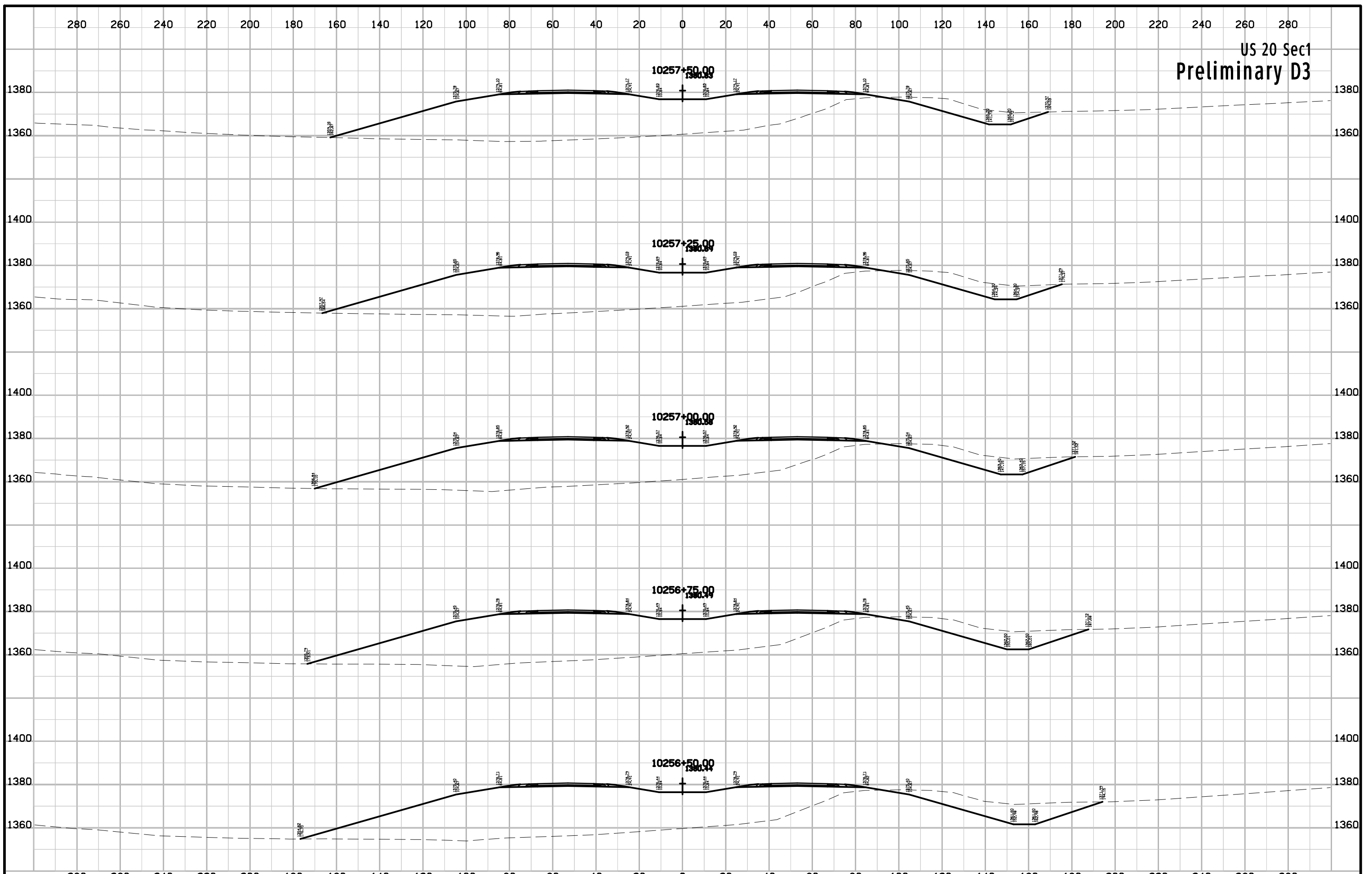
US 20 Sec1
Preliminary D3



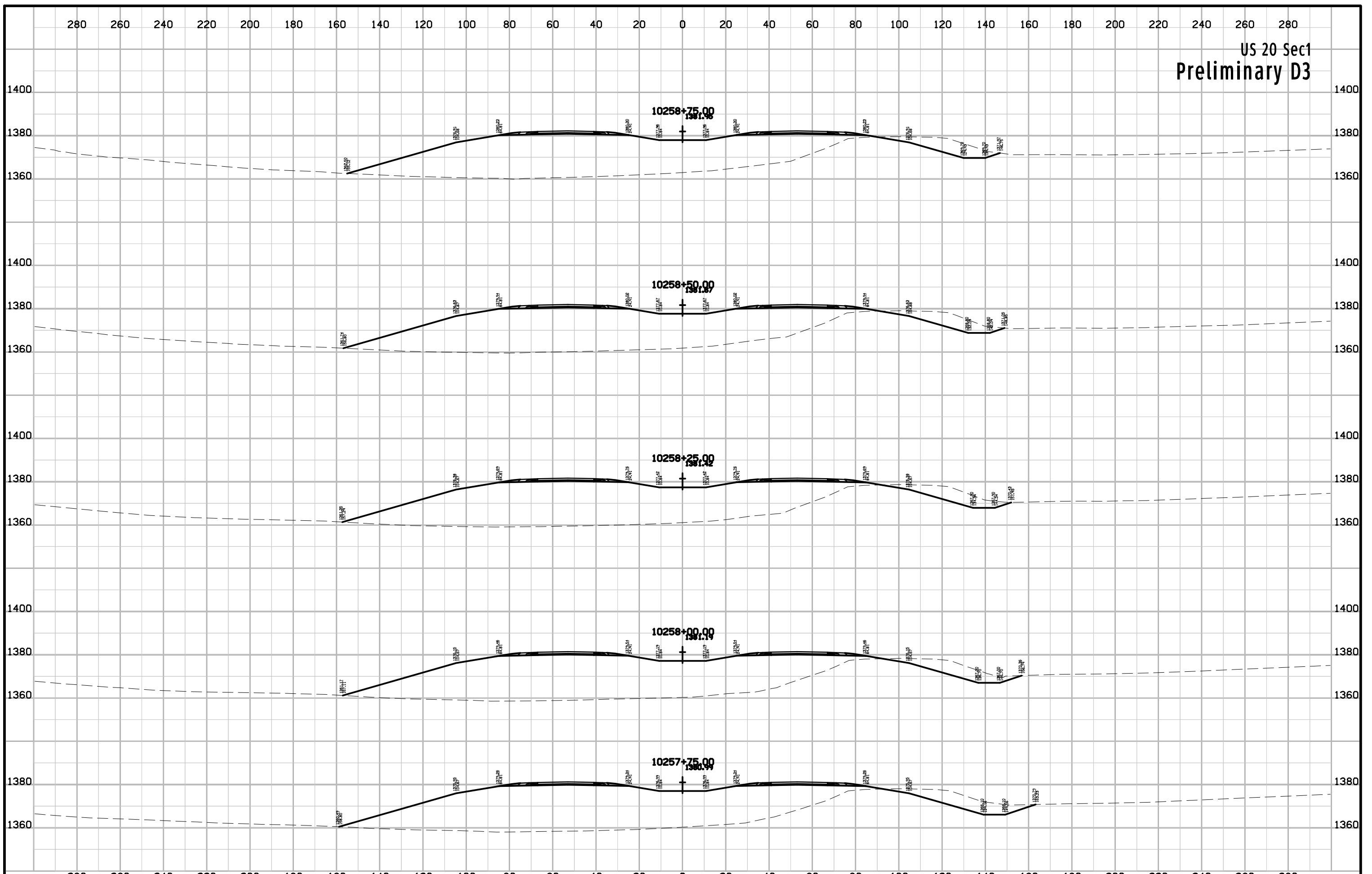
US 20 Sec1
Preliminary D3



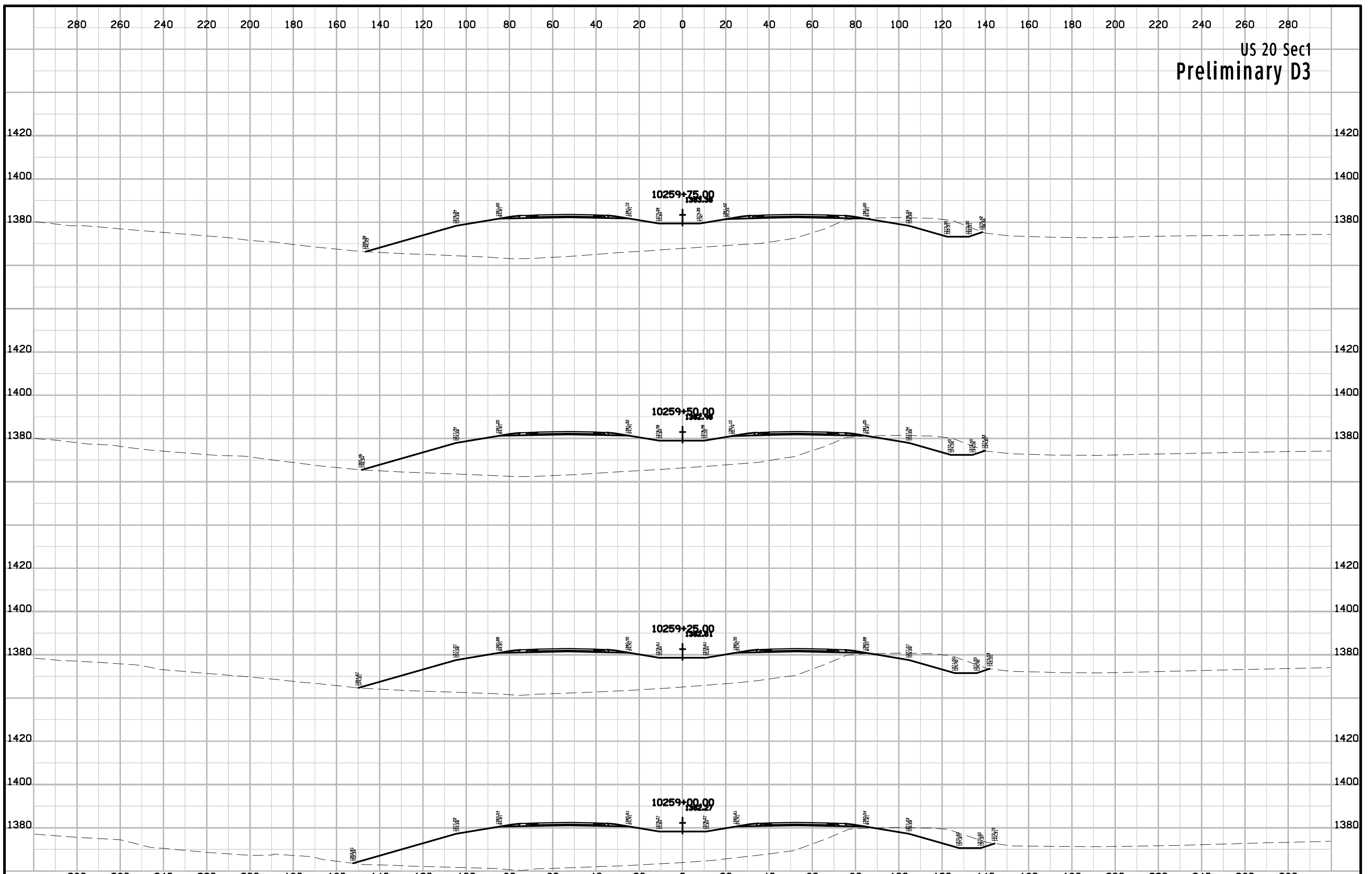
US 20 Sec1
Preliminary D3



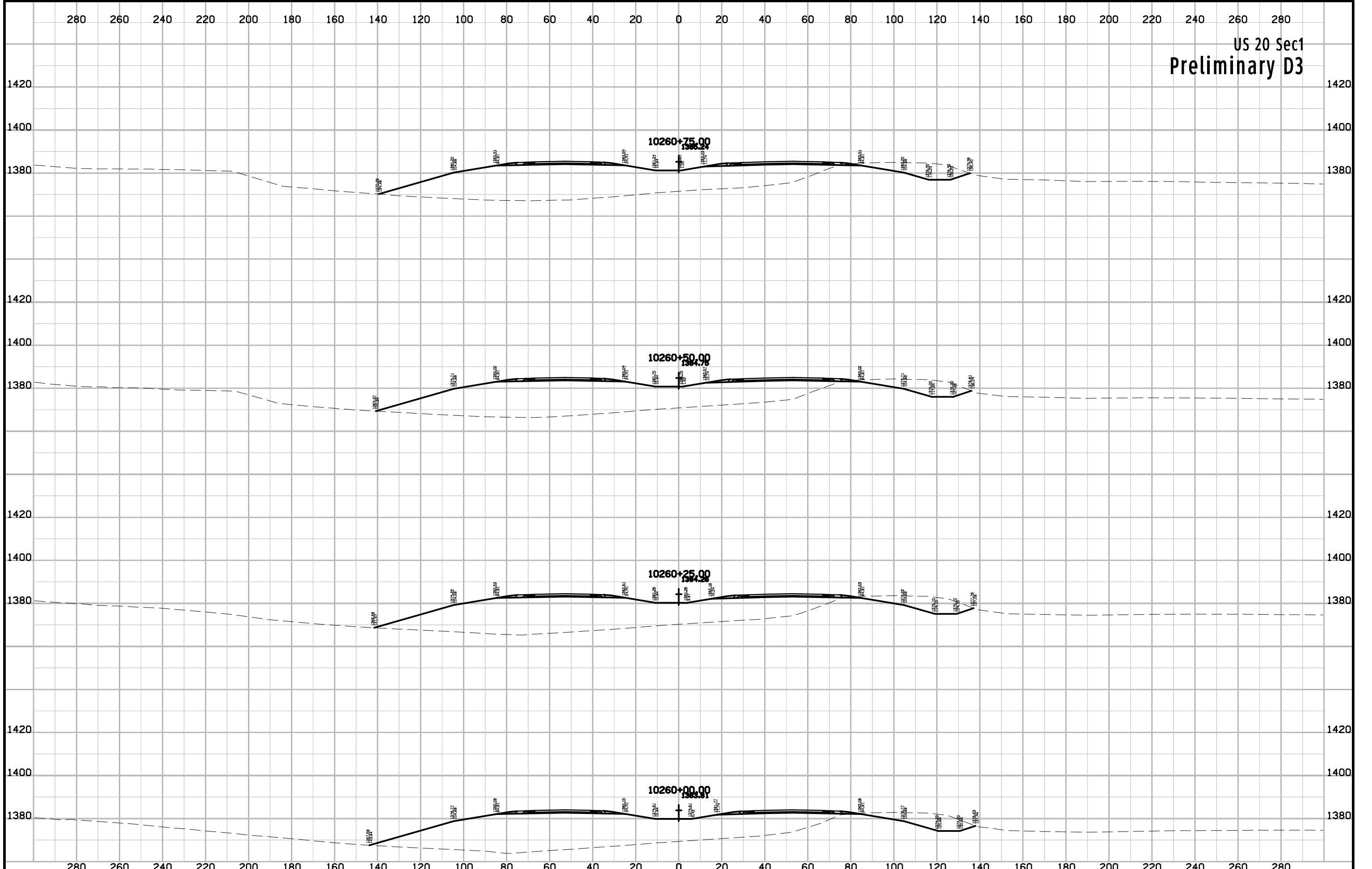
US 20 Sec1
Preliminary D3



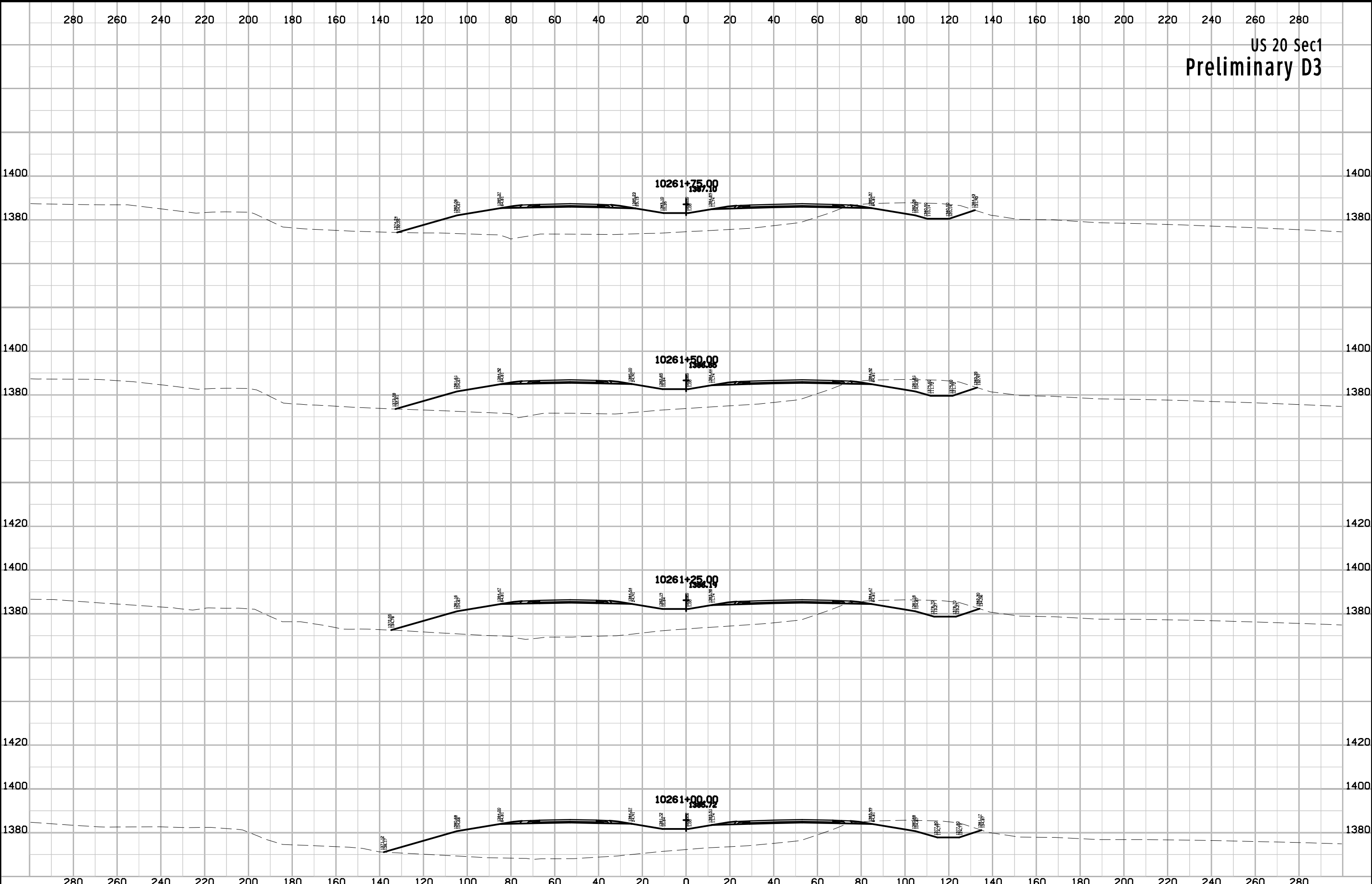
US 20 Sec1
Preliminary D3



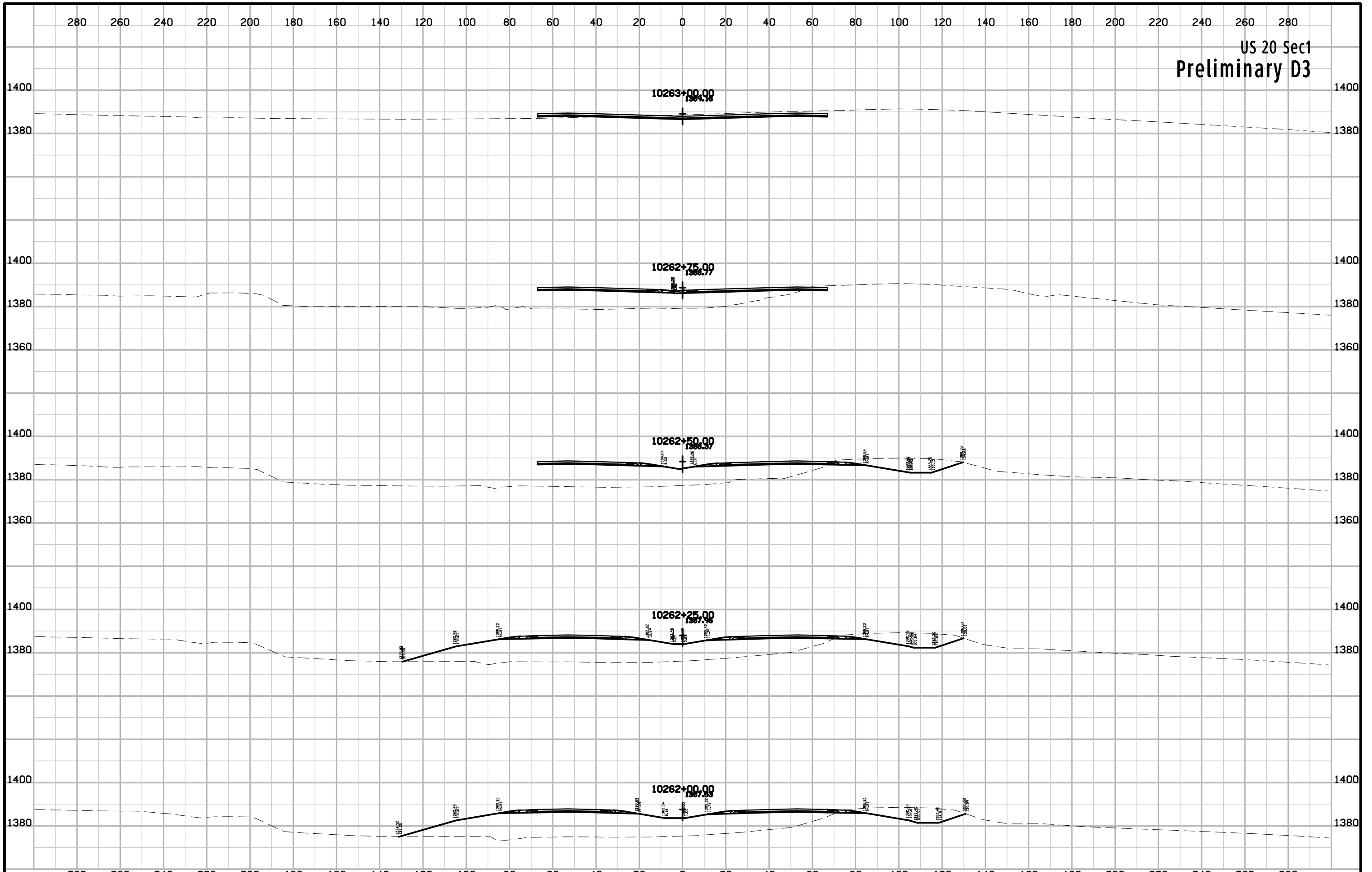
US 20 Sec1
Preliminary D3

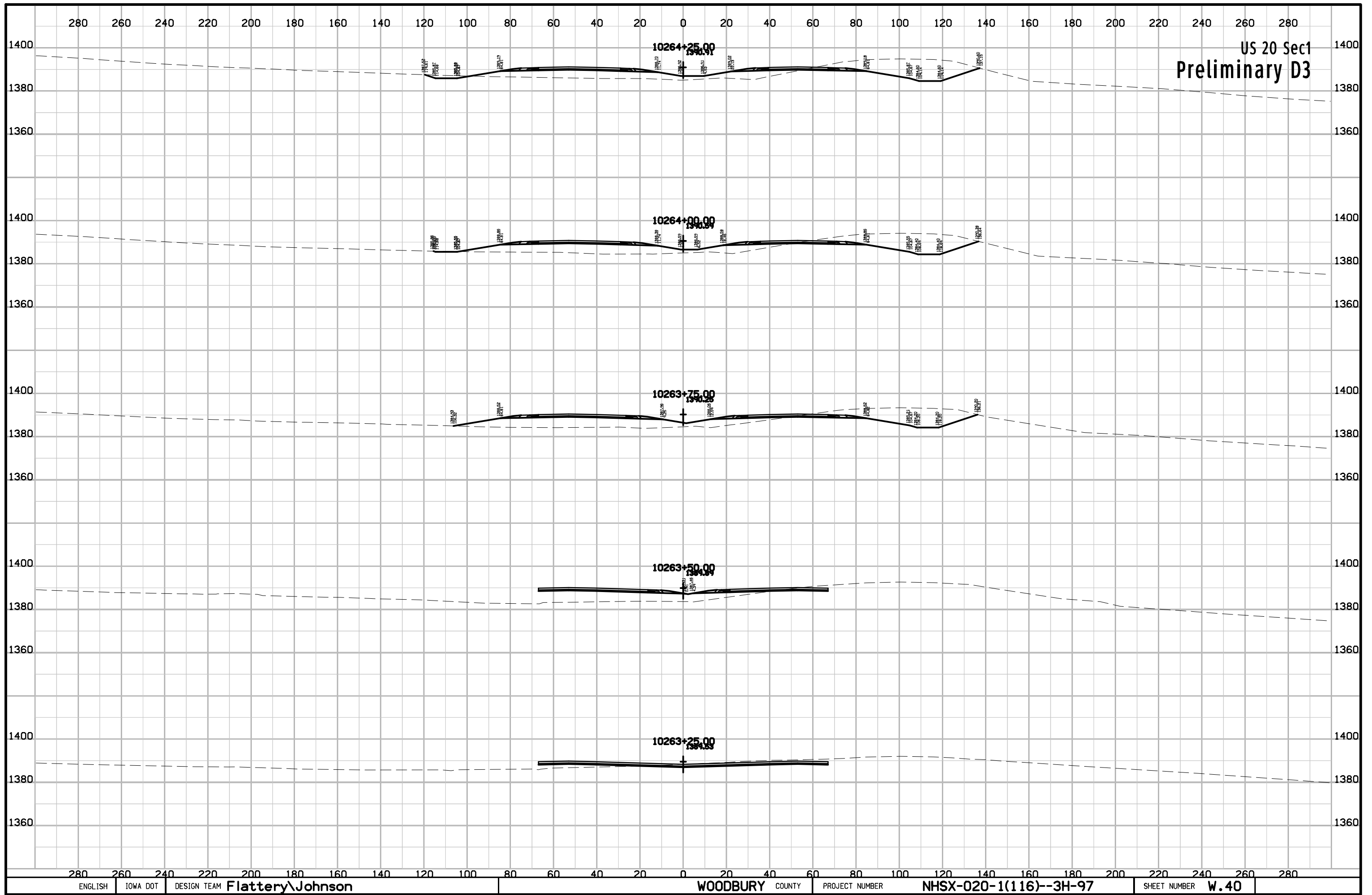


US 20 Sec1
Preliminary D3

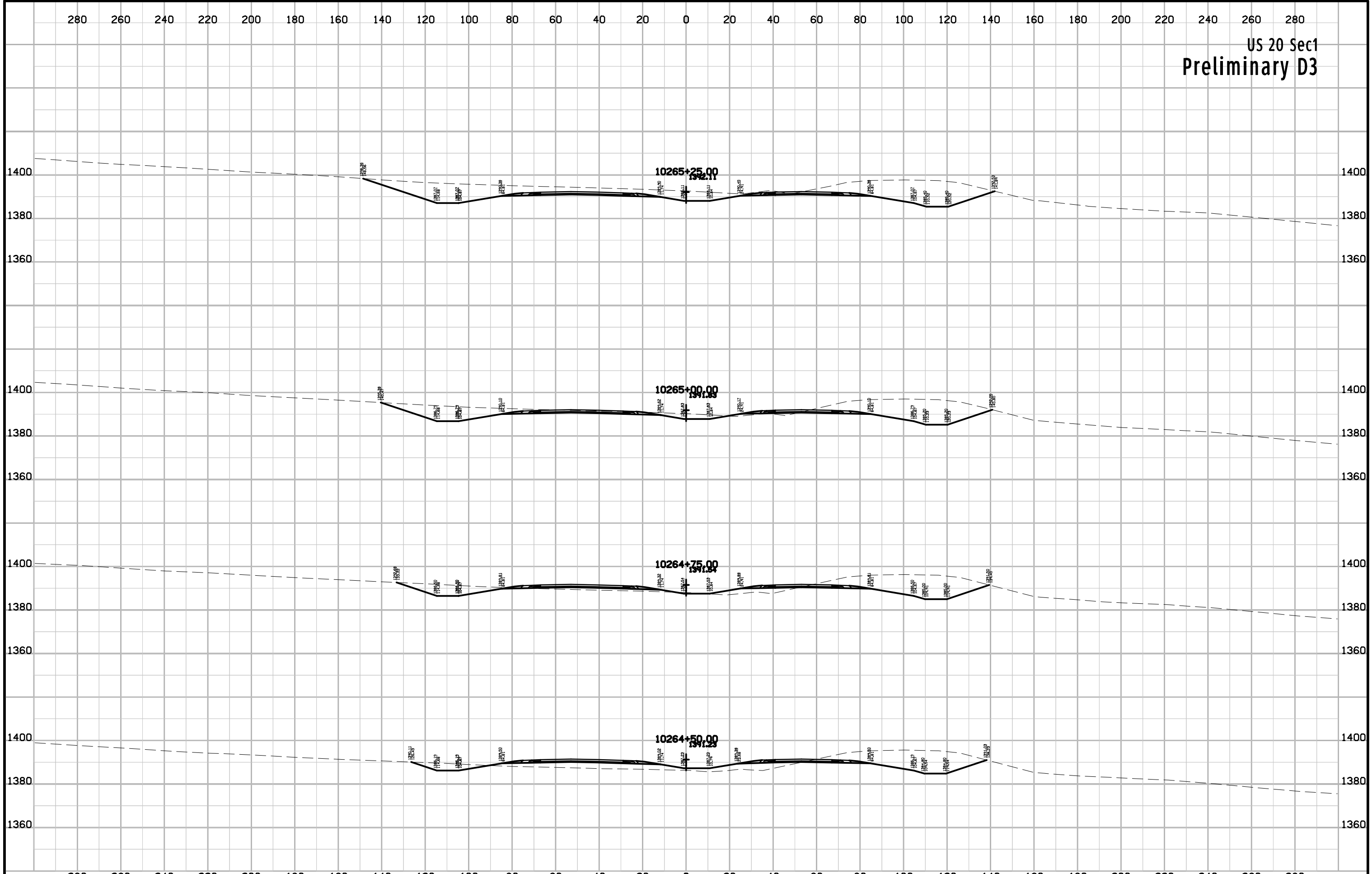


US 20 Sec1
Preliminary D3

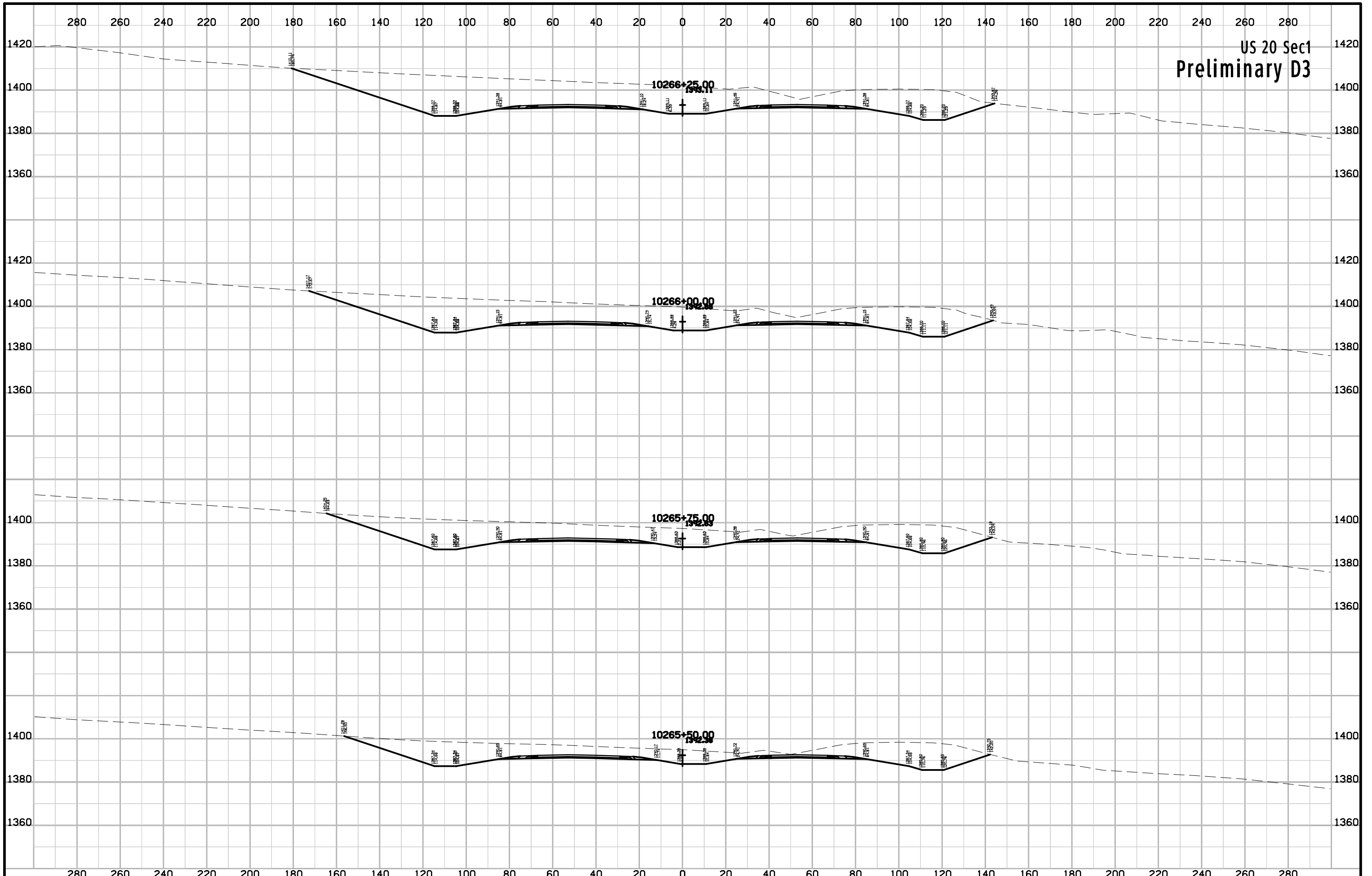




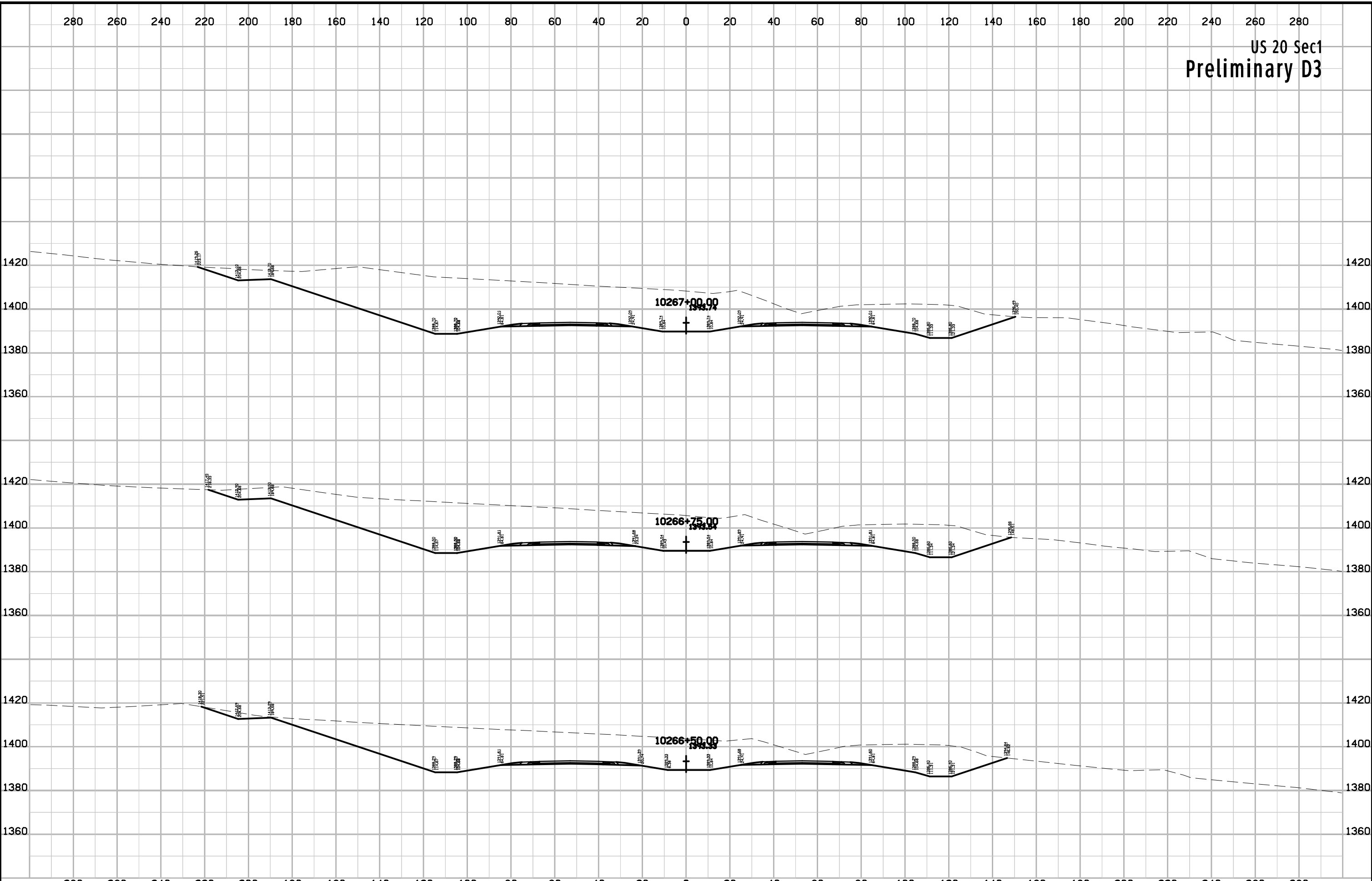
US 20 Sec1
Preliminary D3



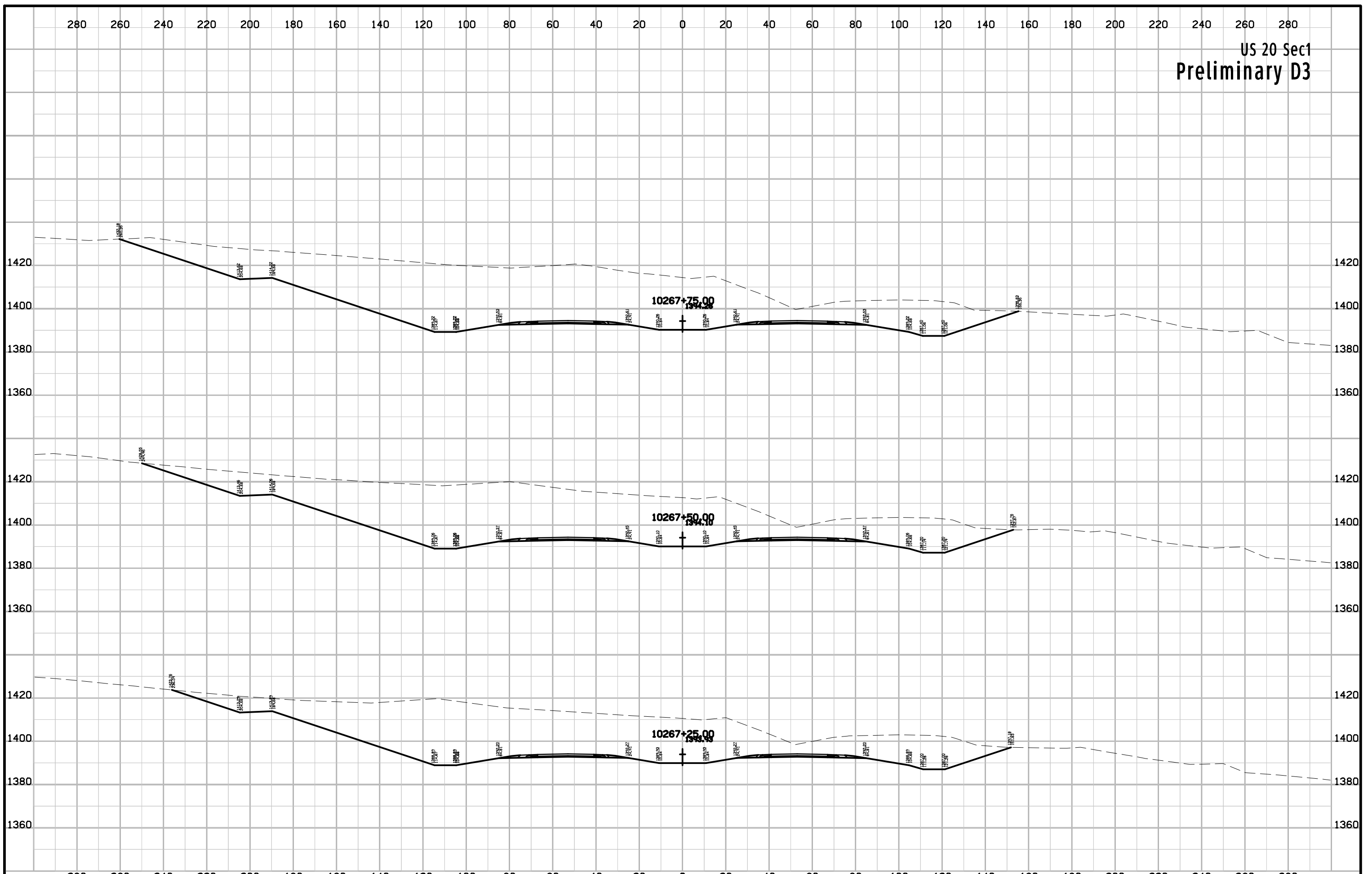
US 20 Sec1
Preliminary D3



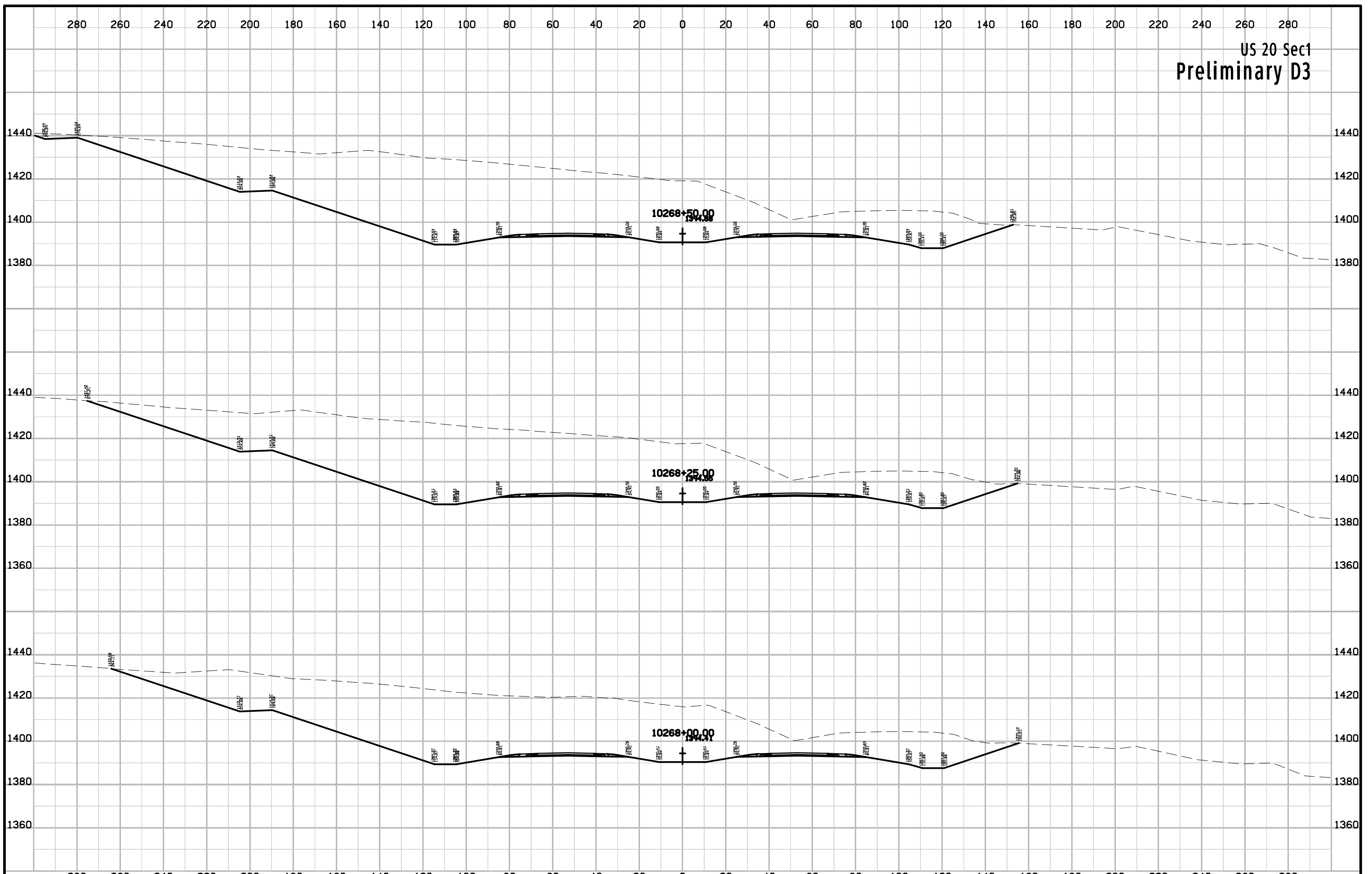
US 20 Sec1
Preliminary D3



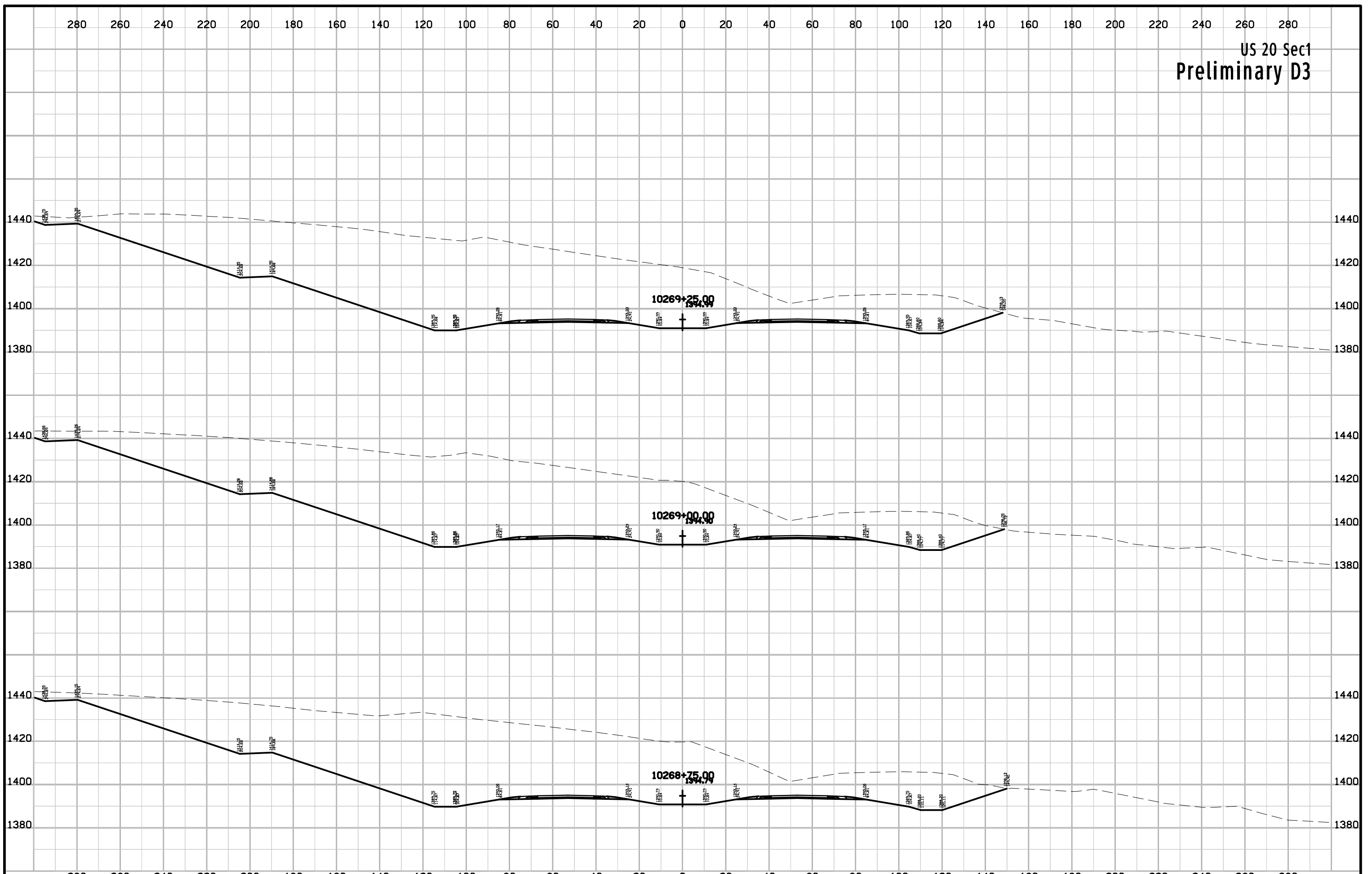
US 20 Sec1
Preliminary D3



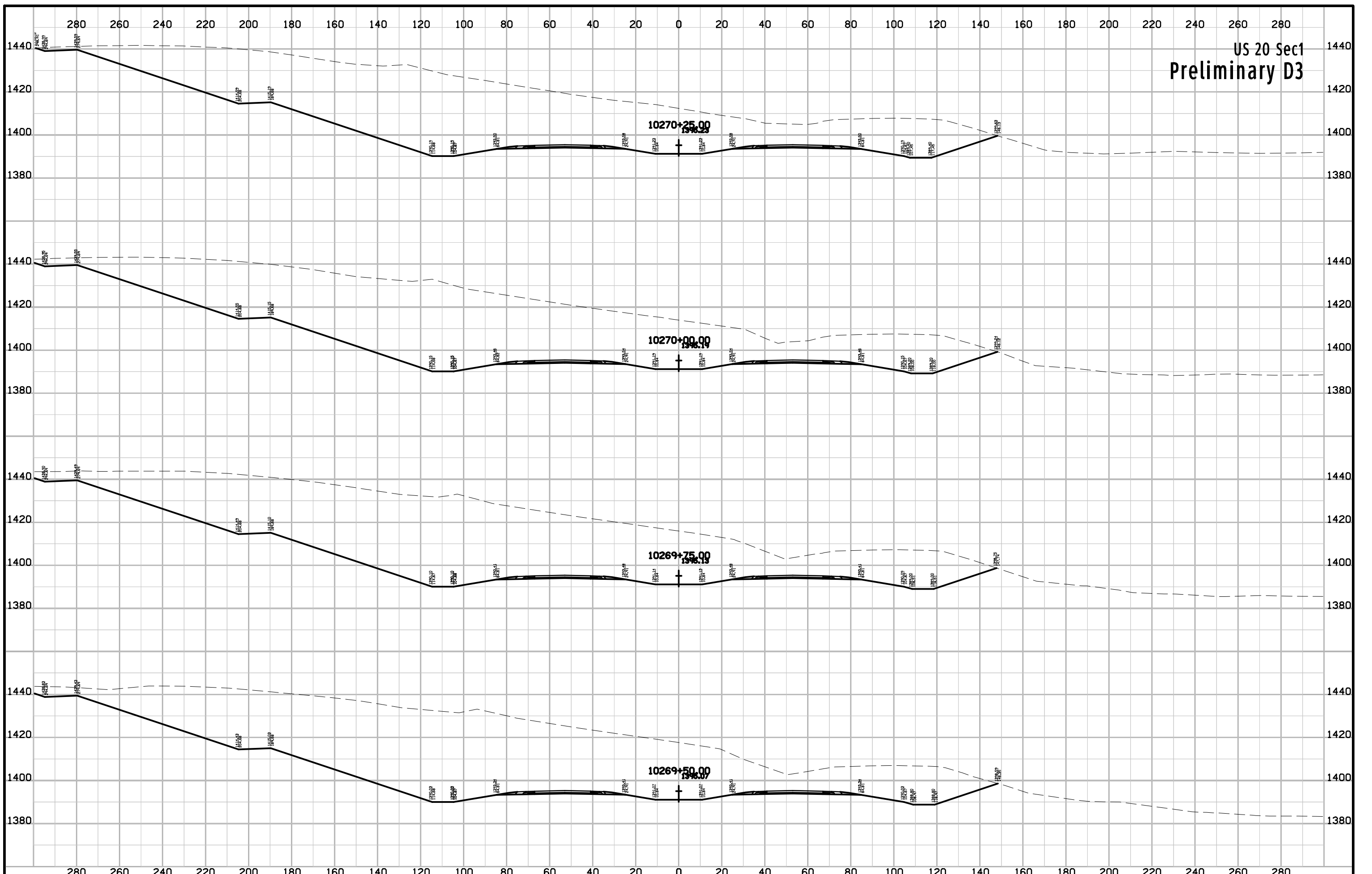
US 20 Sec1
Preliminary D3



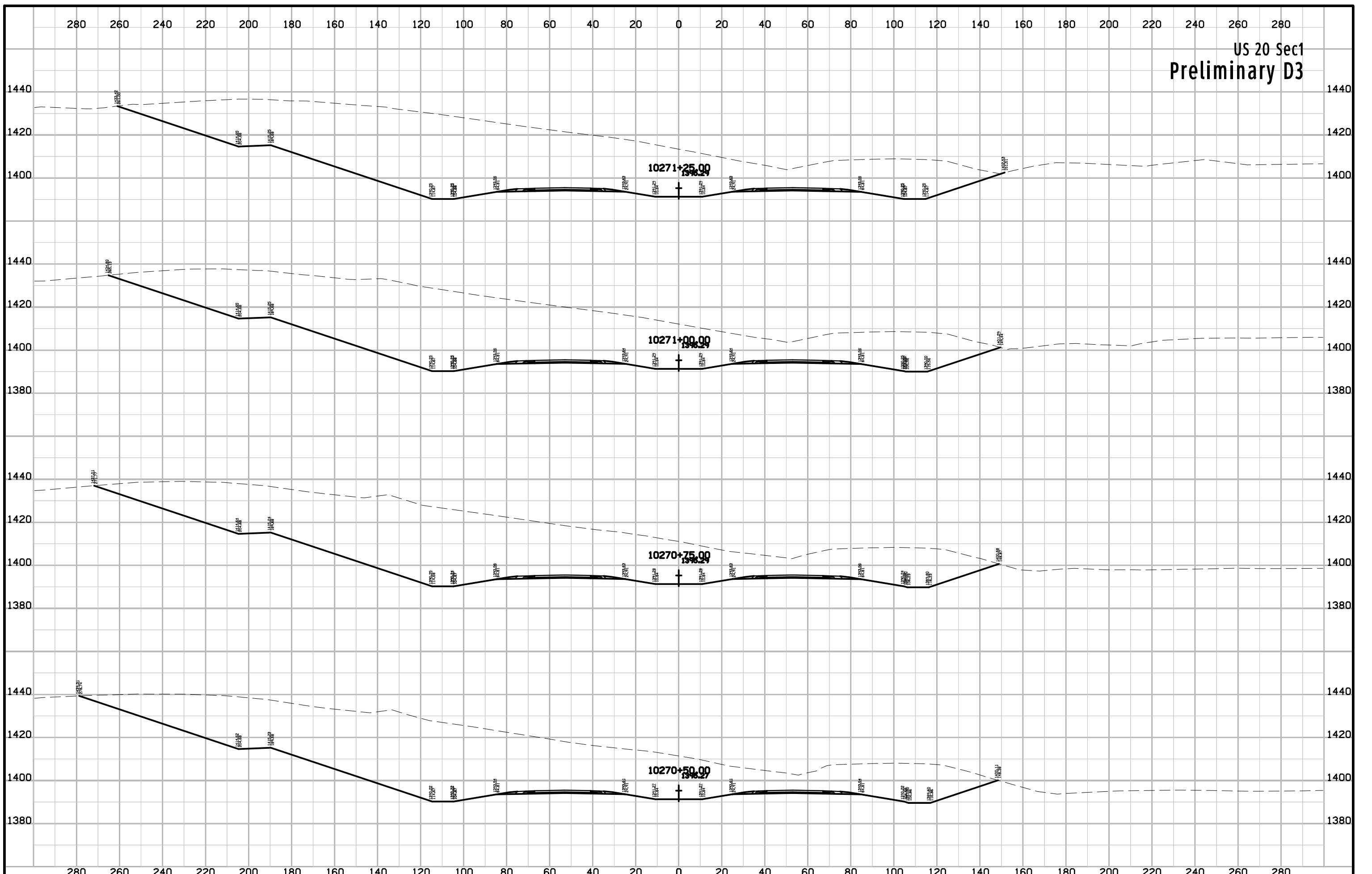
US 20 Sec1
Preliminary D3



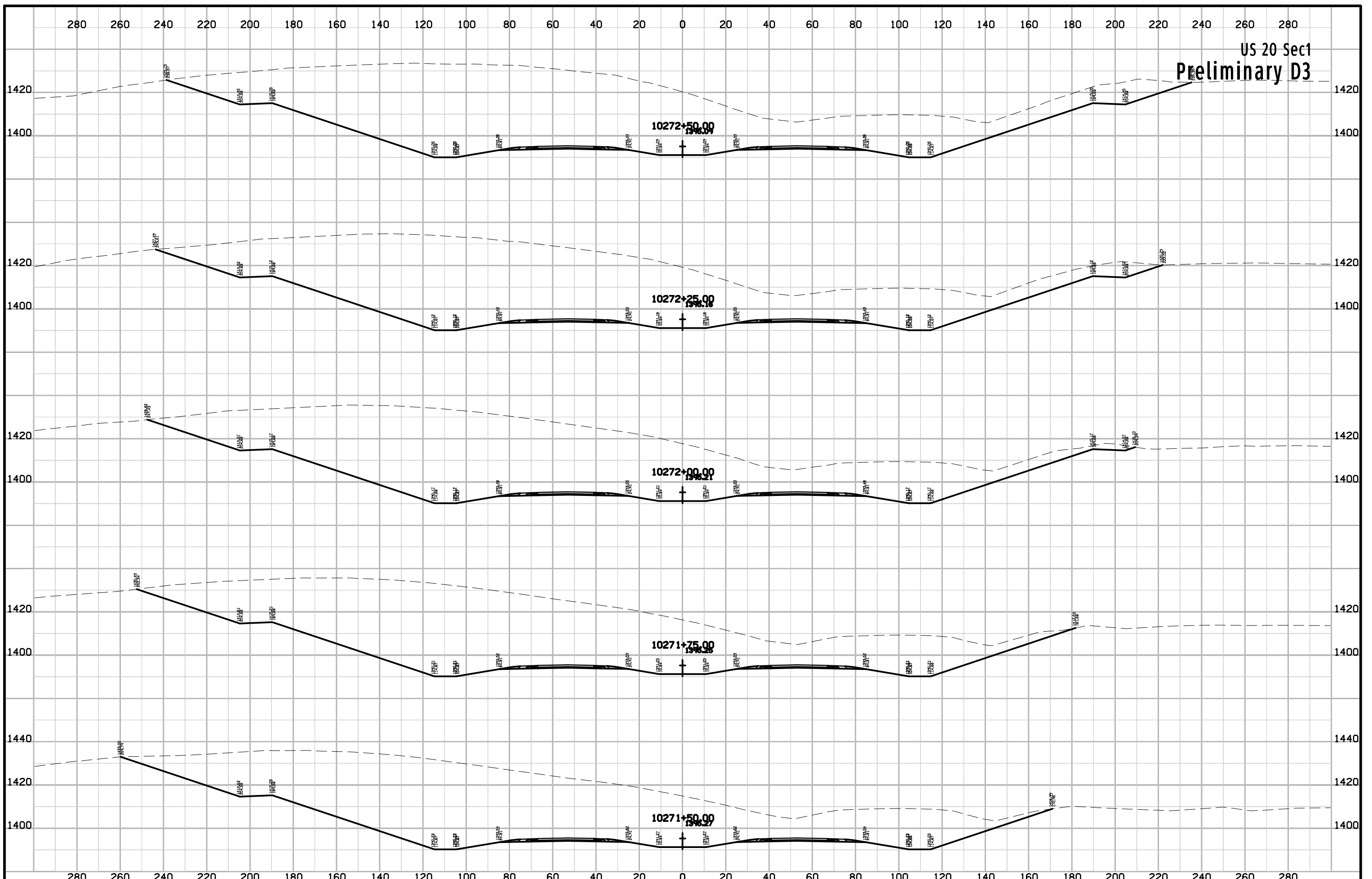
US 20 Sec1
Preliminary D3



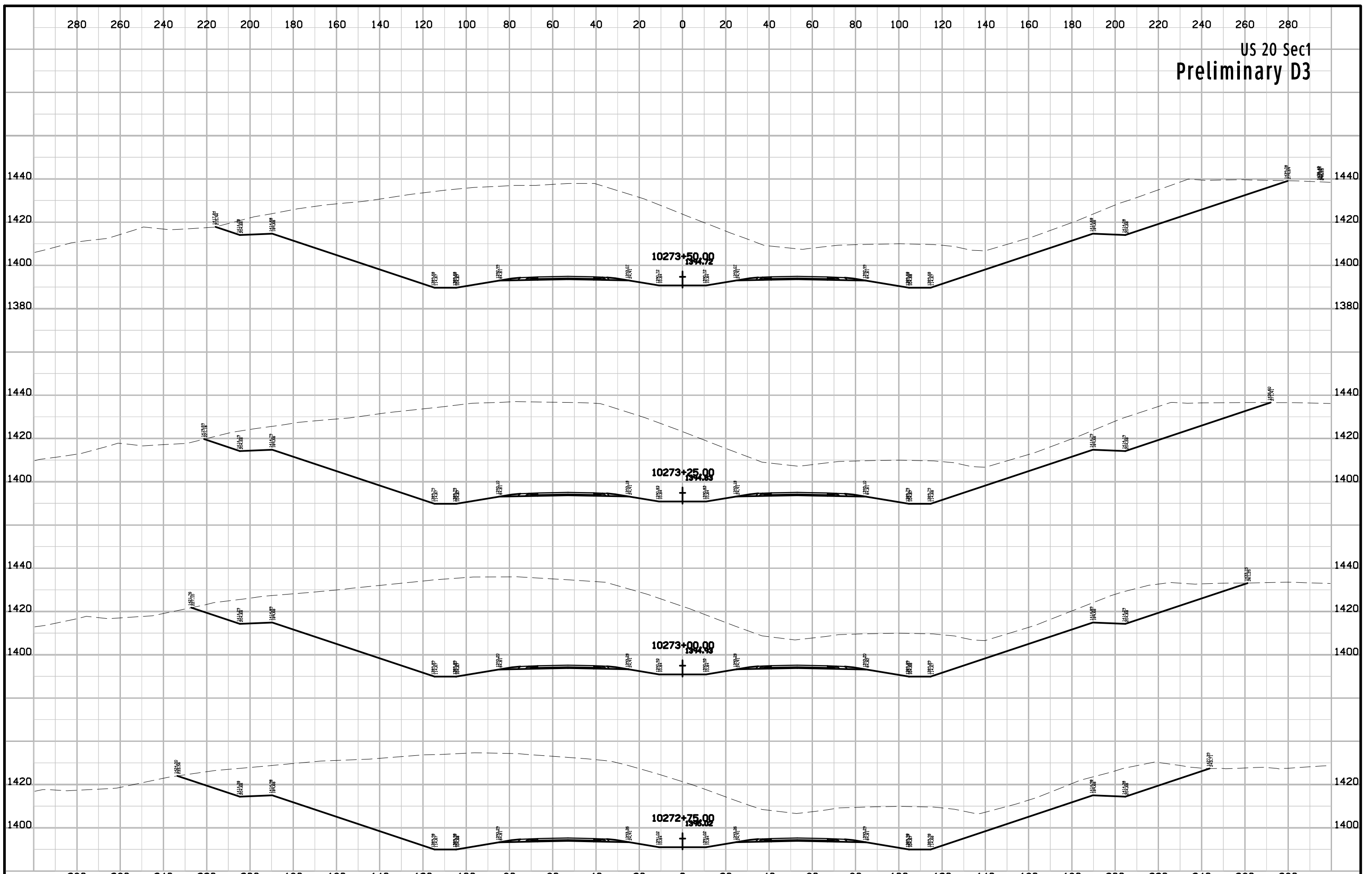
US 20 Sec1
Preliminary D3

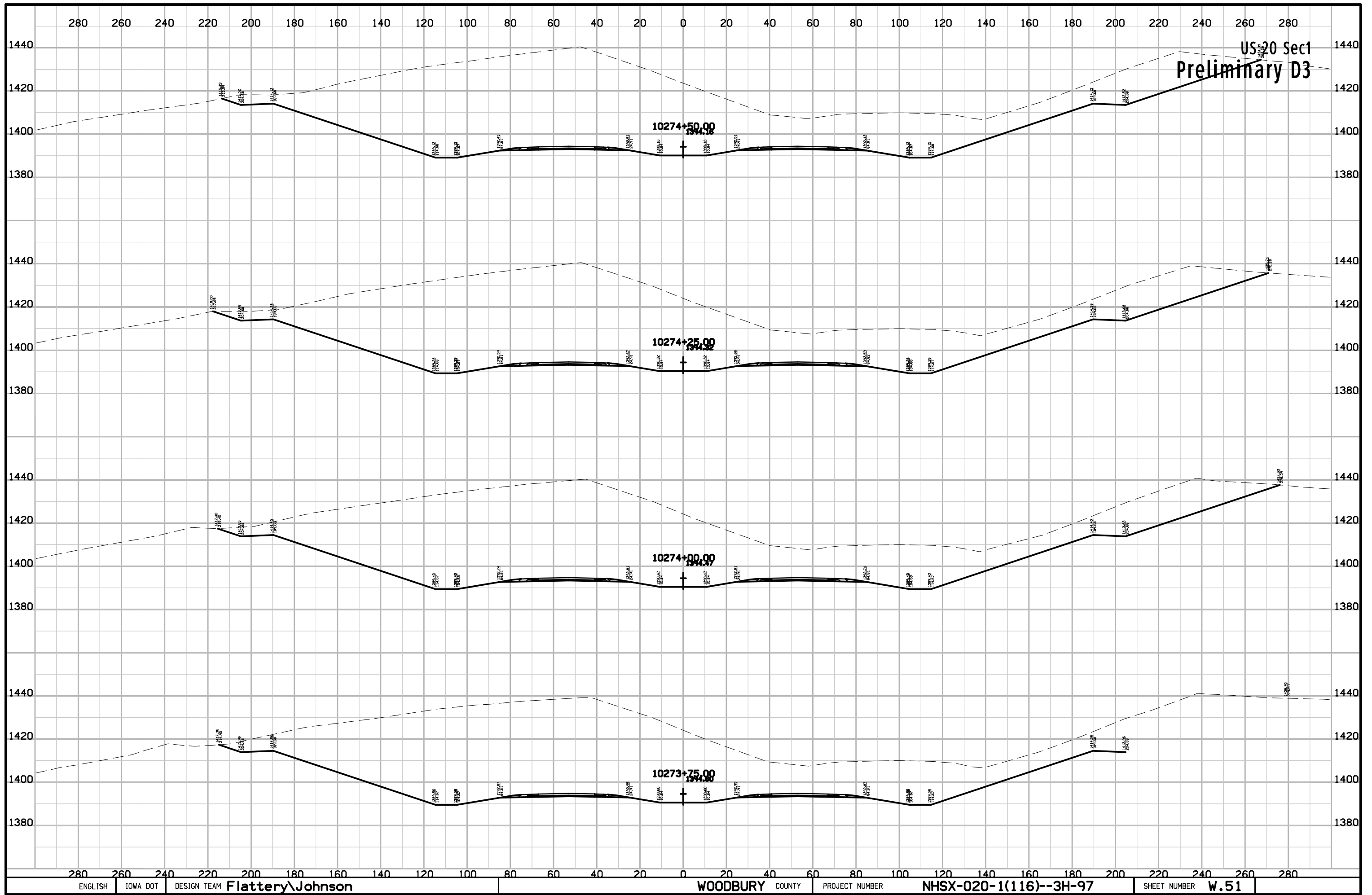


US 20 Sec1
Preliminary D3



US 20 Sec1
Preliminary D3

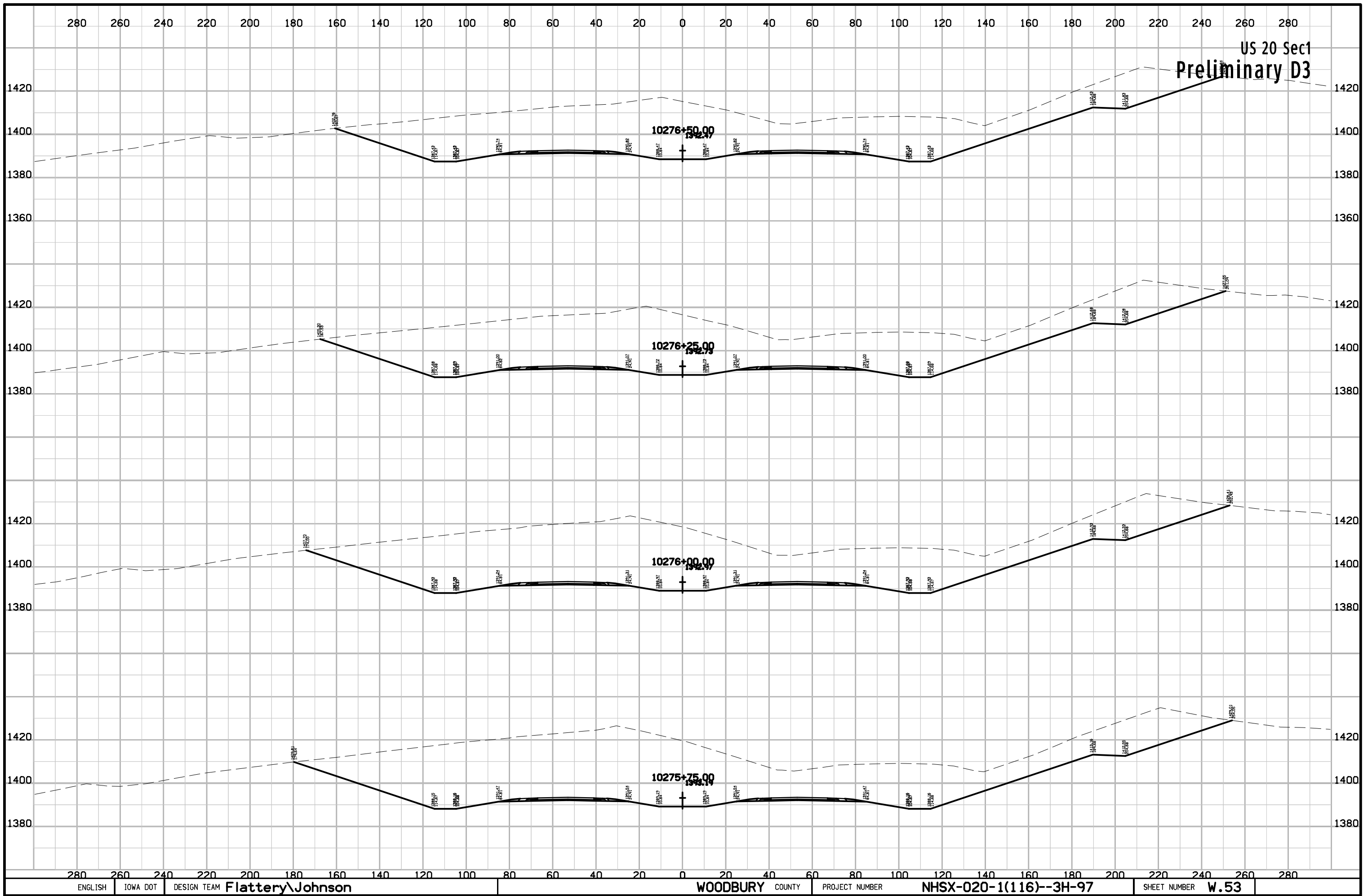




US 20 Sec 1
Preliminary D3

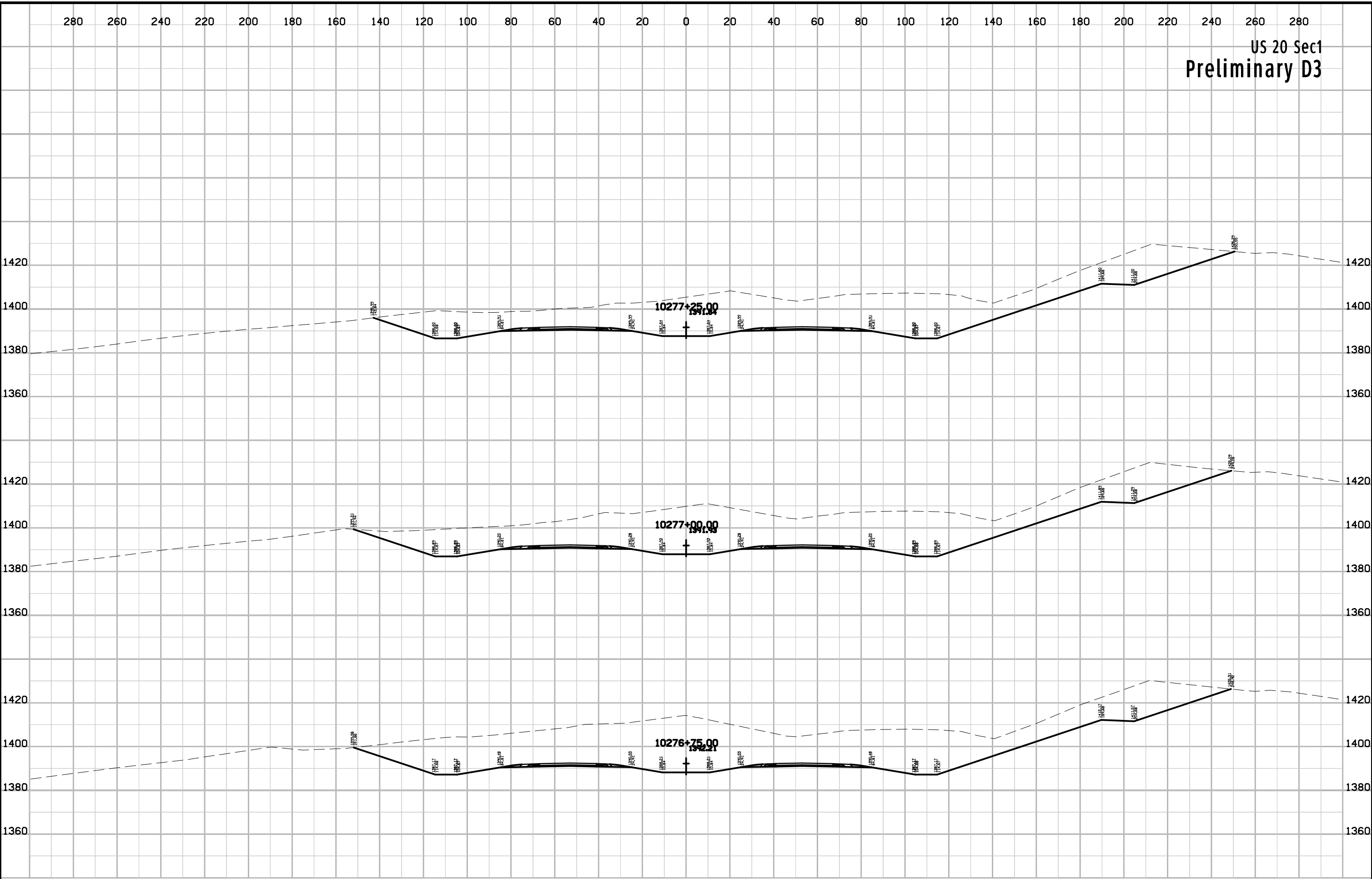


US 20 Sec1
Preliminary D3

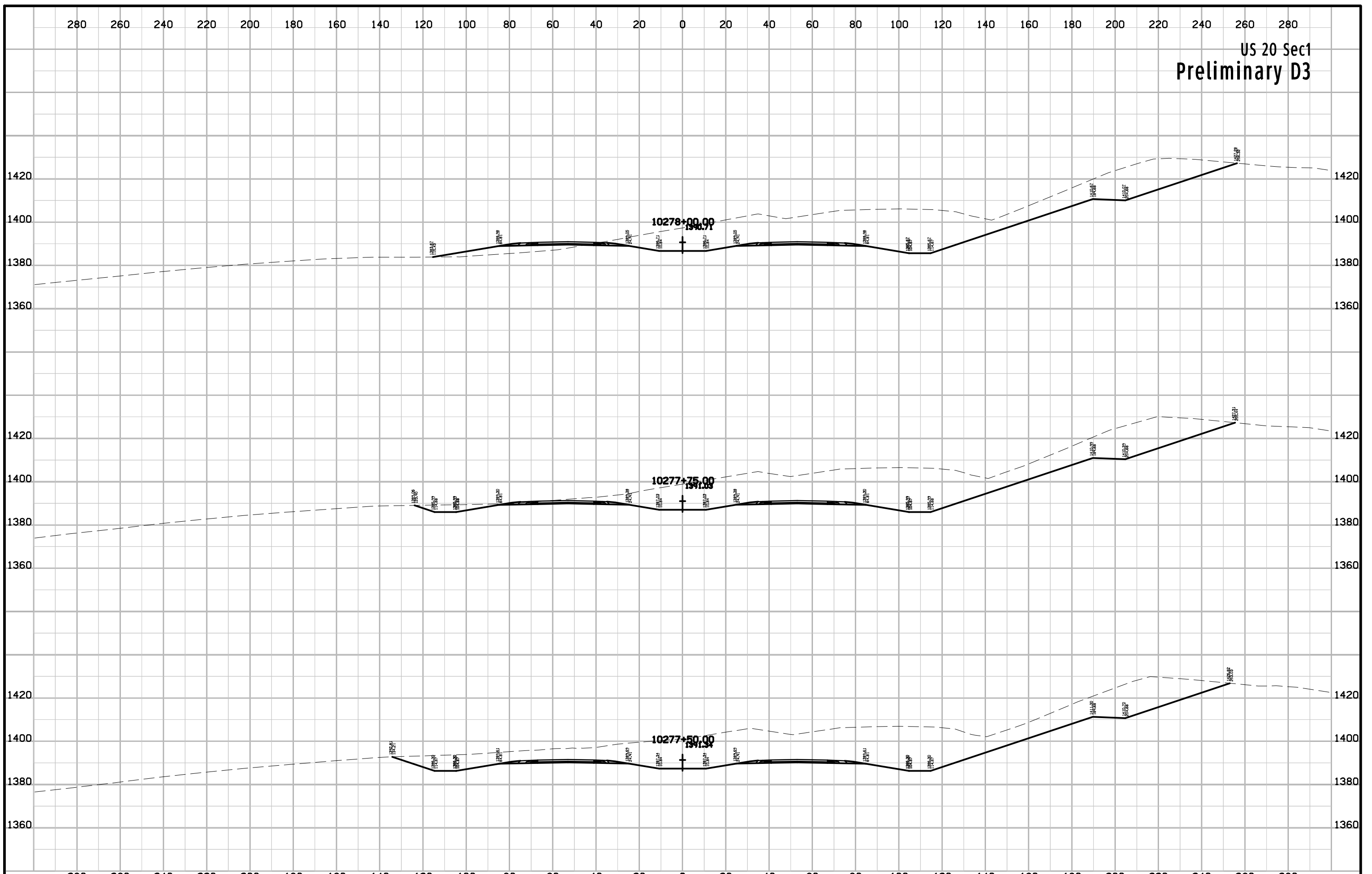


US 20 Sec1
Preliminary D3

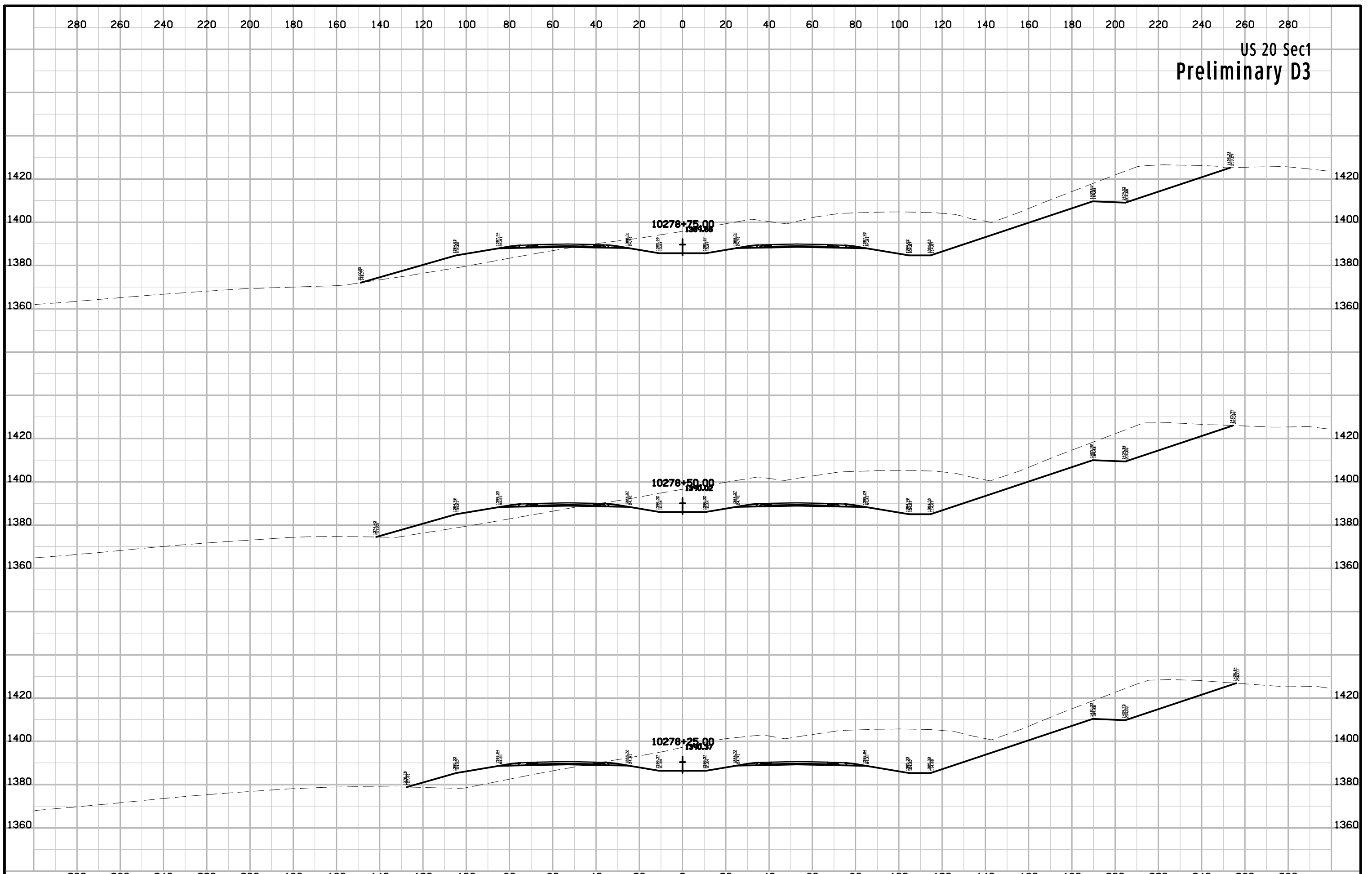
US 20 Sec1
Preliminary D3



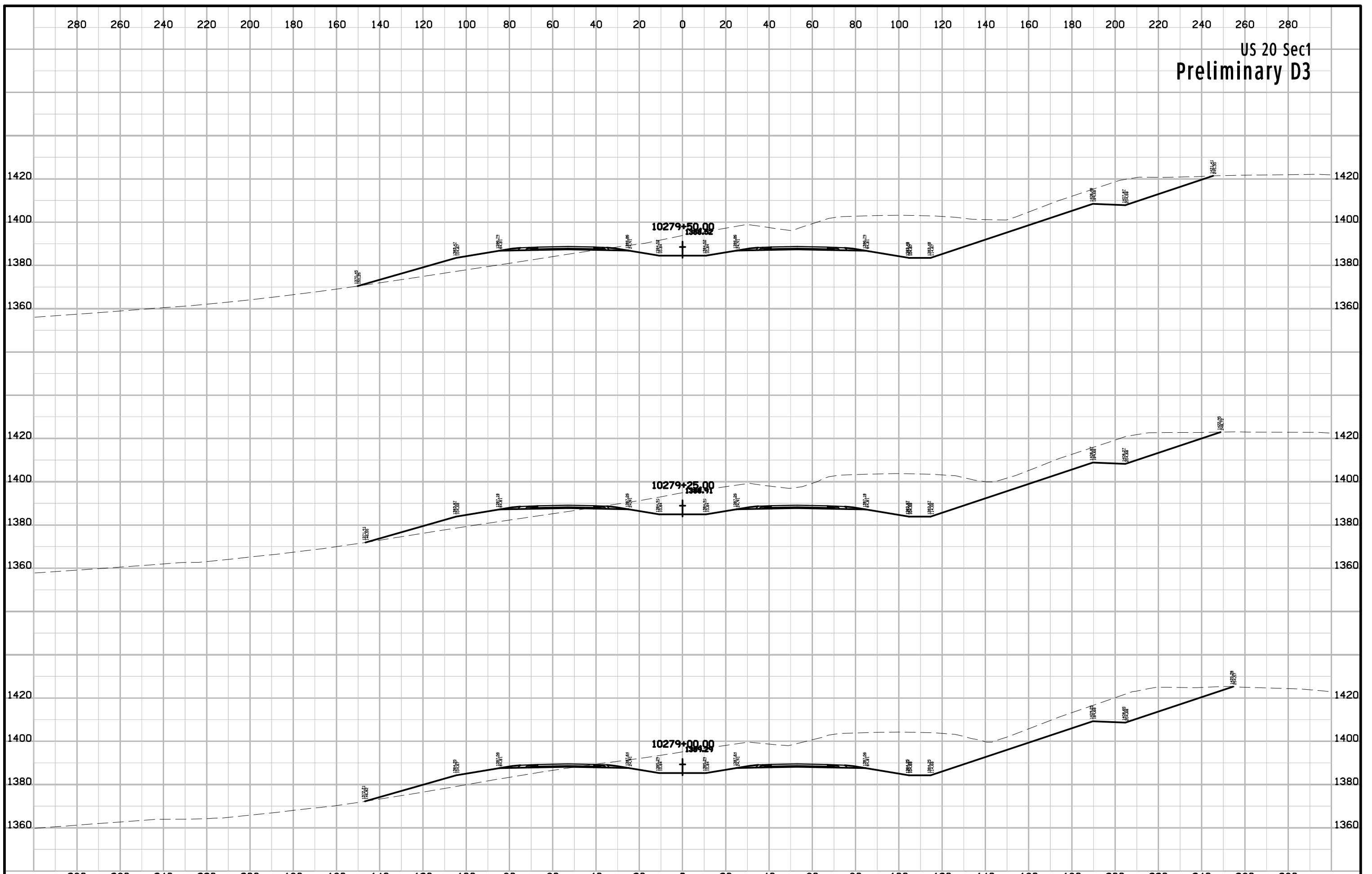
US 20 Sec1
Preliminary D3



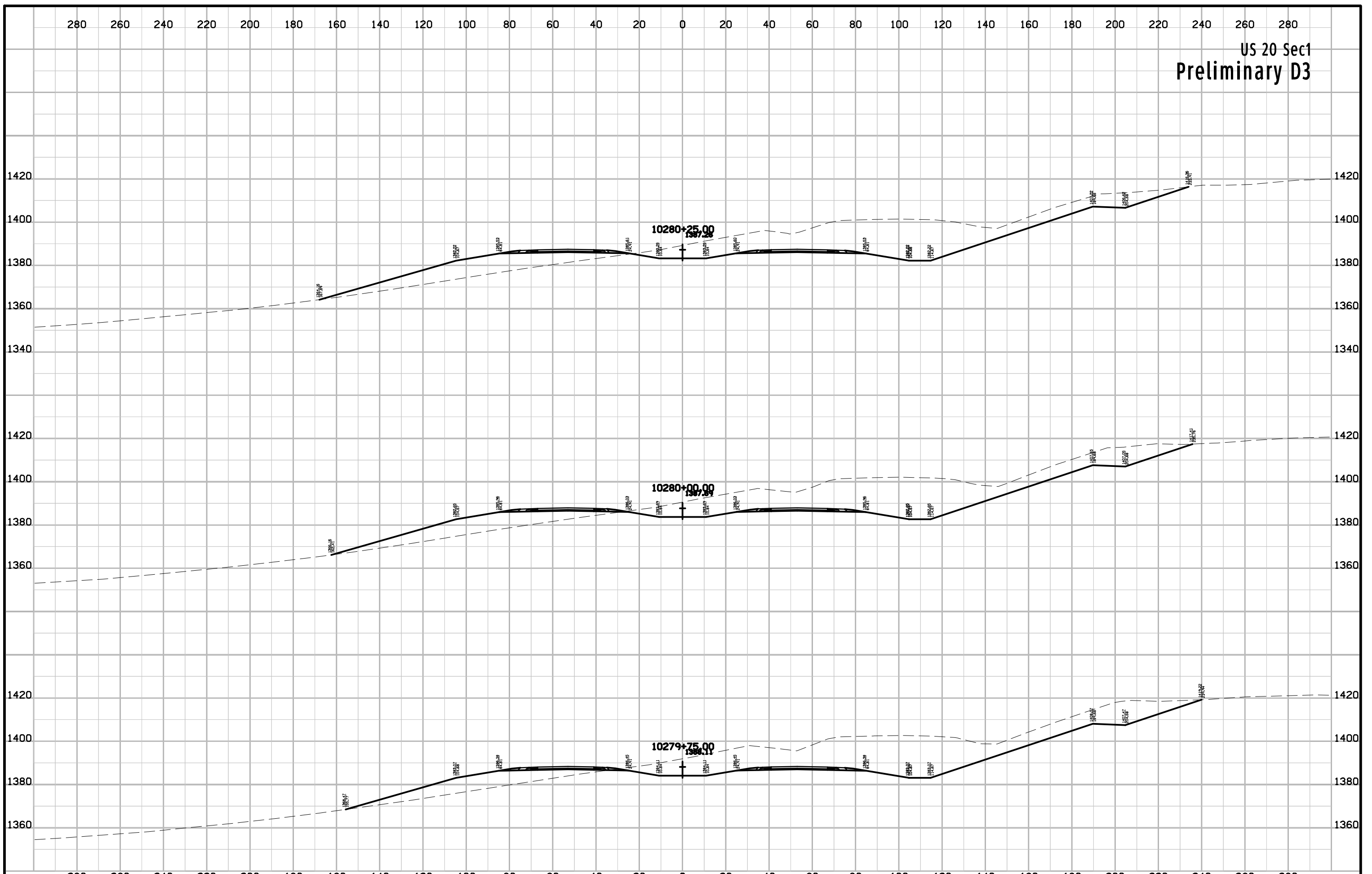
US 20 Sec1
Preliminary D3



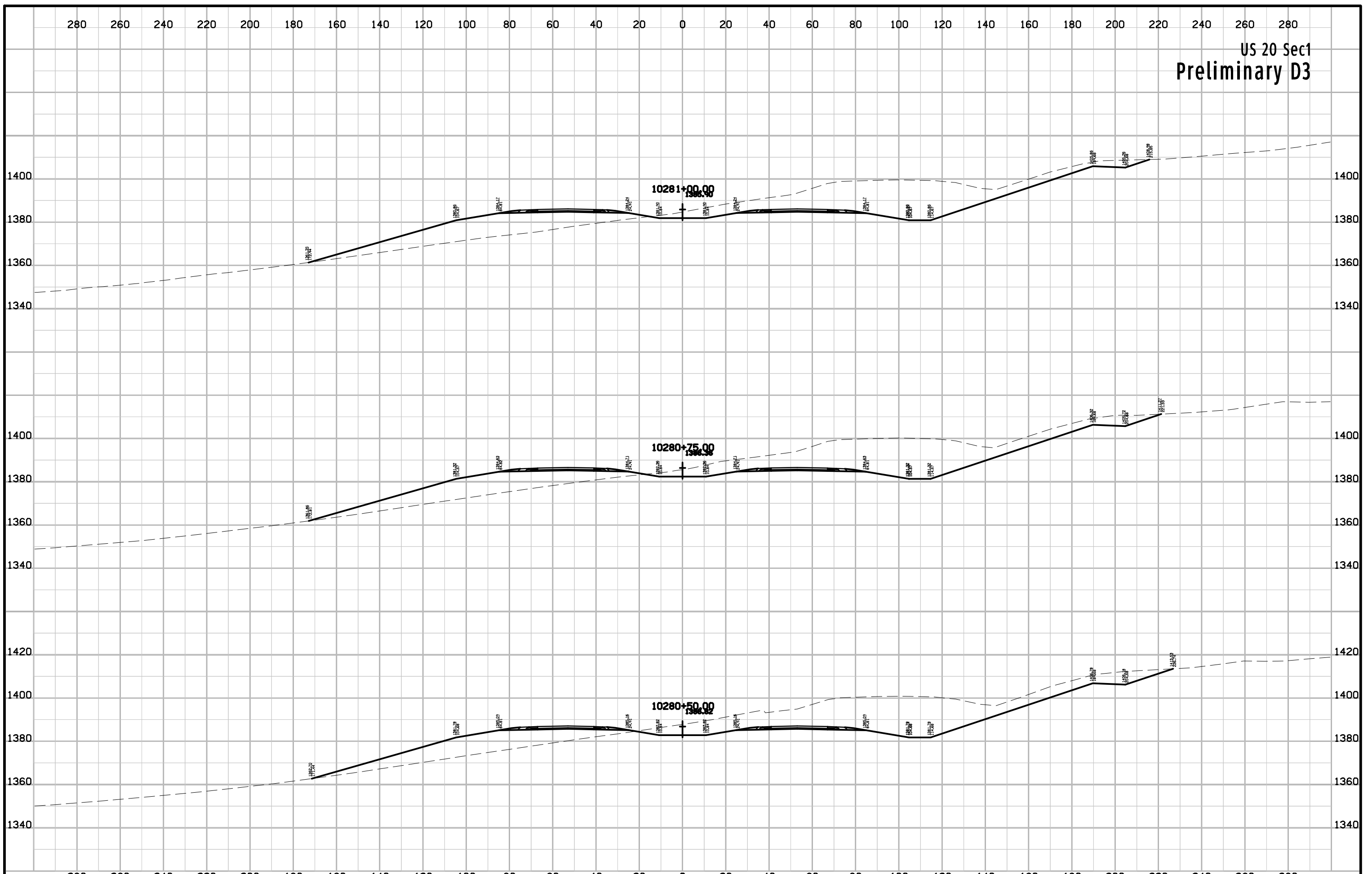
US 20 Sec1
Preliminary D3



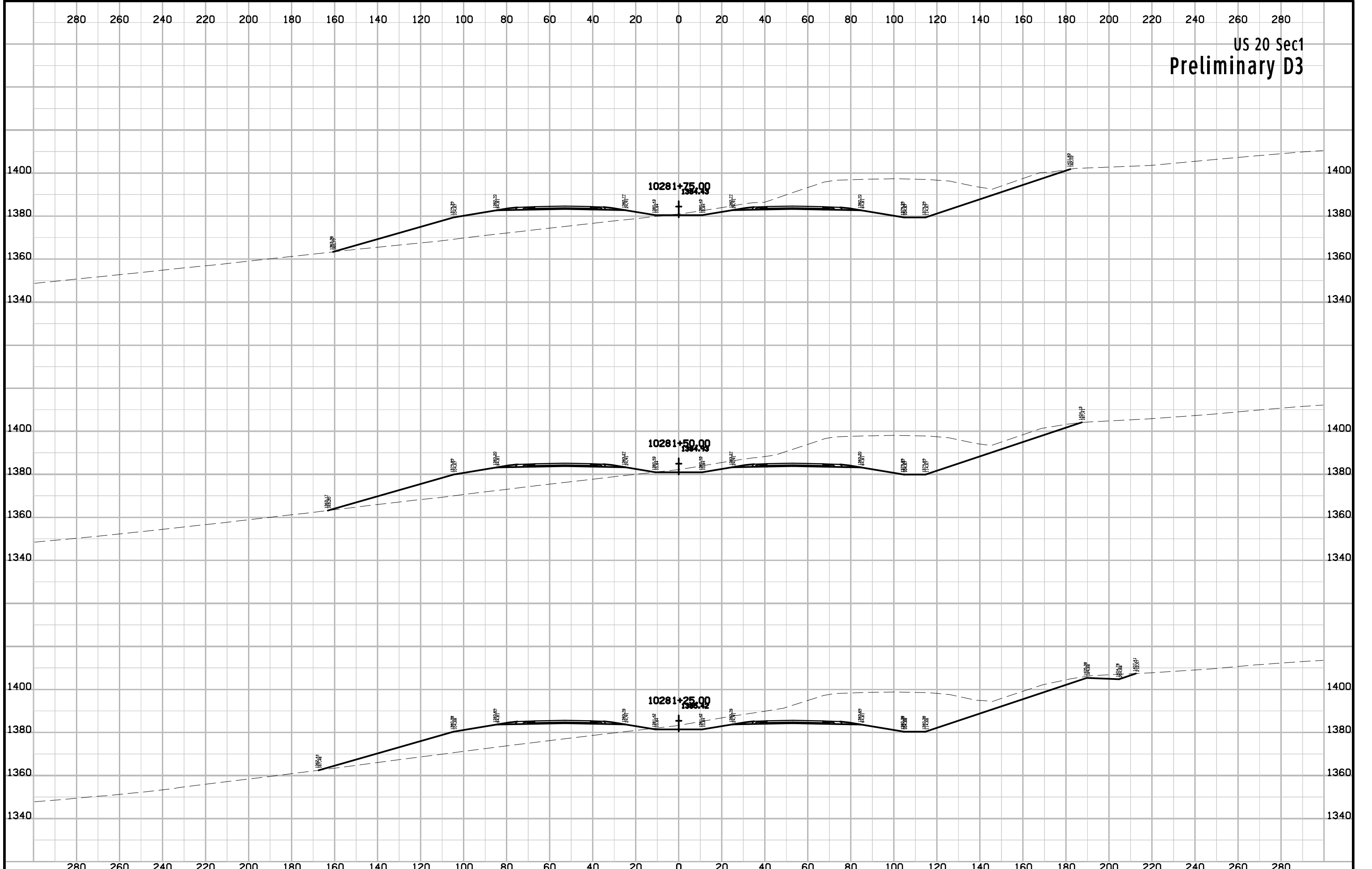
US 20 Sec1
Preliminary D3



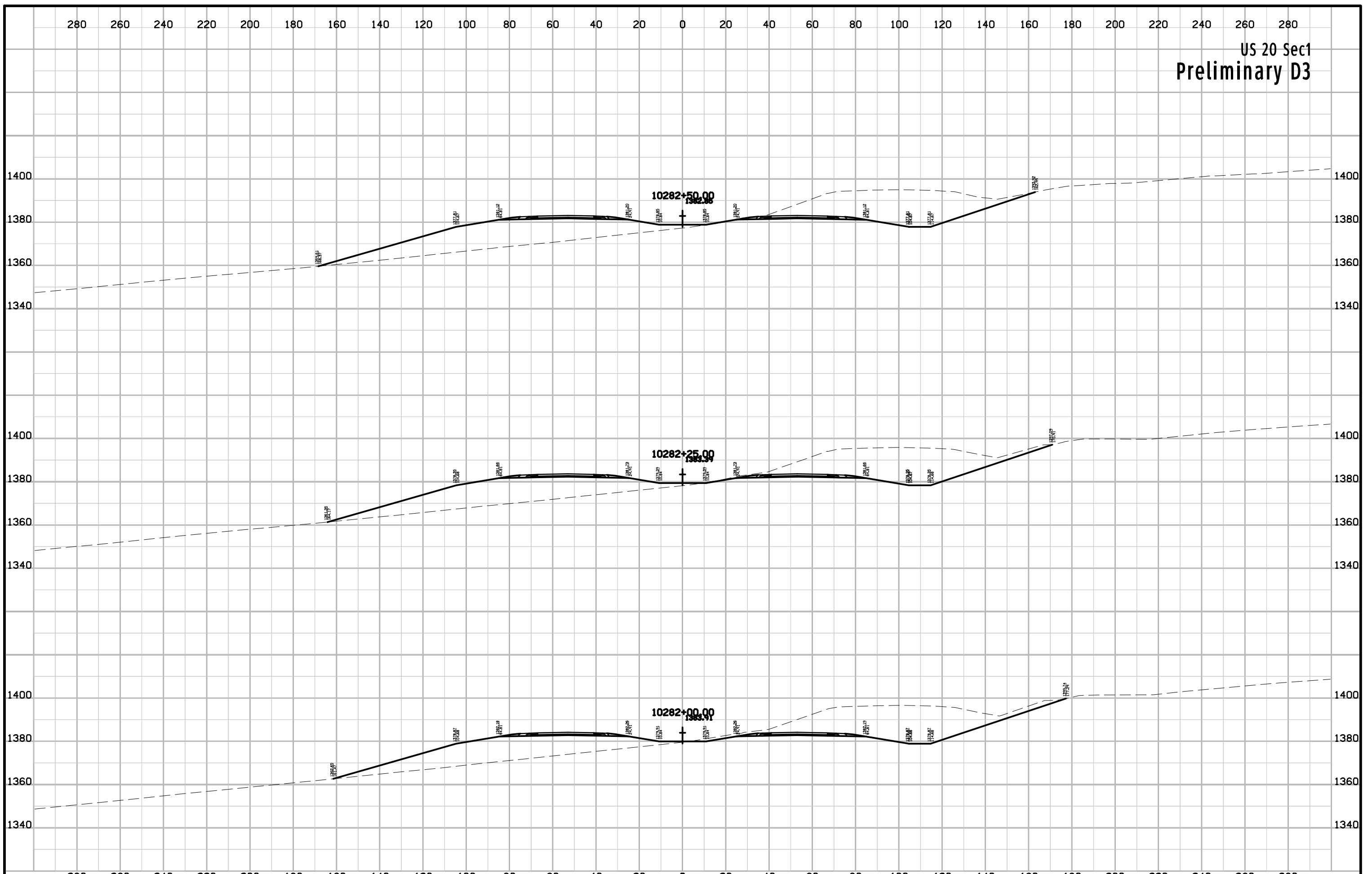
US 20 Sec1
Preliminary D3



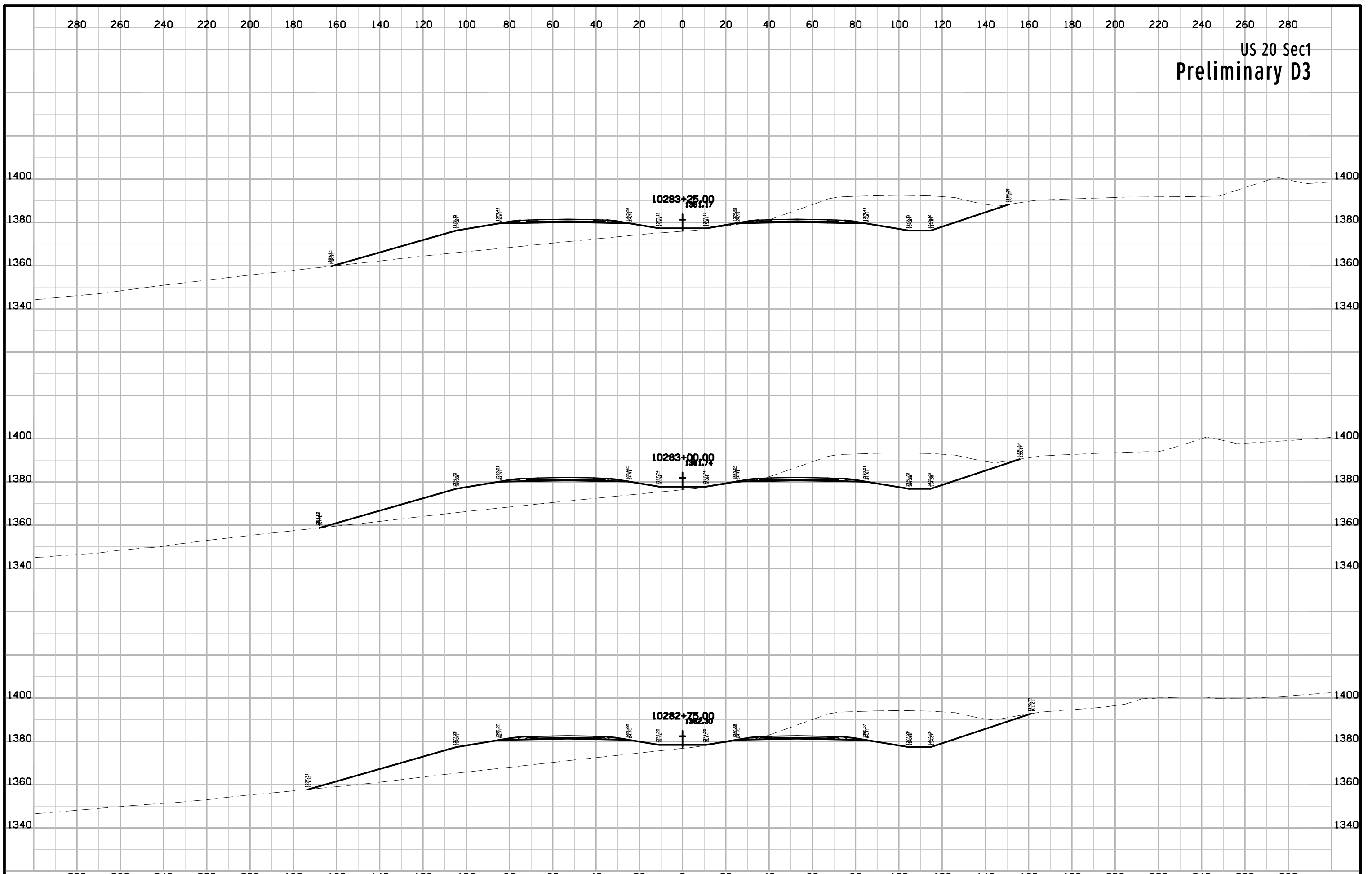
US 20 Sec1
Preliminary D3



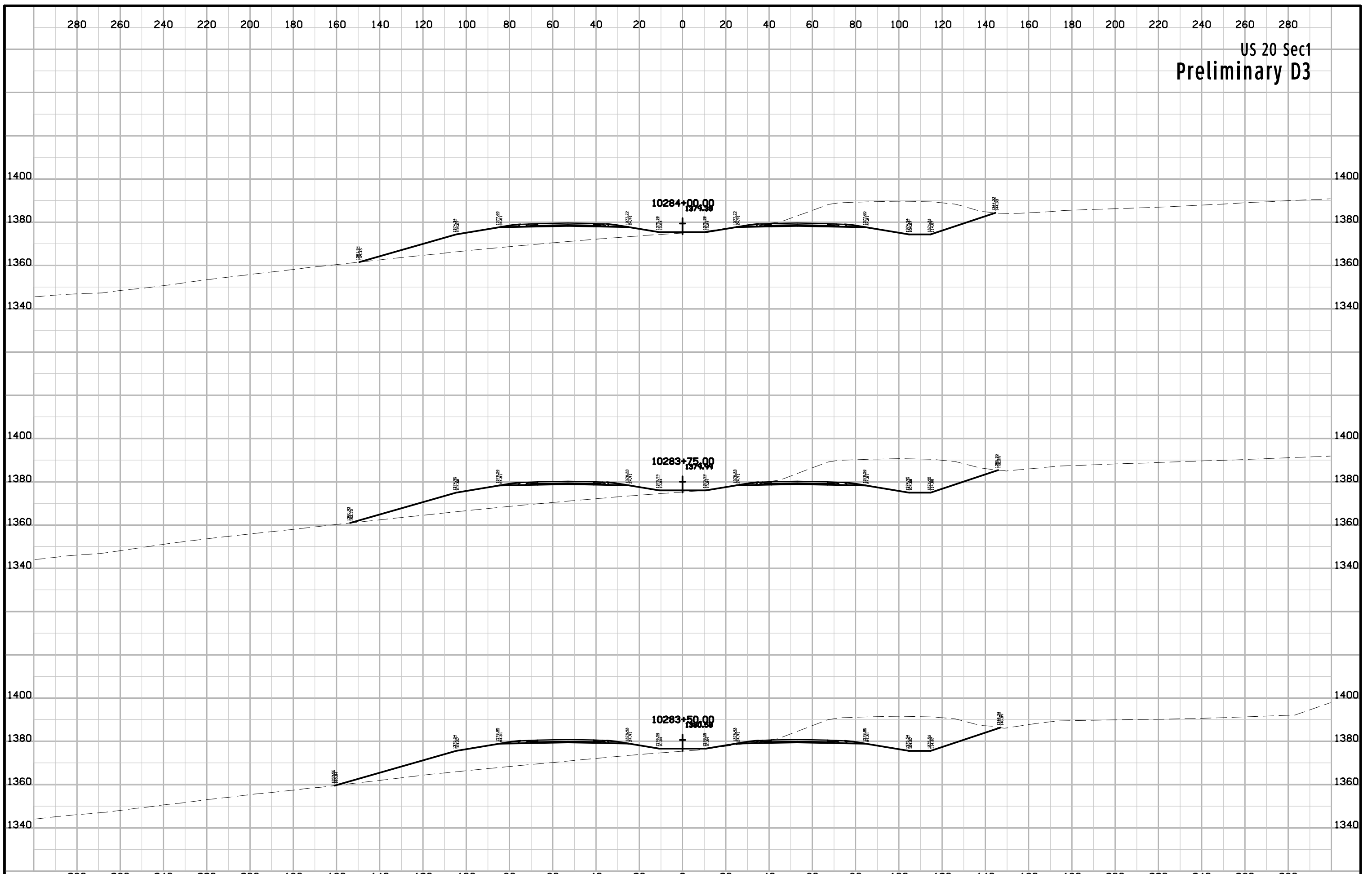
US 20 Sec1
Preliminary D3



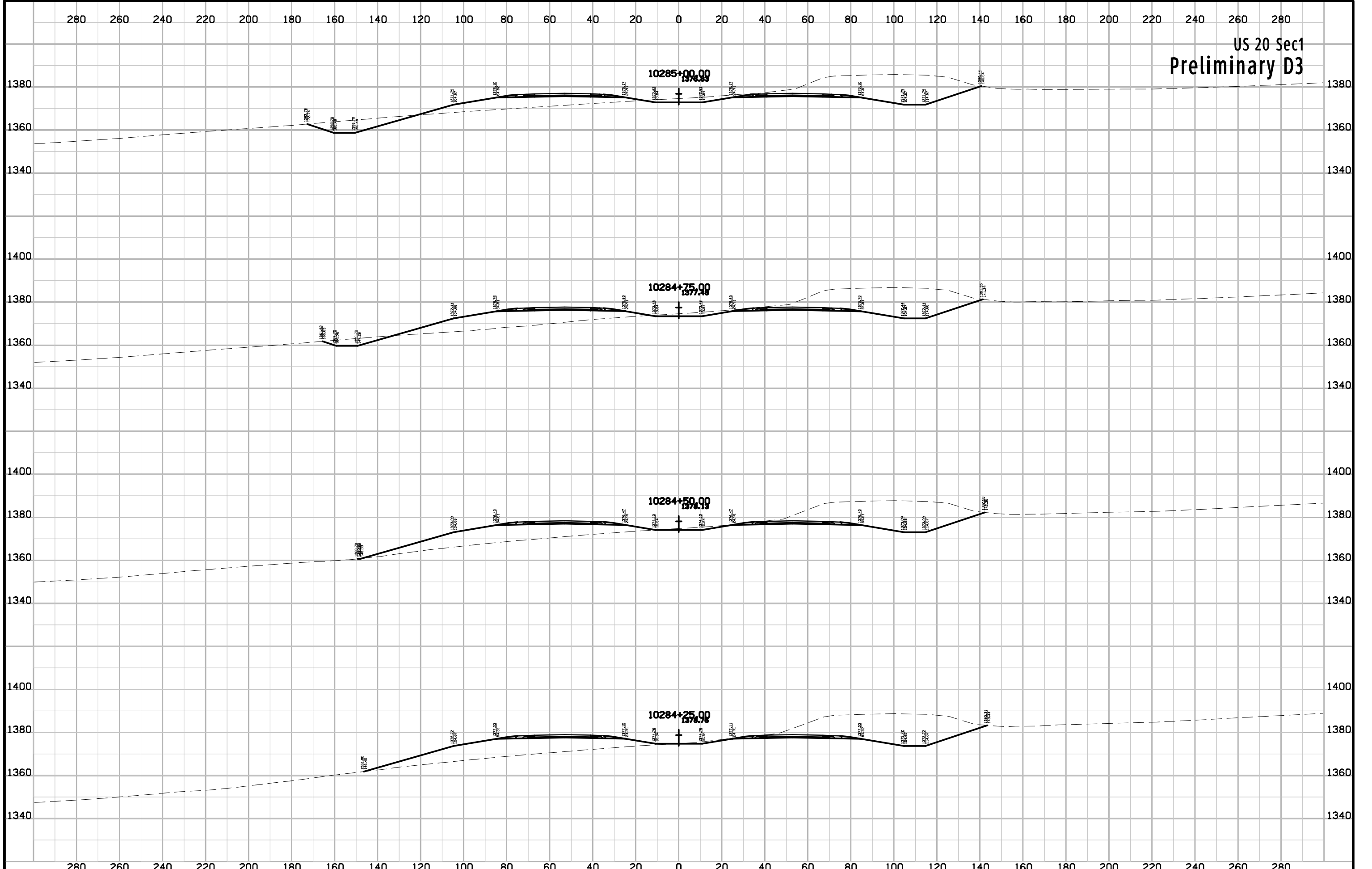
US 20 Sec1
Preliminary D3



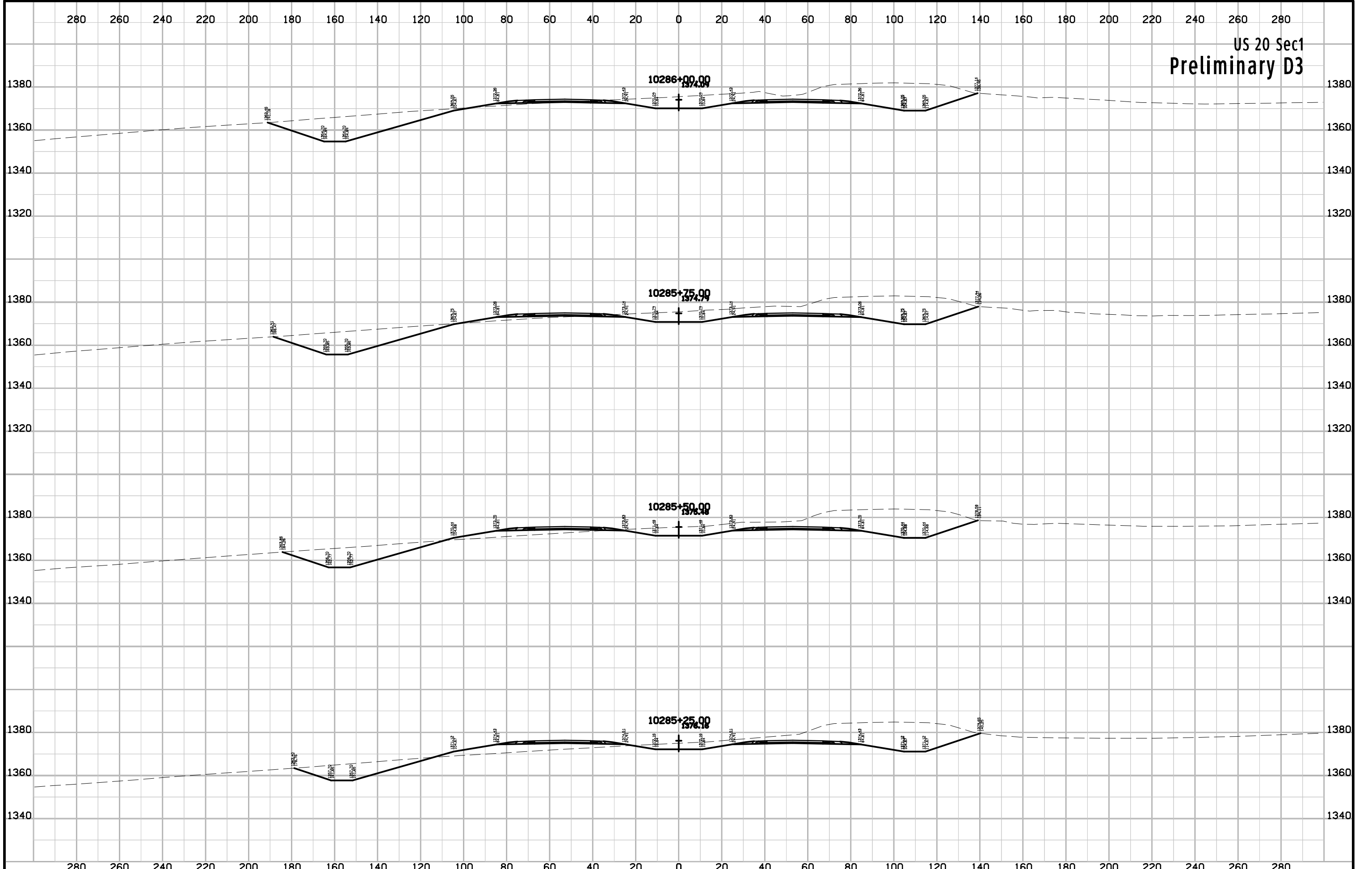
US 20 Sec1
Preliminary D3

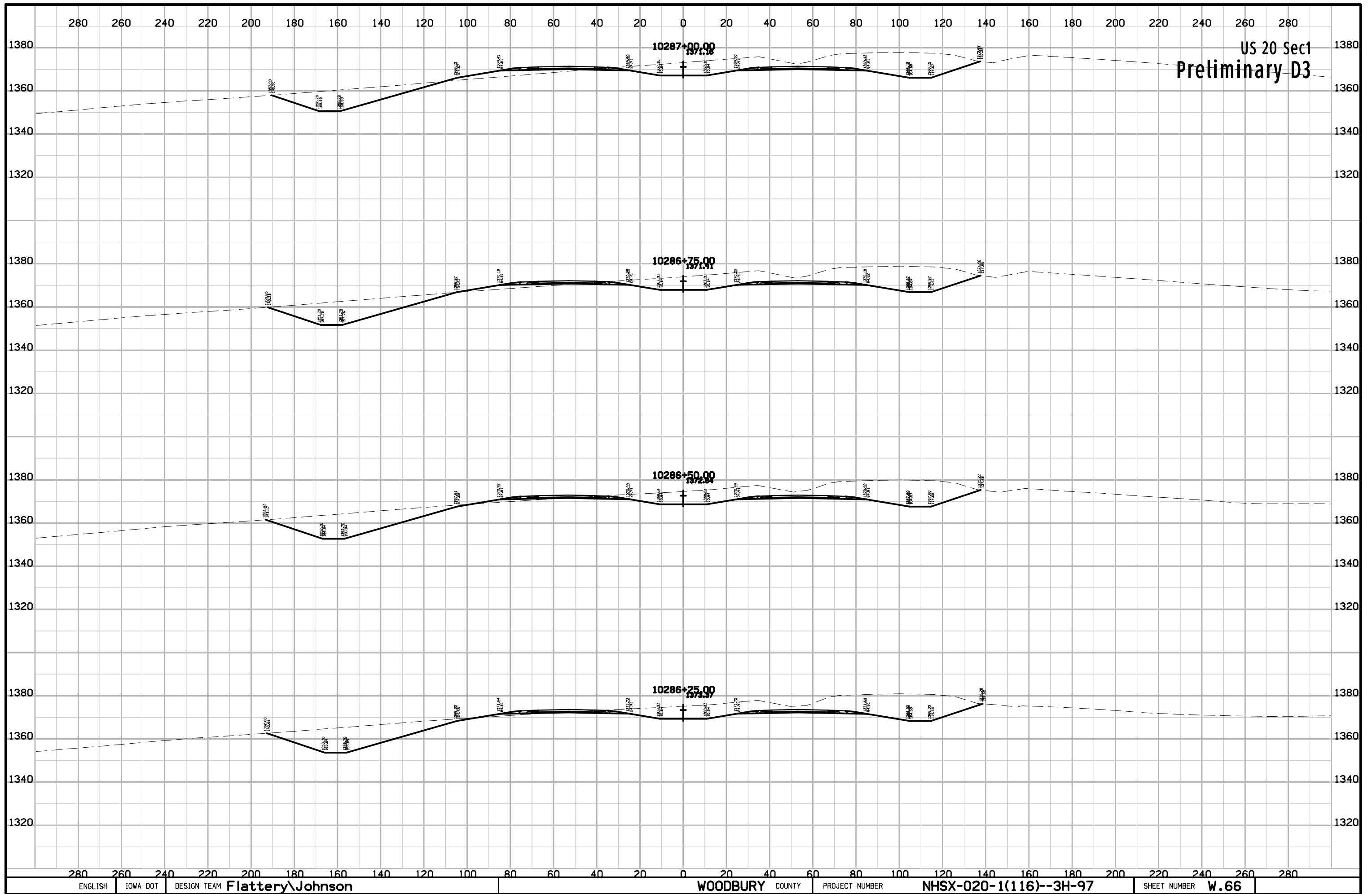


US 20 Sec1
Preliminary D3

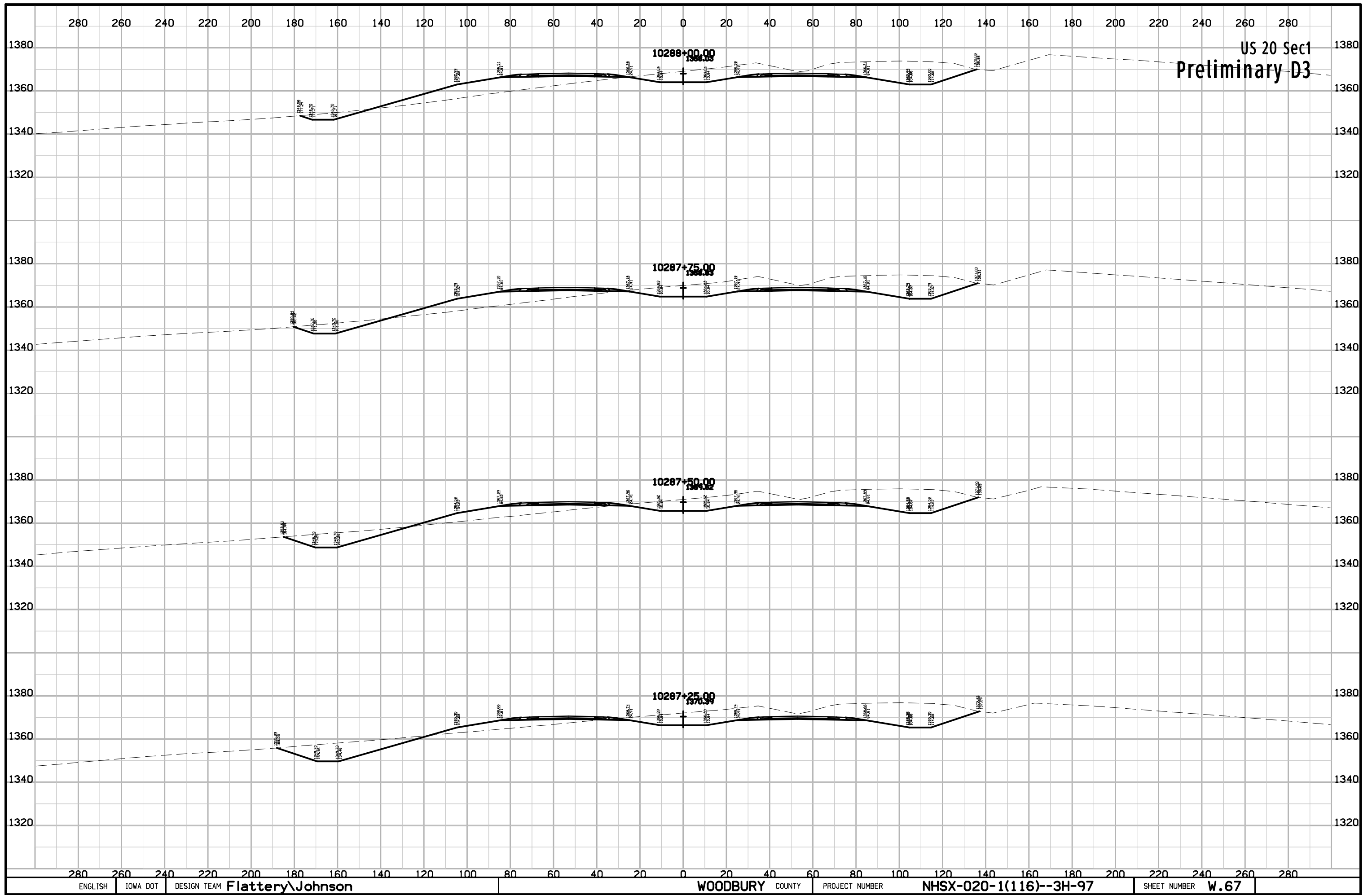


US 20 Sec1
Preliminary D3

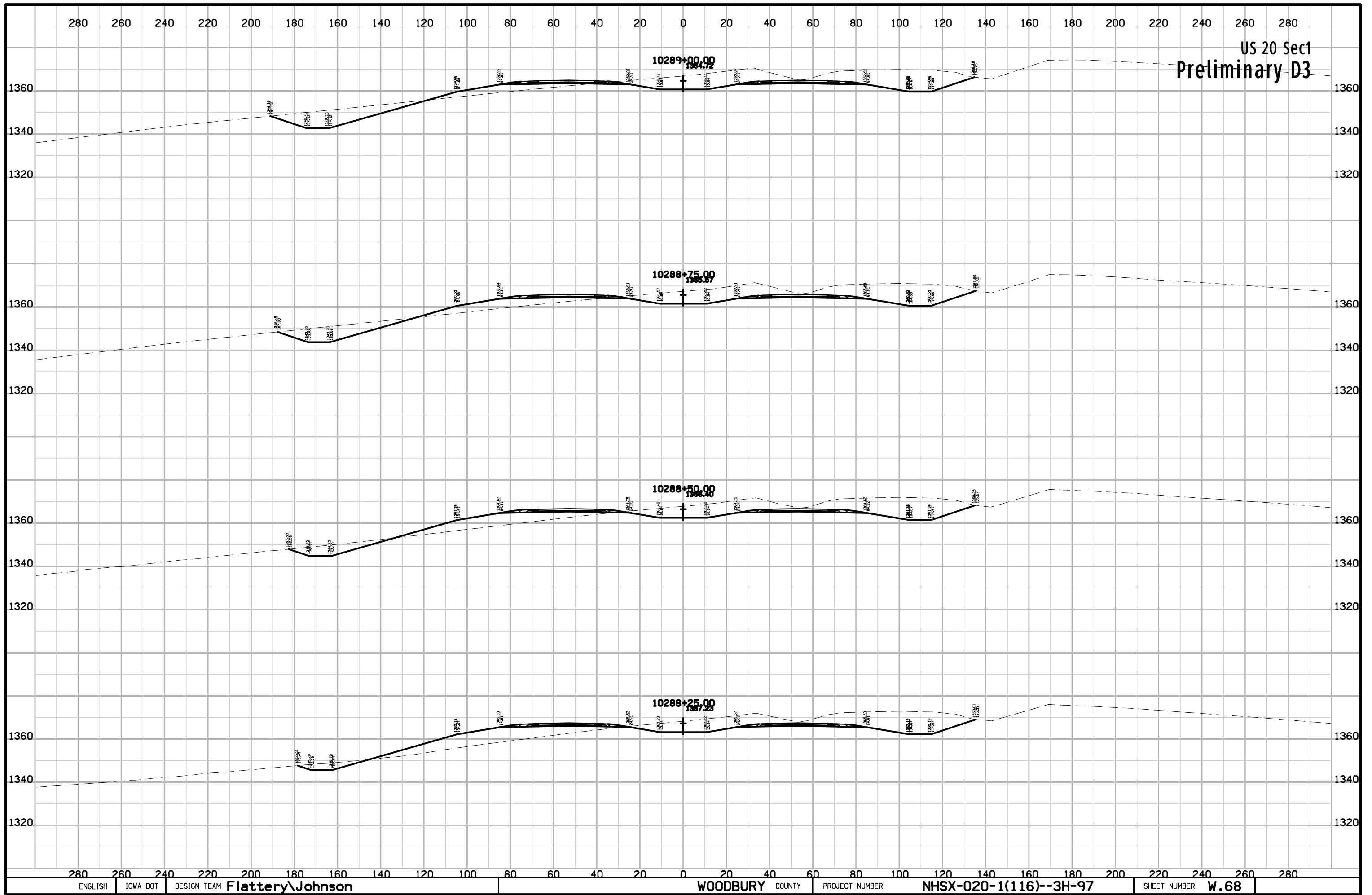




US 20 Sec1
Preliminary D3

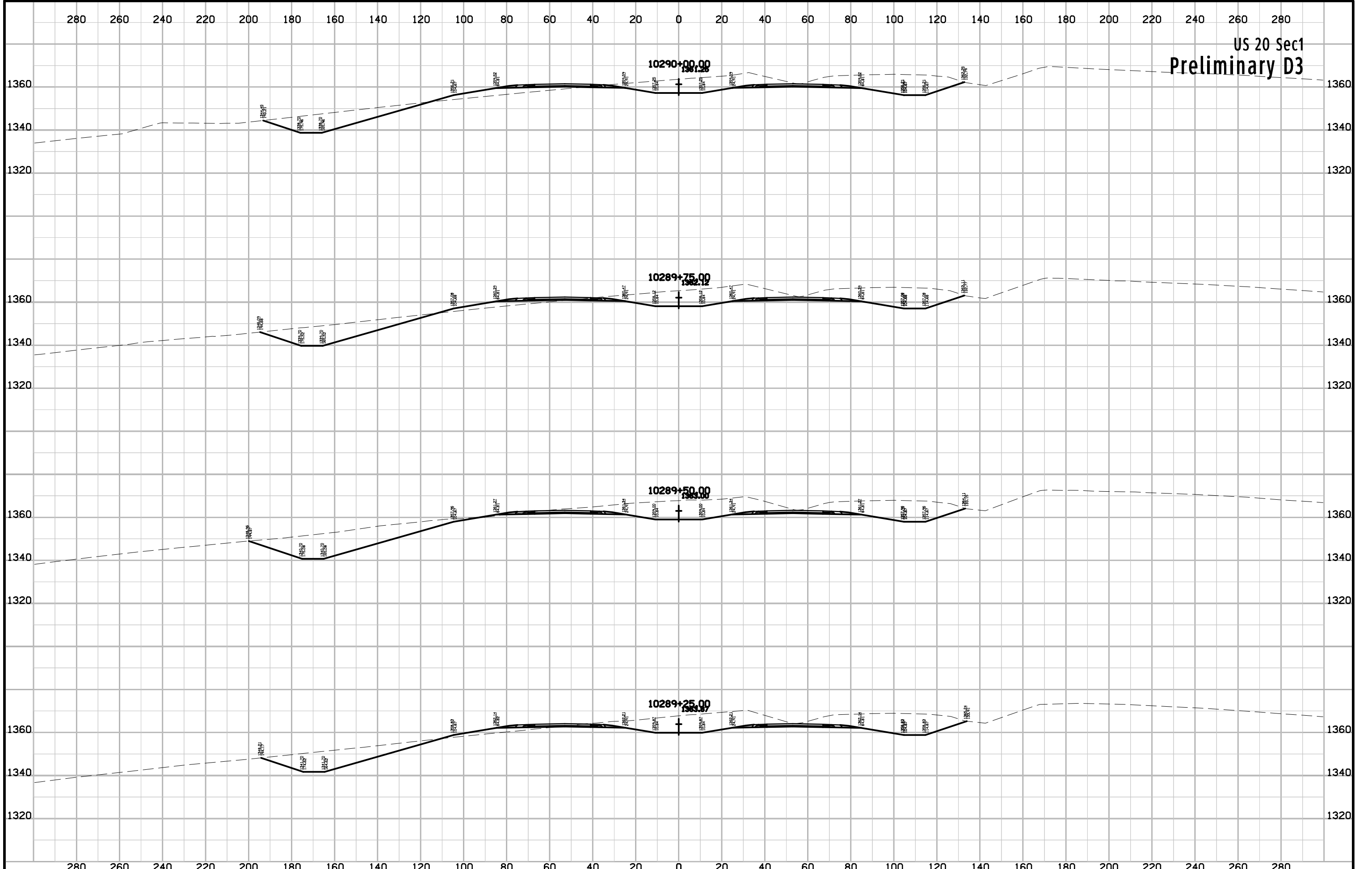


US 20 Sec1
Preliminary D3

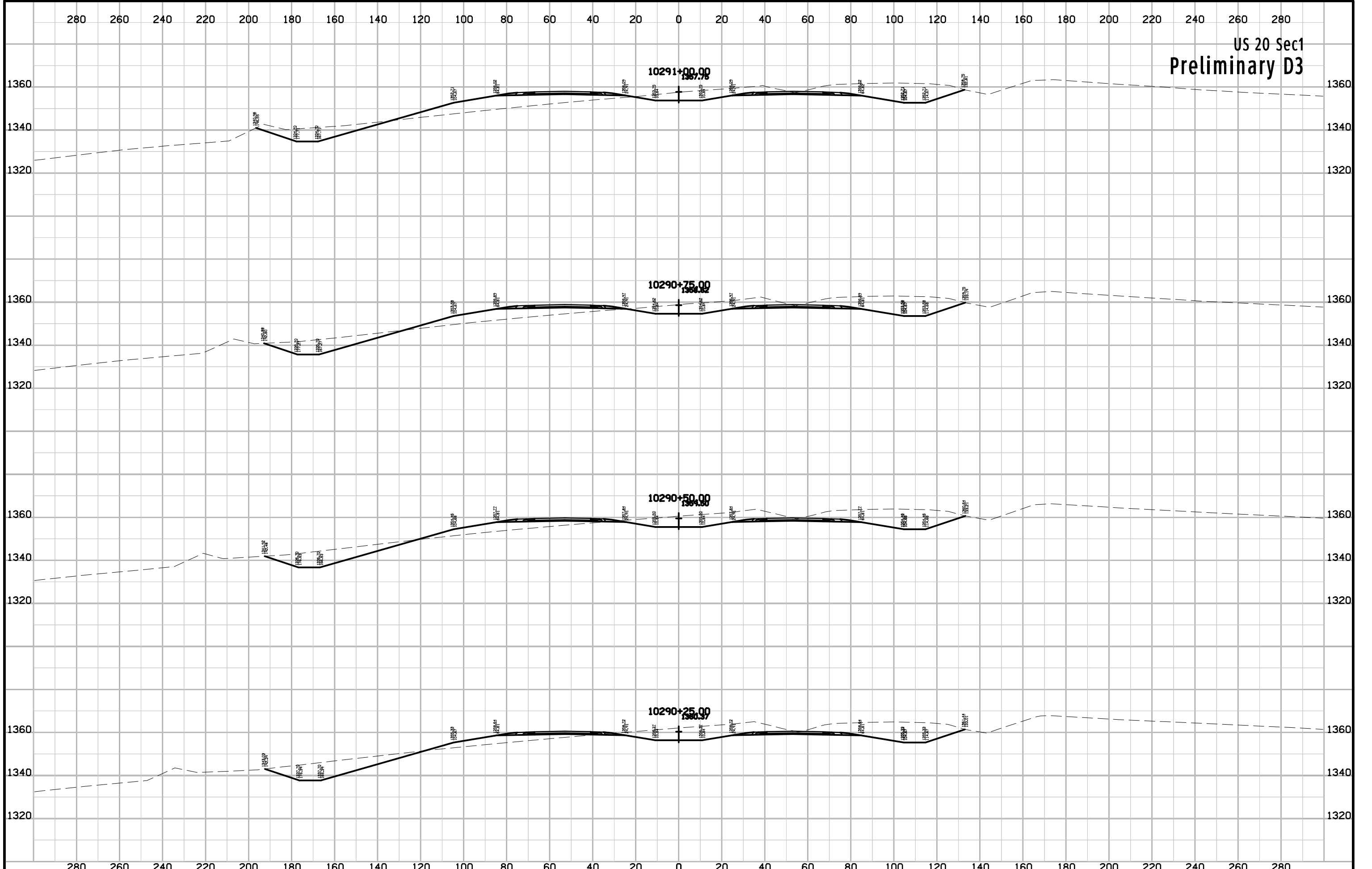


US 20 Sec1
Preliminary D3

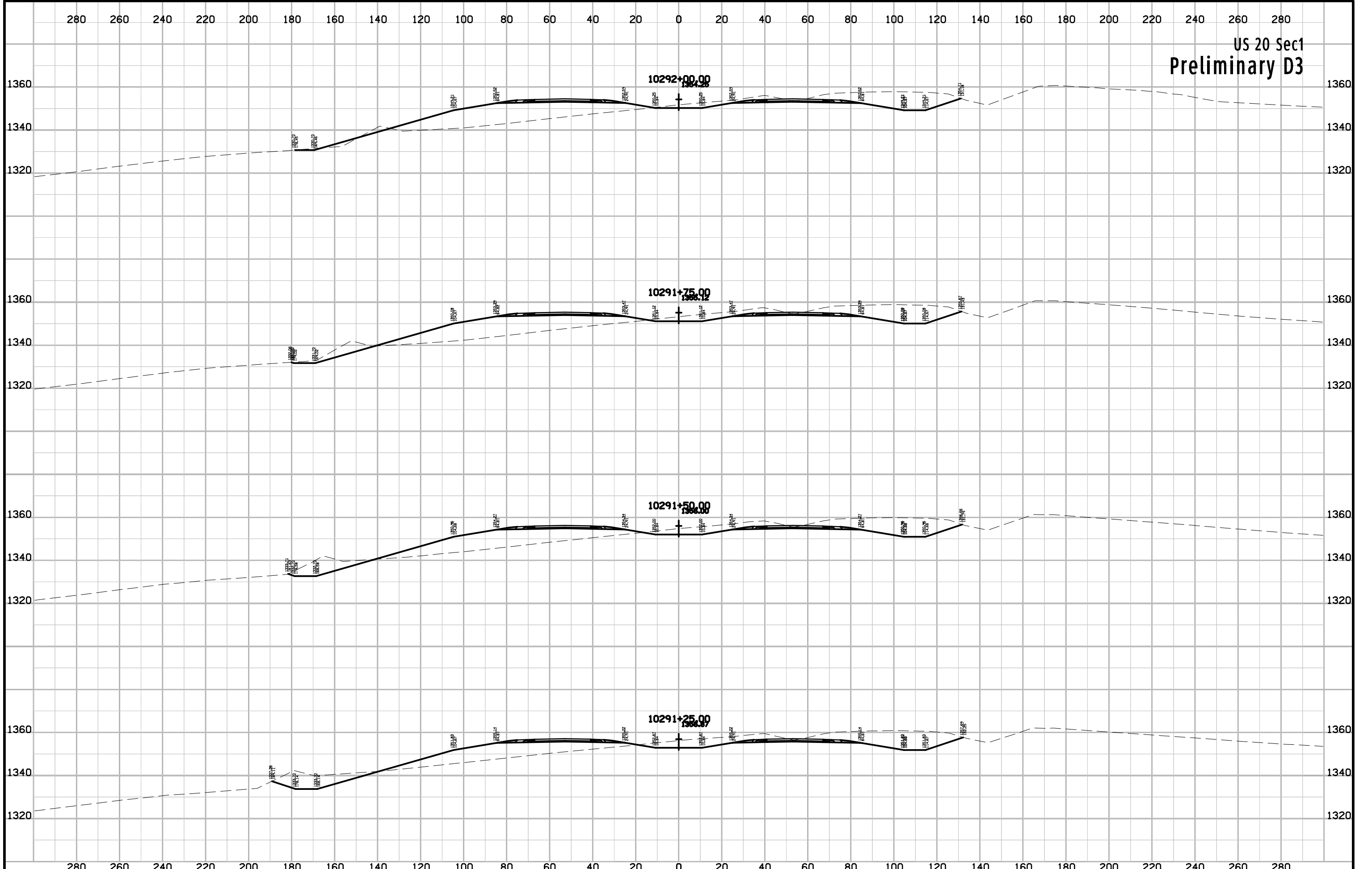
US 20 Sec1
Preliminary D3



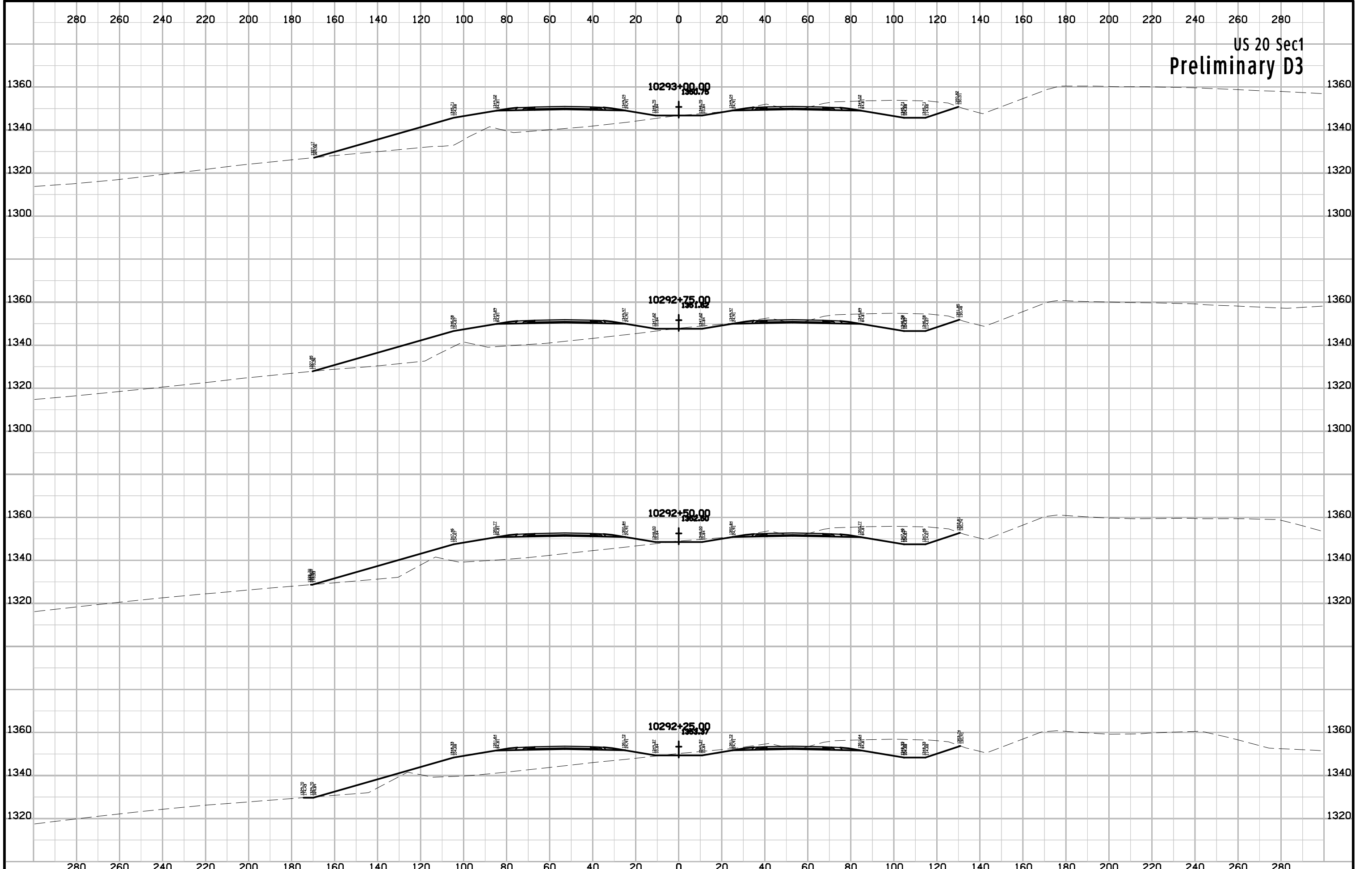
US 20 Sec1
Preliminary D3

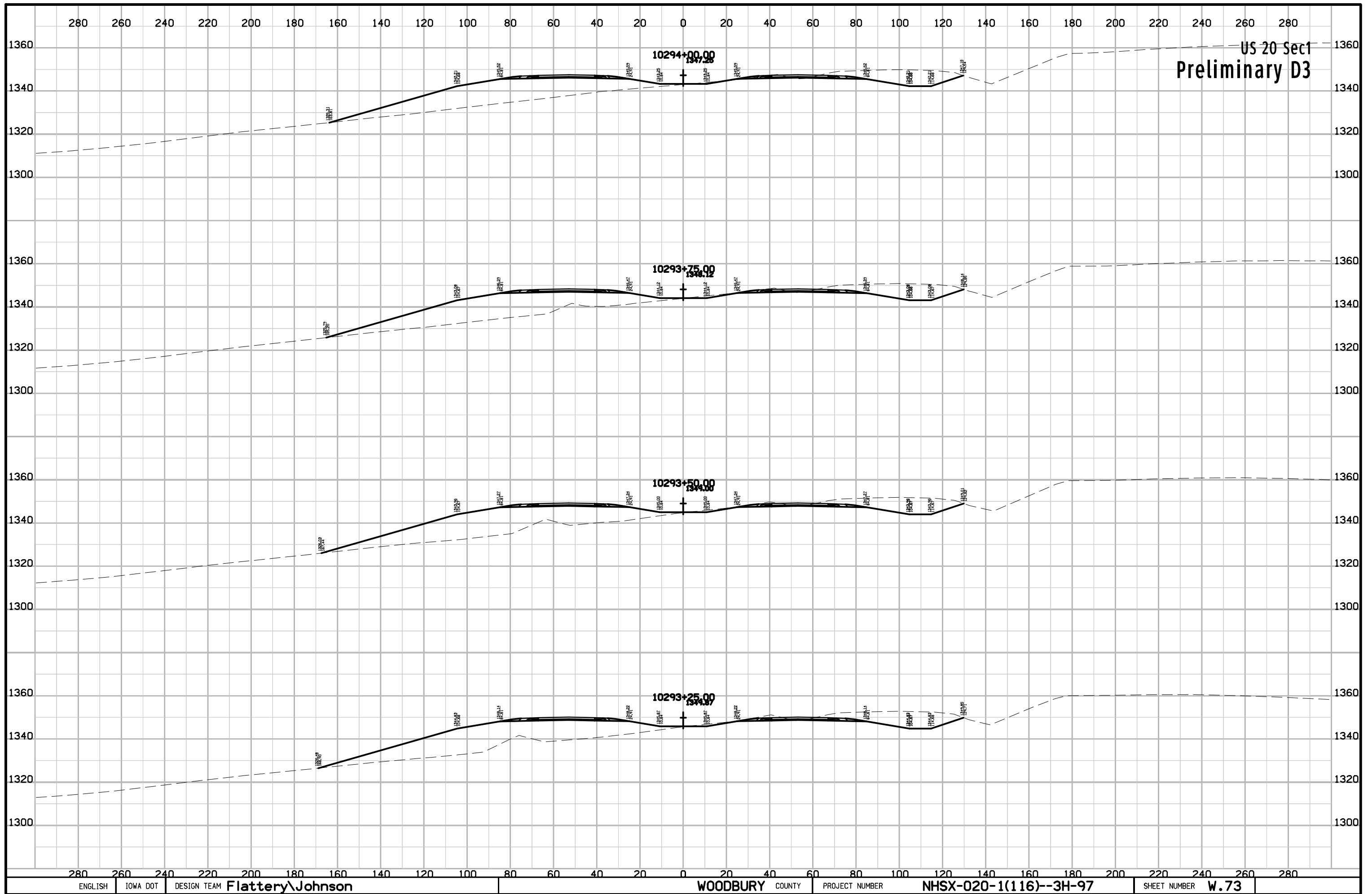


US 20 Sec1
Preliminary D3

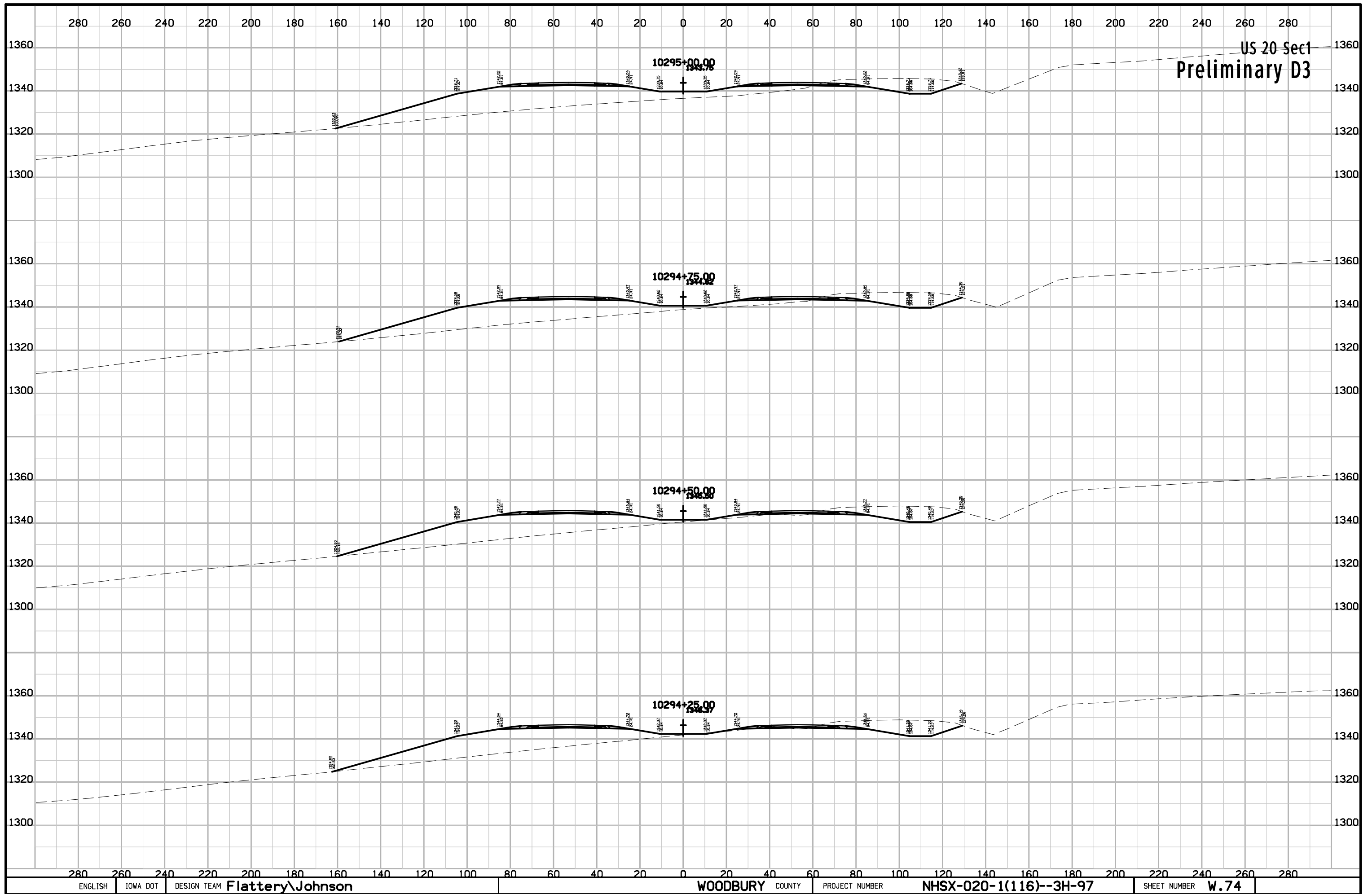


US 20 Sec1
Preliminary D3

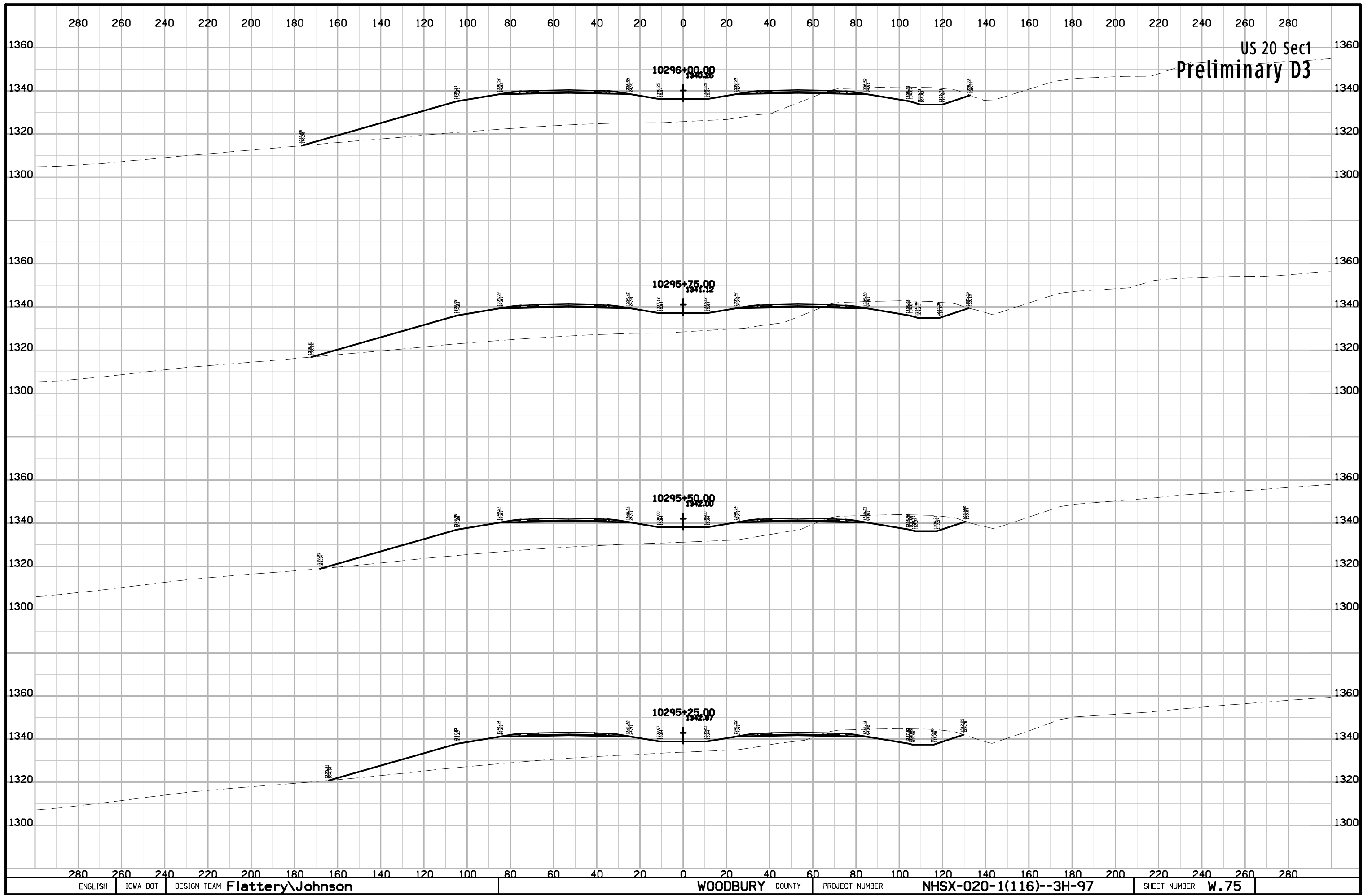




US 20 Sec1
Preliminary D3

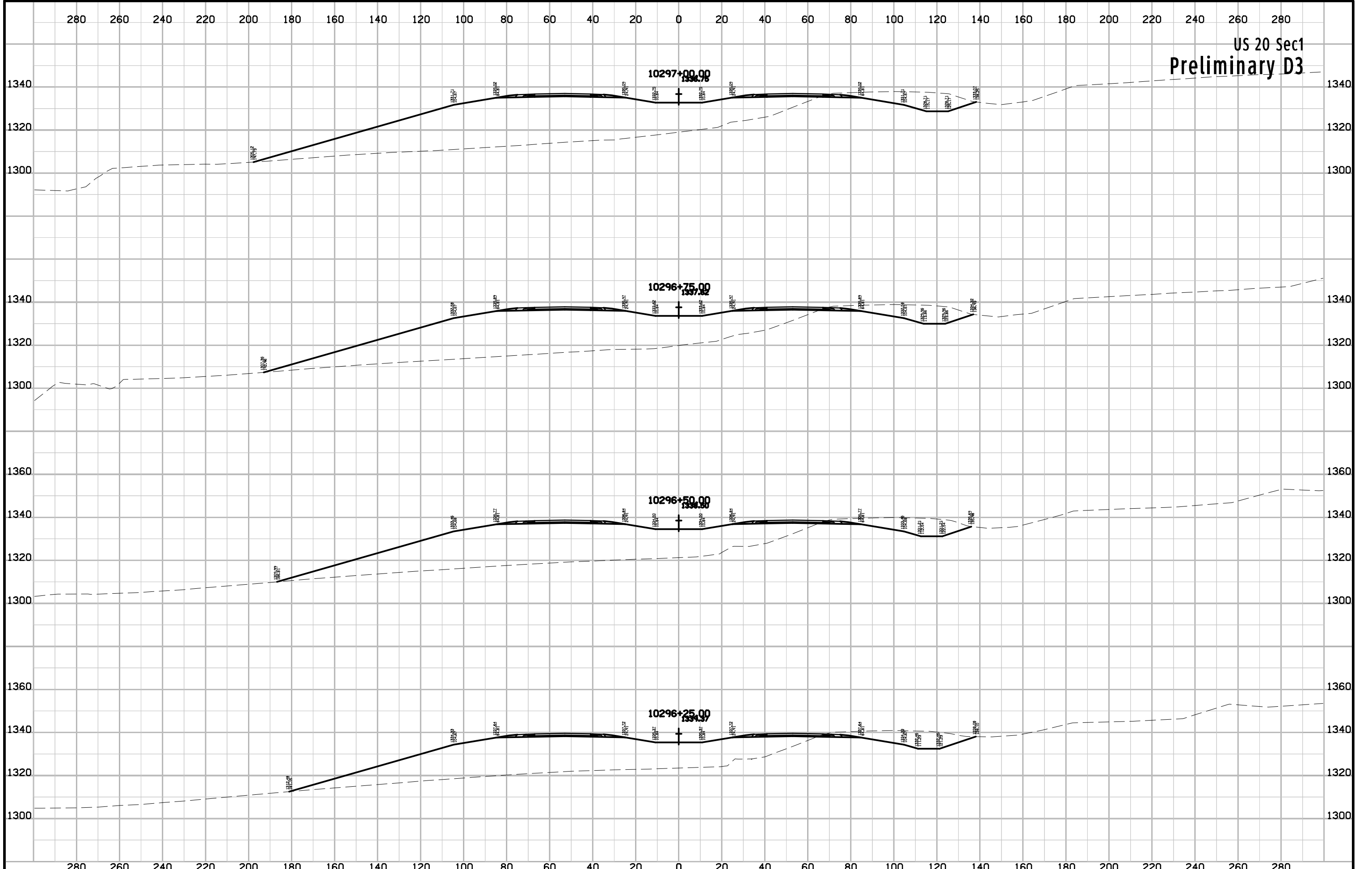


US 20-Sec1
Preliminary D3

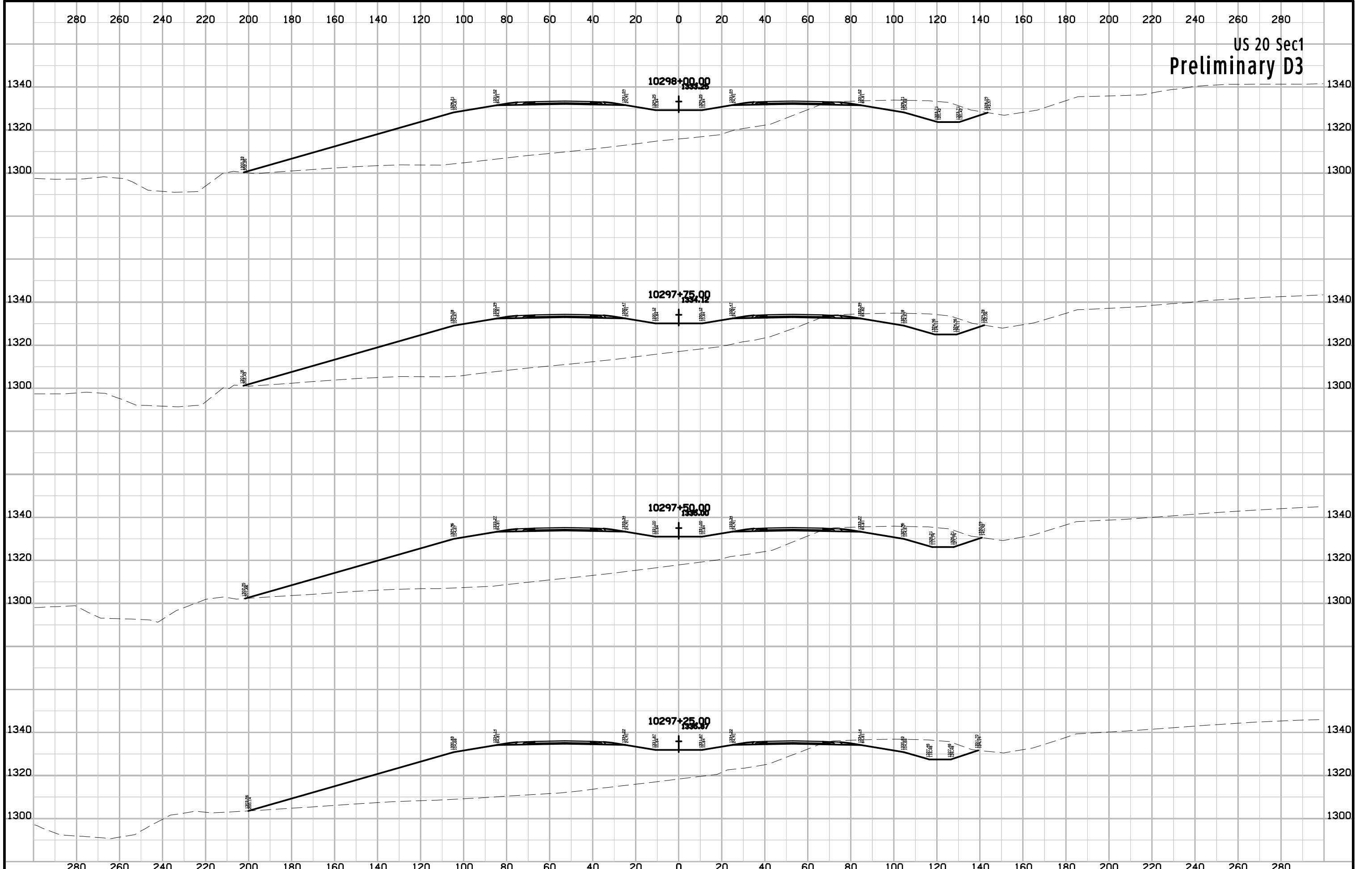


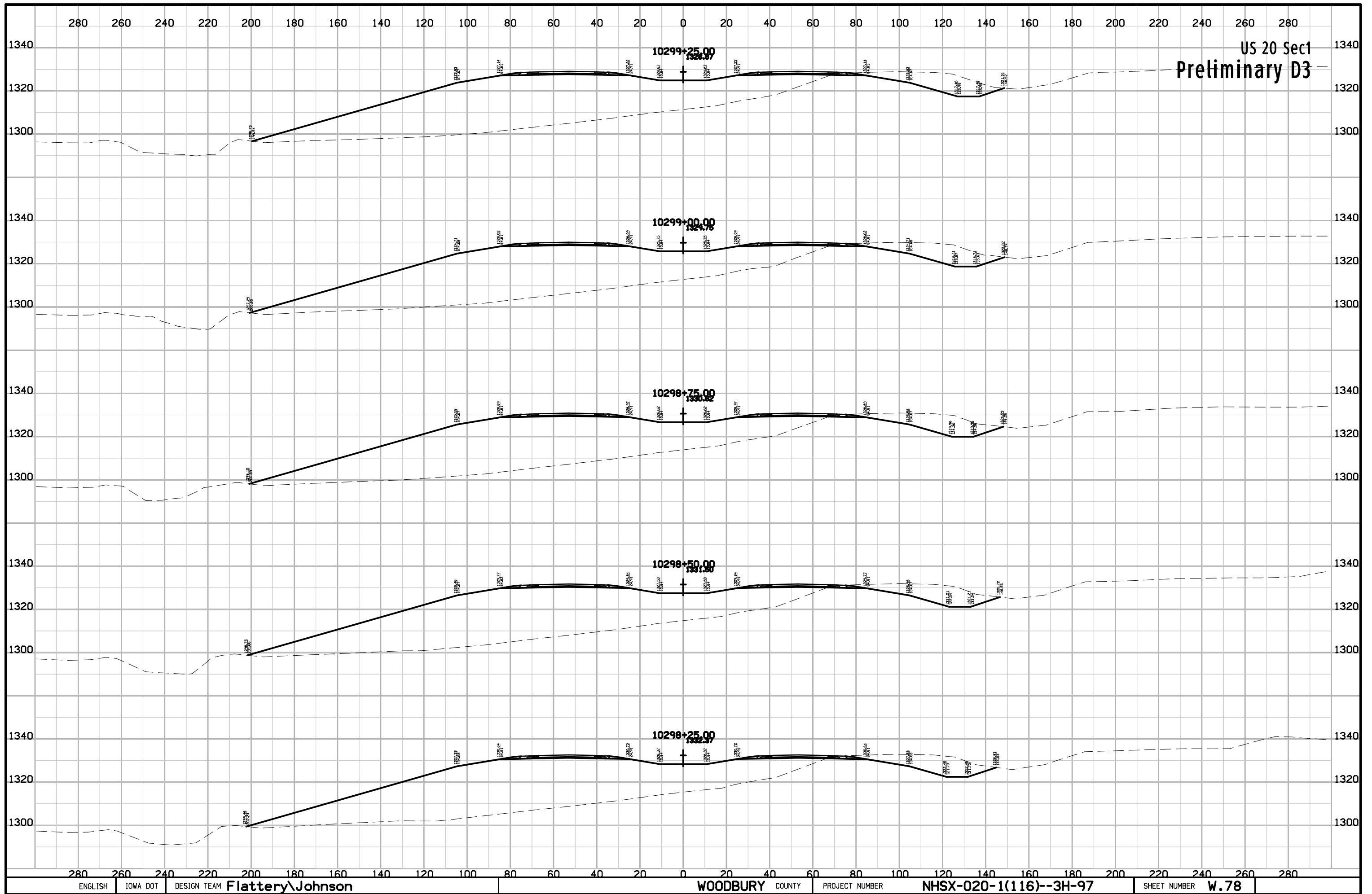
US 20 Sec1
Preliminary D3

US 20 Sec1
Preliminary D3

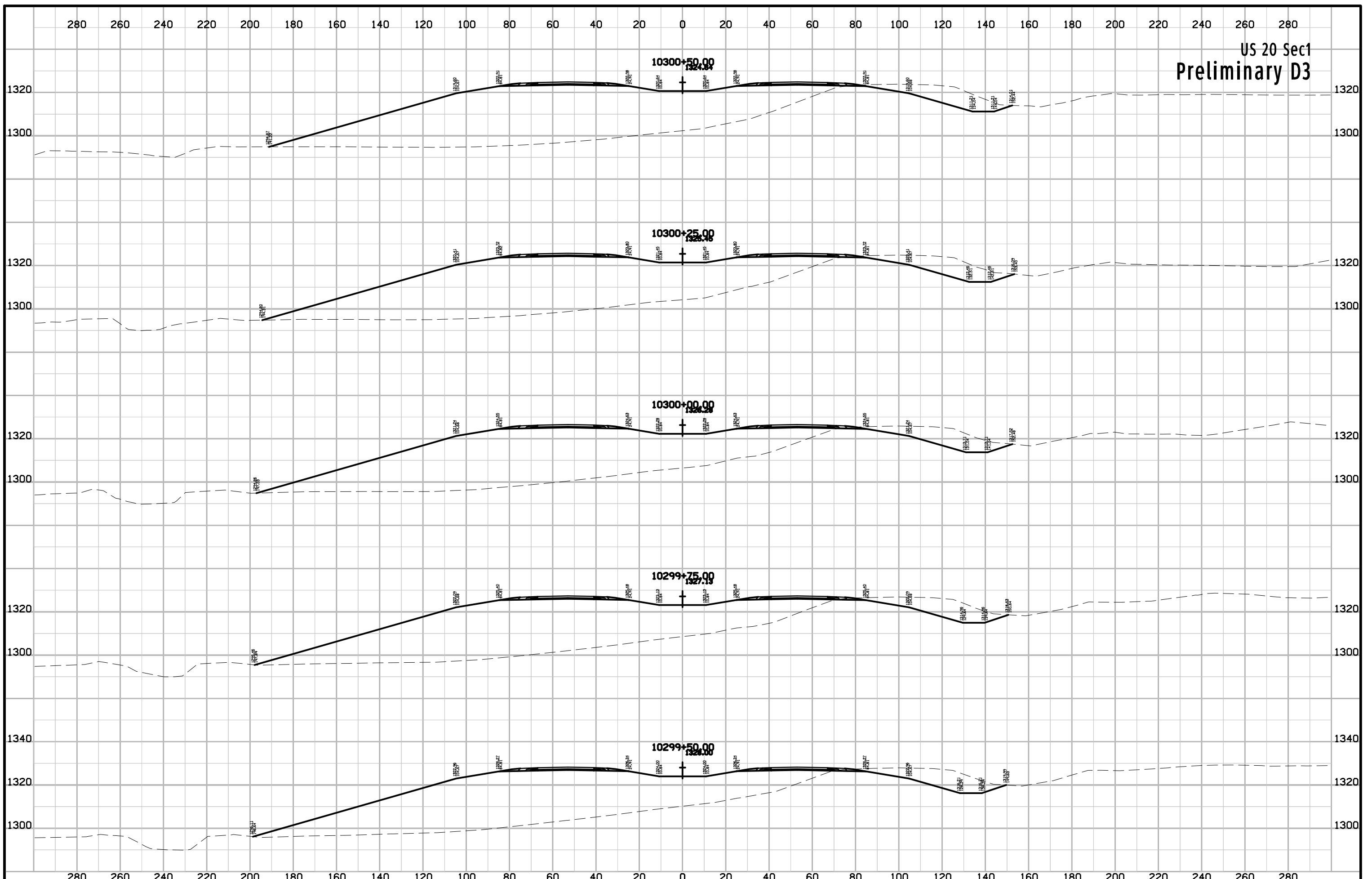


US 20 Sec1
Preliminary D3

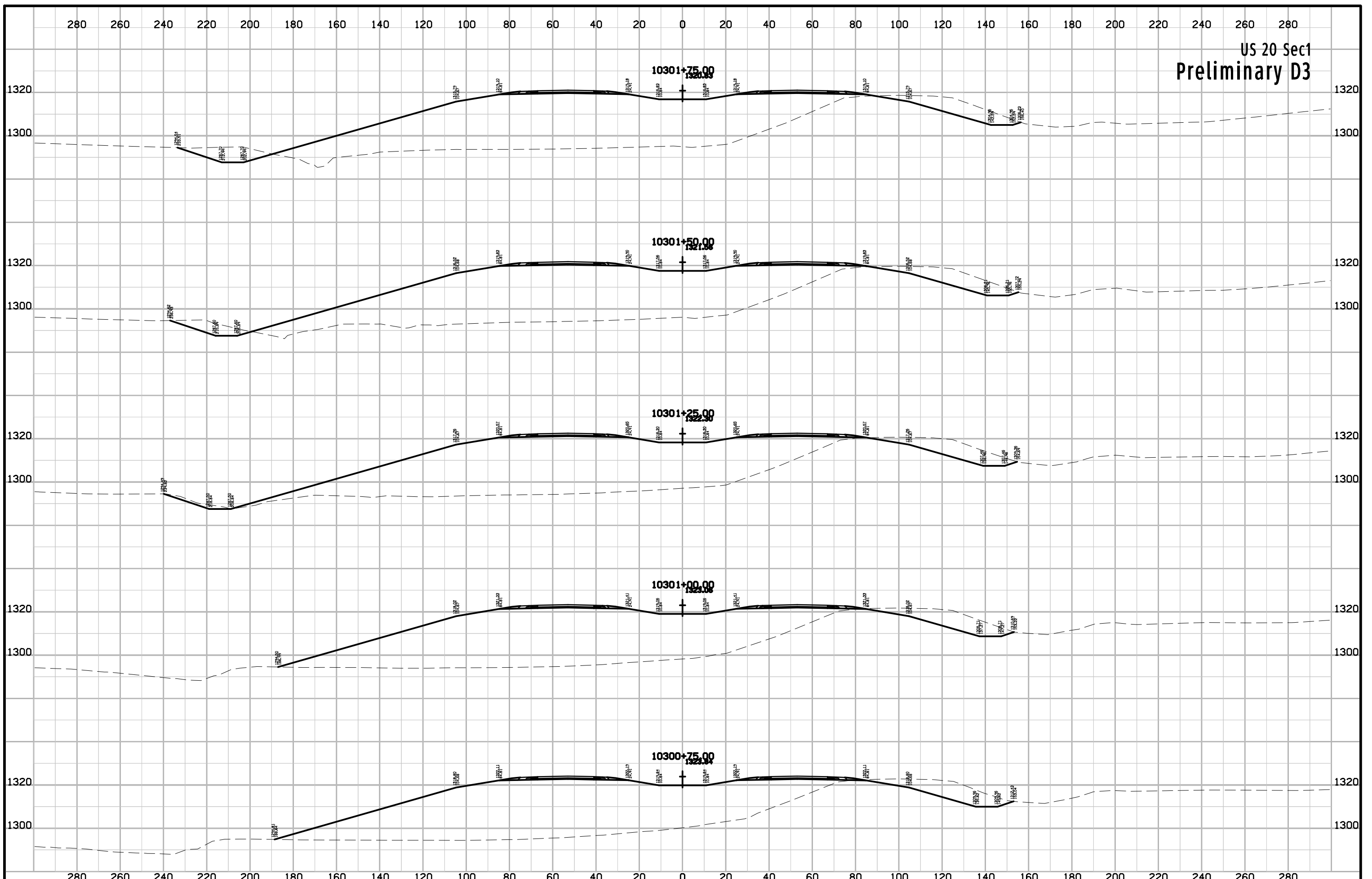




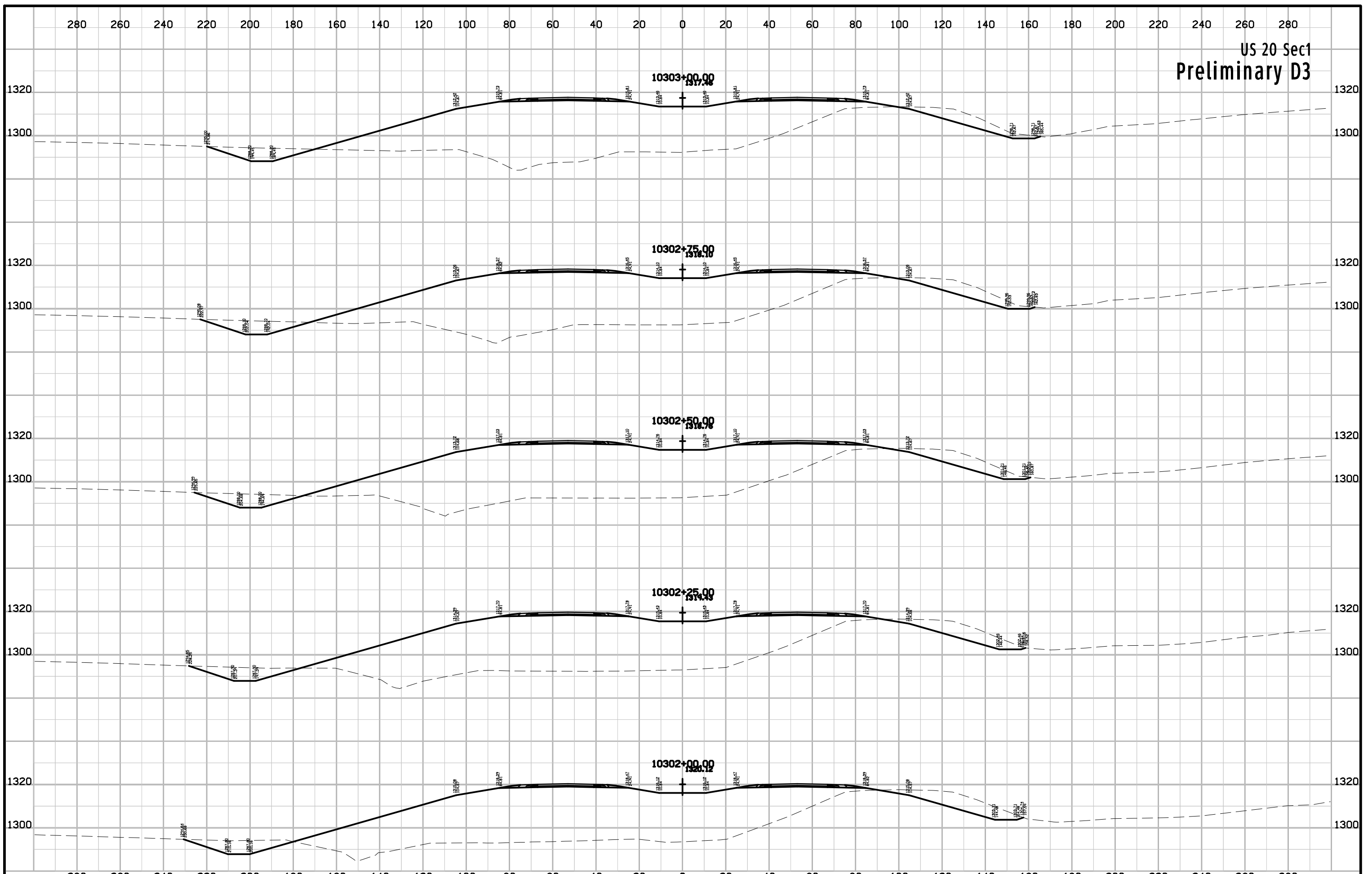
US 20 Sec1
Preliminary D3



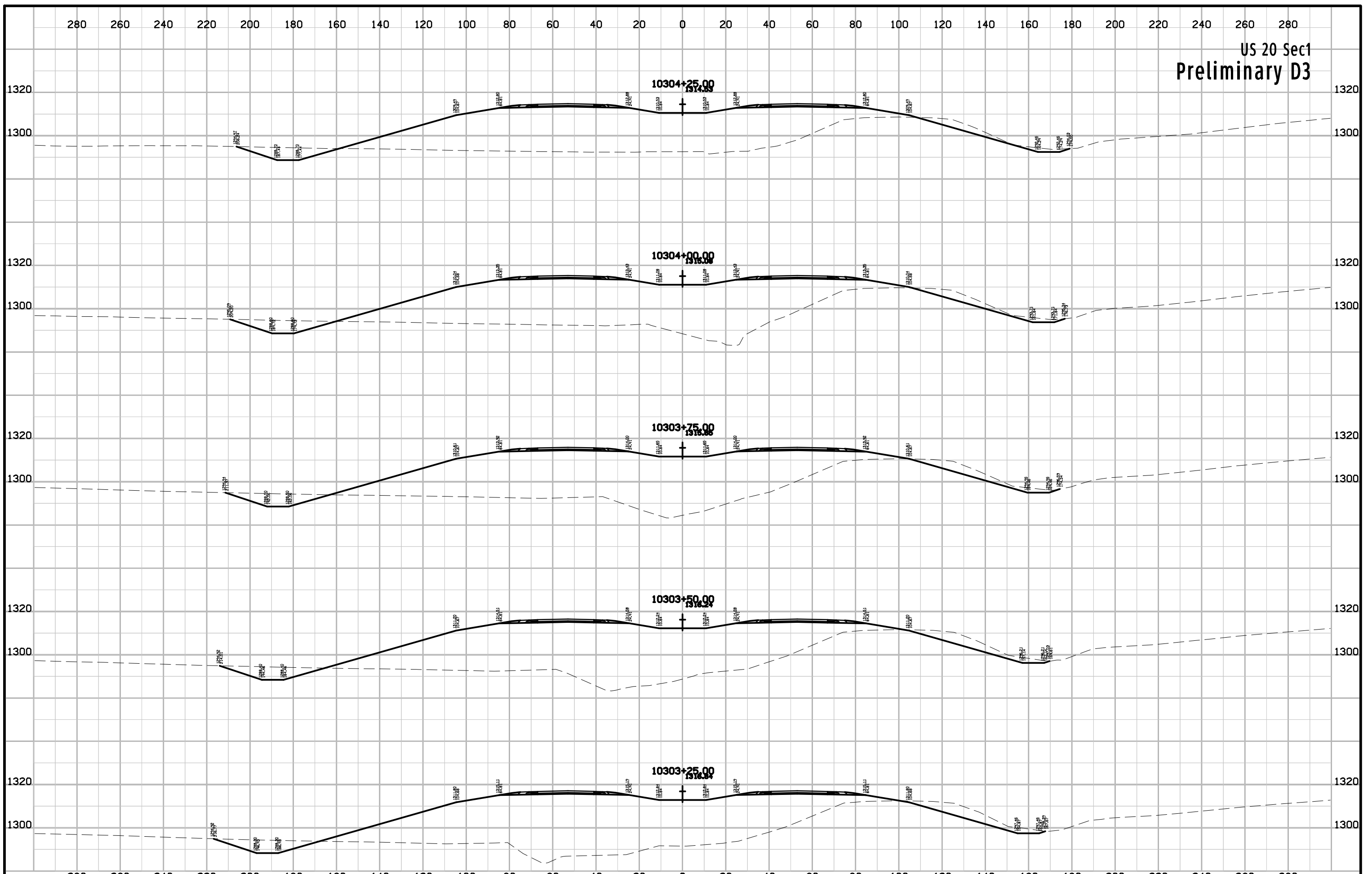
US 20 Sec1
Preliminary D3



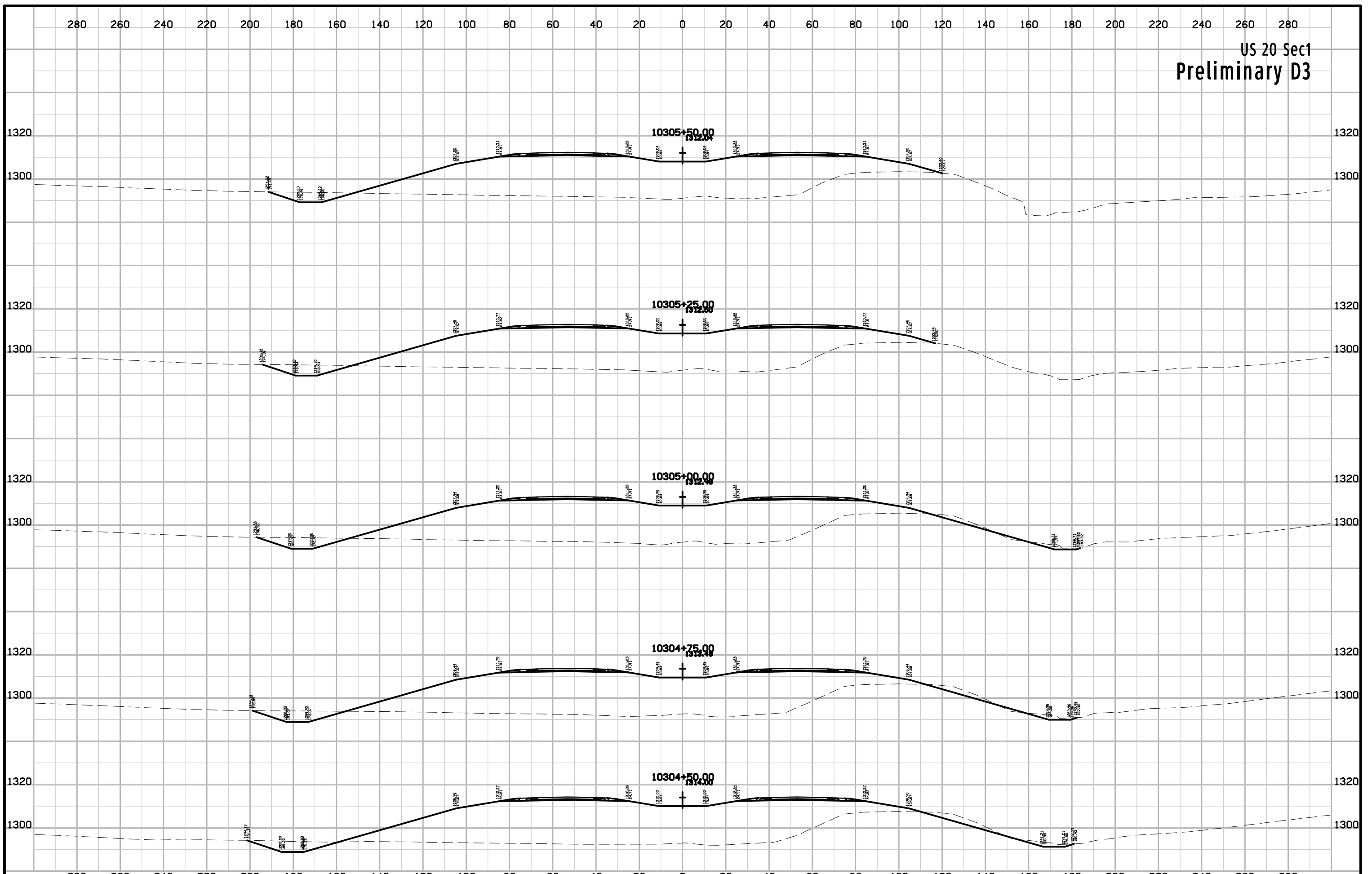
US 20 Sec1
Preliminary D3



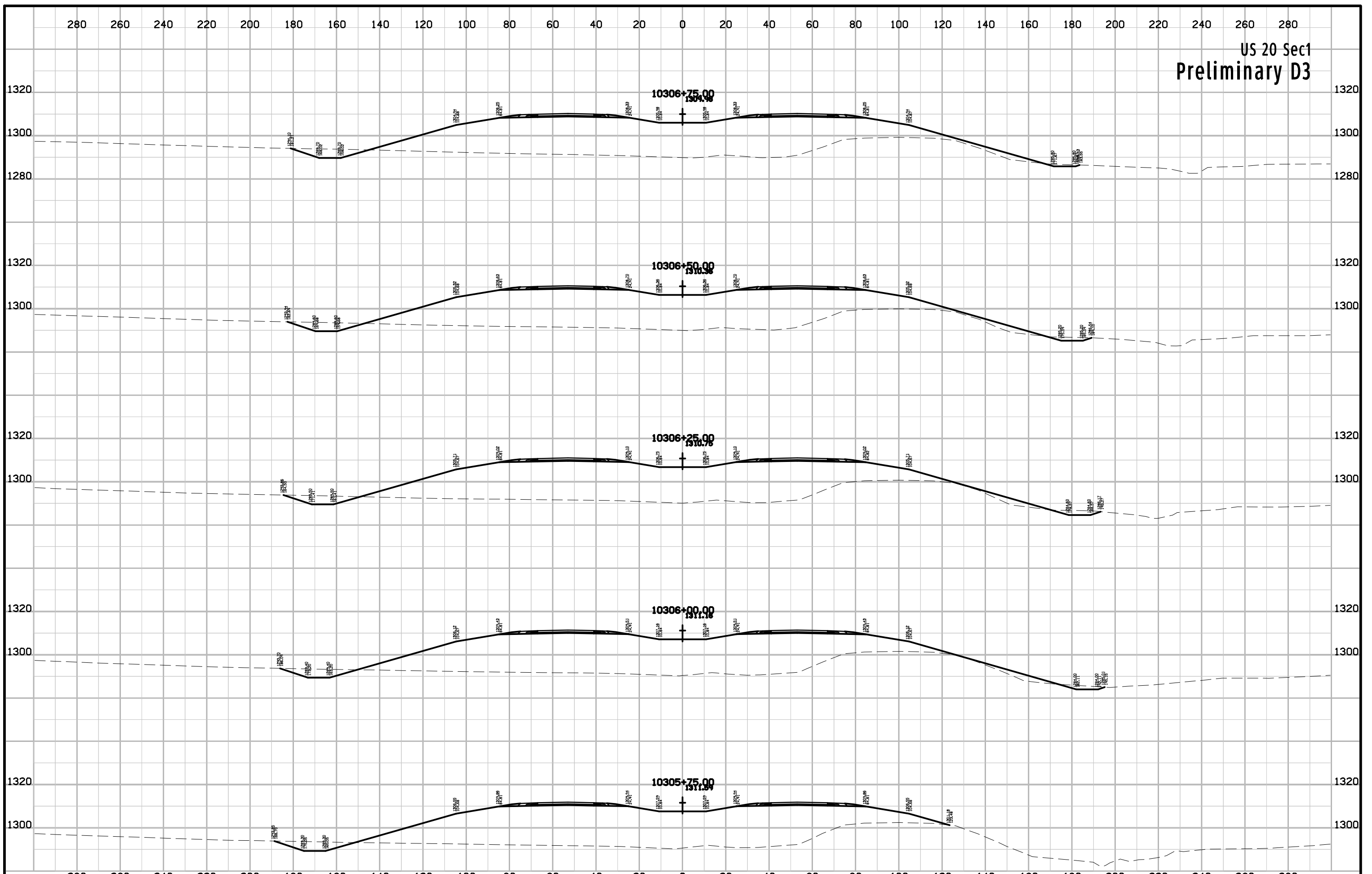
US 20 Sec1
Preliminary D3



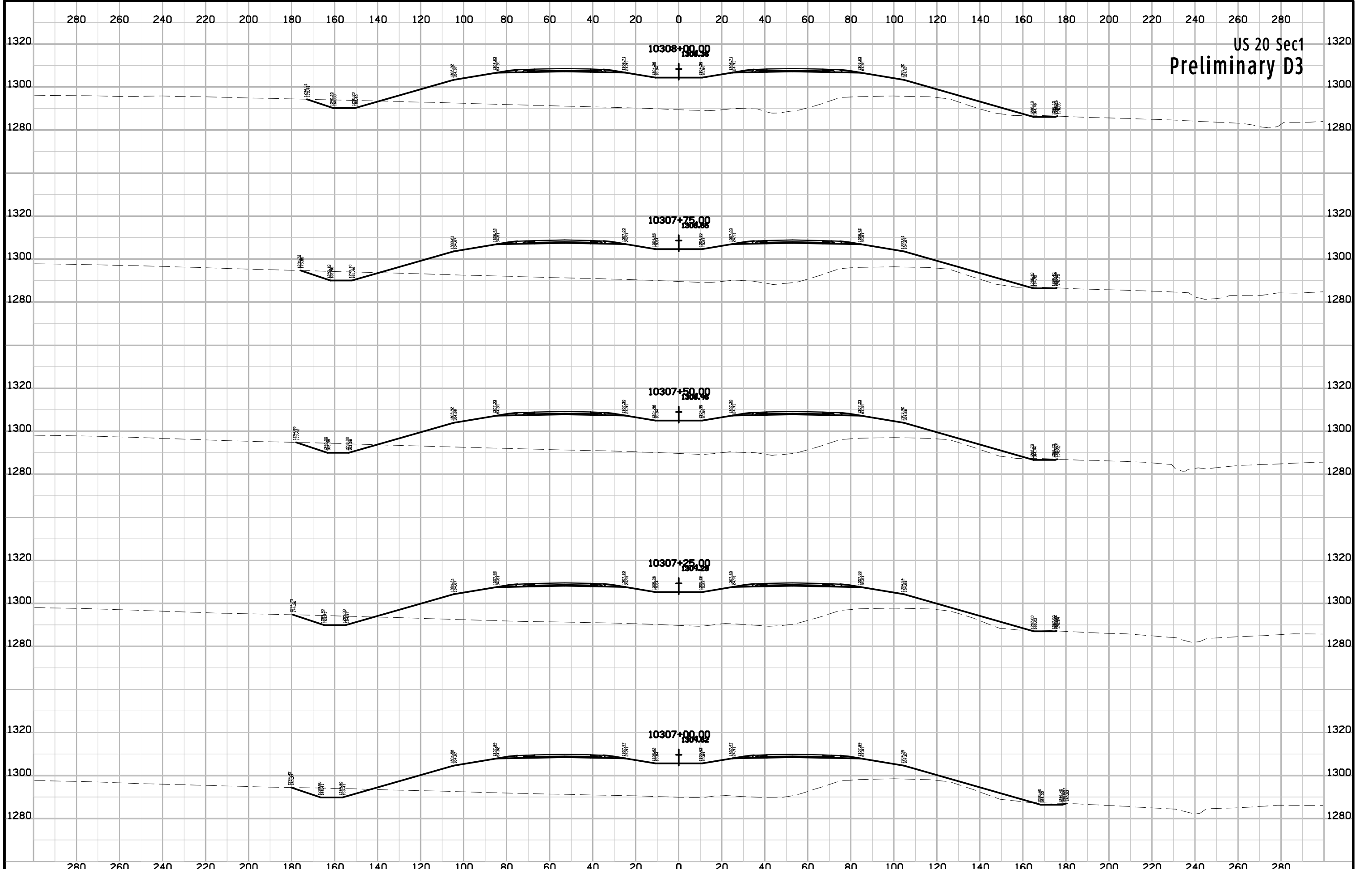
US 20 Sec1
Preliminary D3



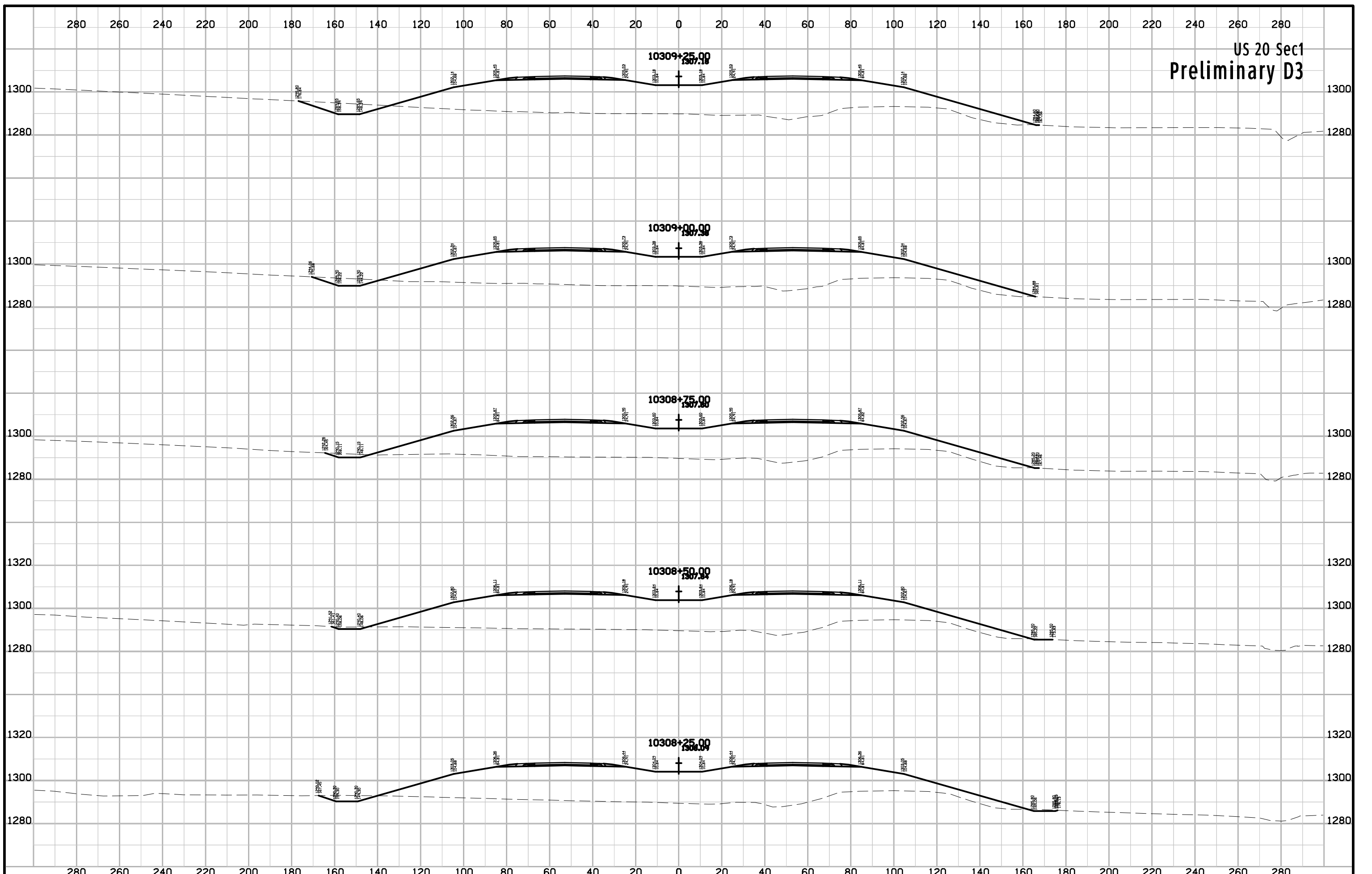
US 20 Sec1
Preliminary D3



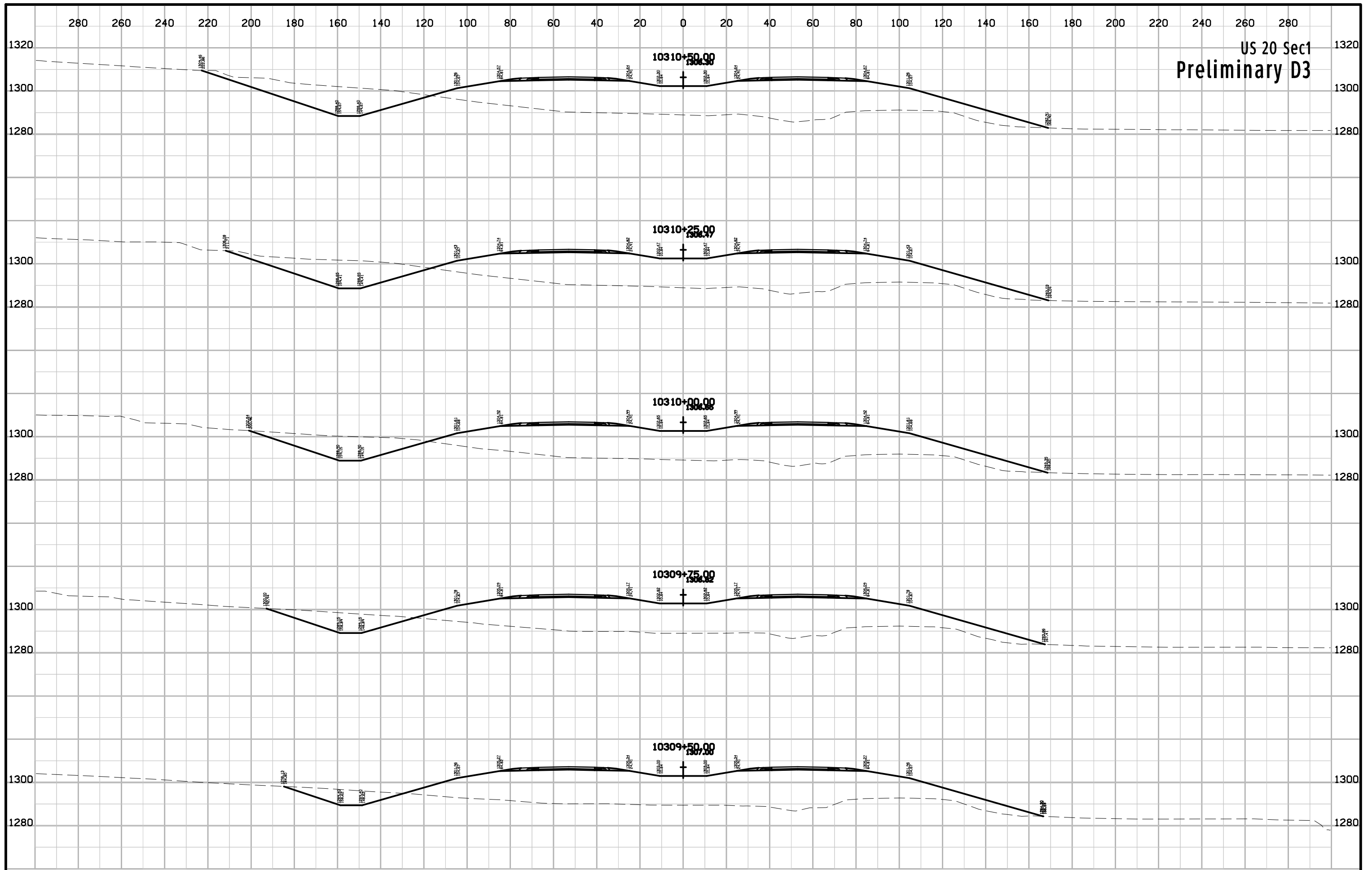
US 20 Sec1
Preliminary D3



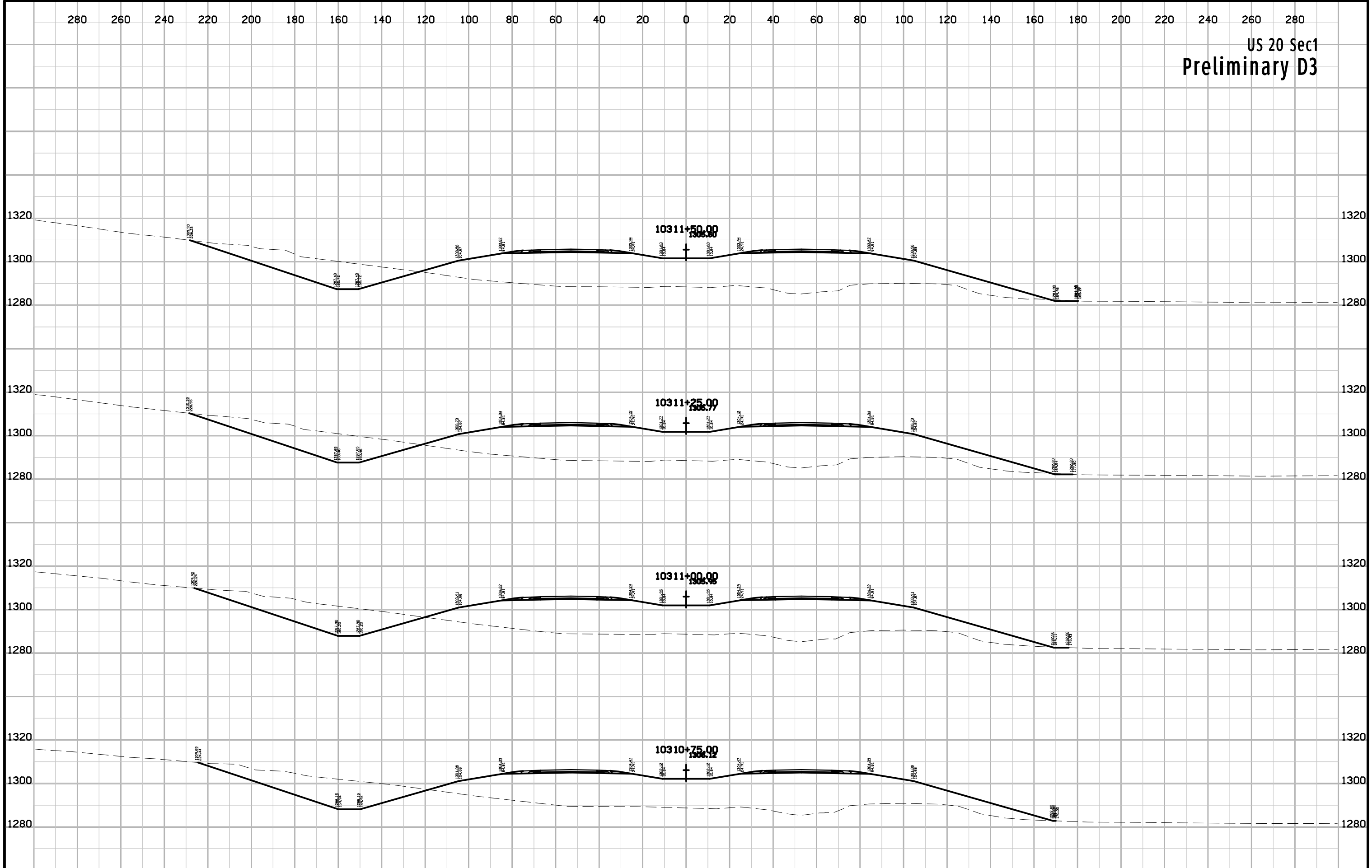
US 20 Sec1
Preliminary D3



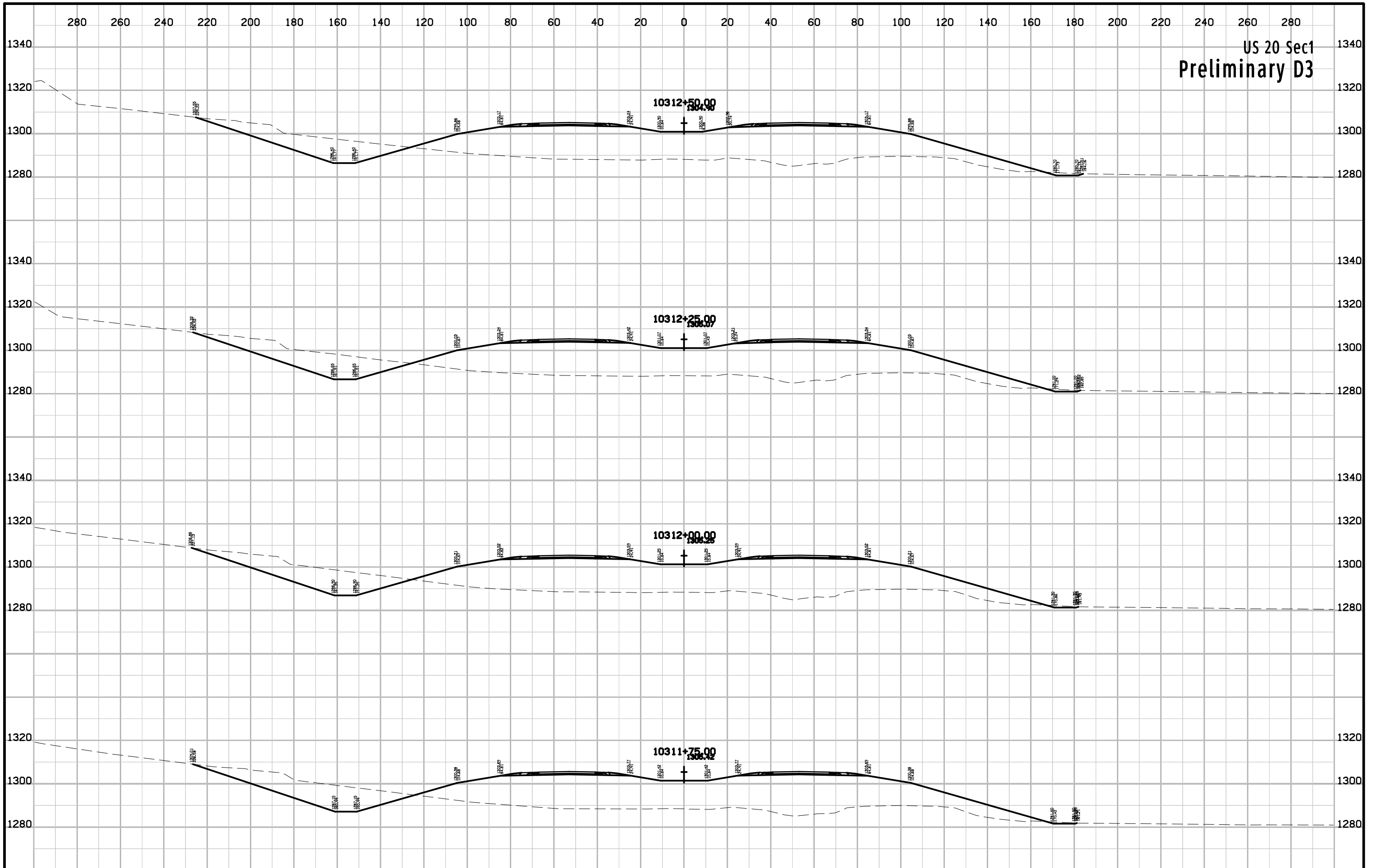
US 20 Sec1
Preliminary D3



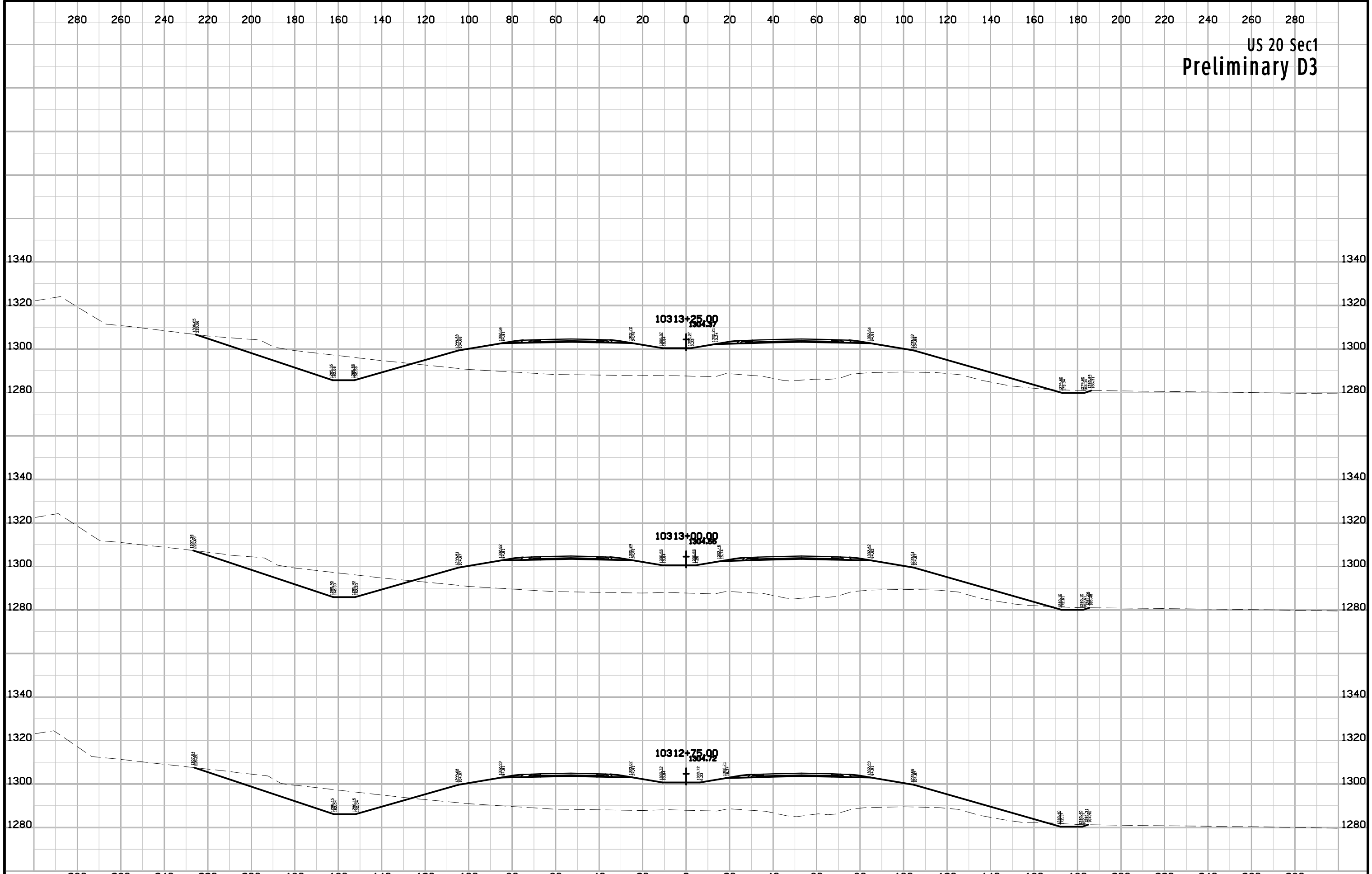
US 20 Sec1
Preliminary D3



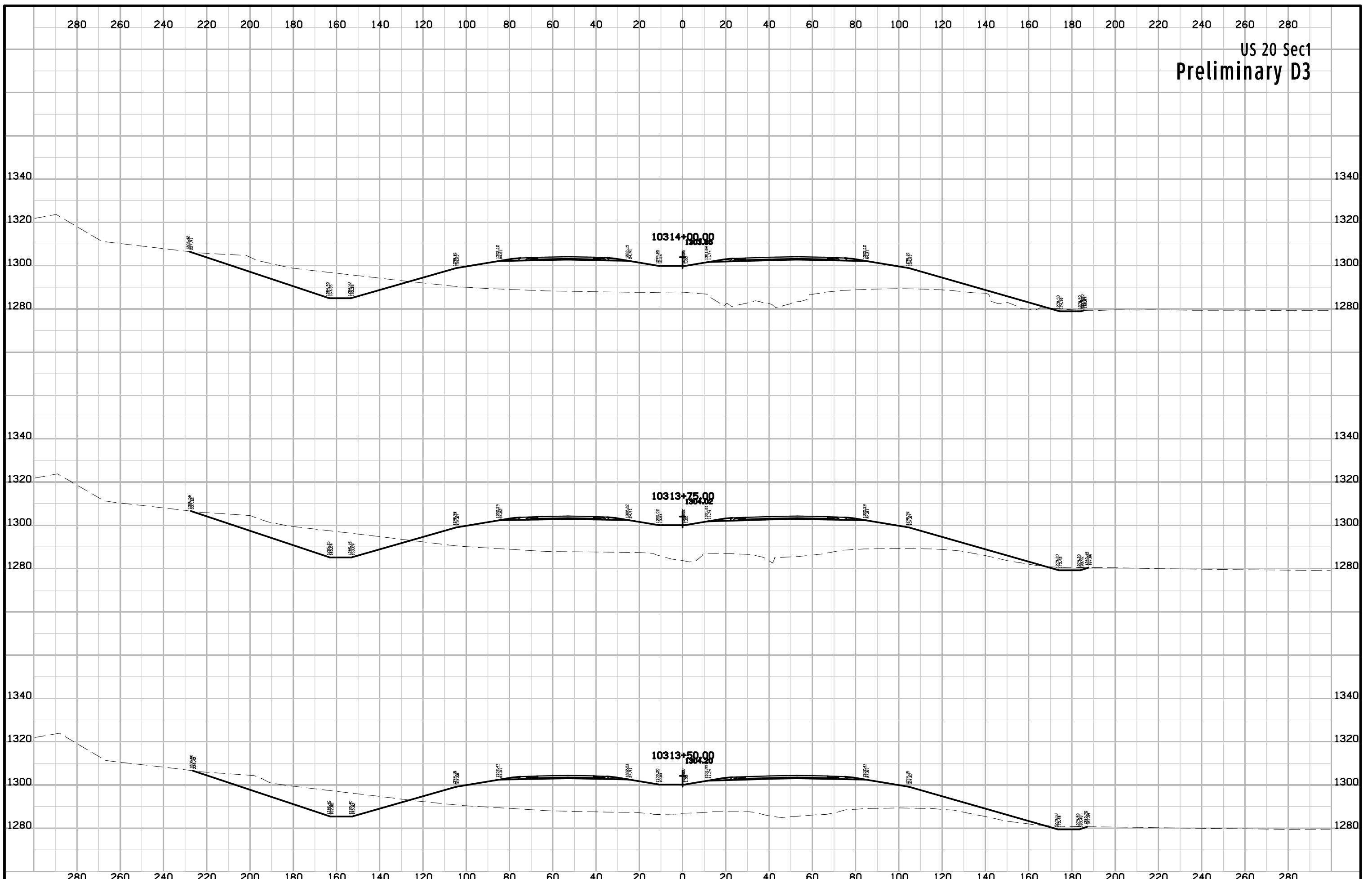
US 20 Sec1
Preliminary D3



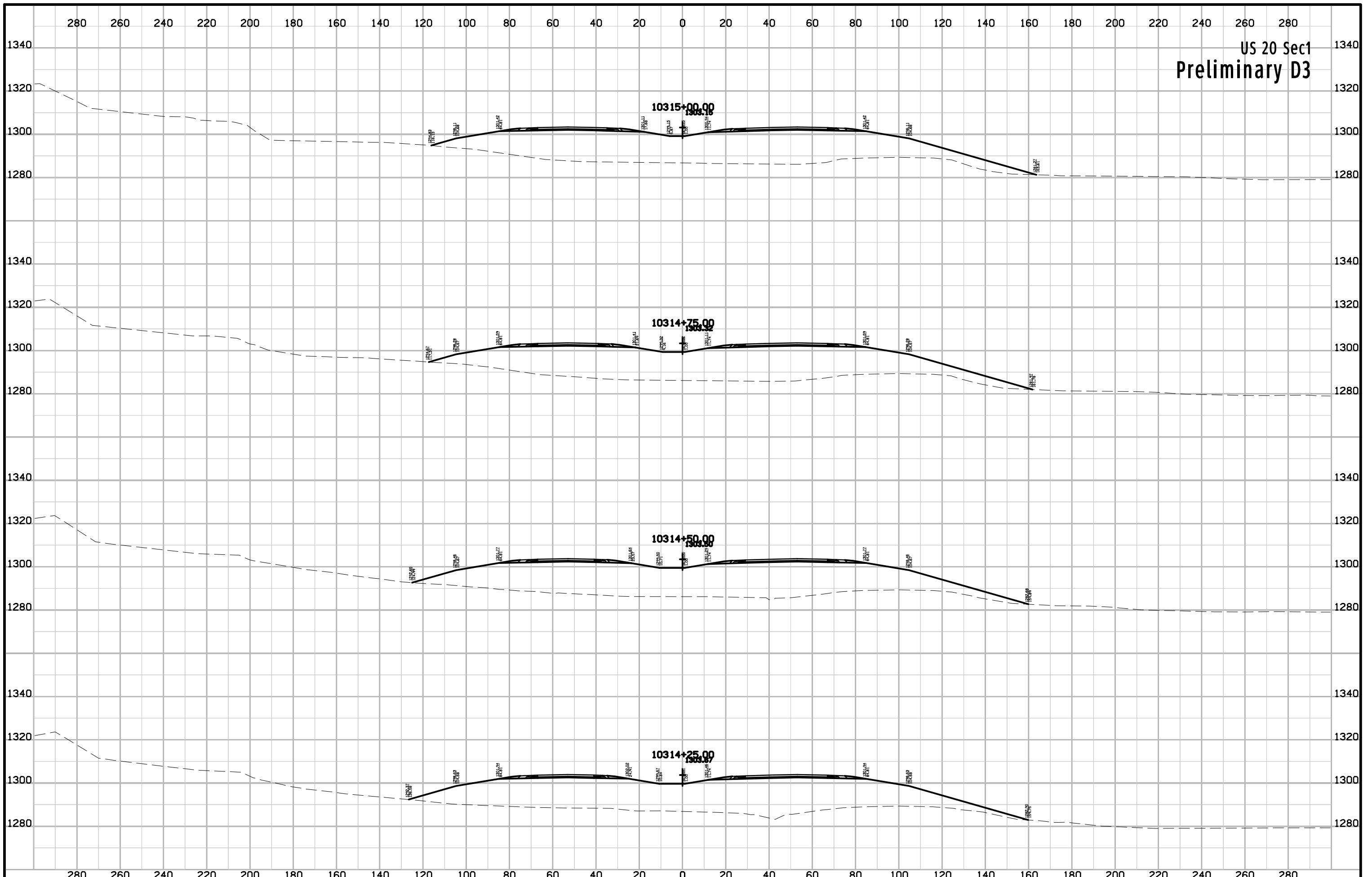
US 20 Sec1
Preliminary D3



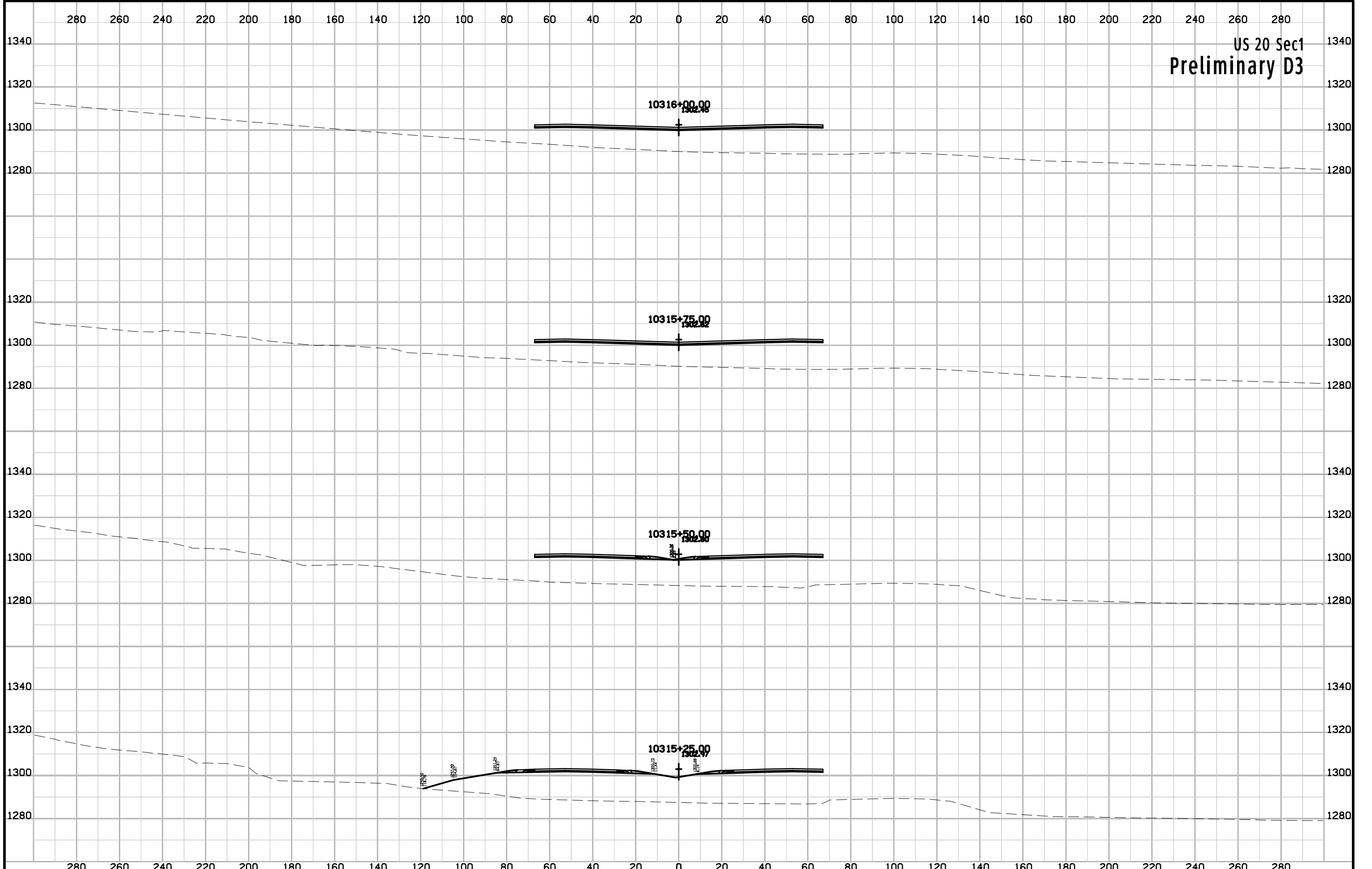
US 20 Sec1
Preliminary D3



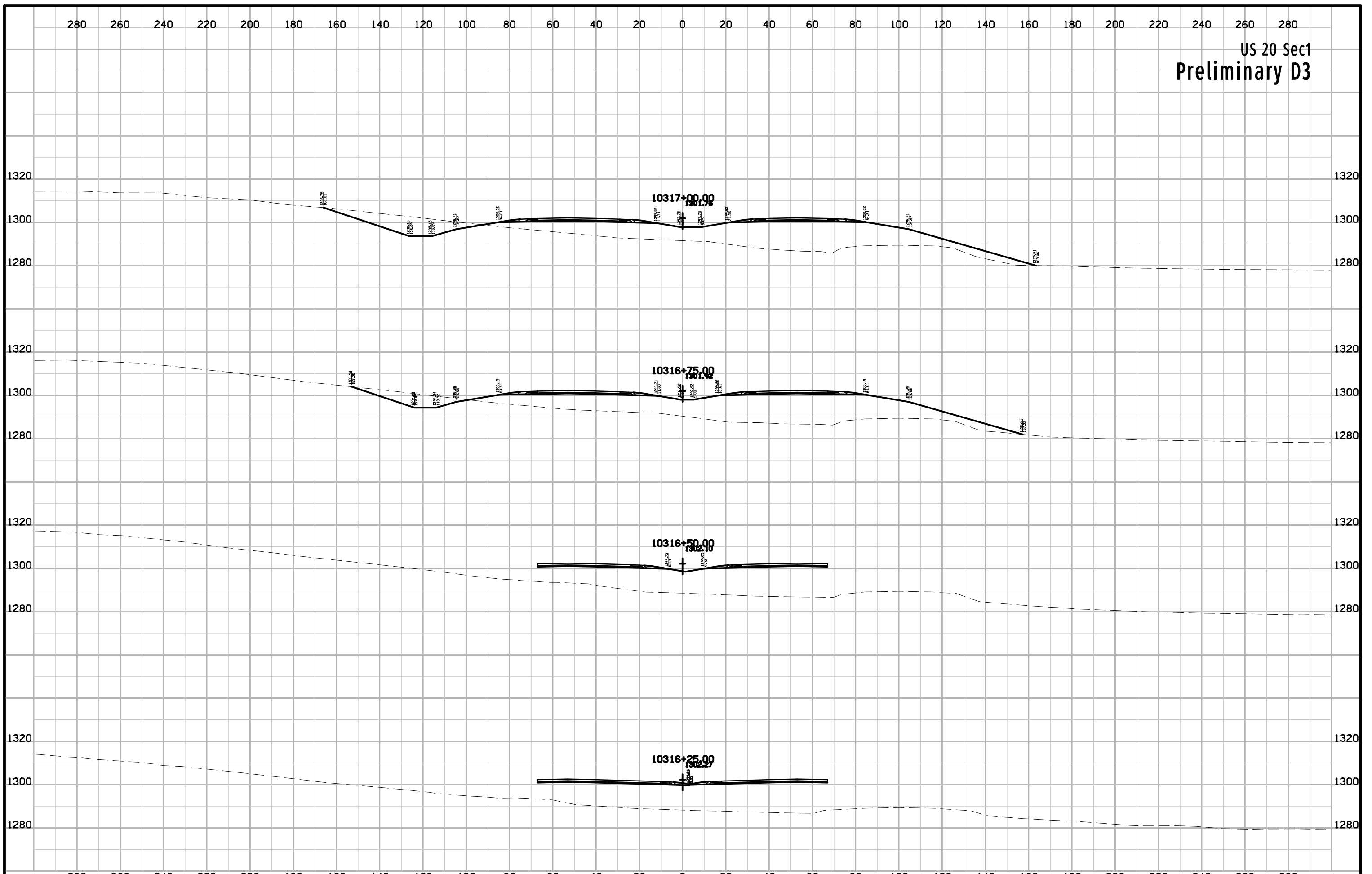
US 20 Sec1
Preliminary D3



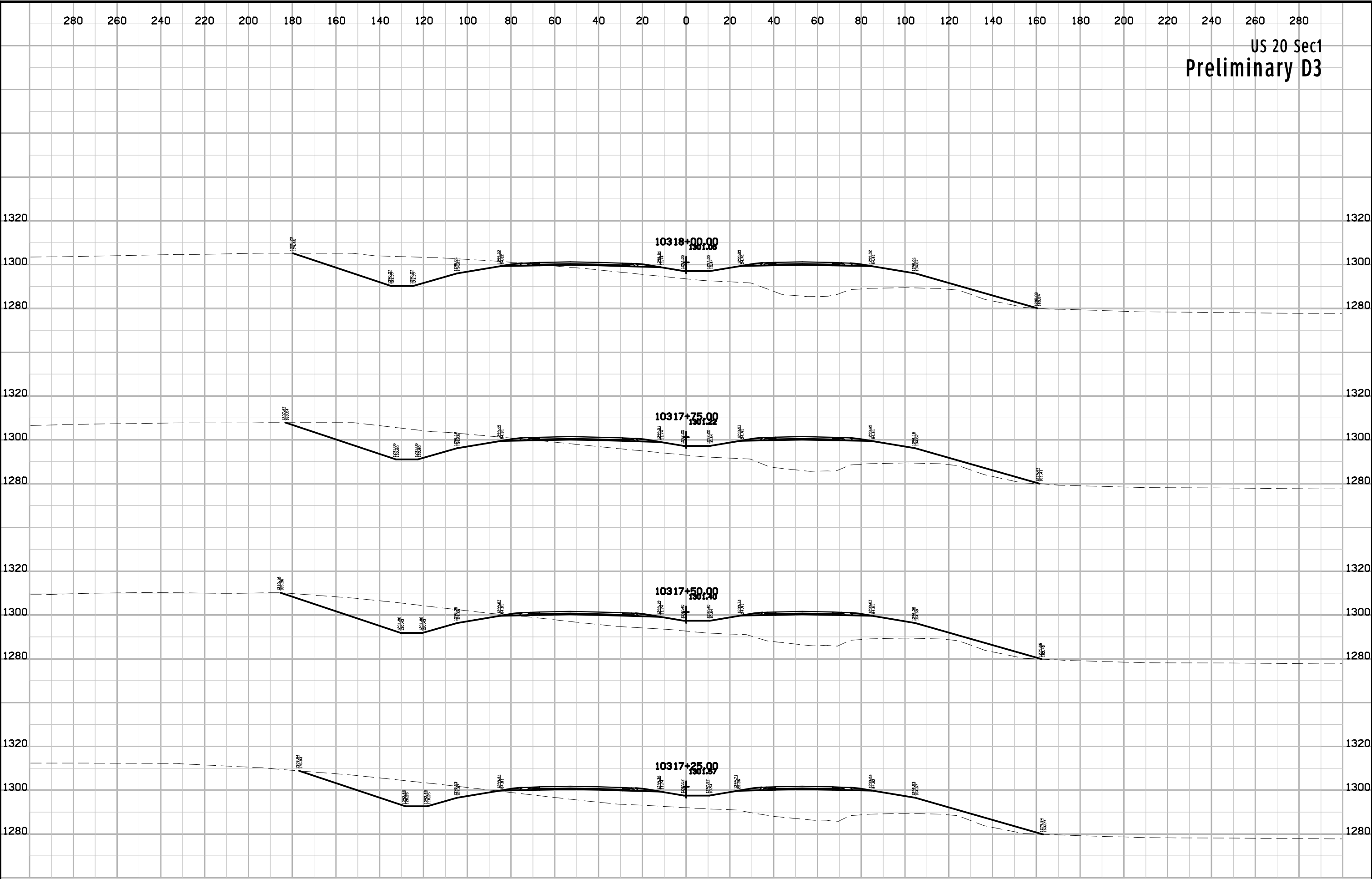
US 20 Sec1
Preliminary D3



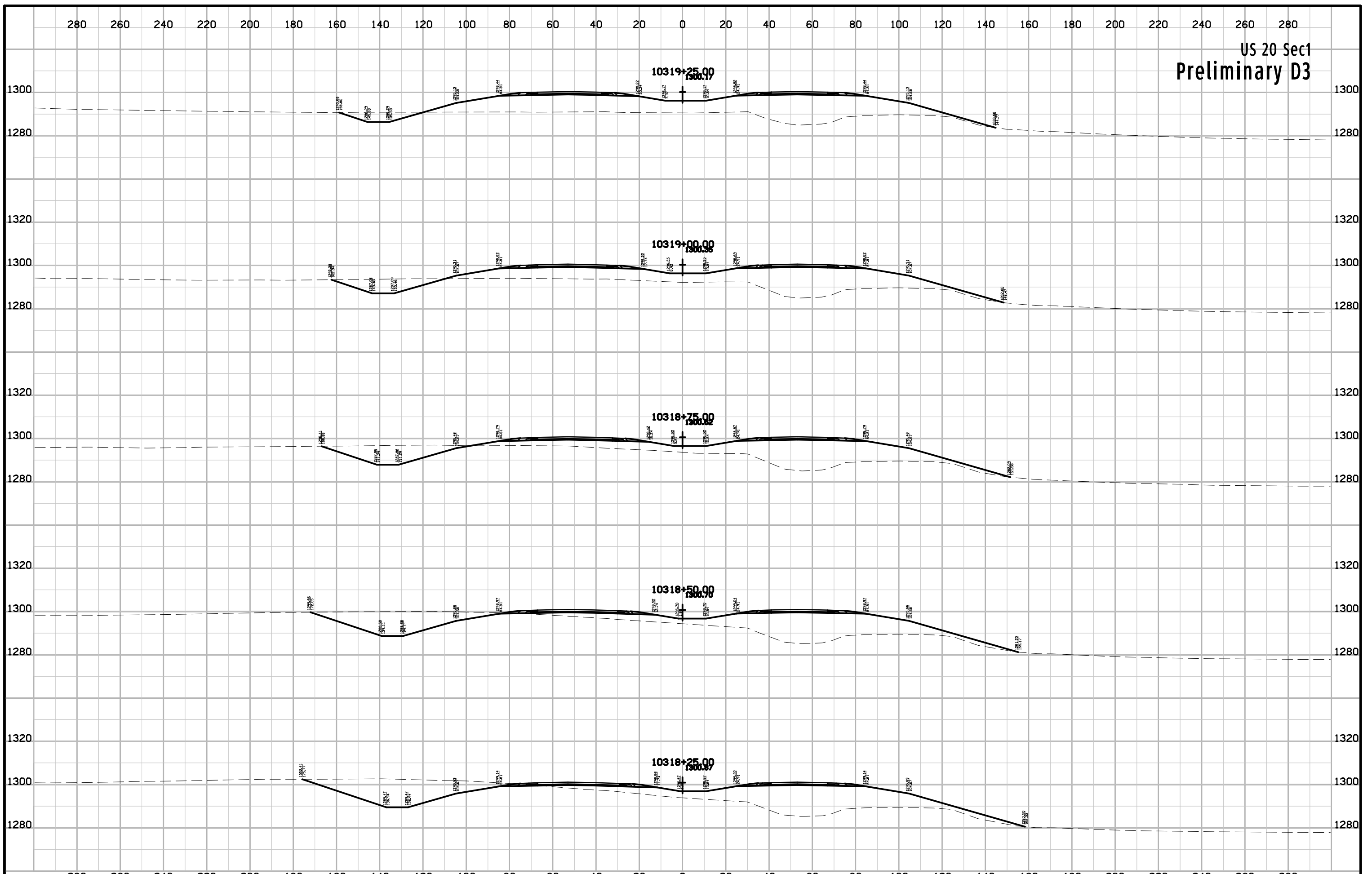
US 20 Sec1
Preliminary D3



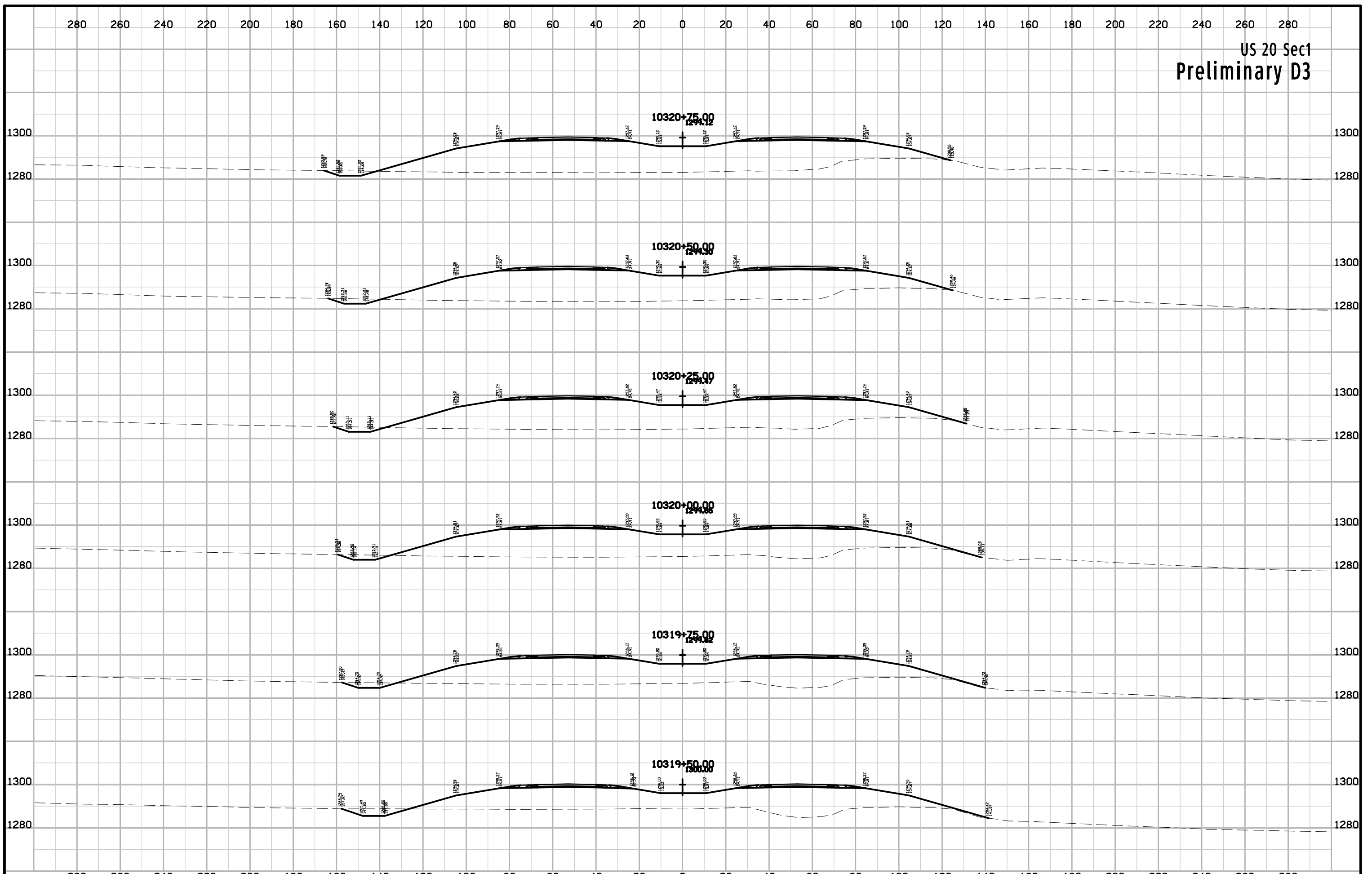
US 20 Sec1
Preliminary D3



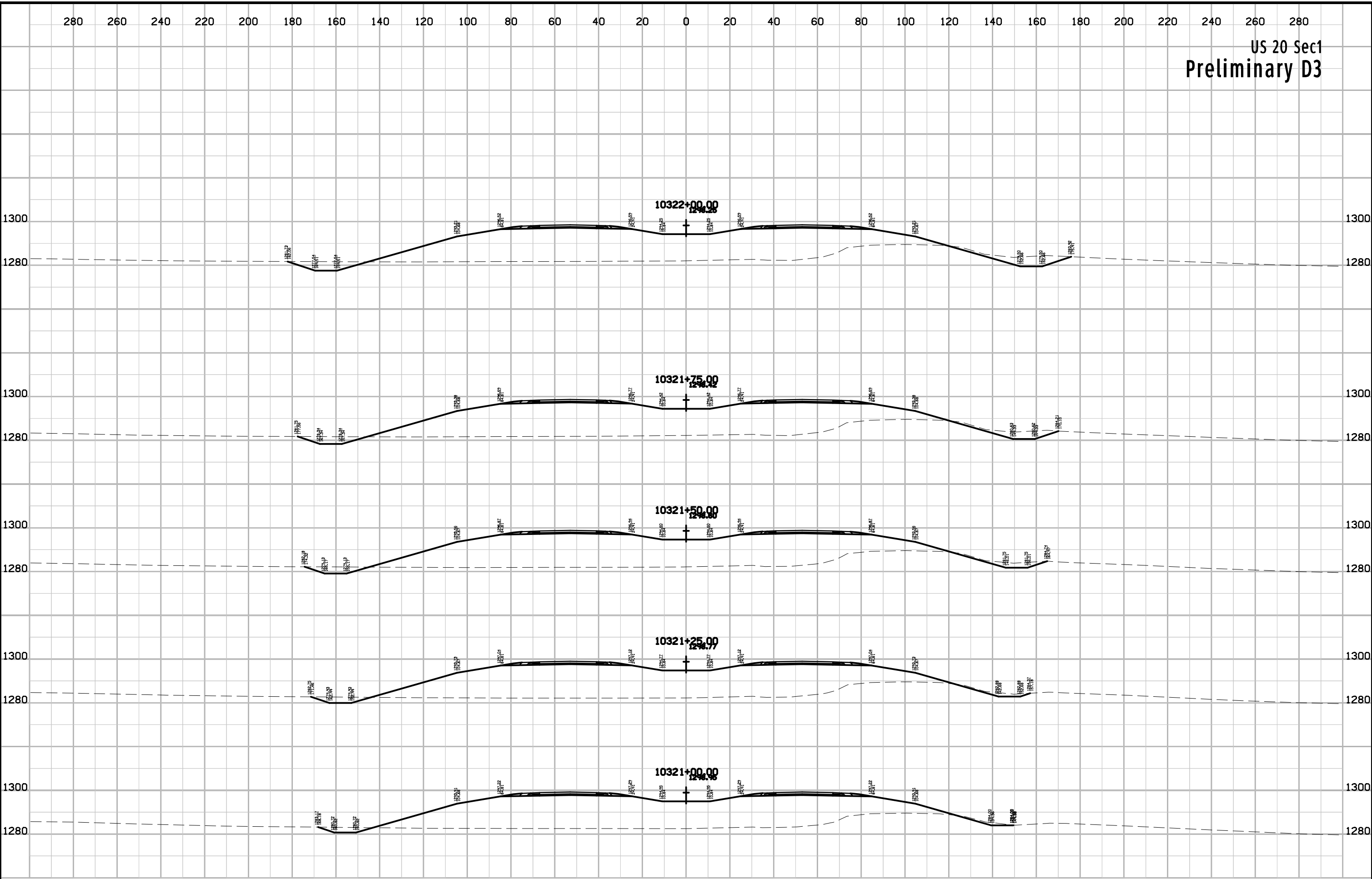
US 20 Sec1
Preliminary D3



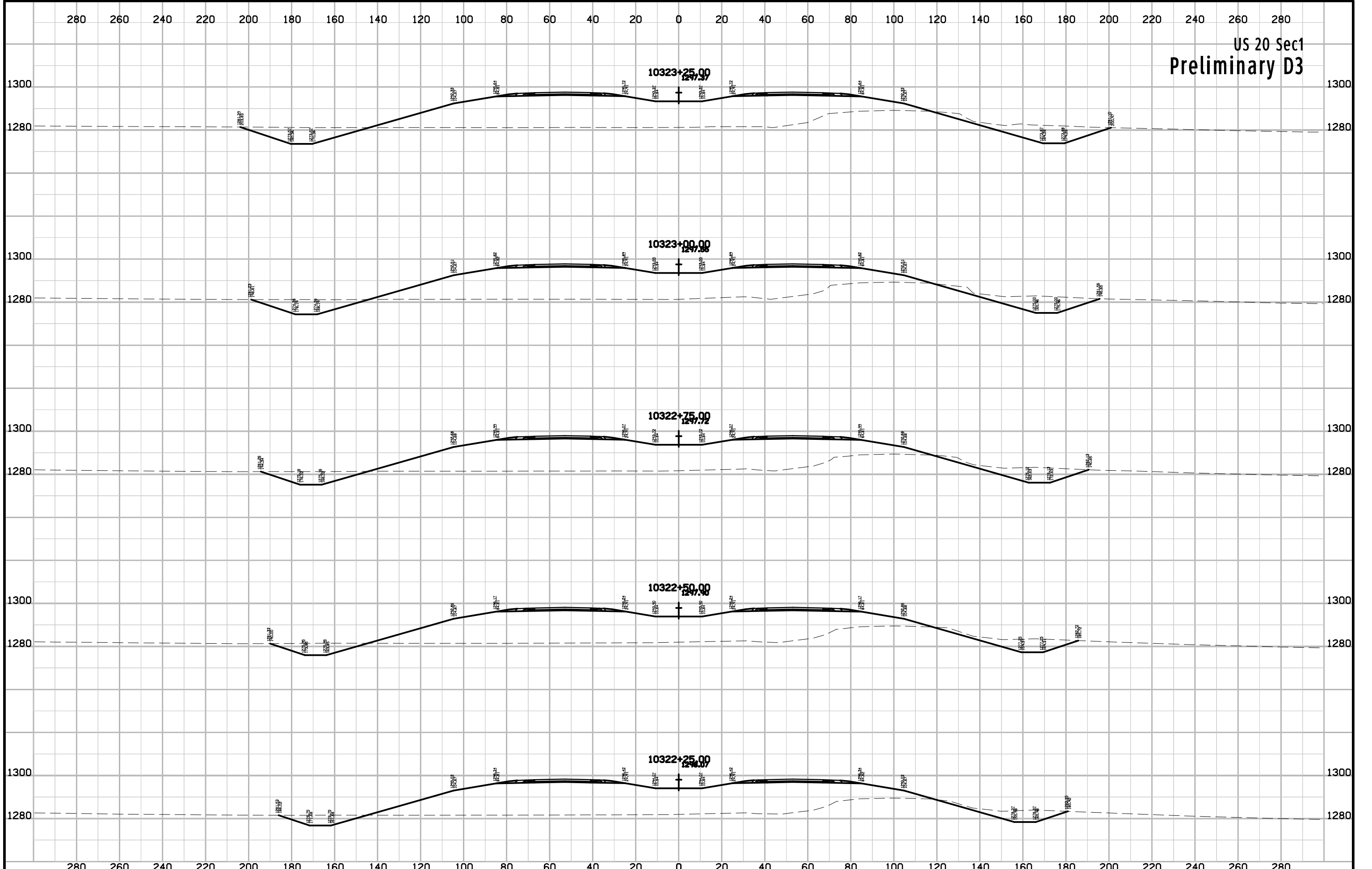
US 20 Sec1
Preliminary D3



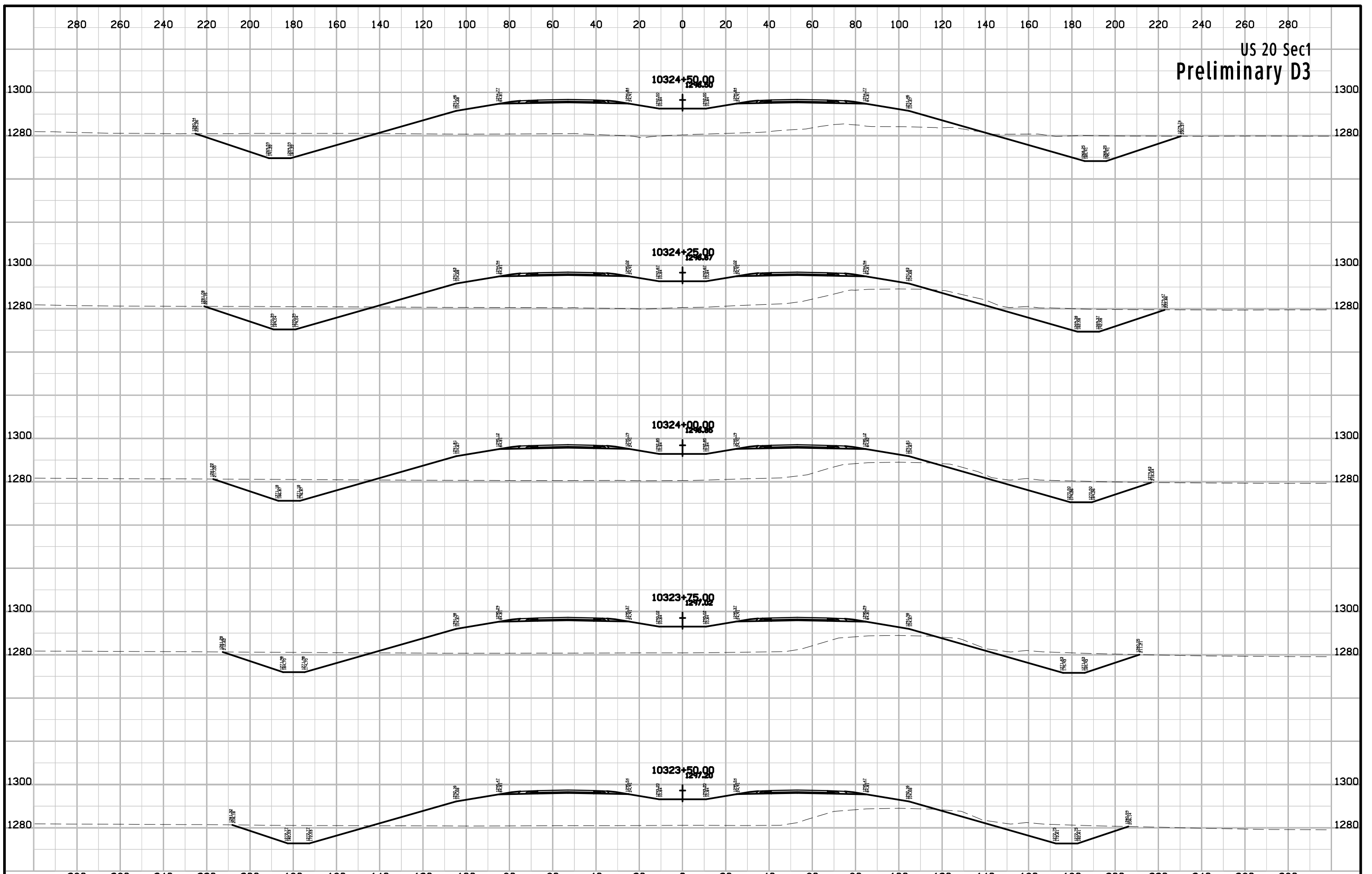
US 20 Sec1
Preliminary D3



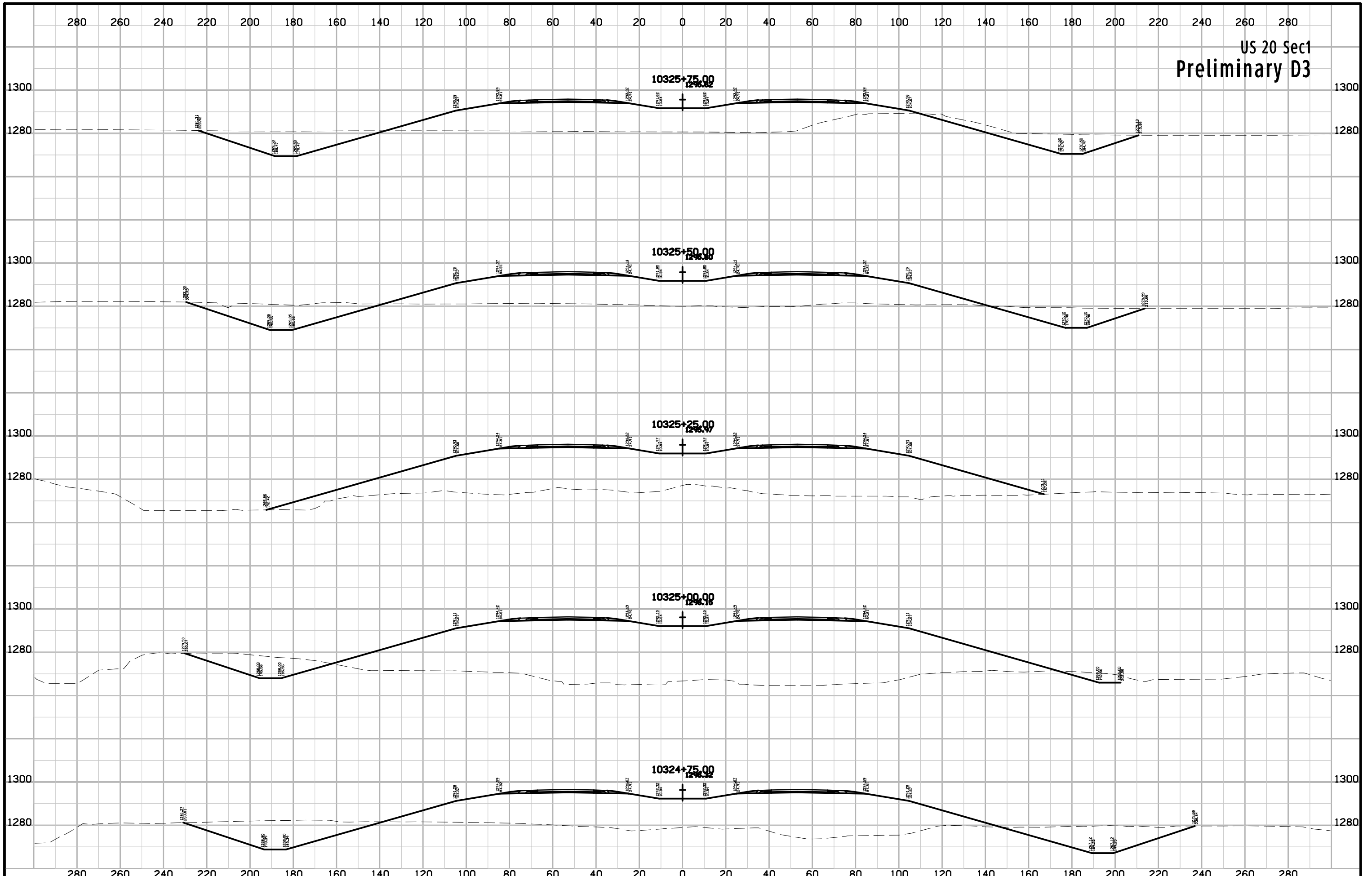
US 20 Sec1
Preliminary D3



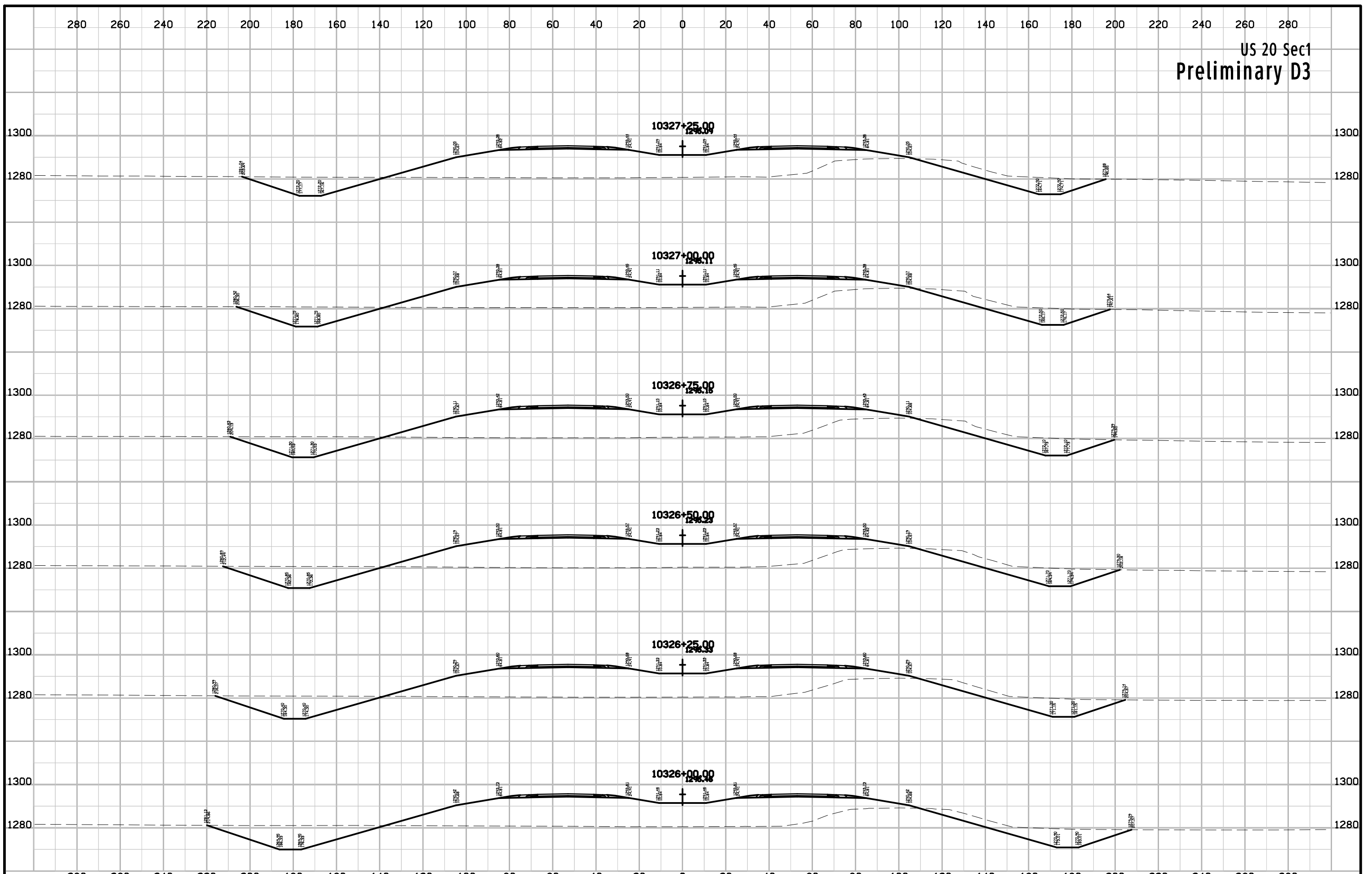
US 20 Sec1
Preliminary D3



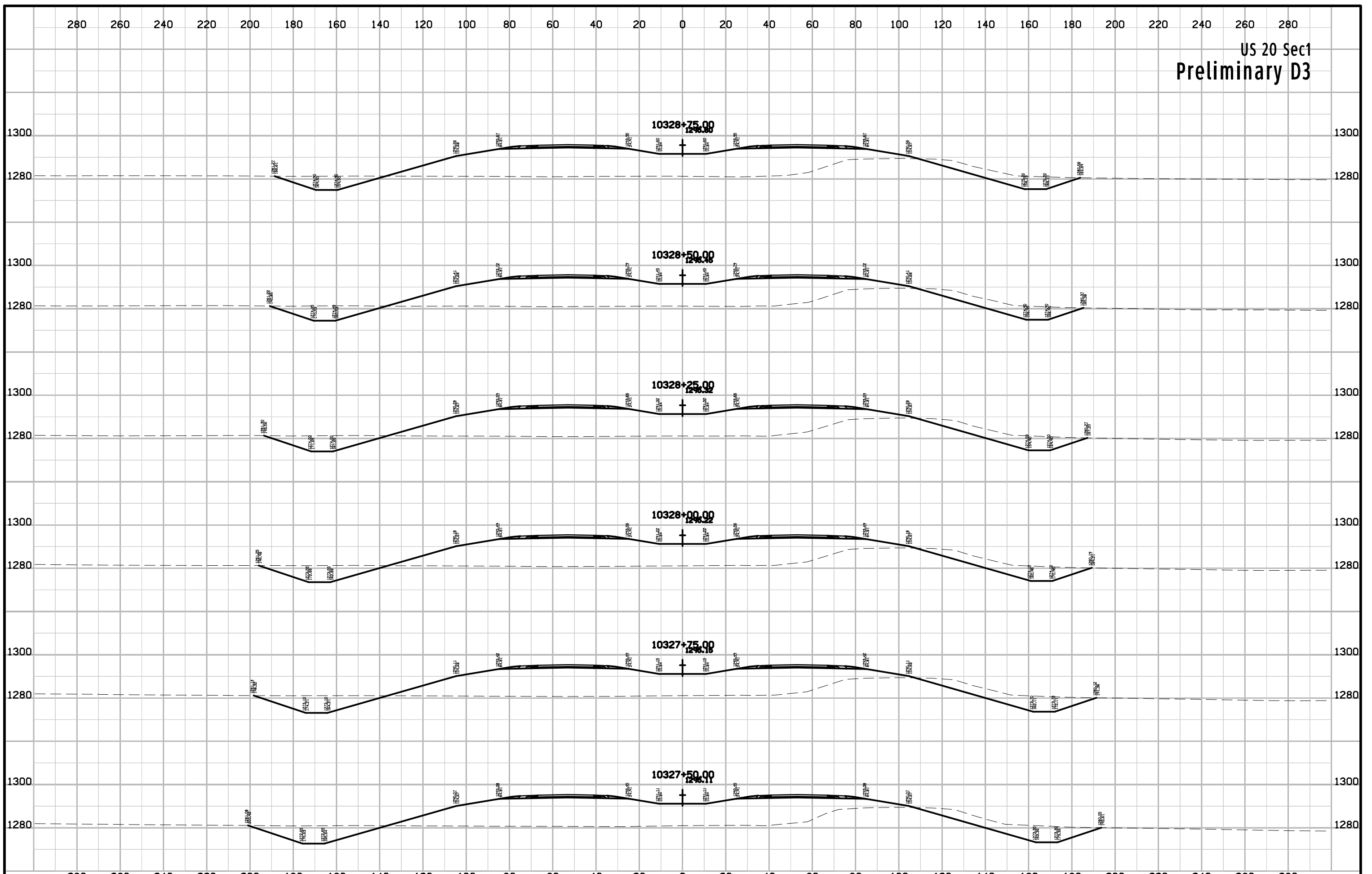
US 20 Sec1
Preliminary D3



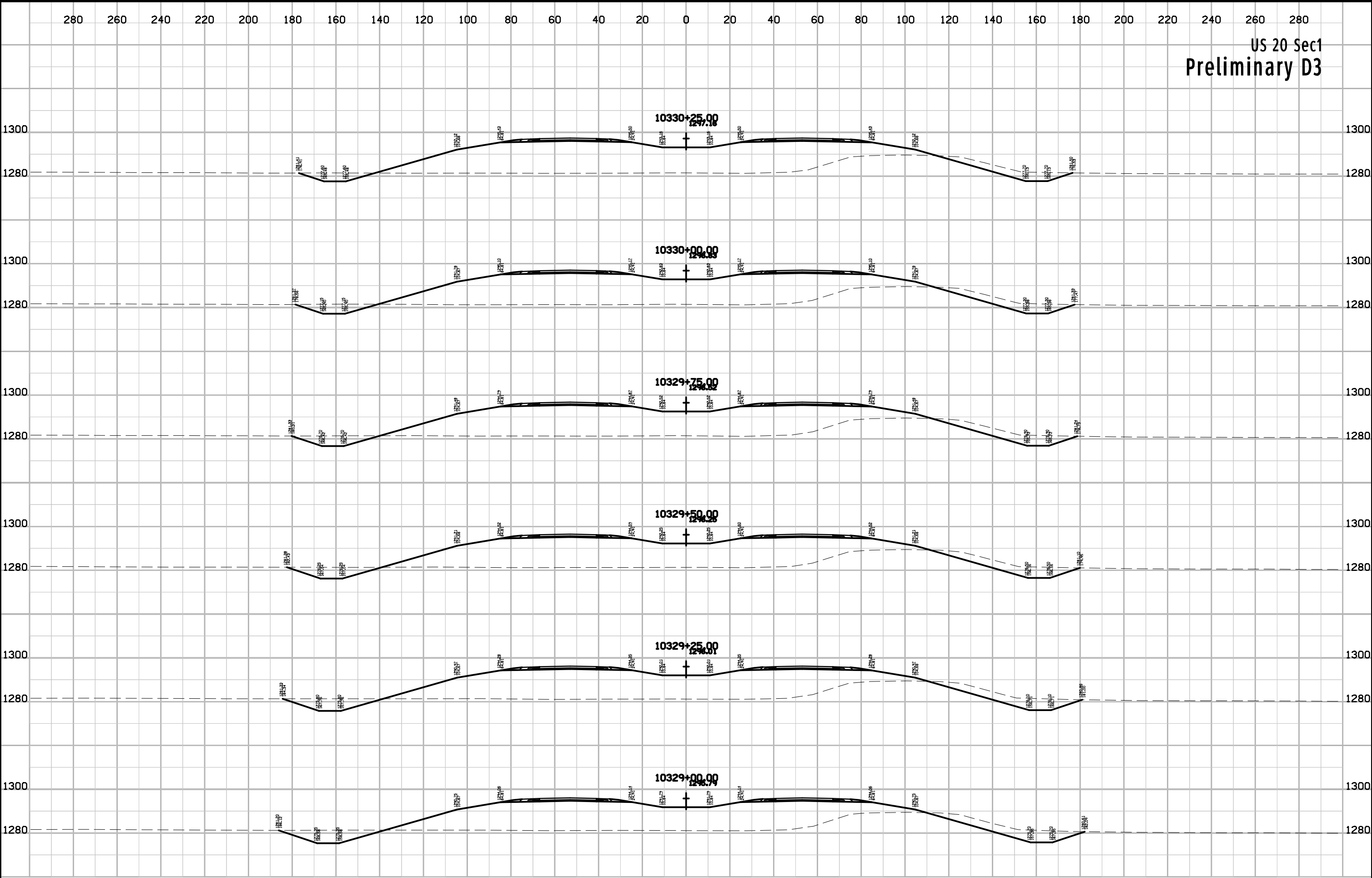
US 20 Sec1
Preliminary D3



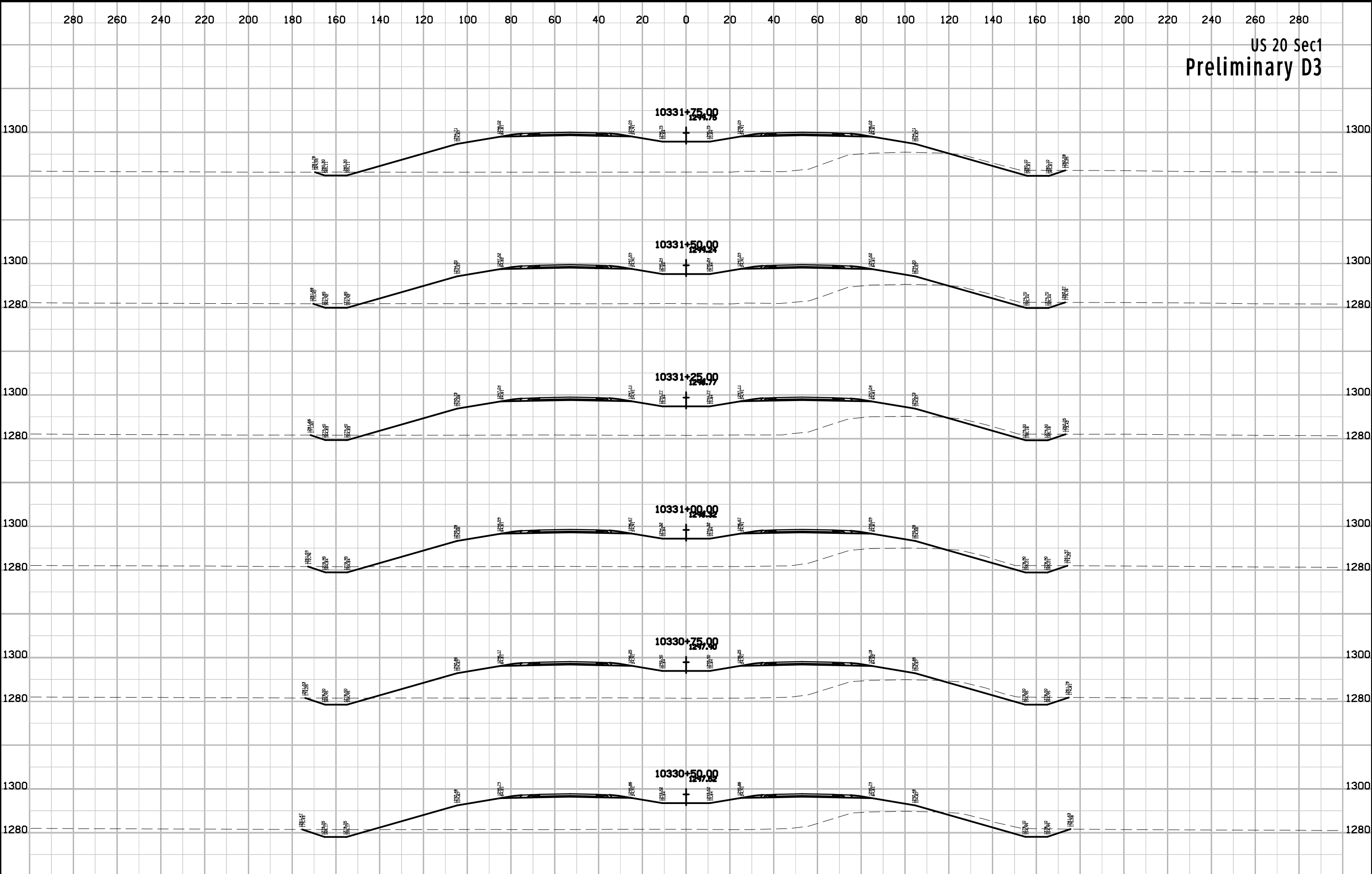
US 20 Sec1
Preliminary D3



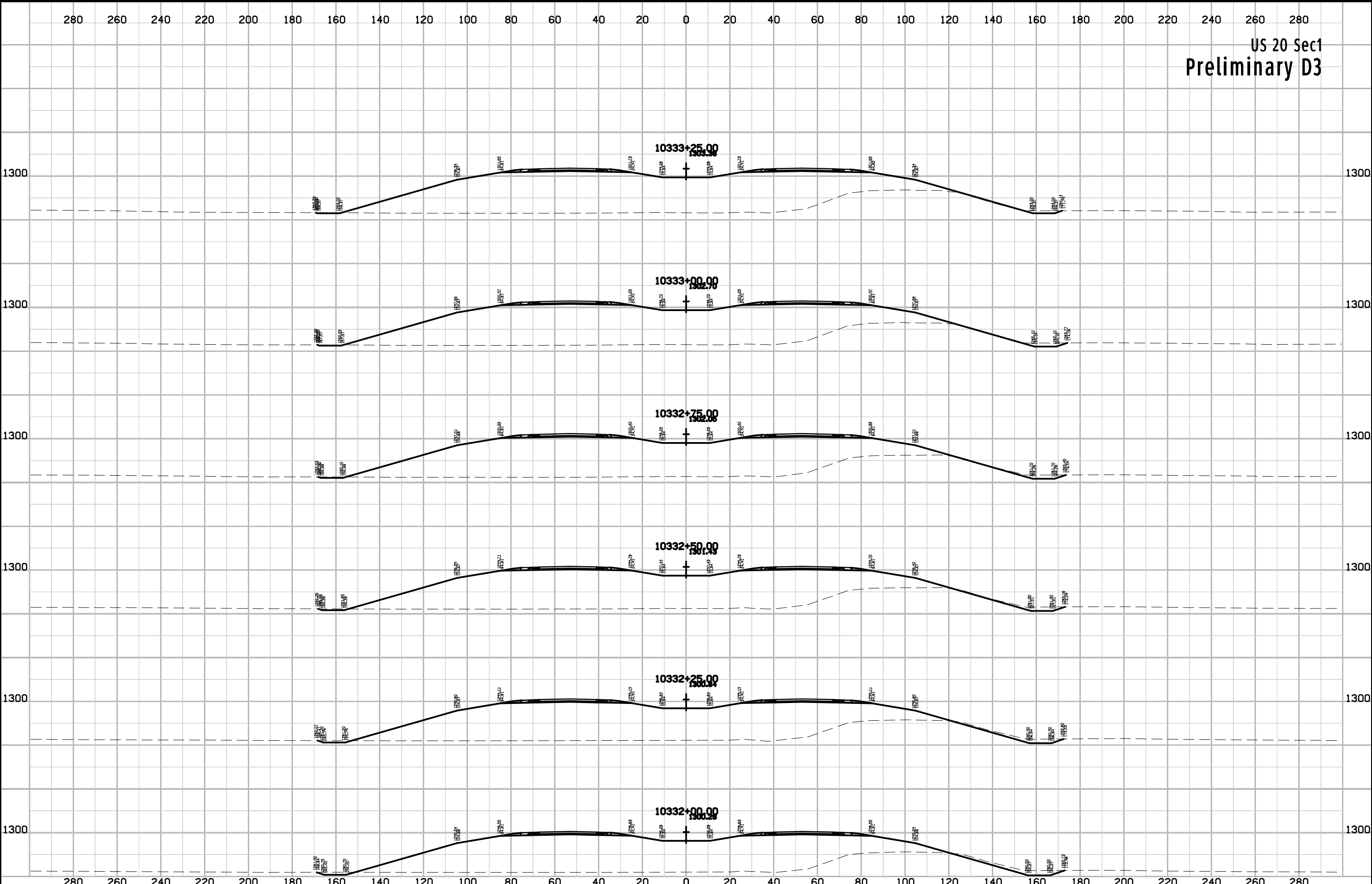
US 20 Sec1
Preliminary D3



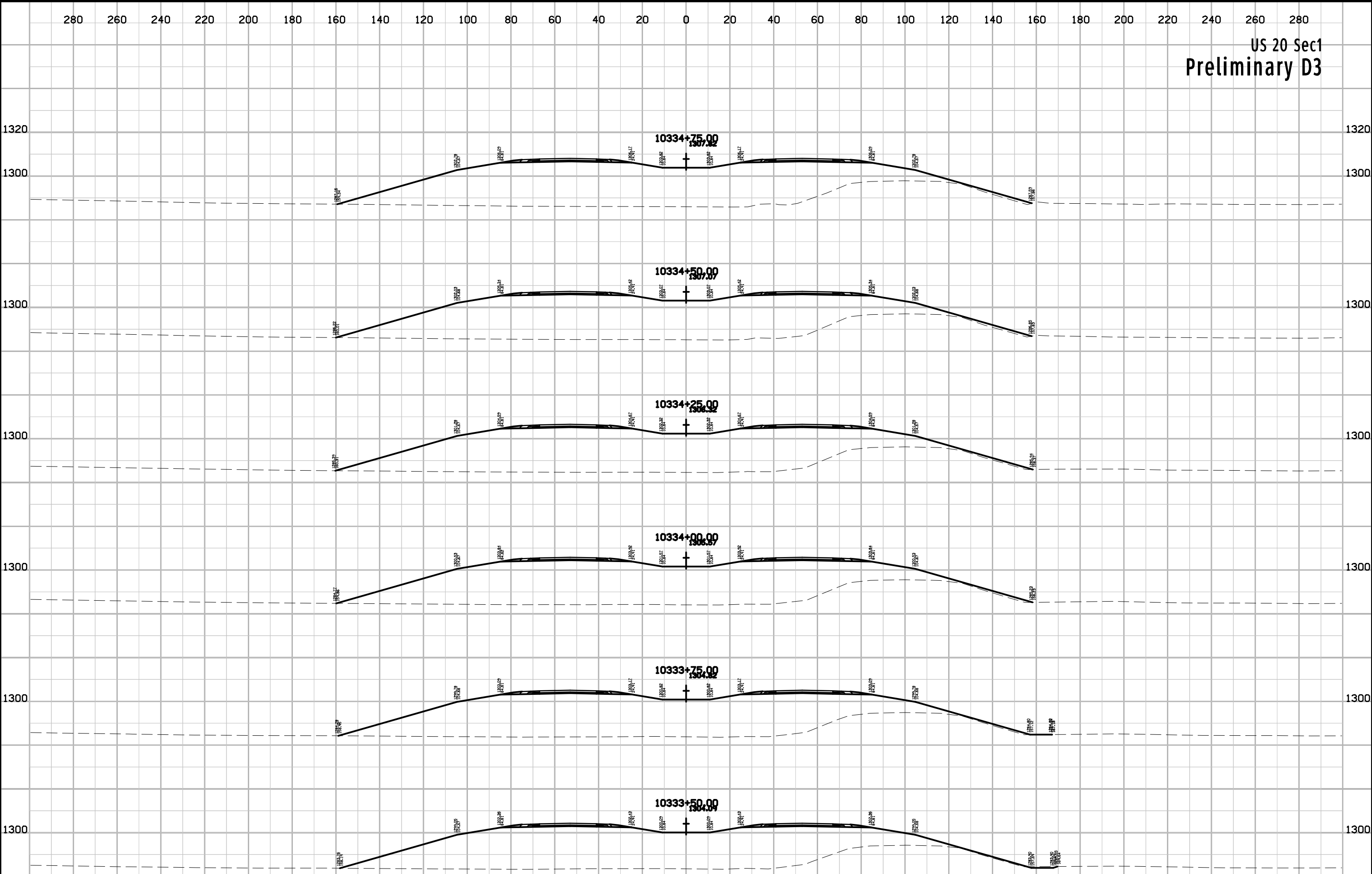
US 20 Sec1
Preliminary D3



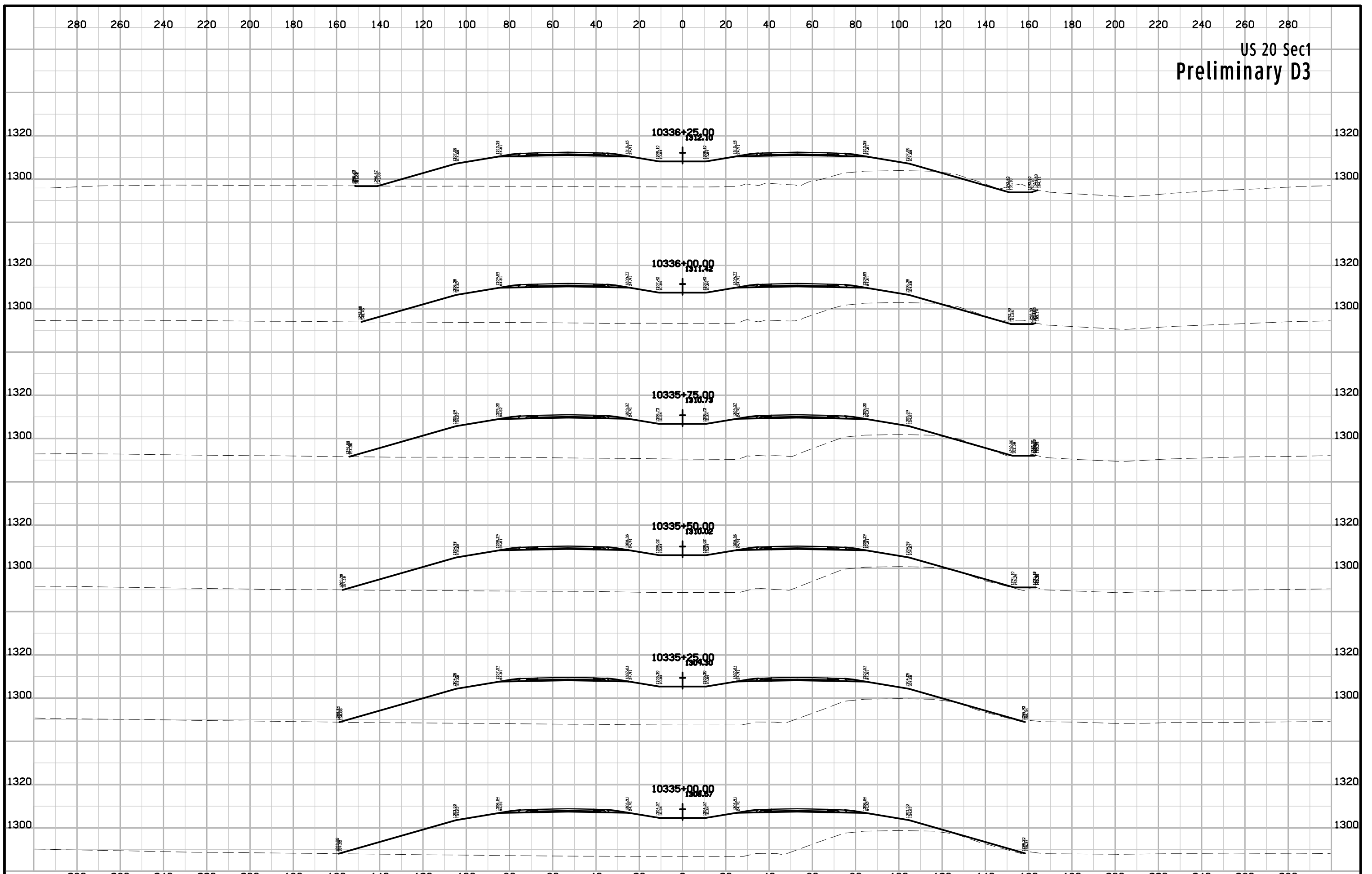
US 20 Sec1
Preliminary D3



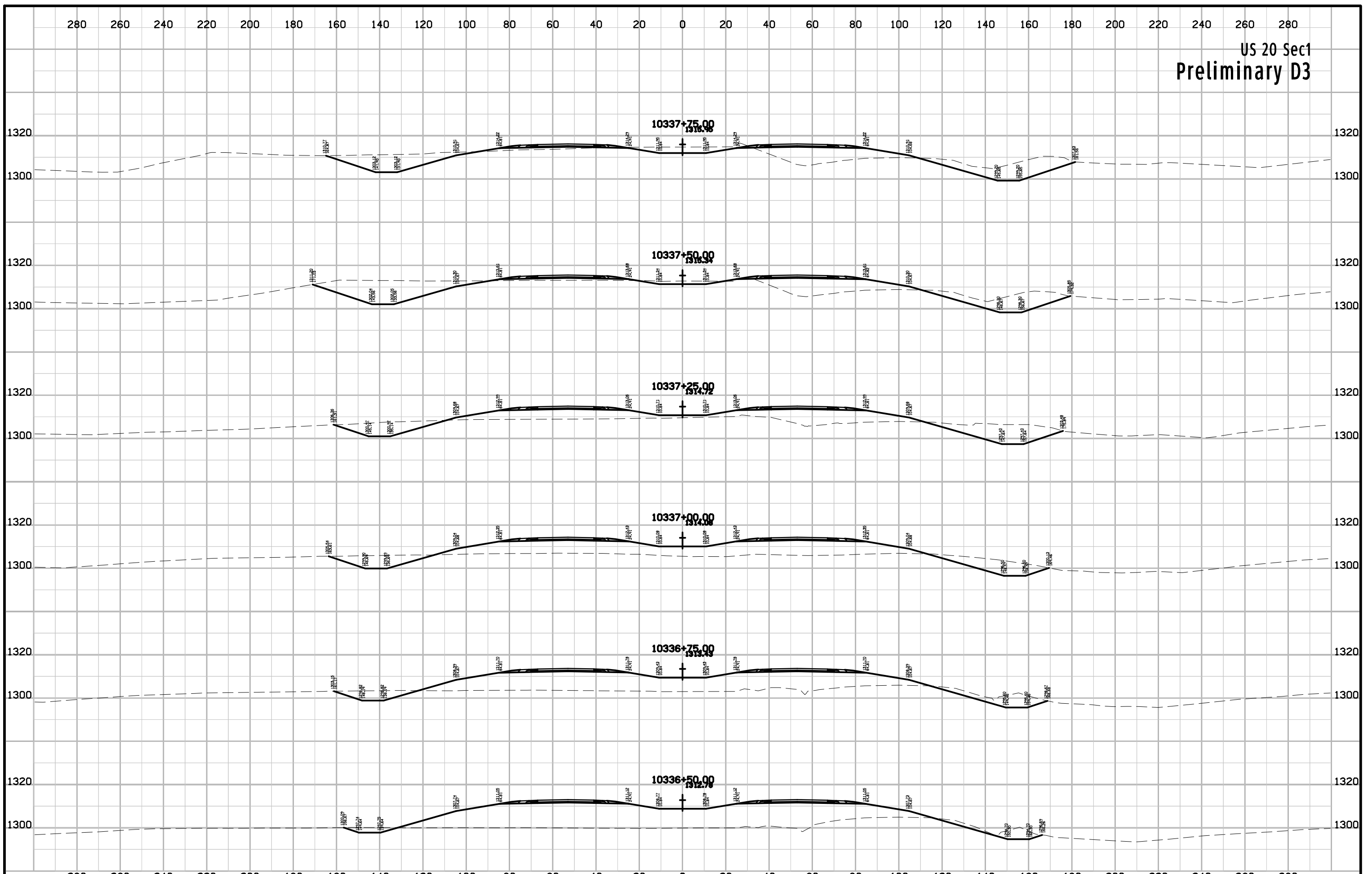
US 20 Sec1
Preliminary D3



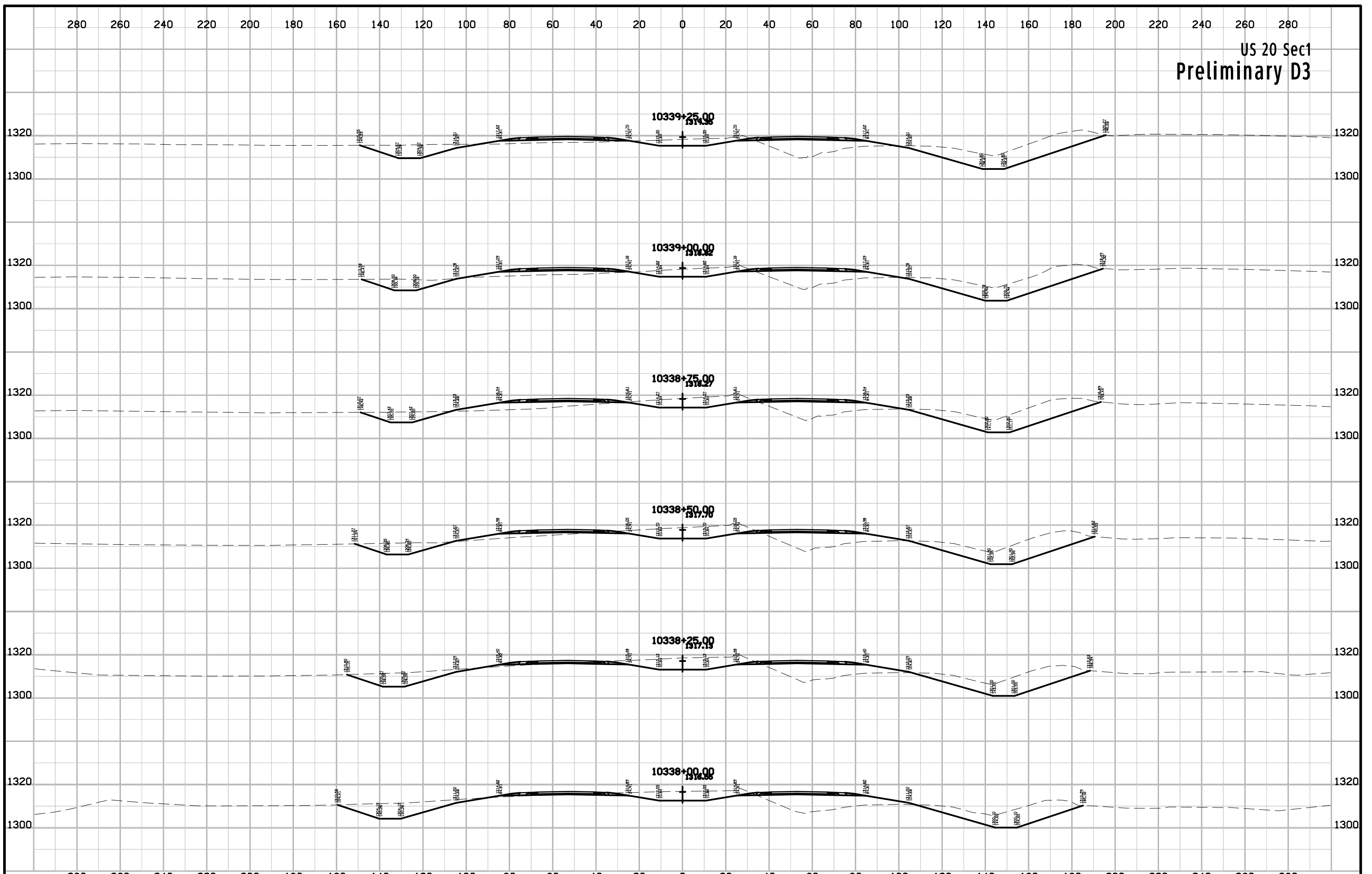
US 20 Sec1
Preliminary D3



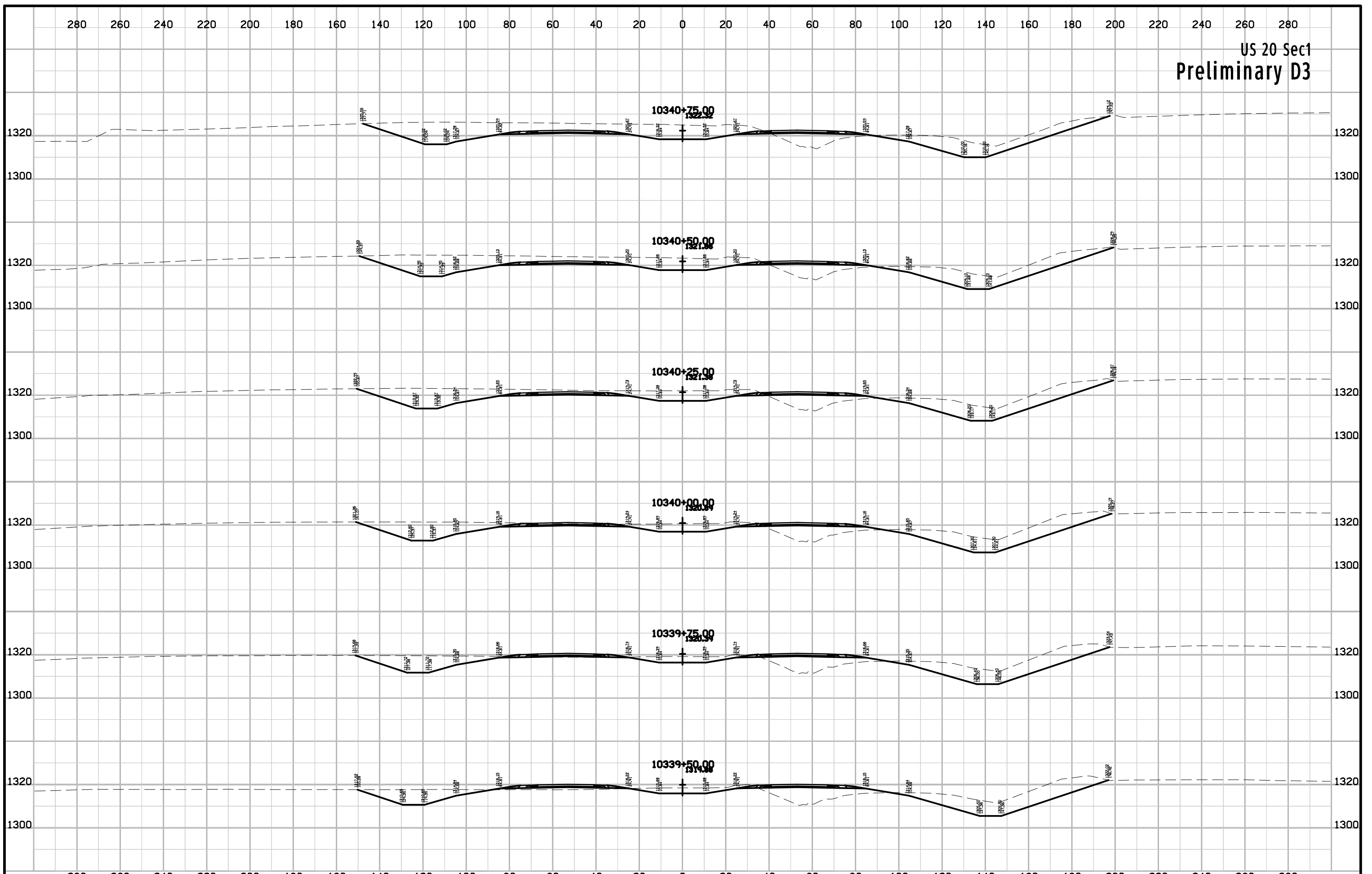
US 20 Sec1
Preliminary D3



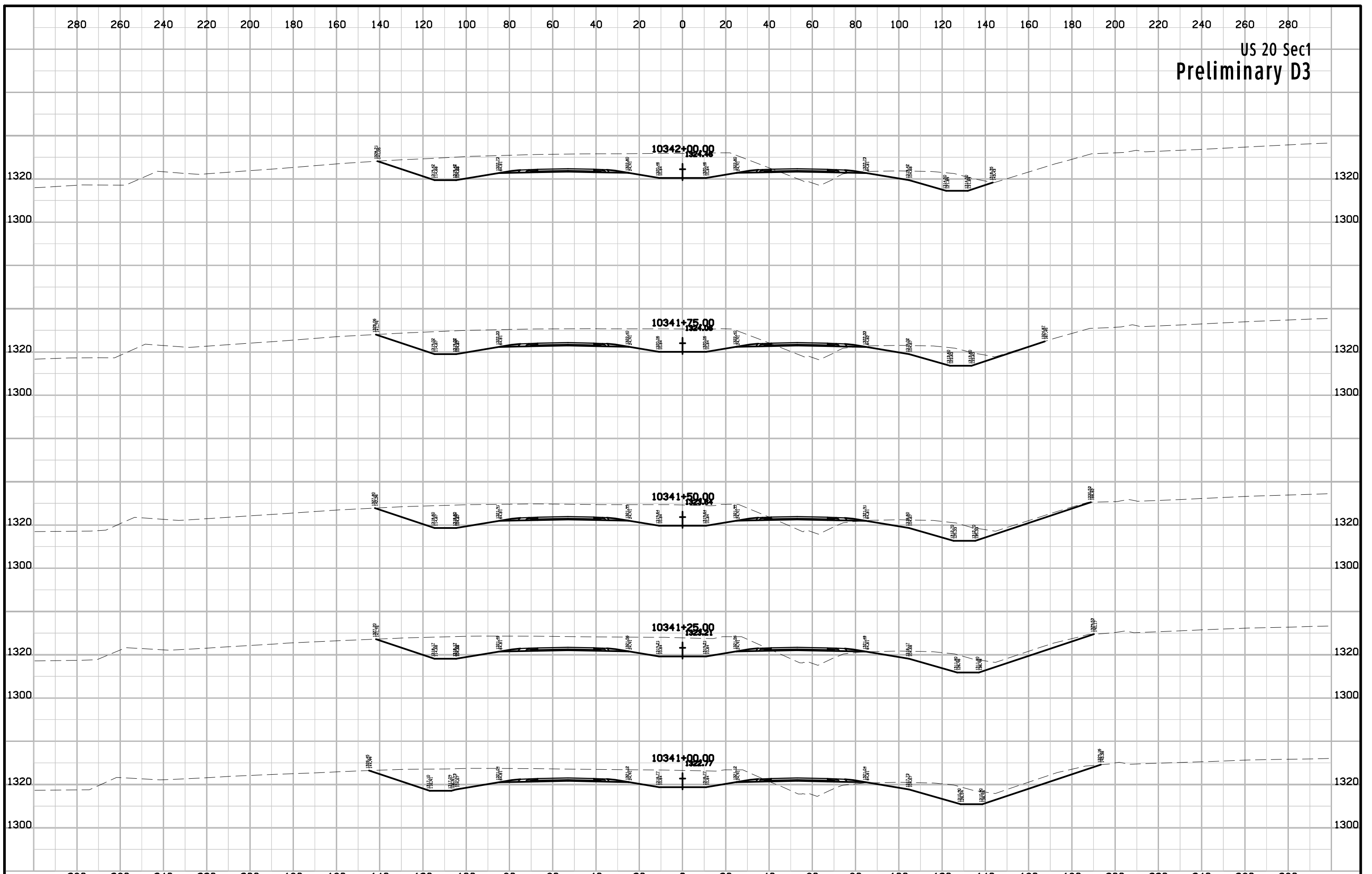
US 20 Sec1
Preliminary D3

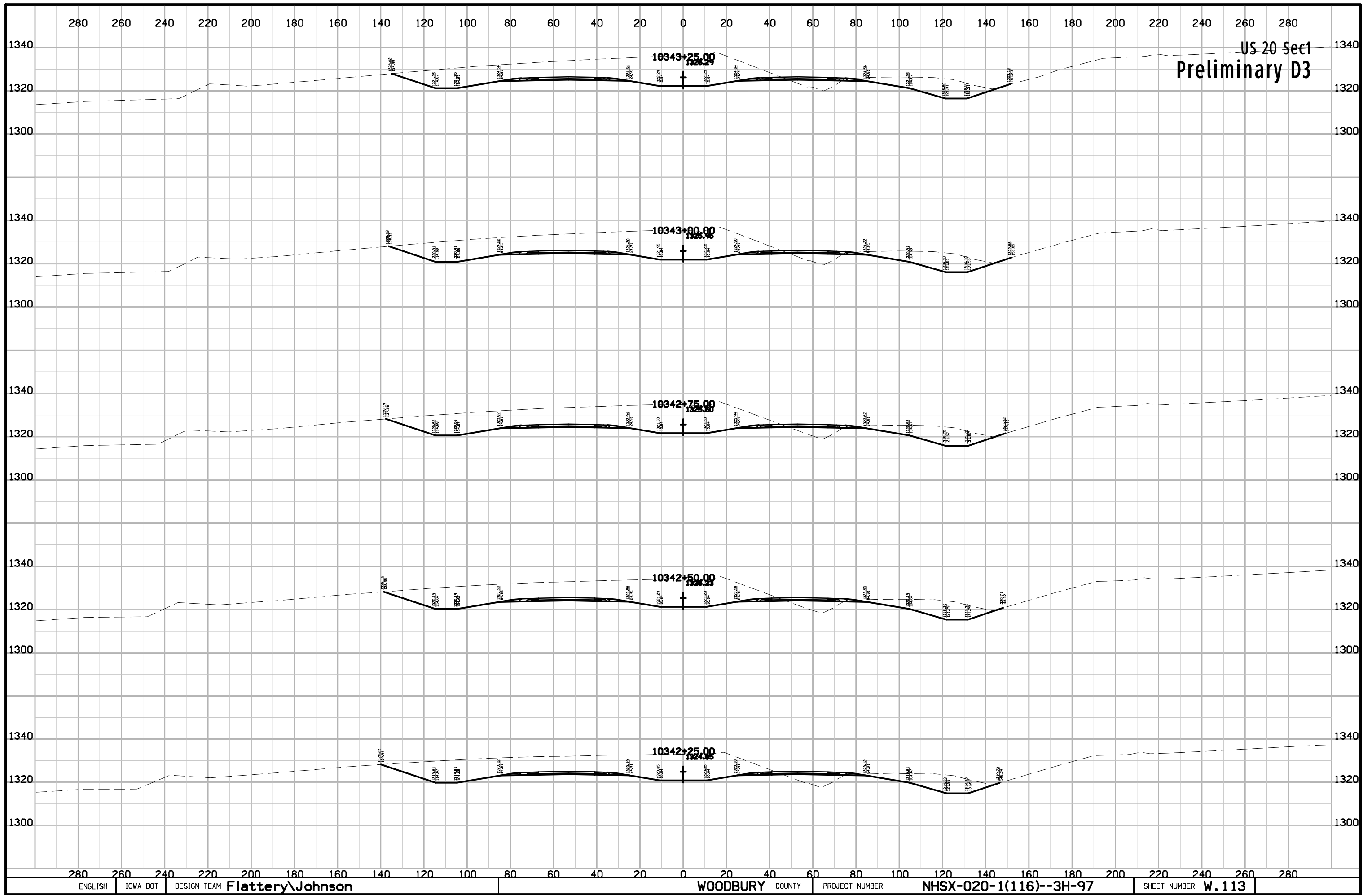


US 20 Sec1
Preliminary D3



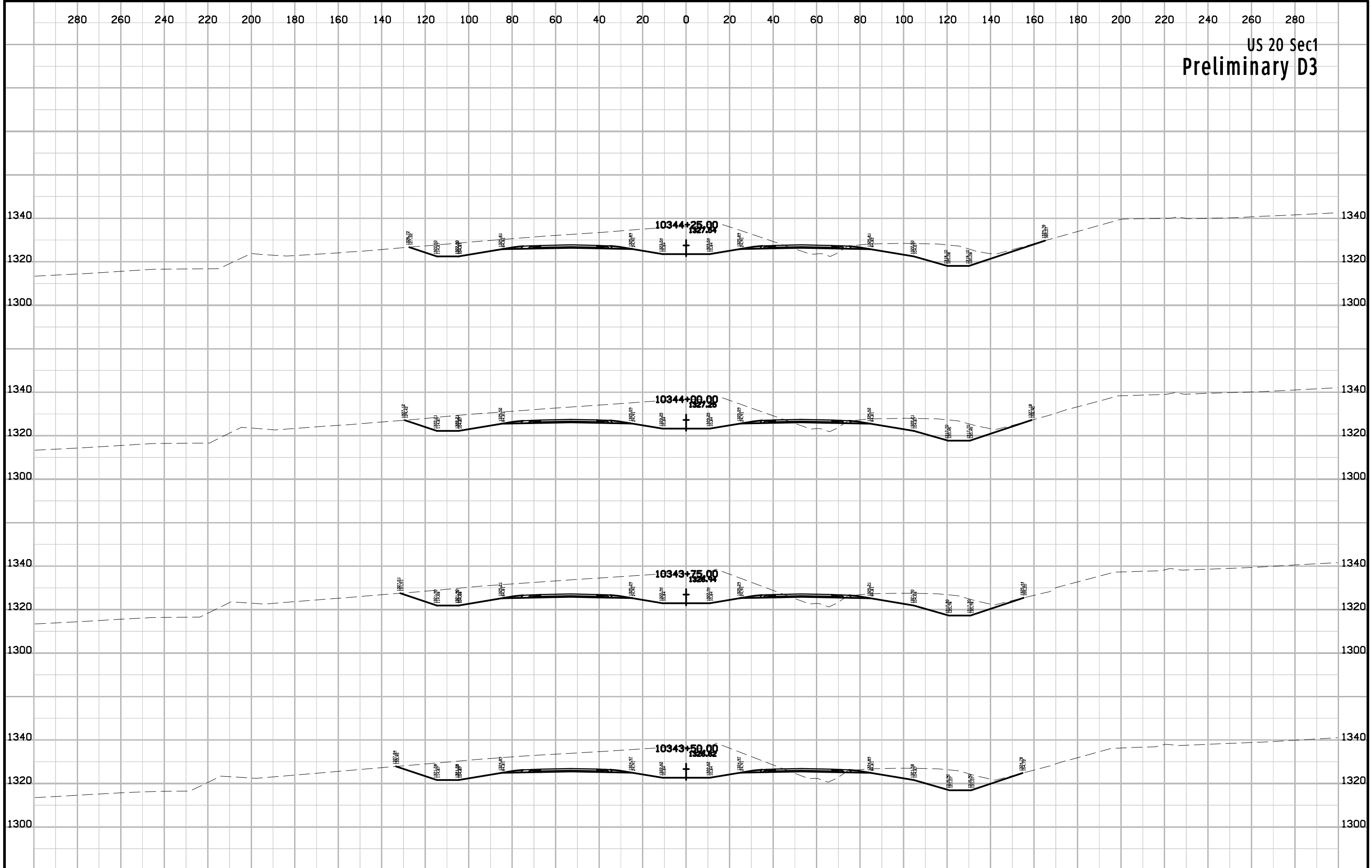
US 20 Sec1
Preliminary D3



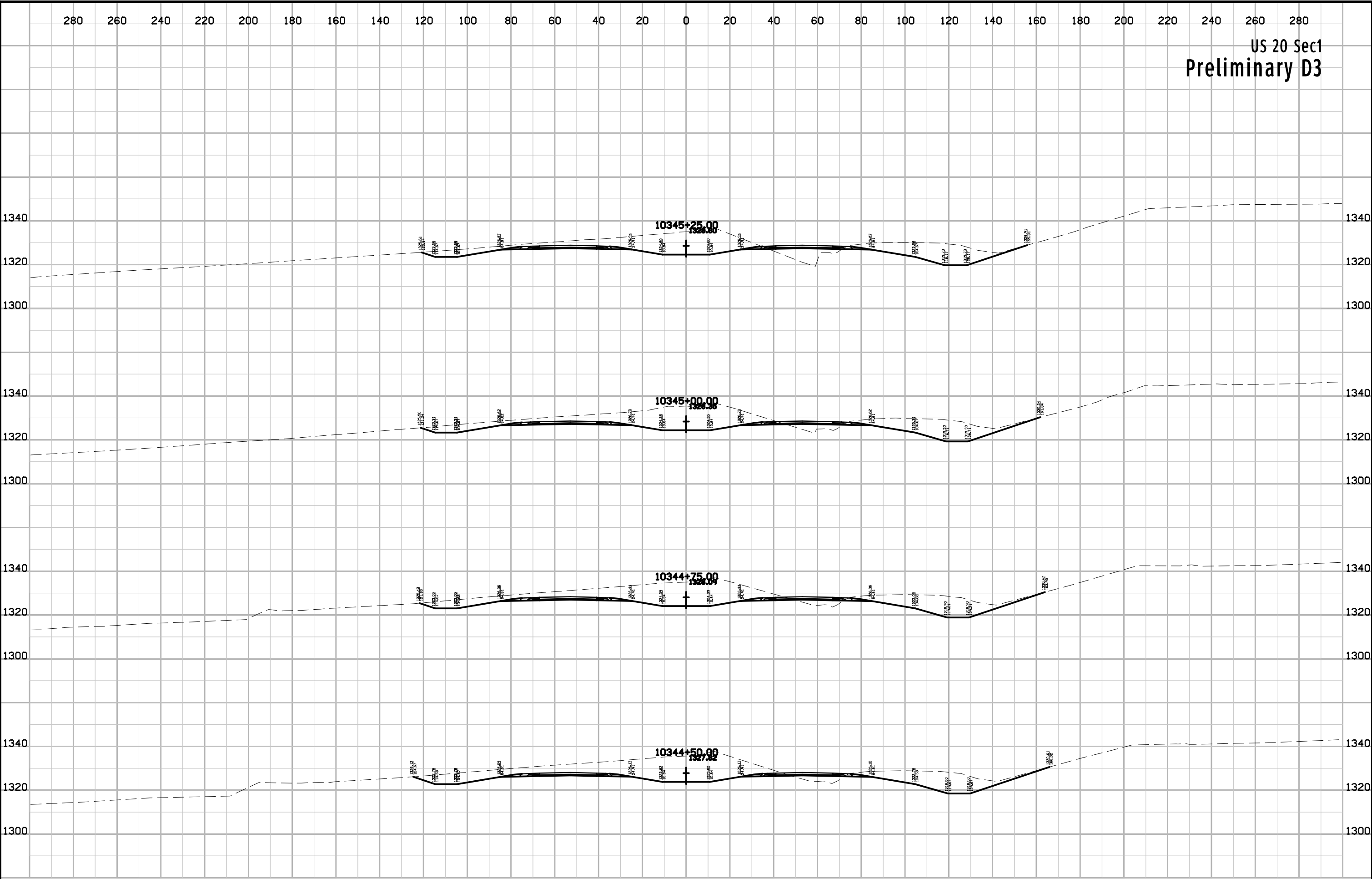


US-20 Sec1
Preliminary D3

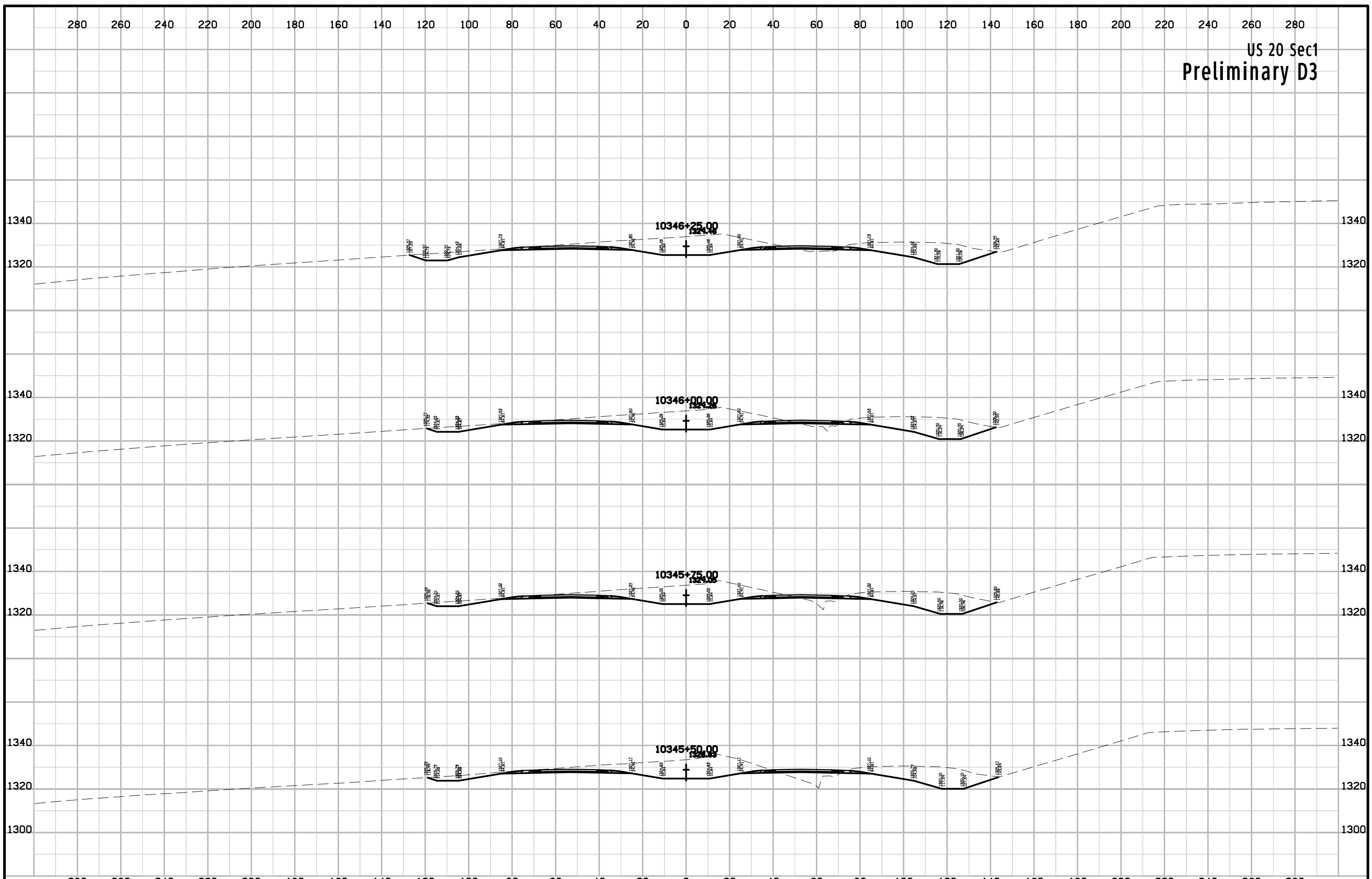
US 20 Sec1
Preliminary D3

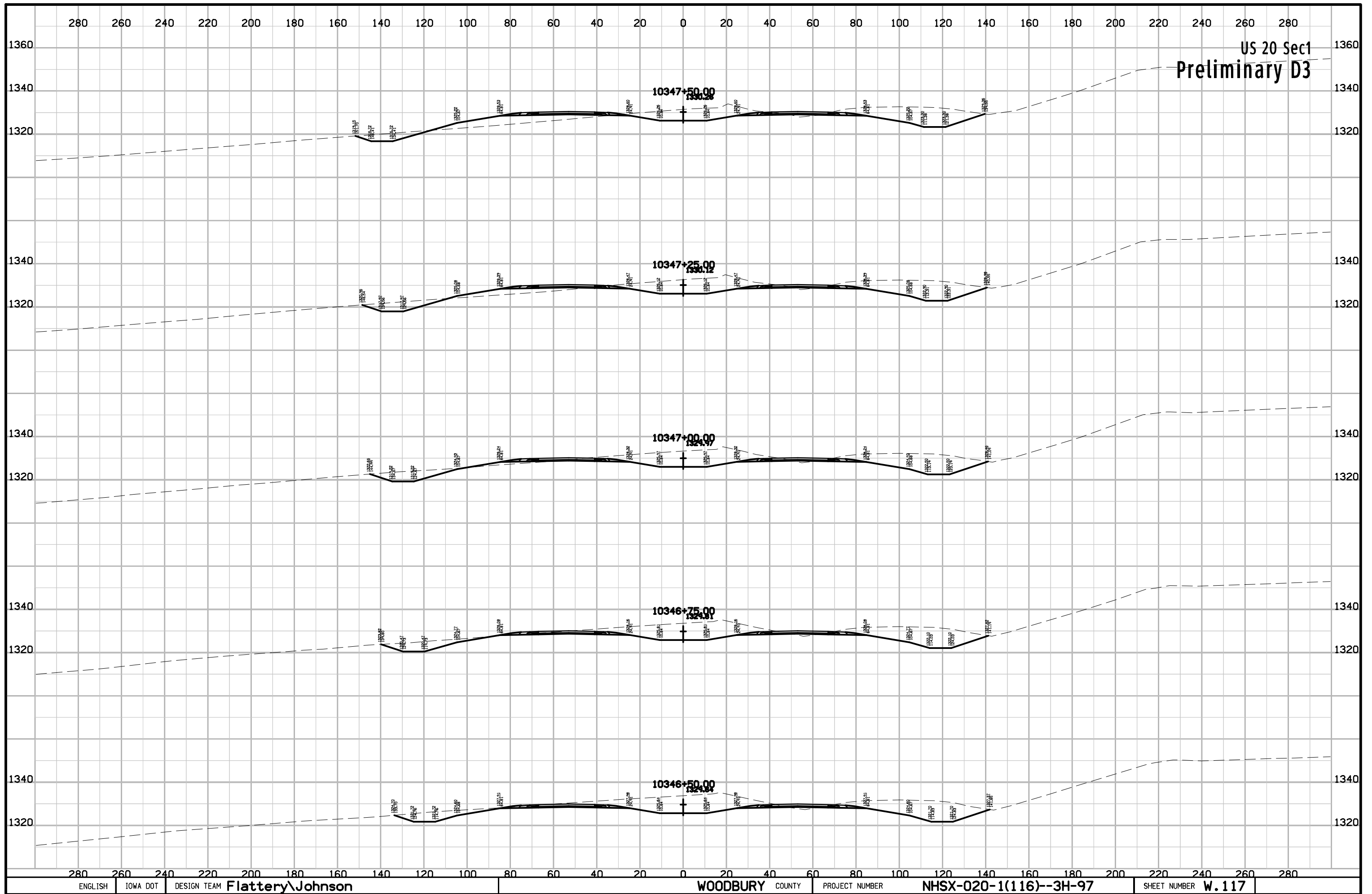


US 20 Sec1
Preliminary D3

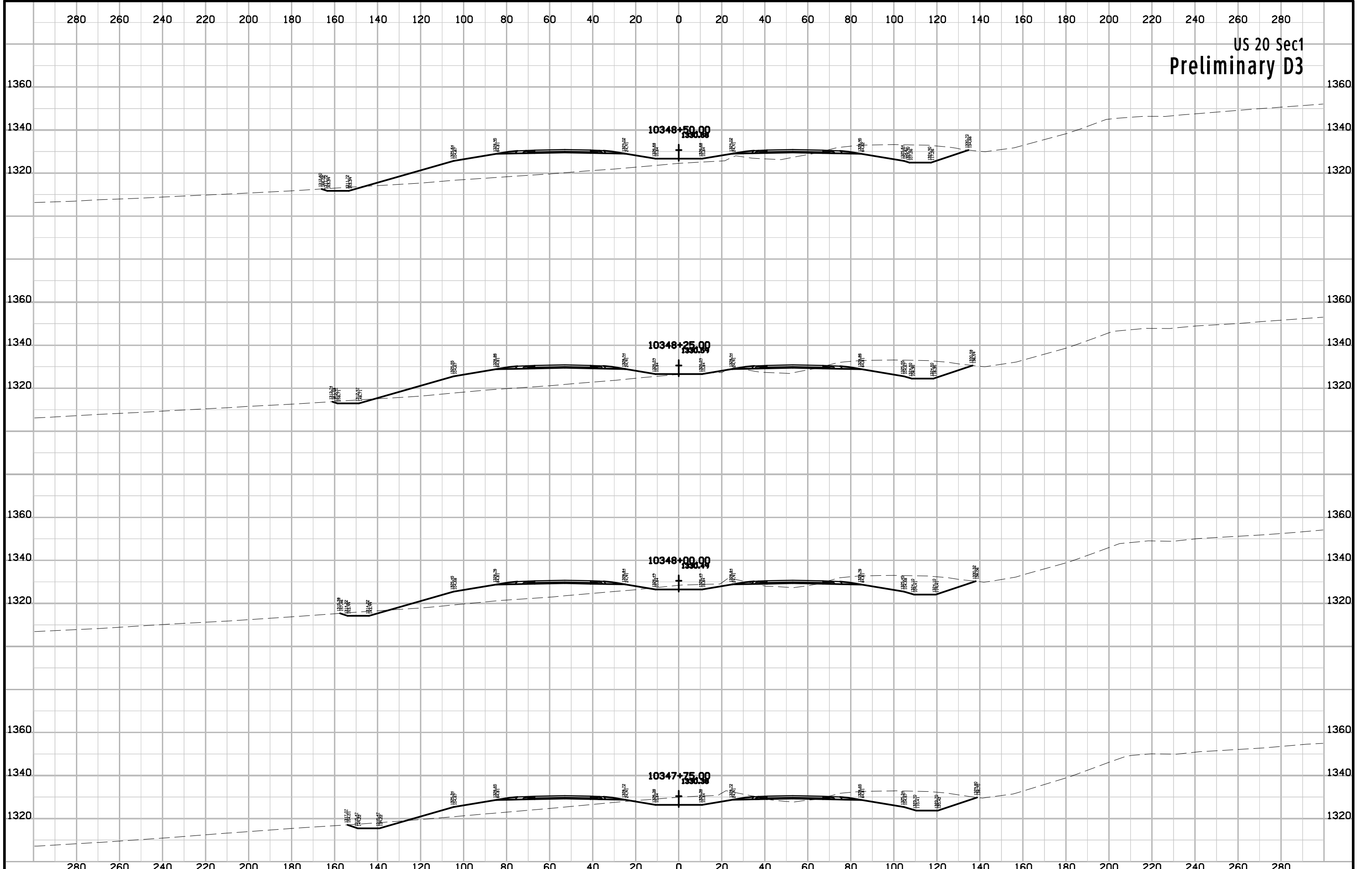


US 20 Sec1
Preliminary D3

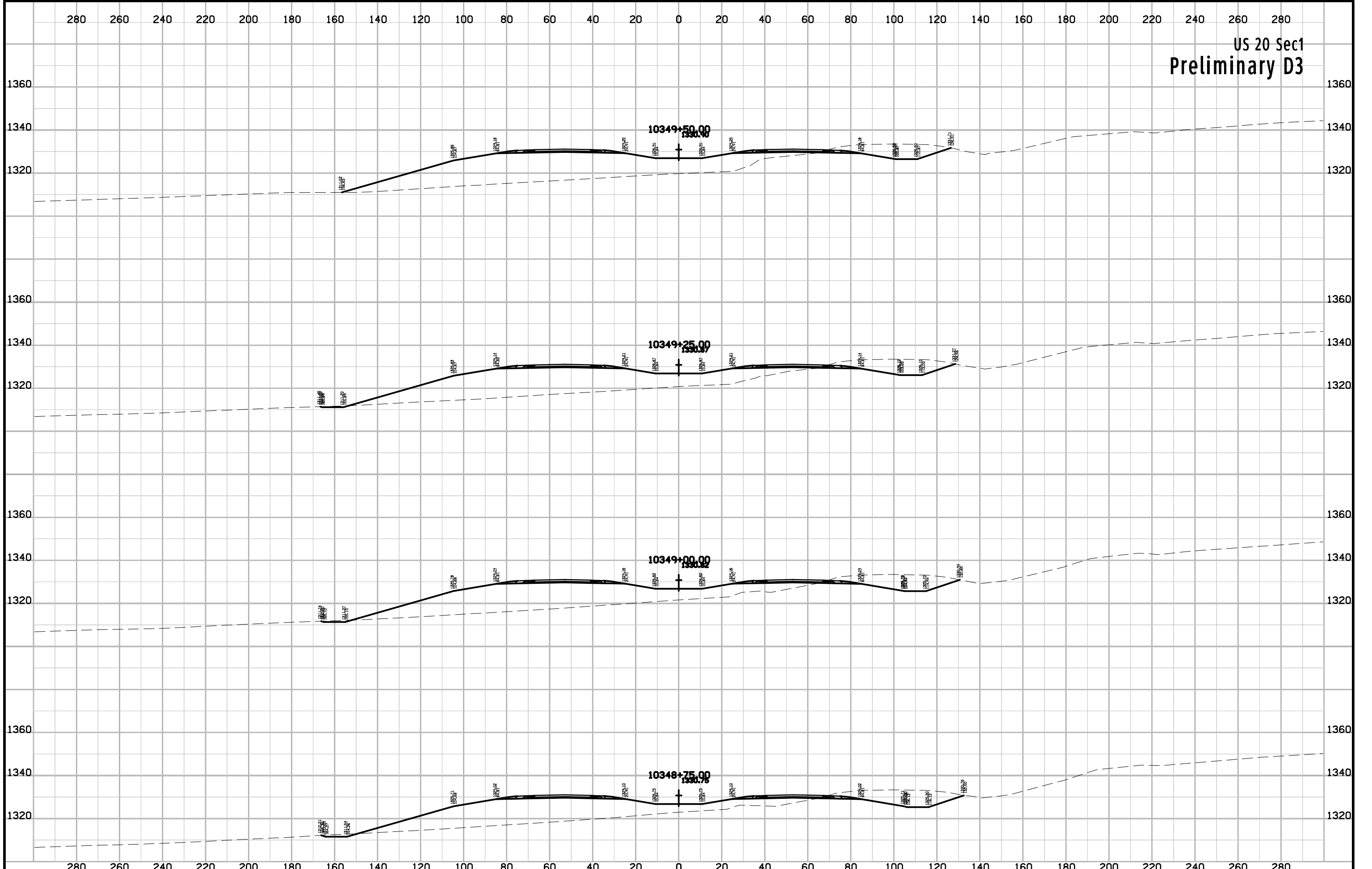




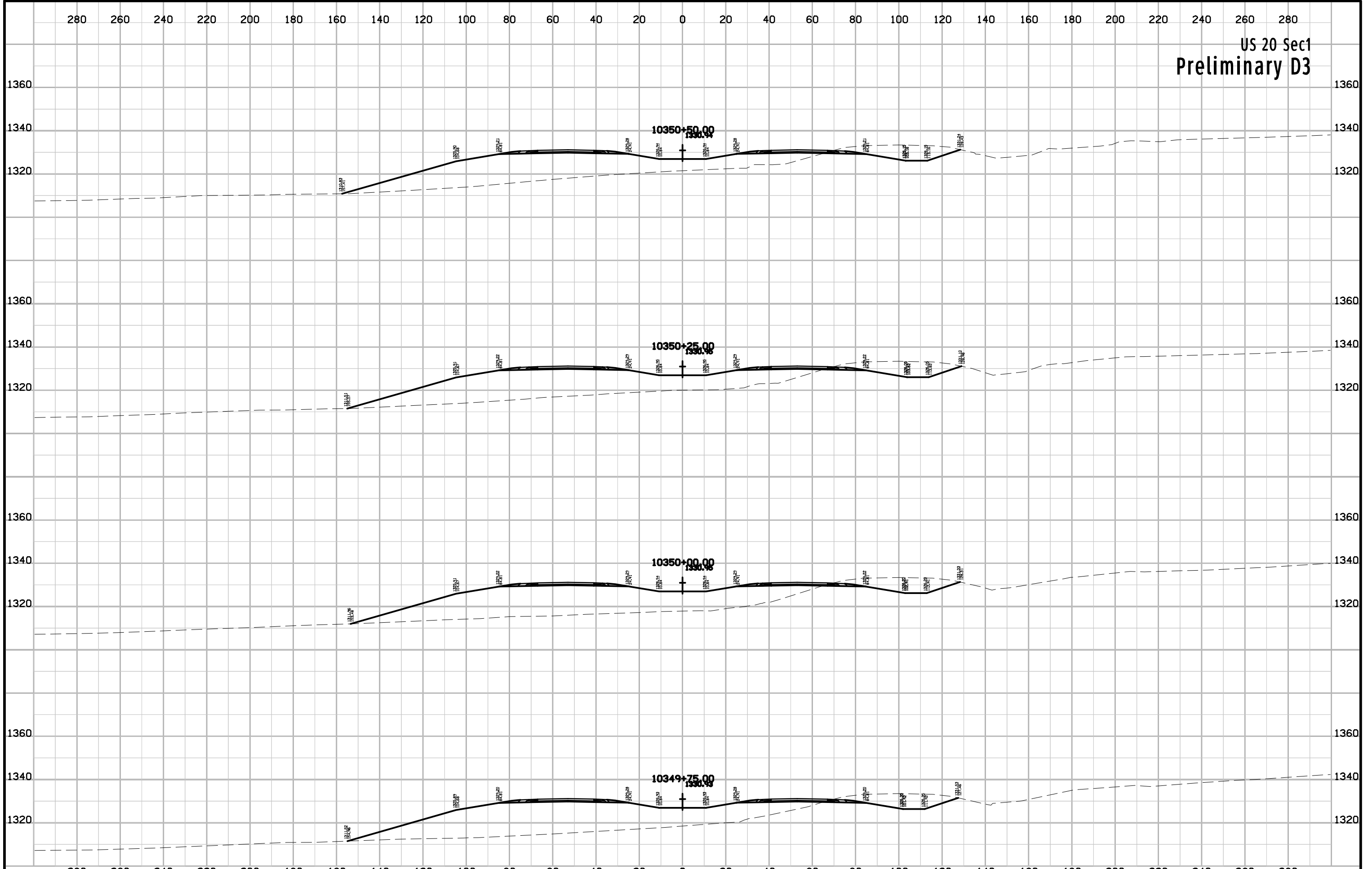
US 20 Sec1
Preliminary D3



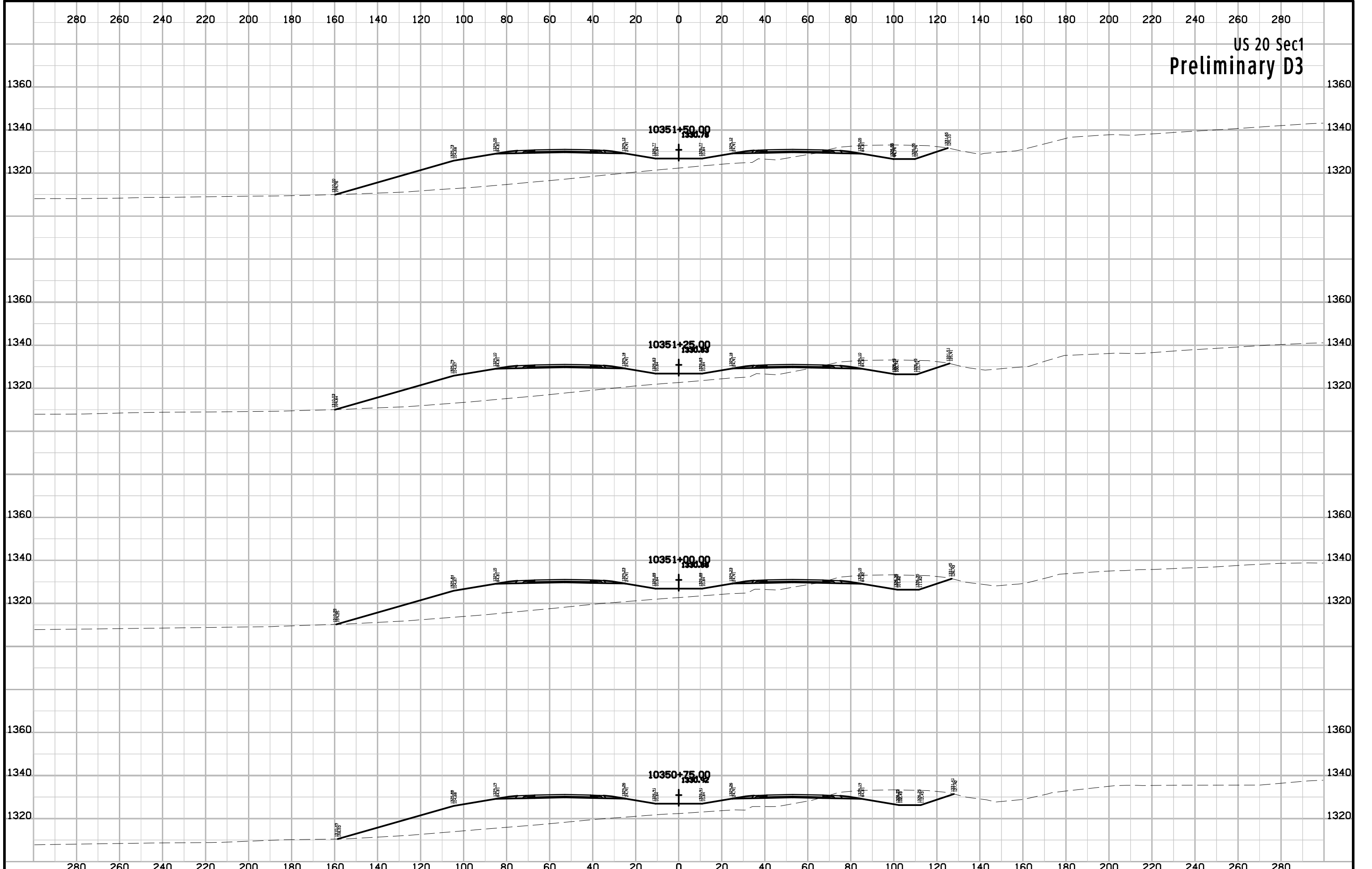
US 20 Sec1
Preliminary D3



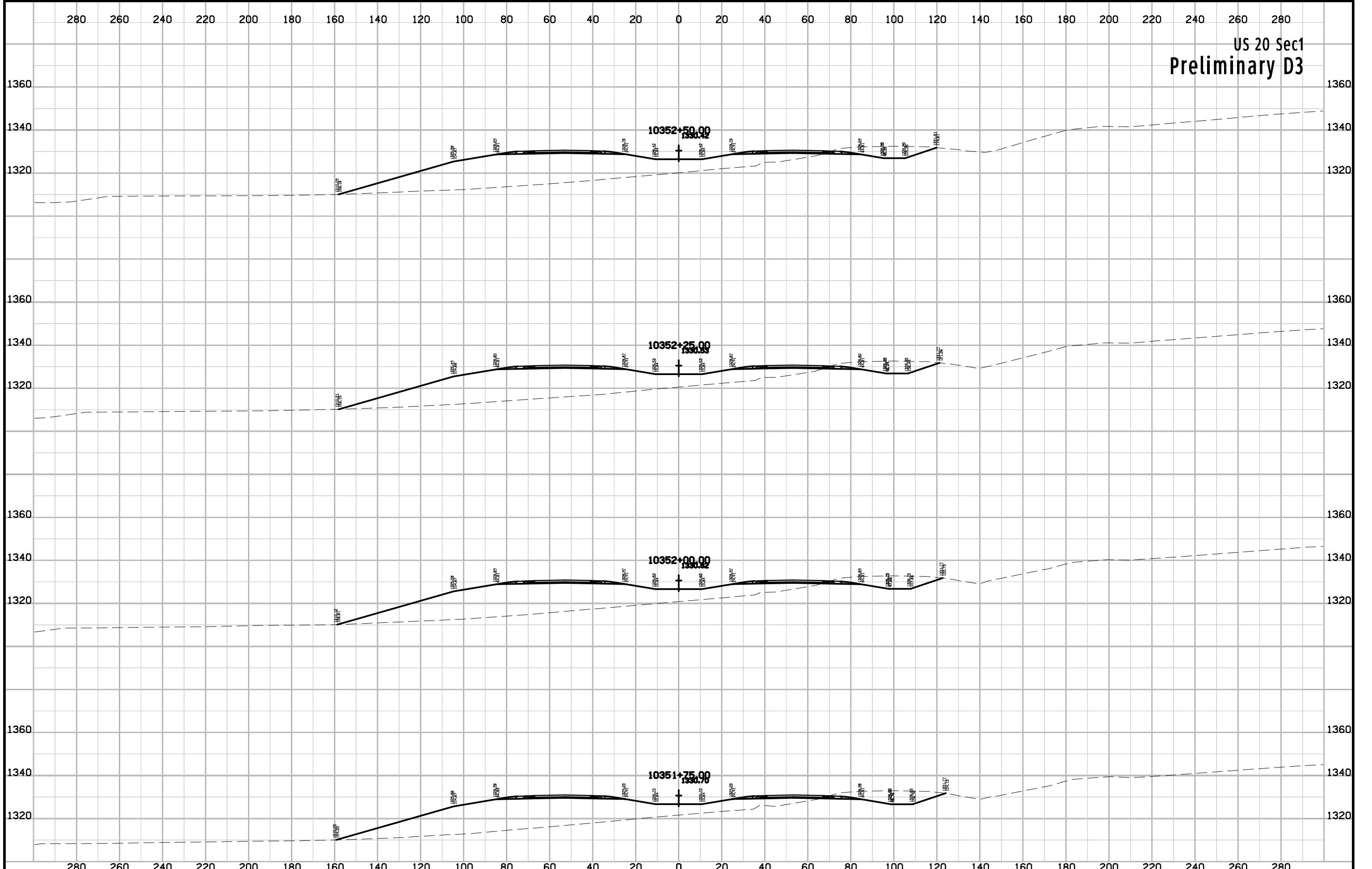
US 20 Sec1
Preliminary D3



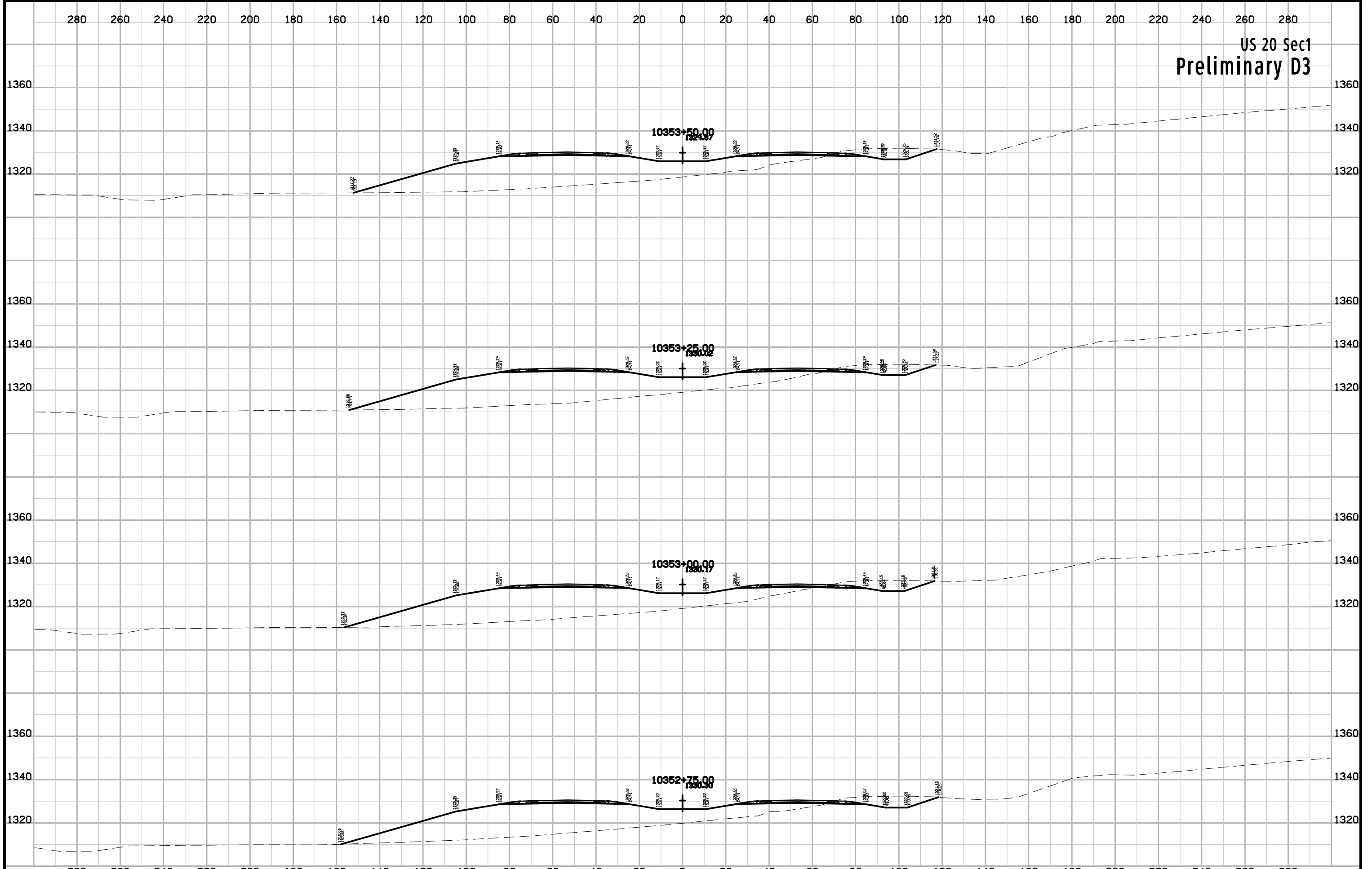
US 20 Sec1
Preliminary D3



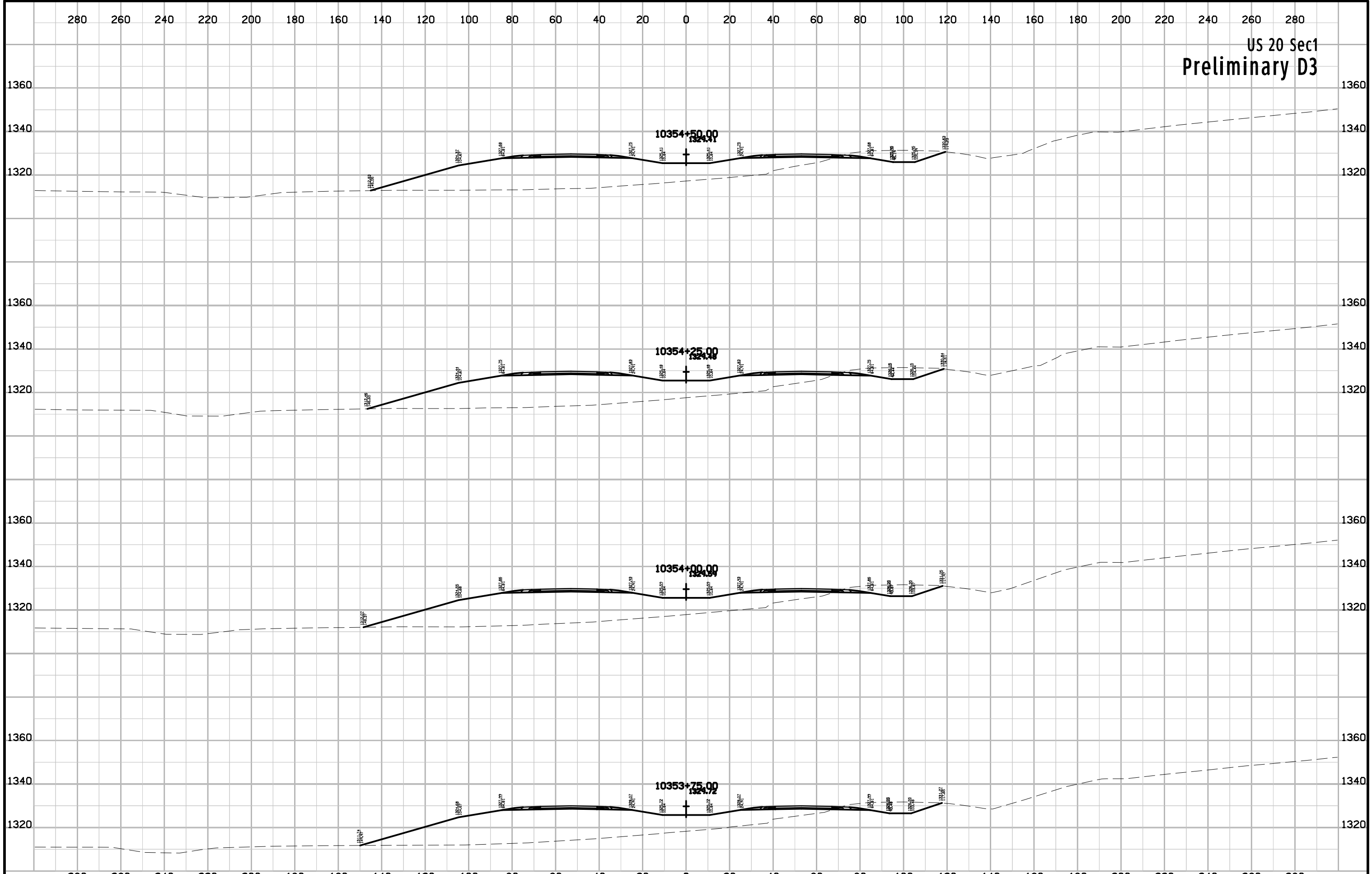
US 20 Sec1
Preliminary D3



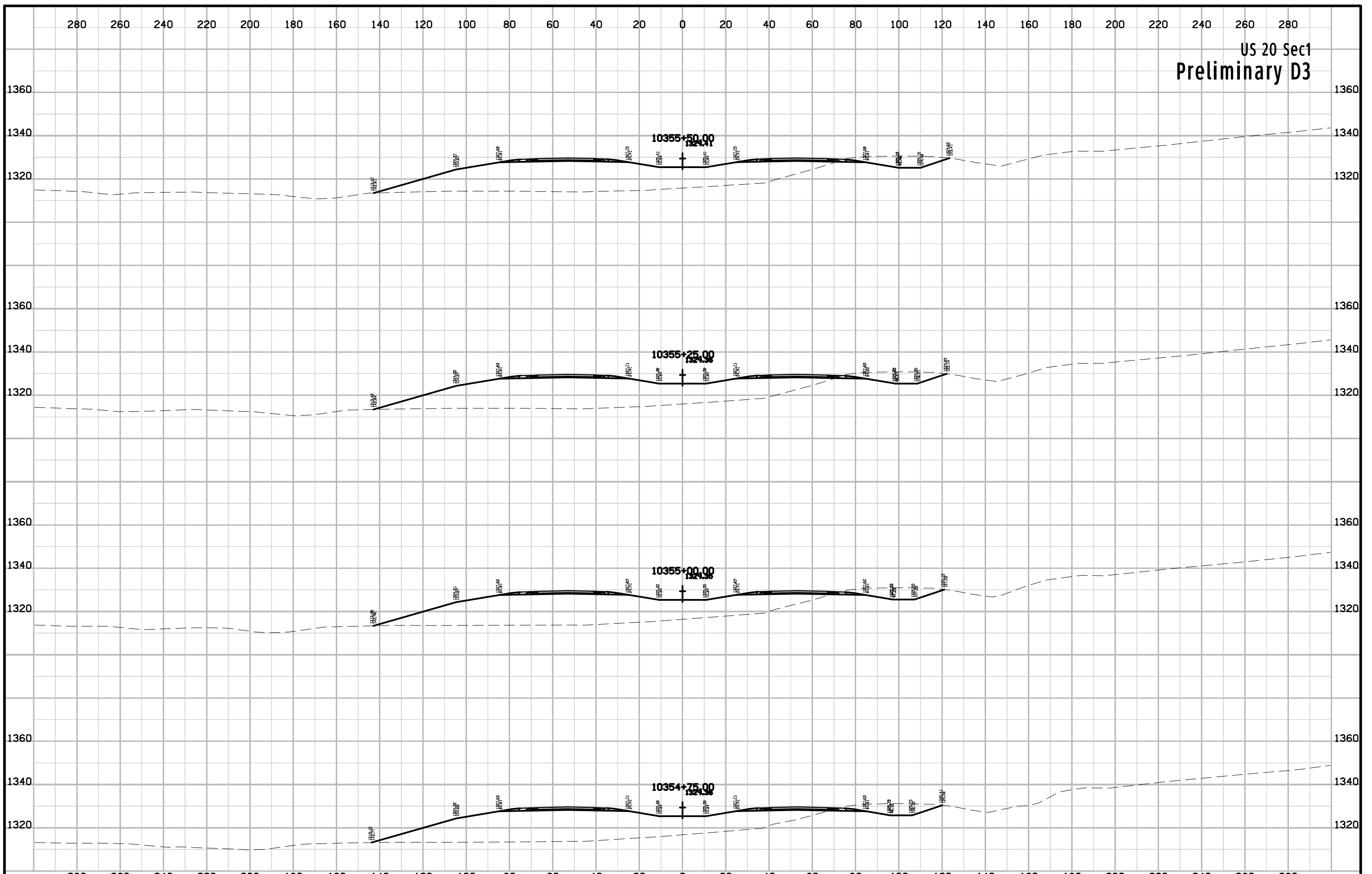
US 20 Sec1
Preliminary D3



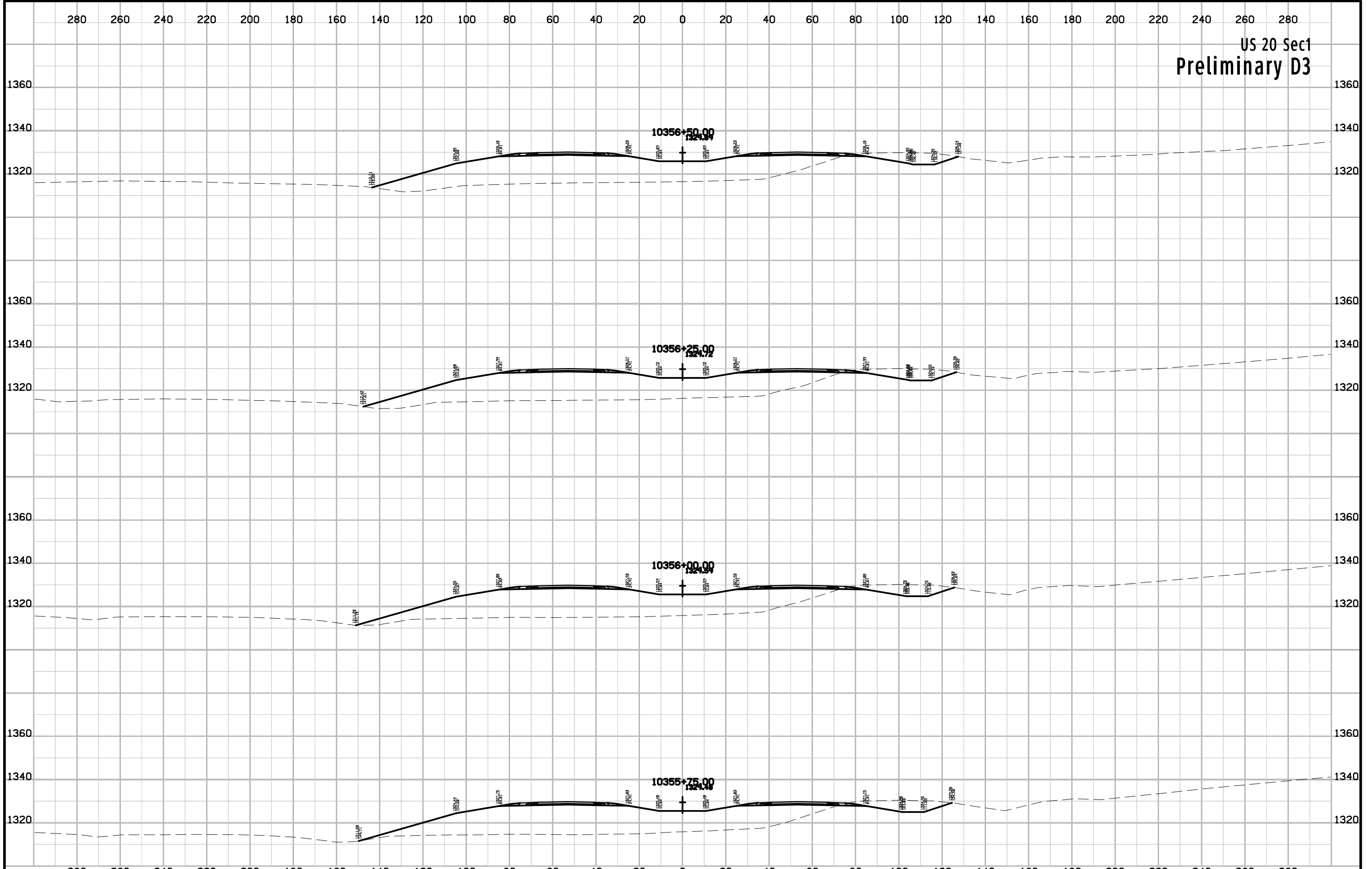
US 20 Sec1
Preliminary D3



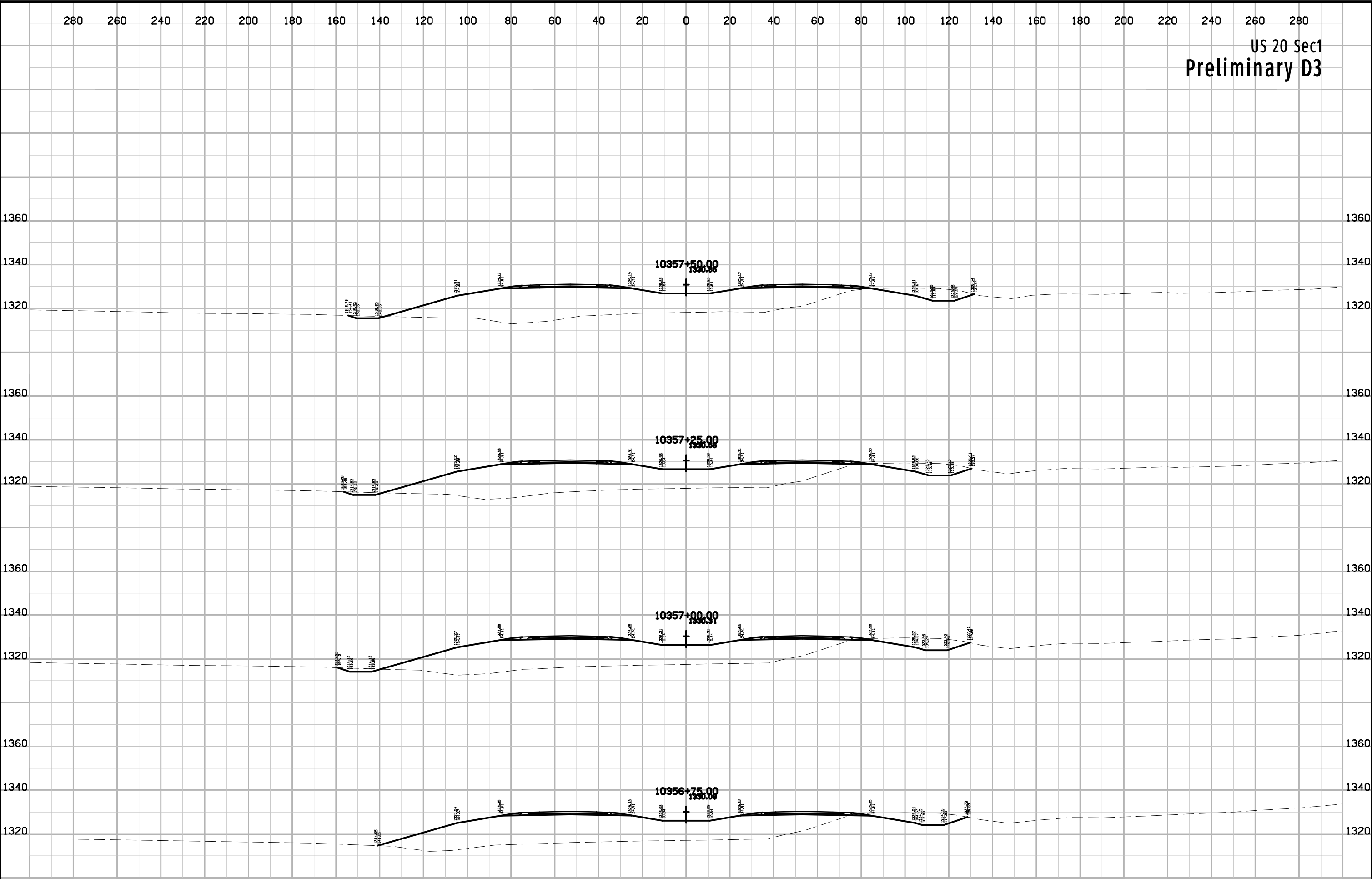
US 20 Sec1
Preliminary D3



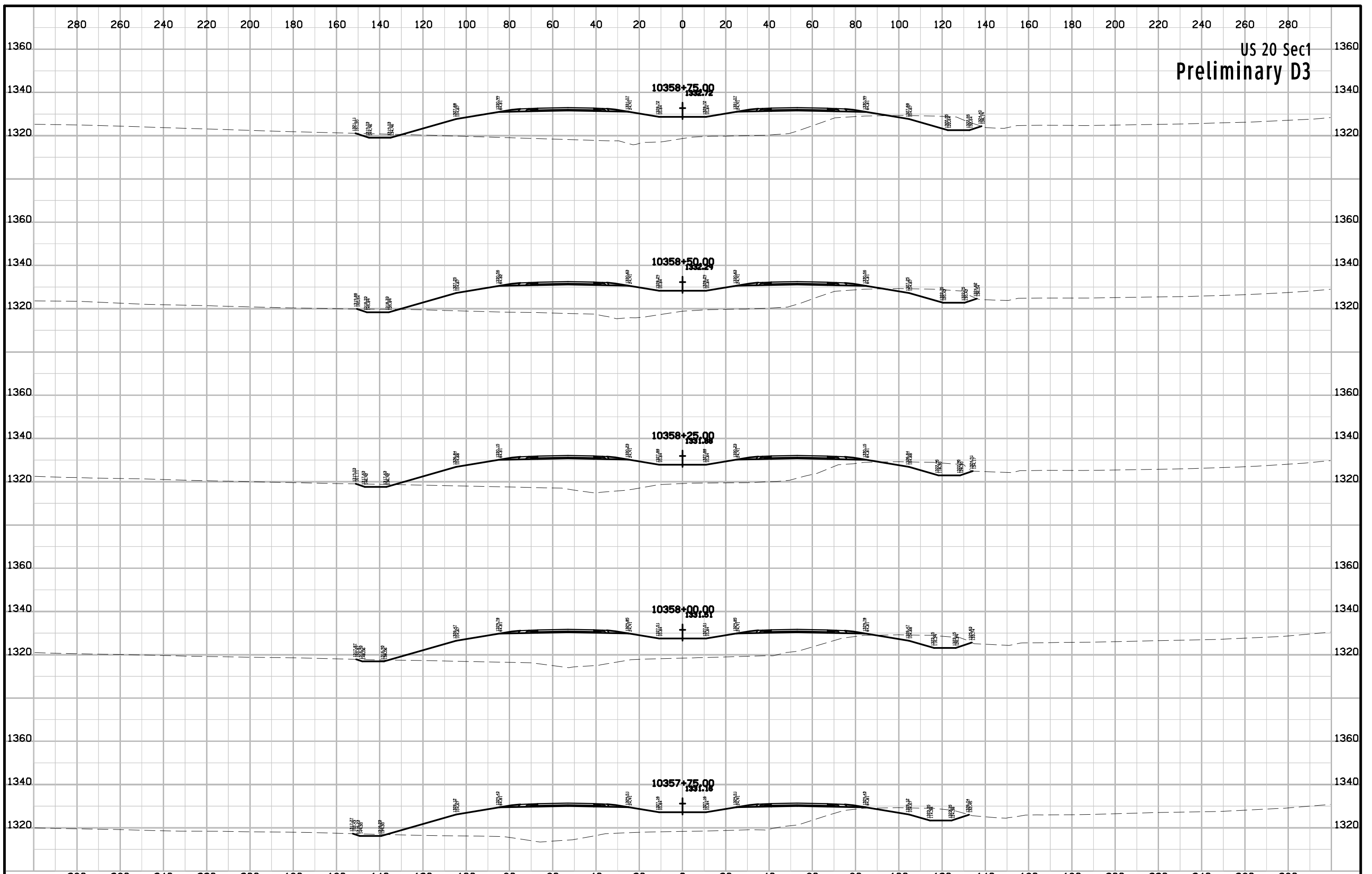
US 20 Sec1
Preliminary D3



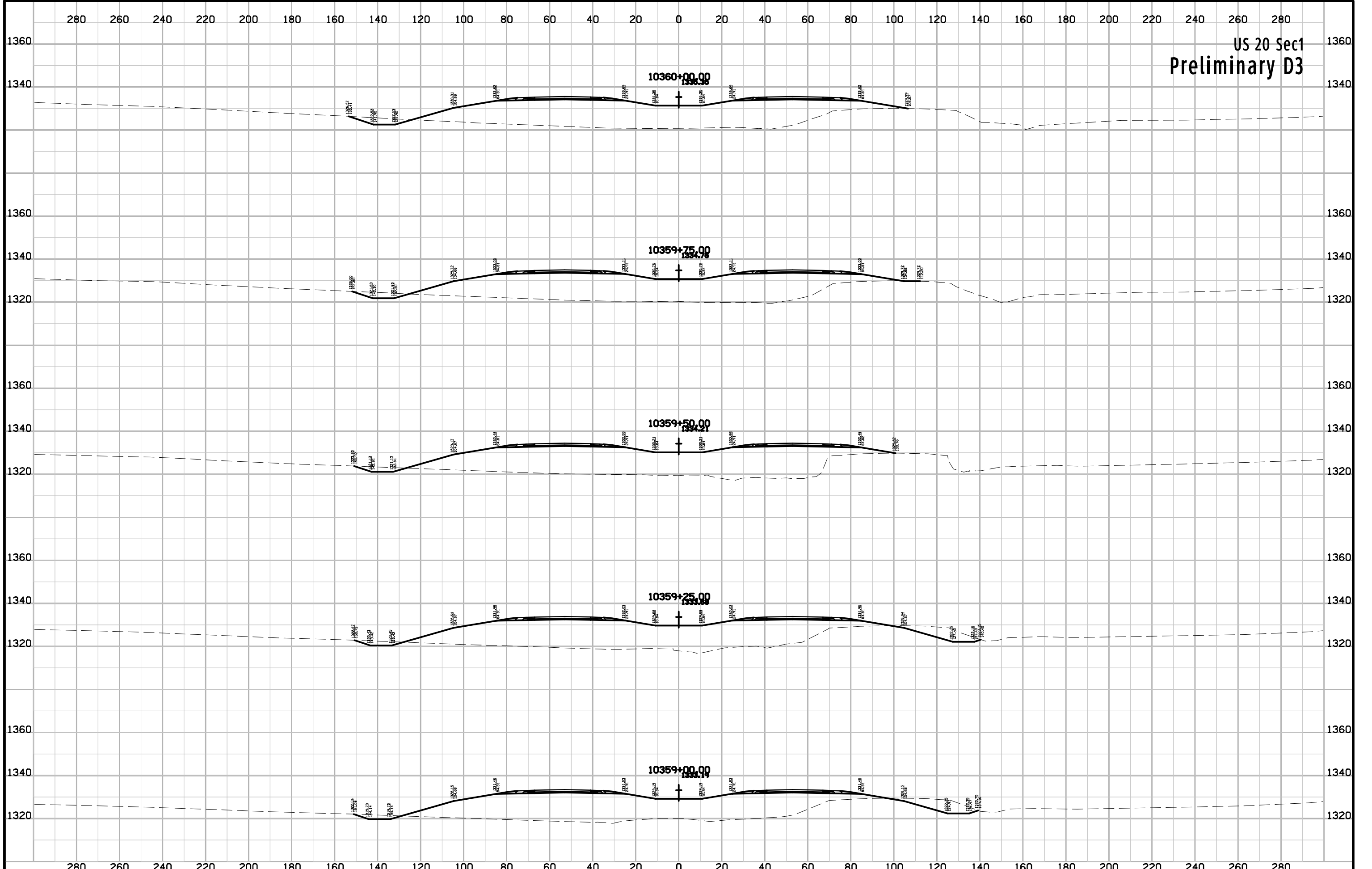
US 20 Sec1
Preliminary D3



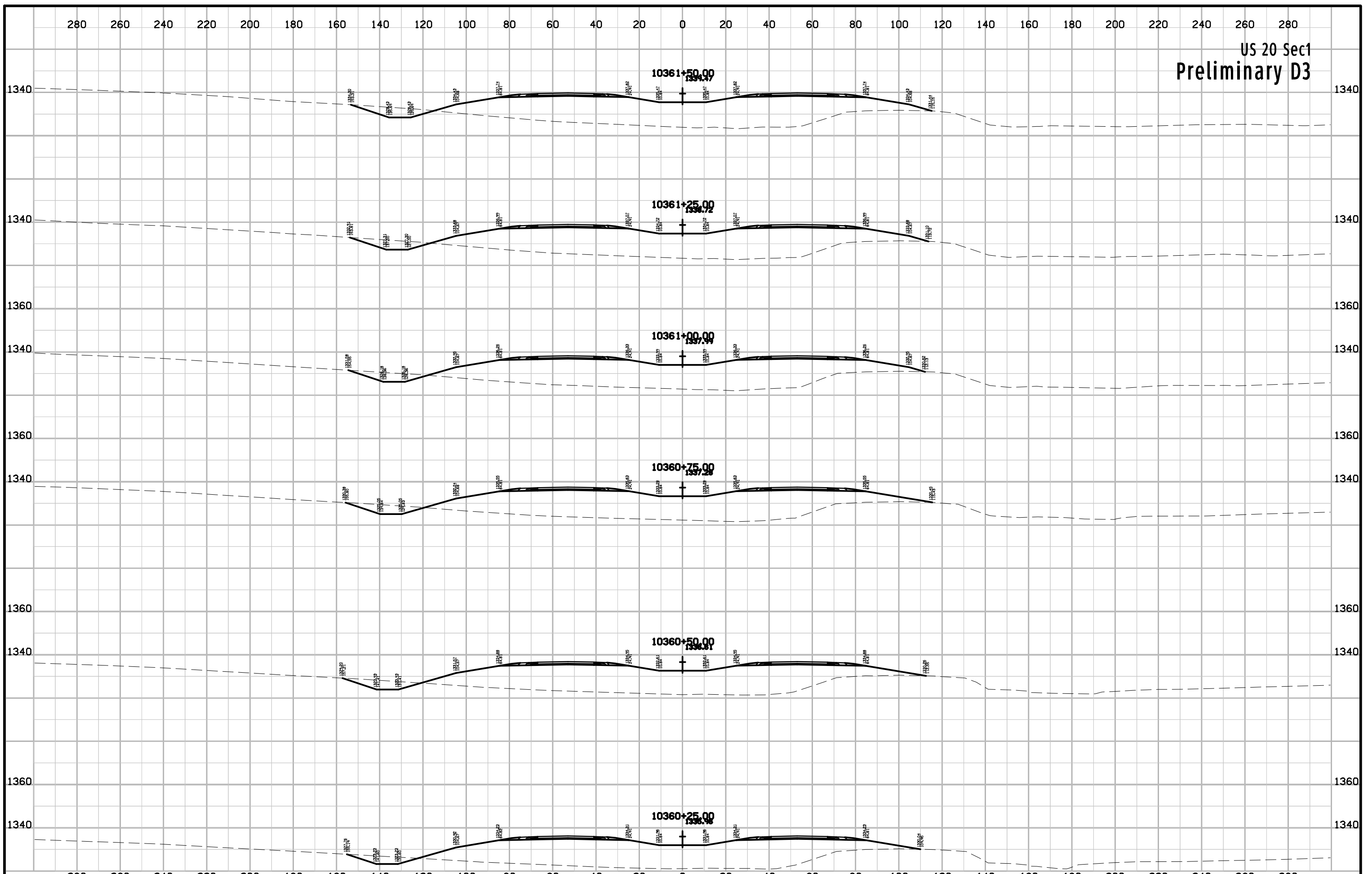
US 20 Sec1
Preliminary D3



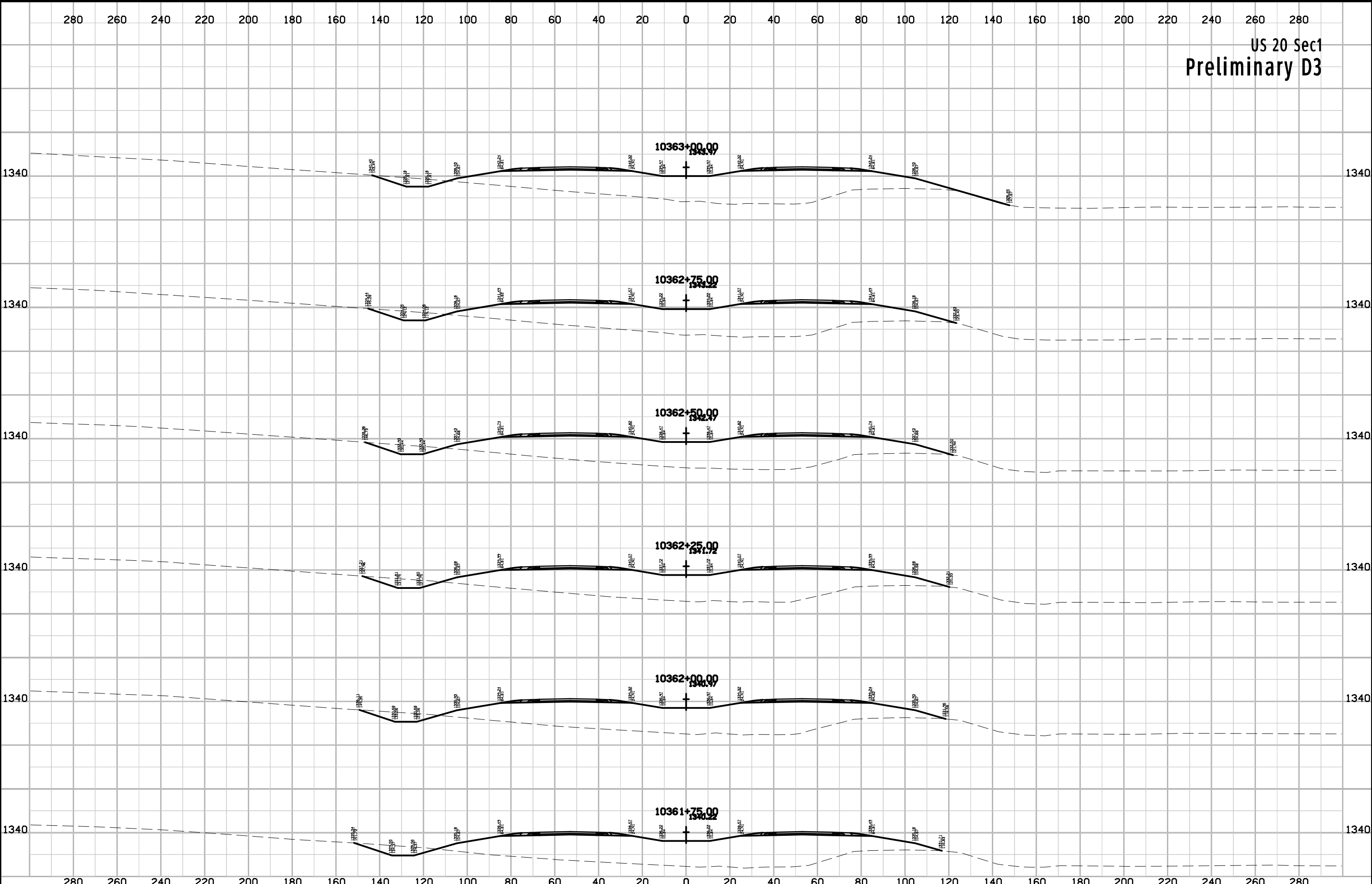
US 20 Sec1
Preliminary D3



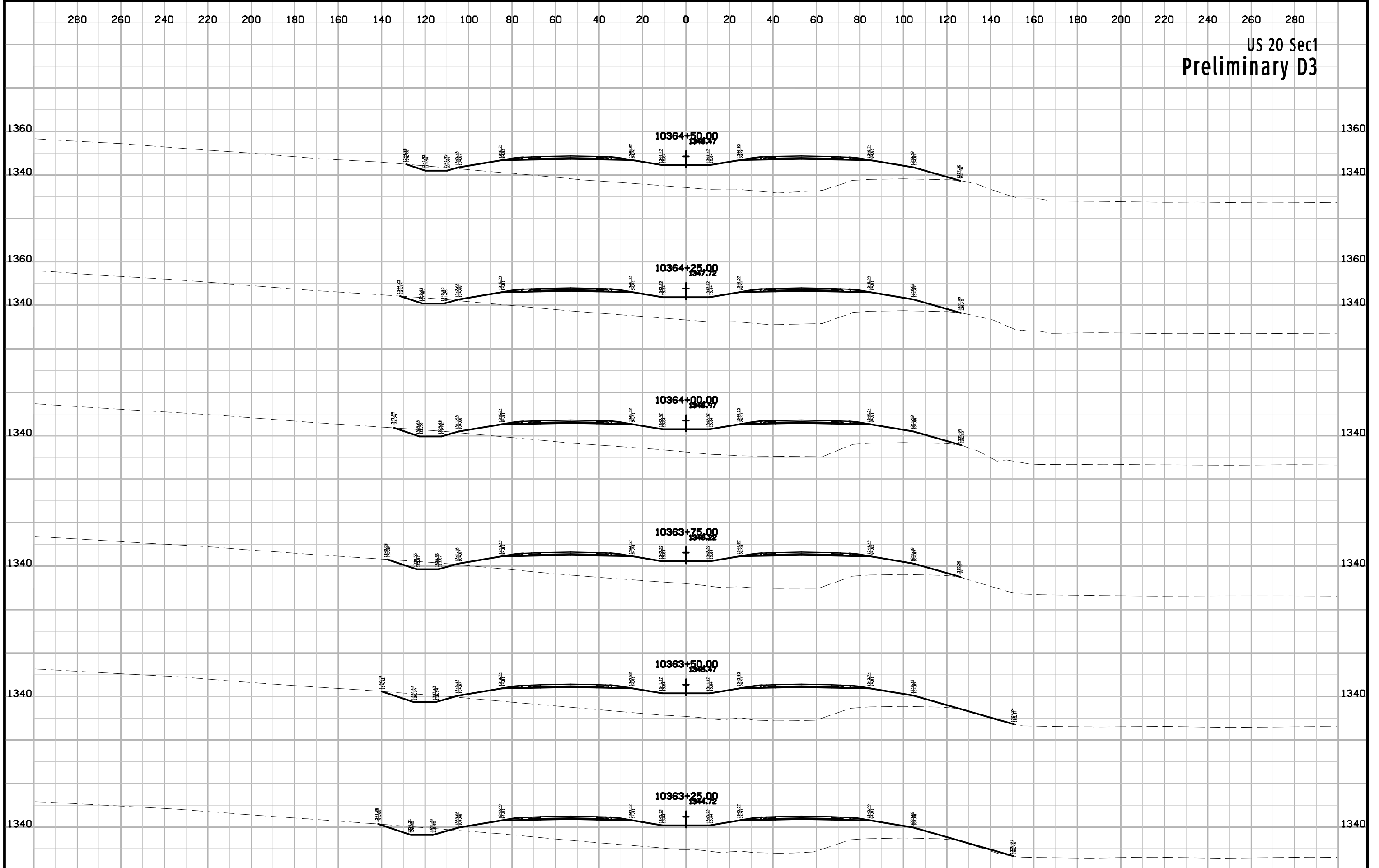
US 20 Sec1
Preliminary D3



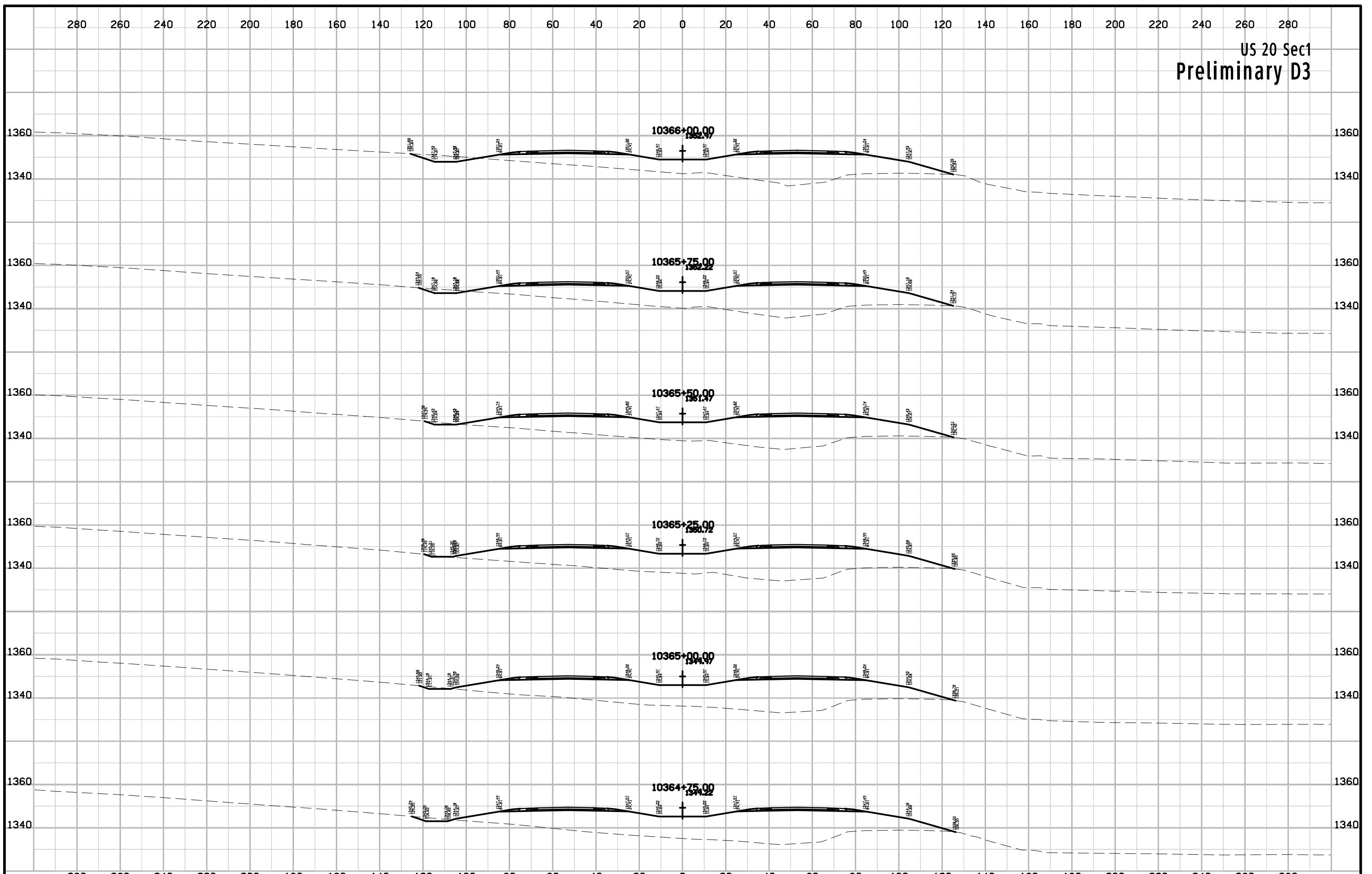
US 20 Sec1
Preliminary D3



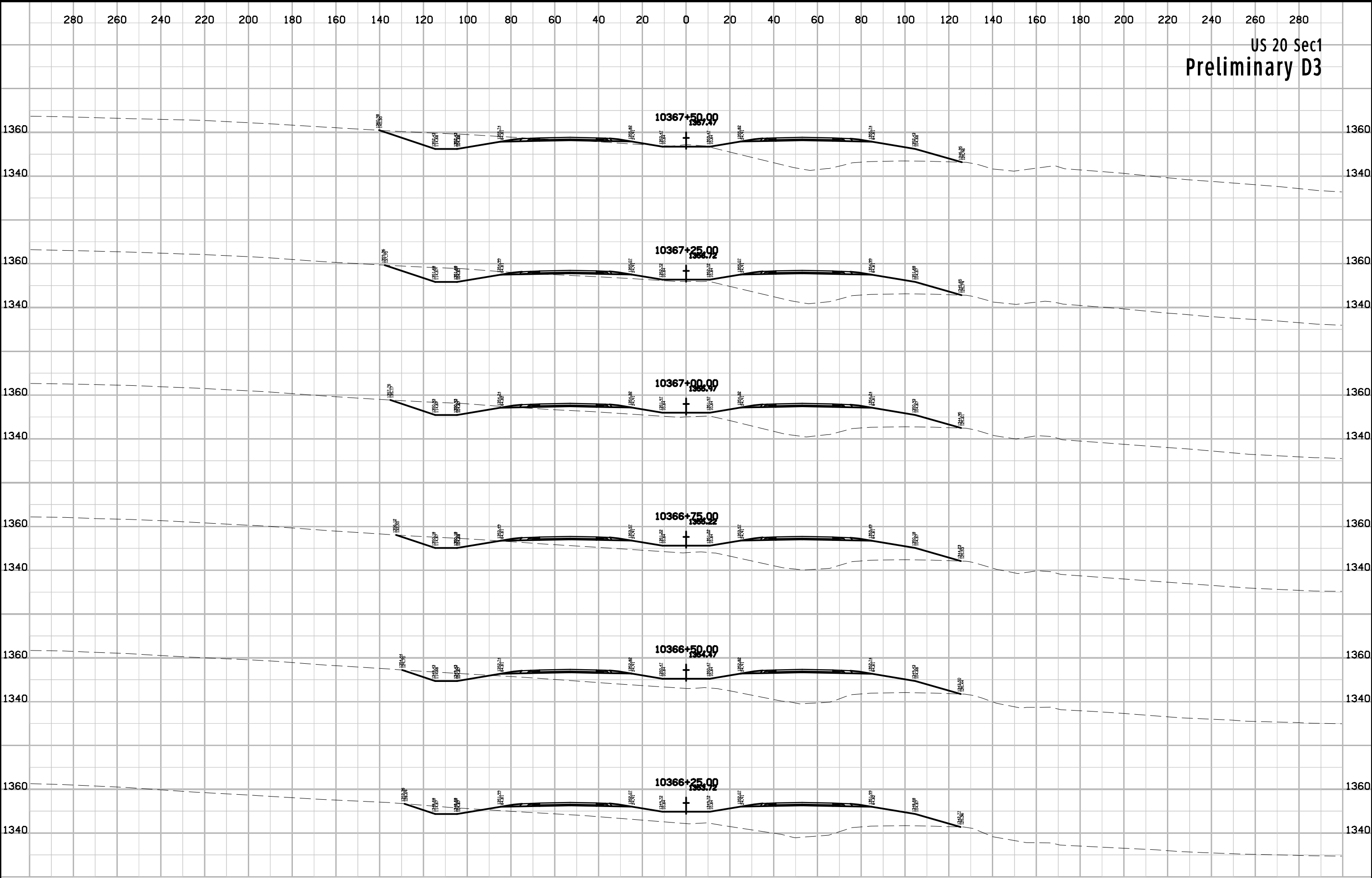
US 20 Sec1
Preliminary D3



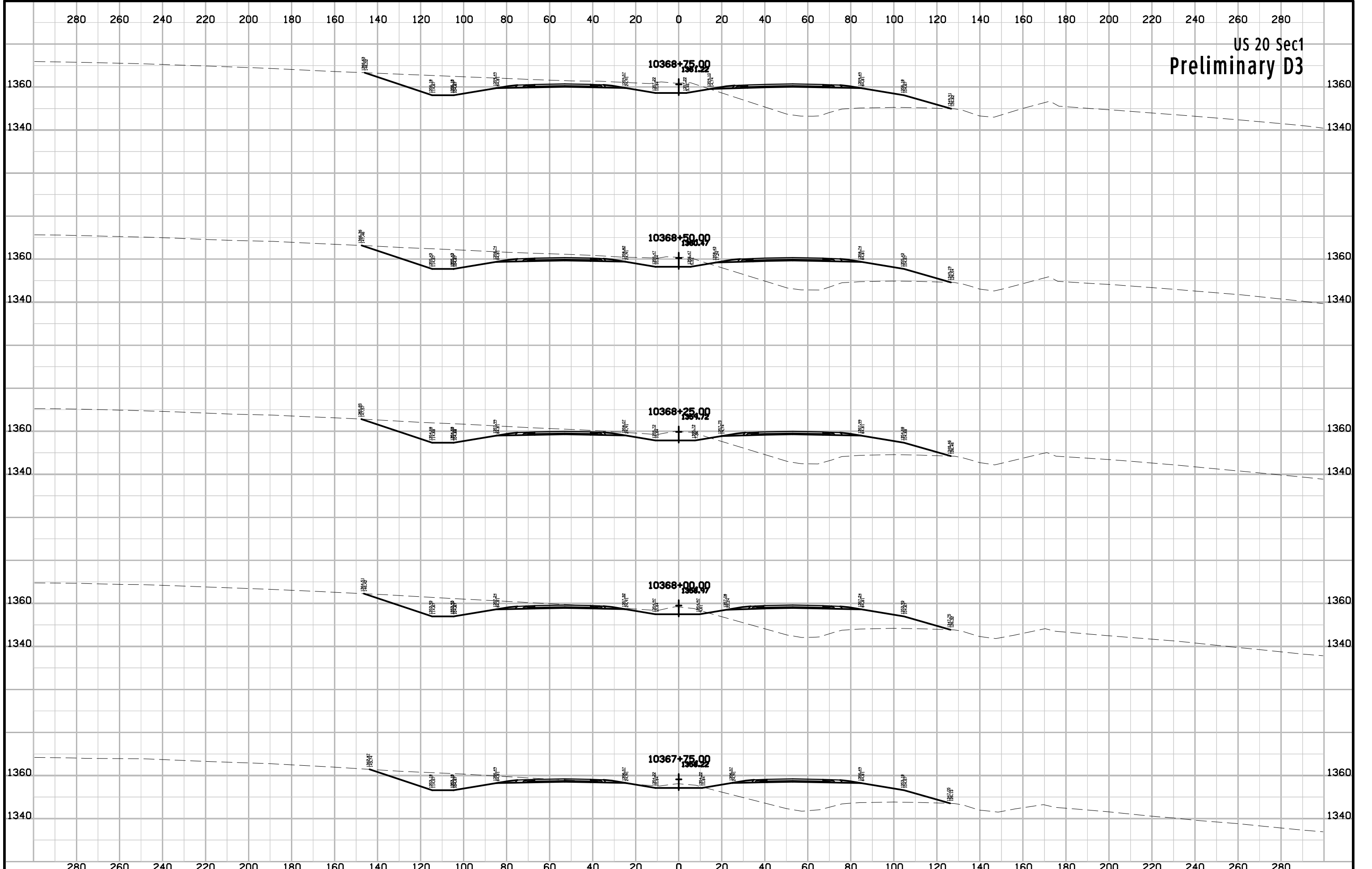
US 20 Sec1
Preliminary D3



US 20 Sec1
Preliminary D3



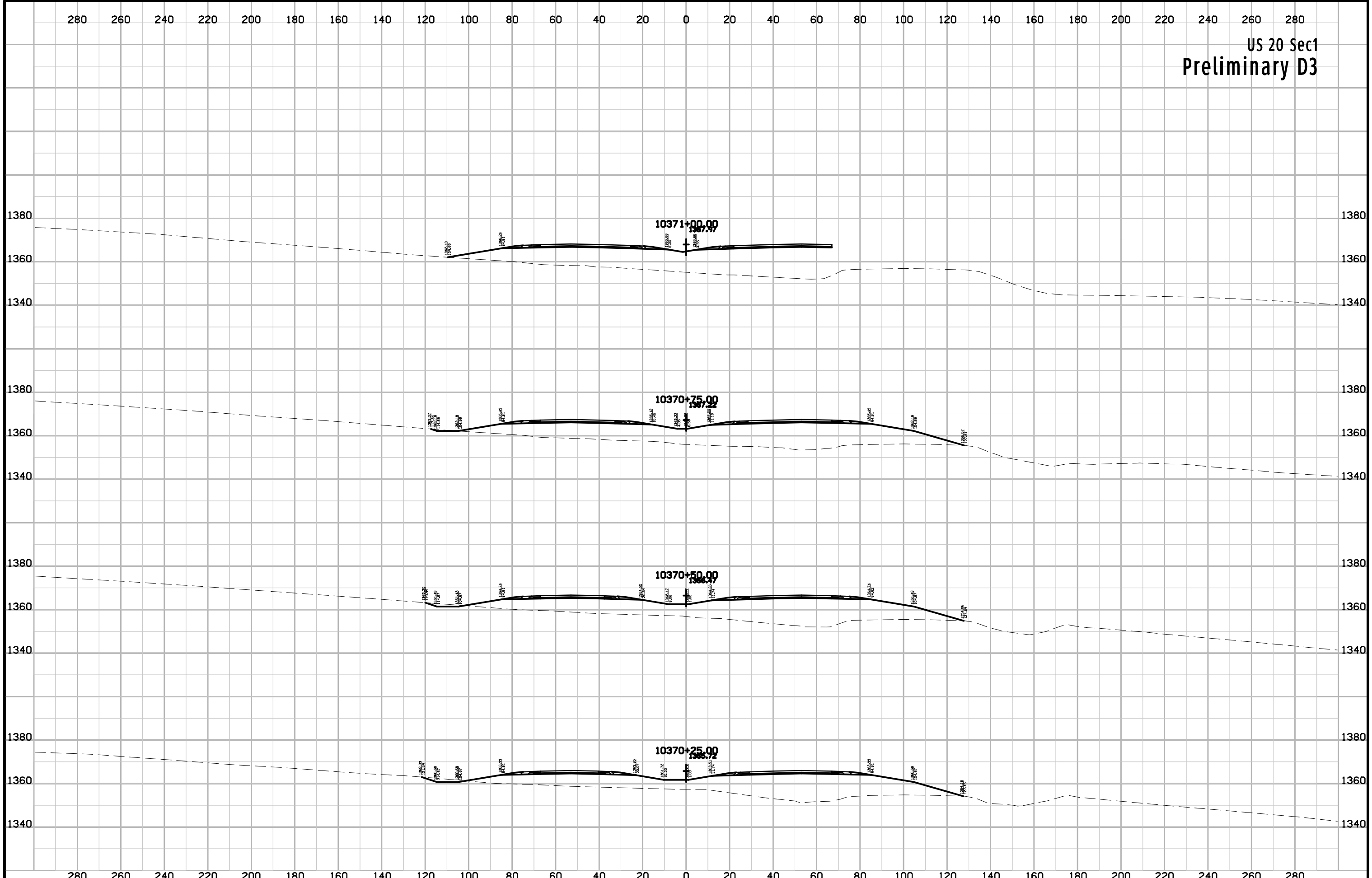
US 20 Sec1
Preliminary D3



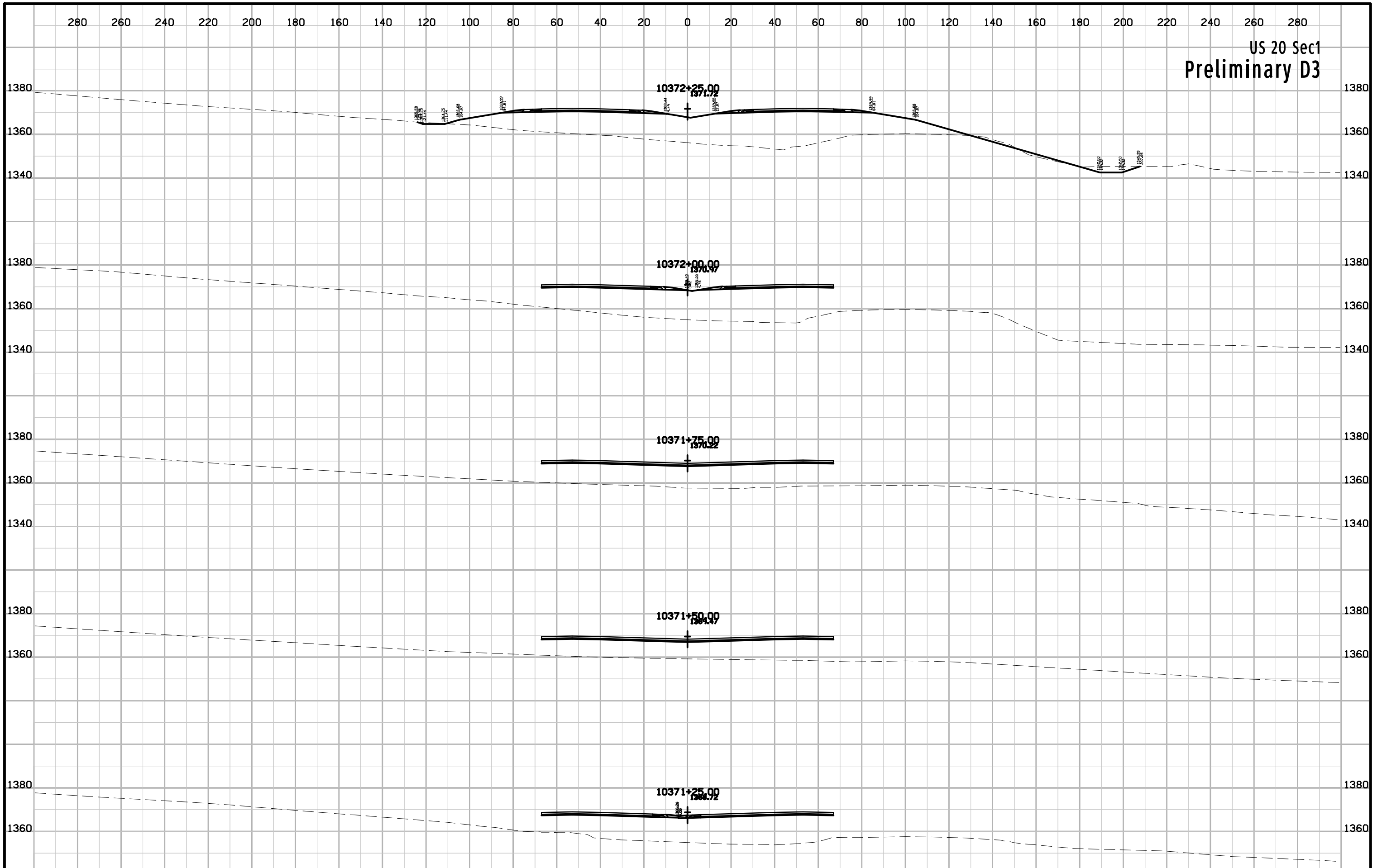


US 20 Sec1
Preliminary D3

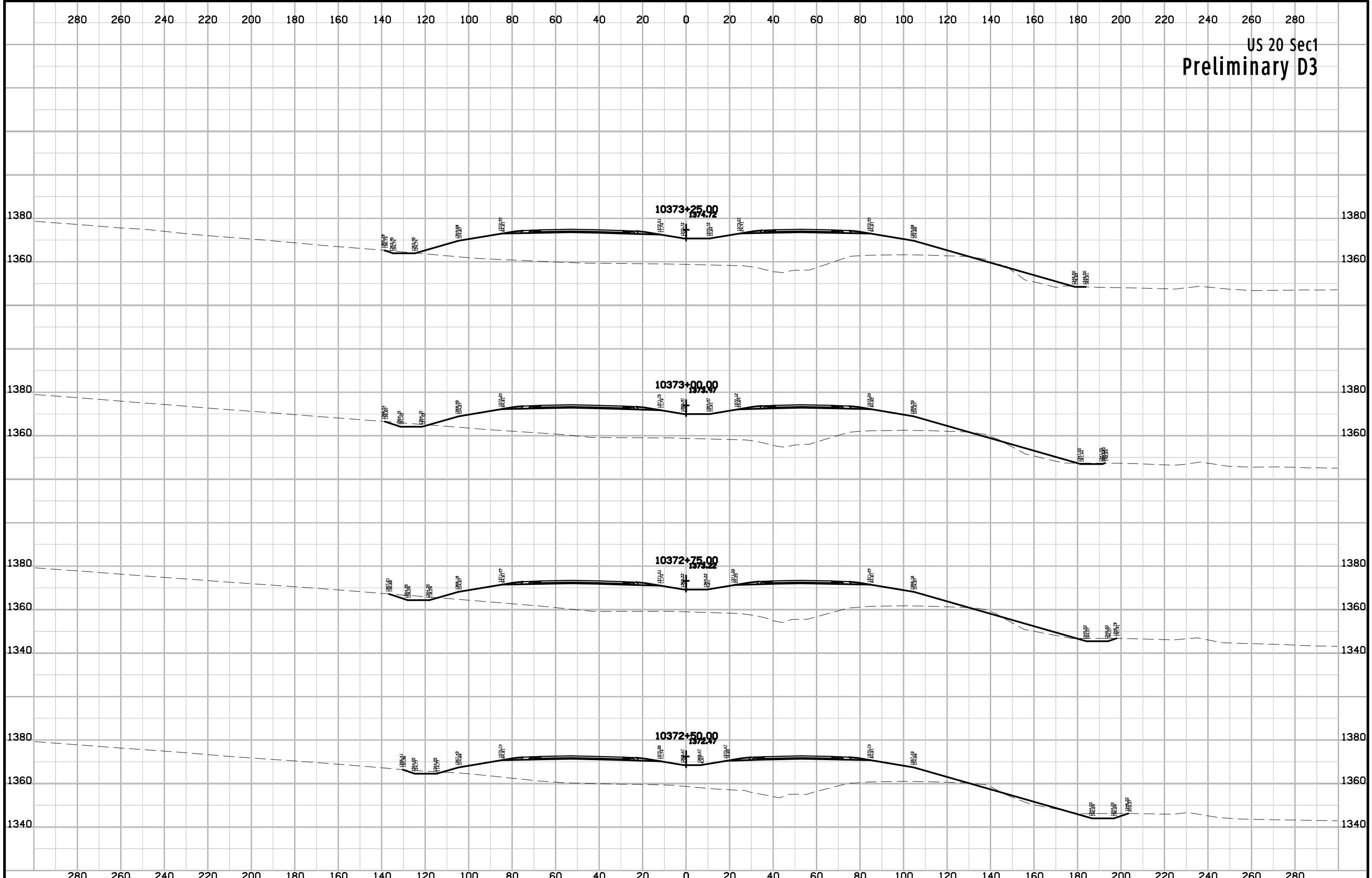
US 20 Sec1
Preliminary D3



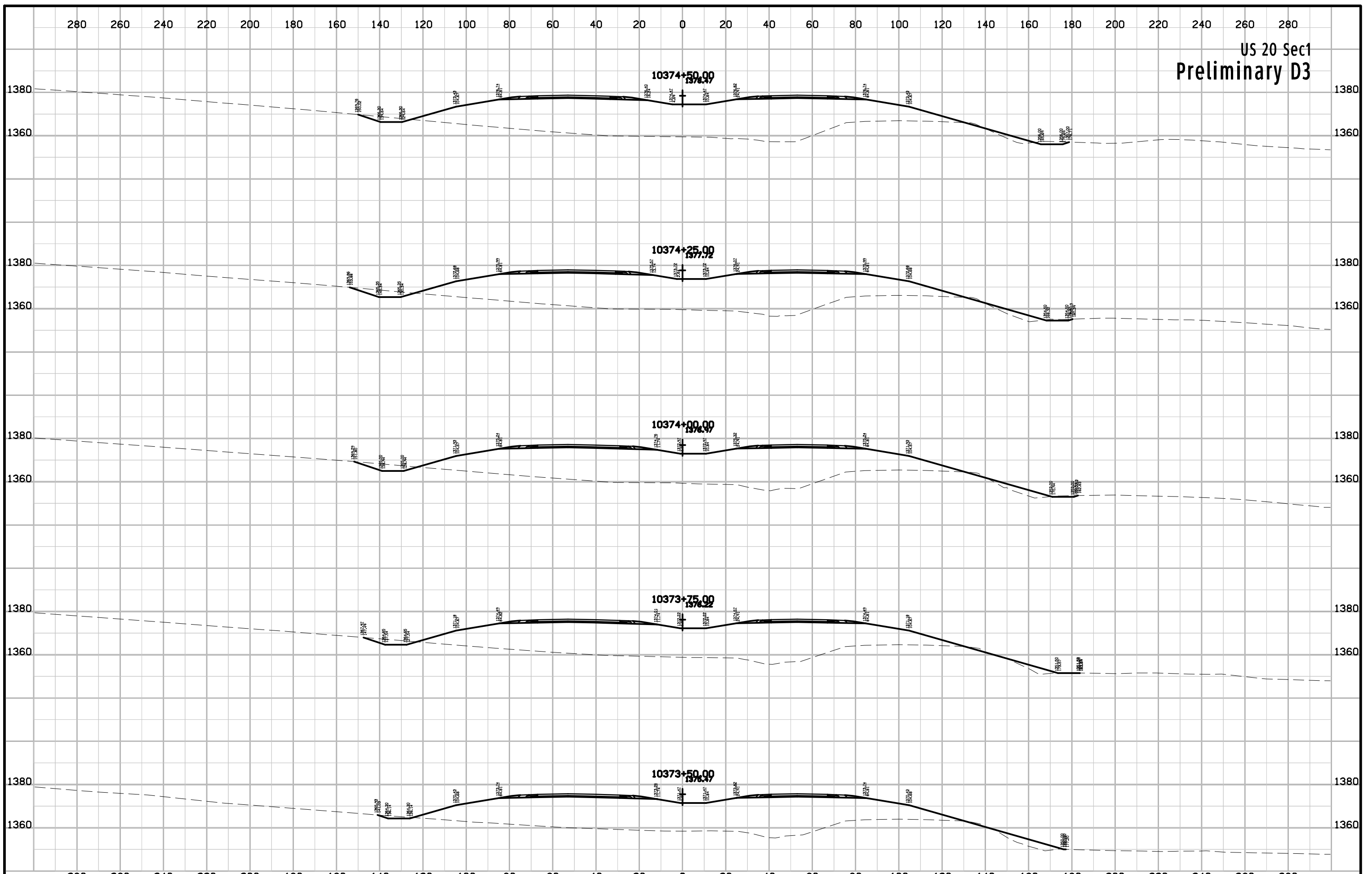
US 20 Sec1
Preliminary D3



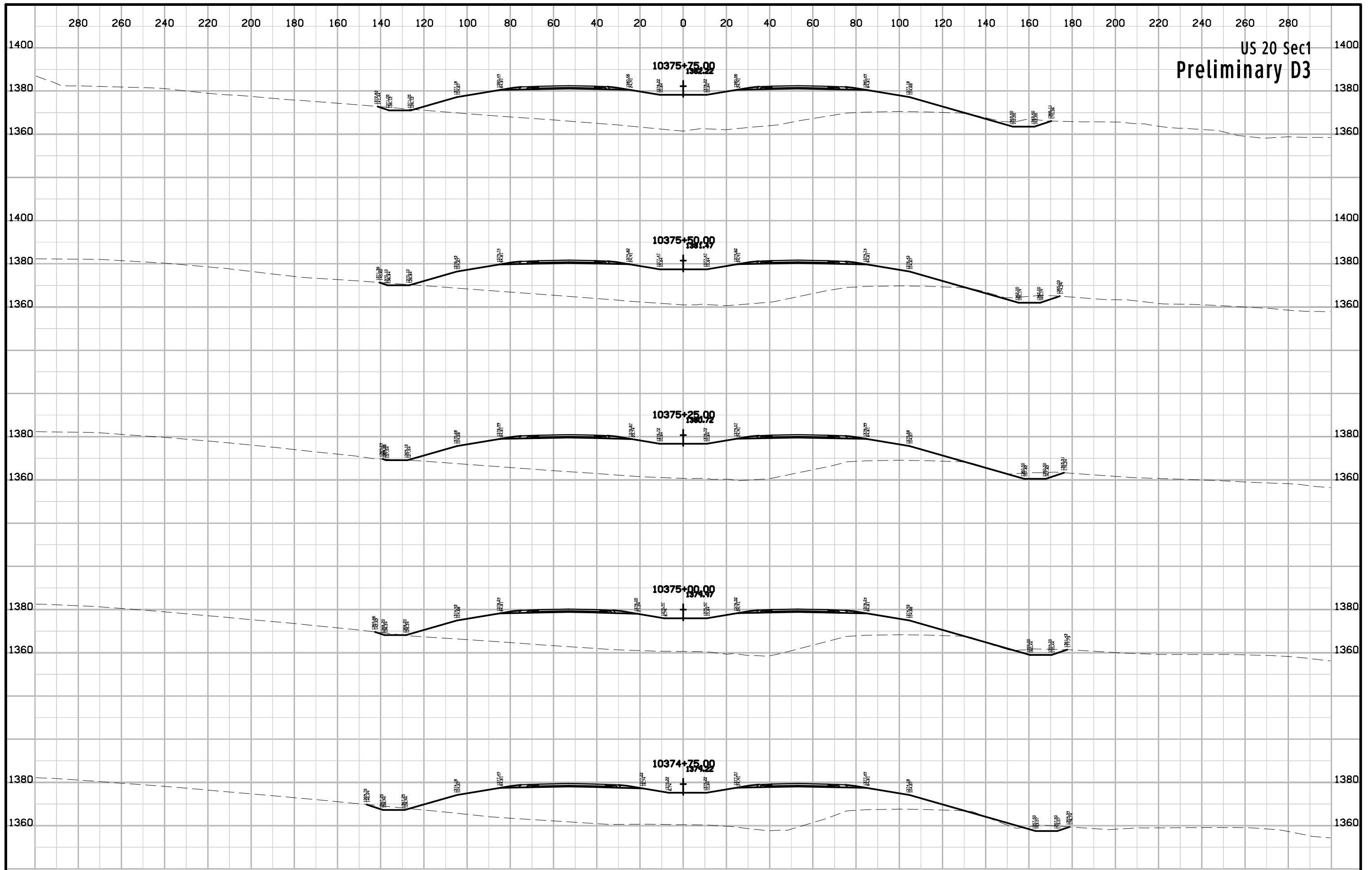
US 20 Sec1
Preliminary D3



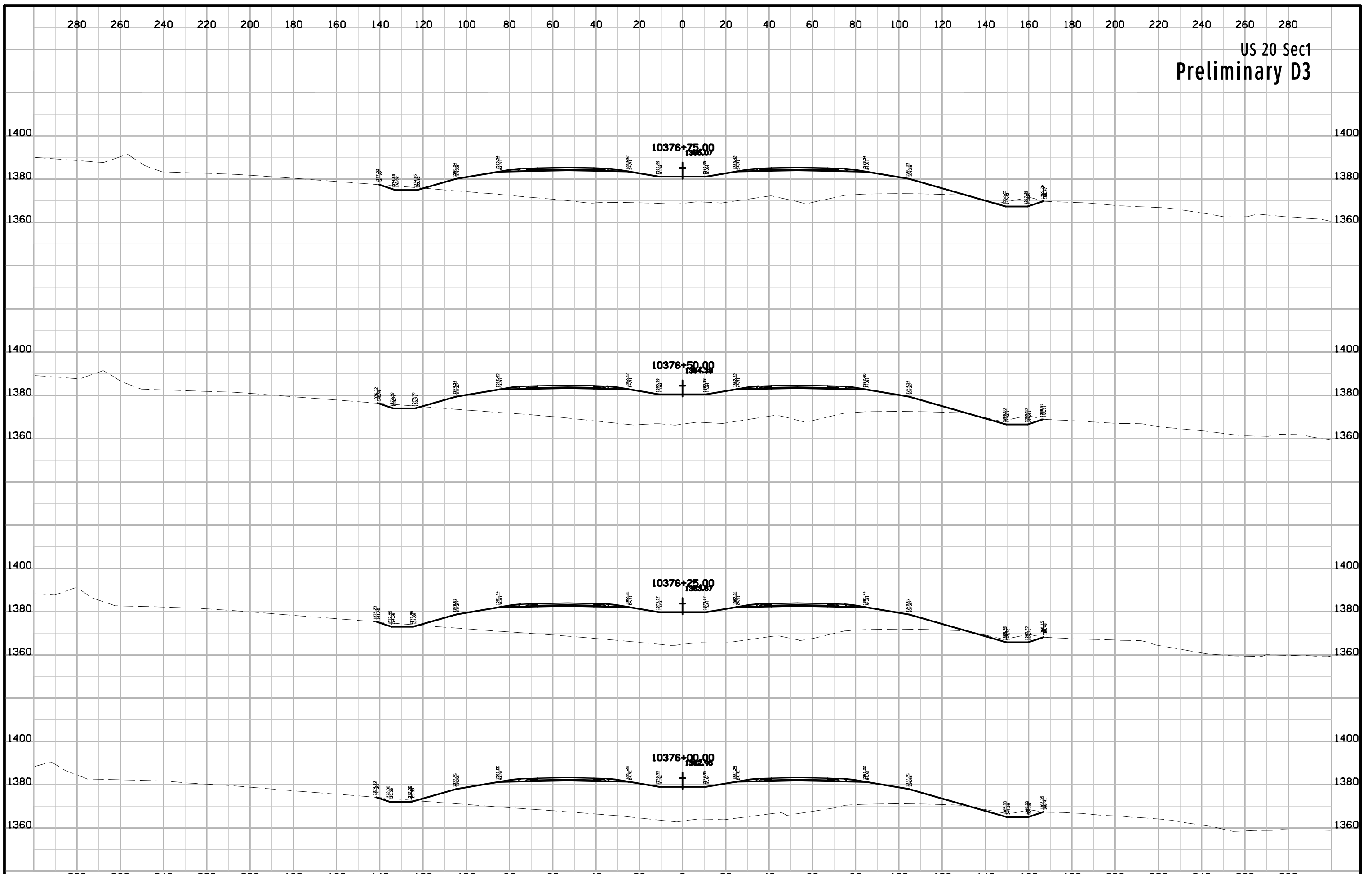
US 20 Sec1
Preliminary D3



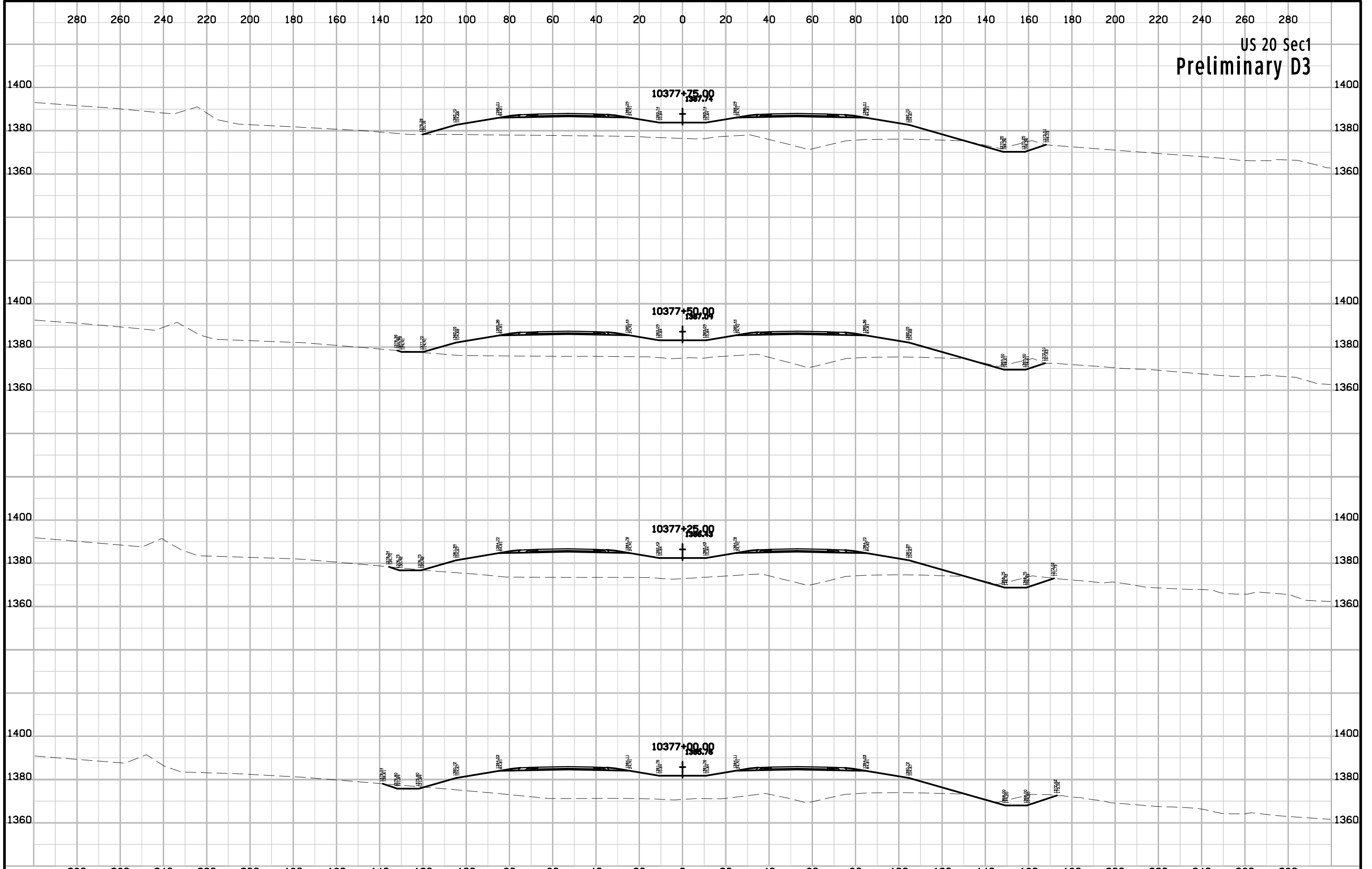
US 20 Sec1
Preliminary D3



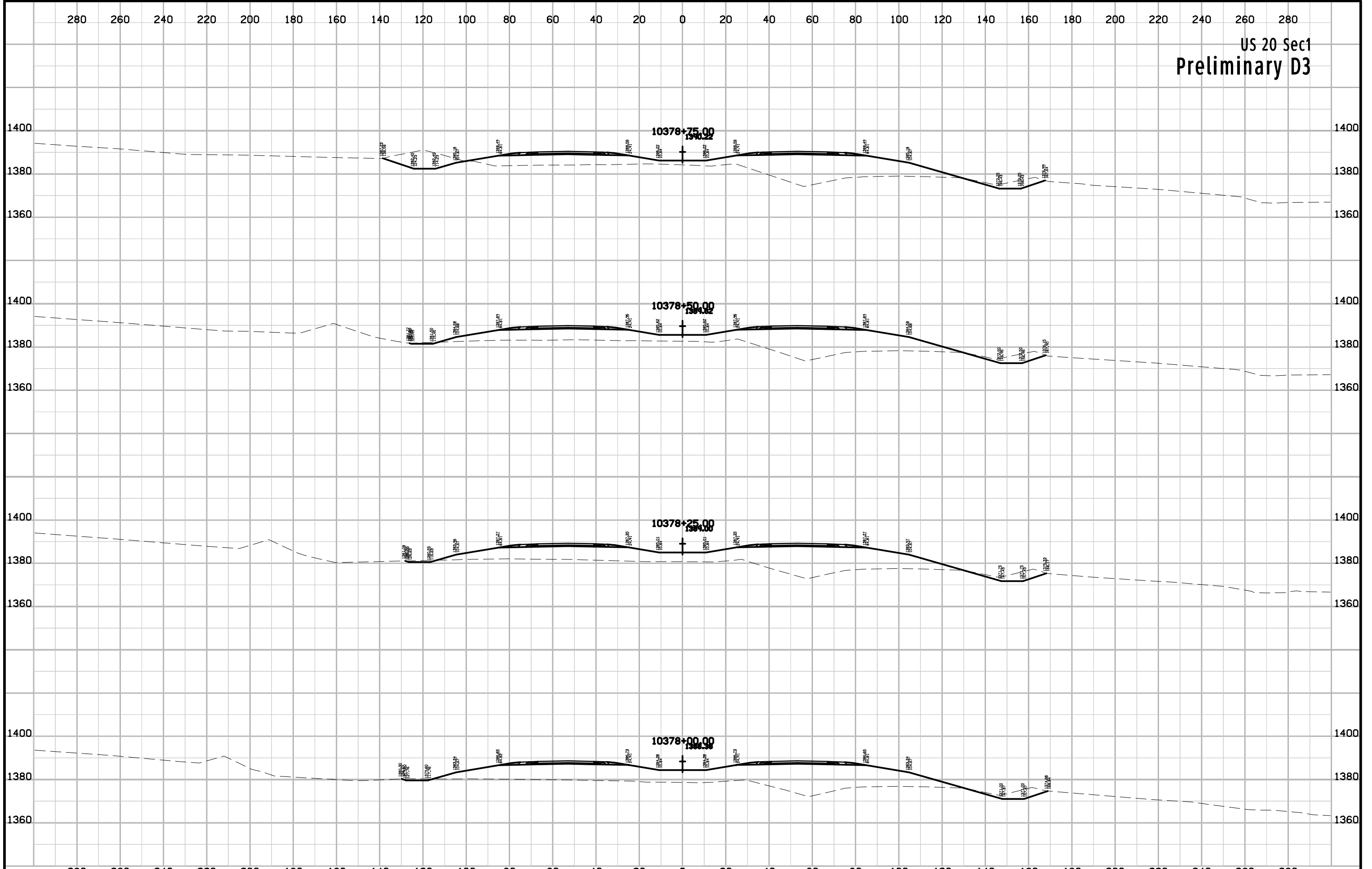
US 20 Sec1
Preliminary D3

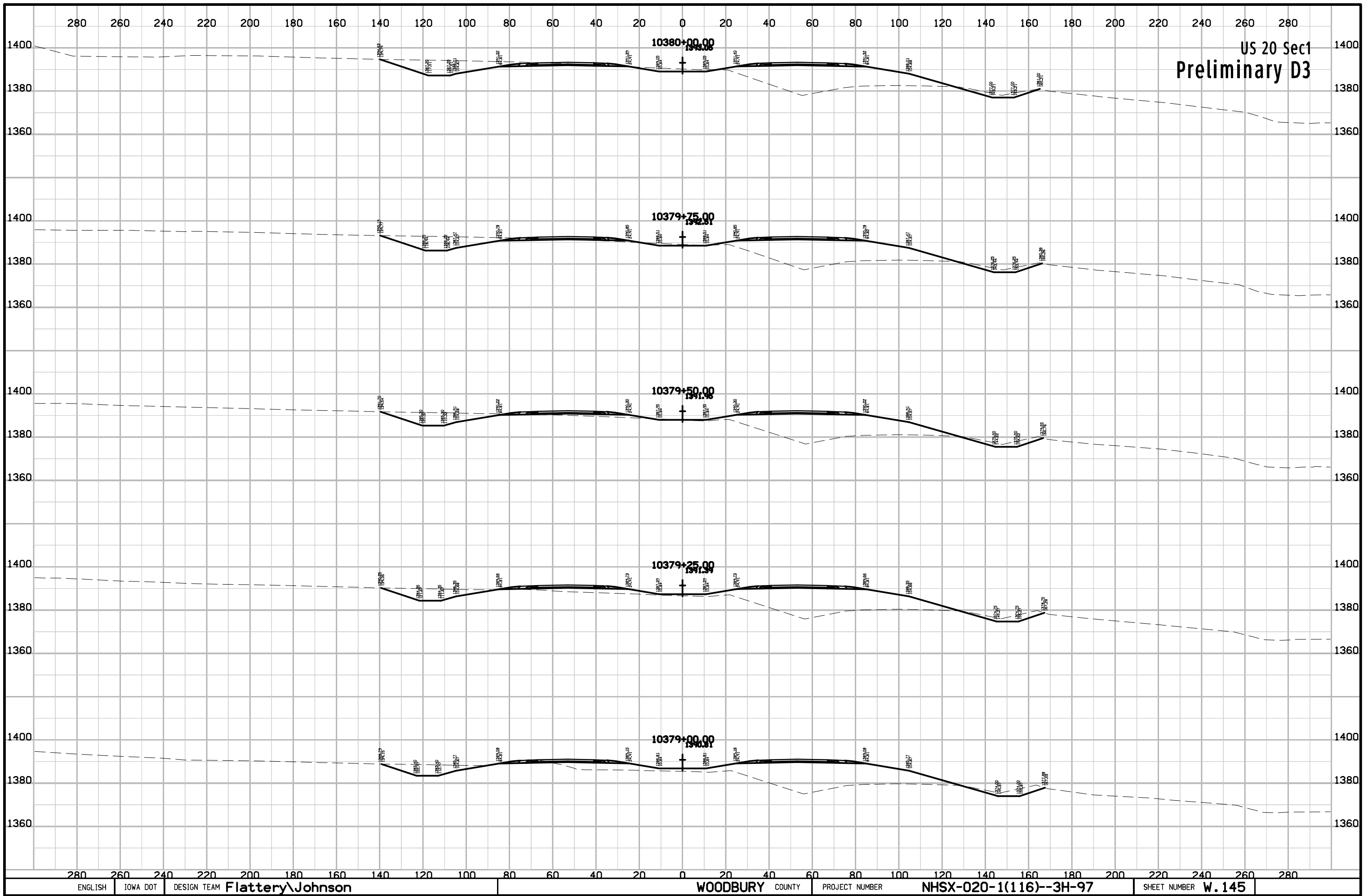


US 20 Sec1
Preliminary D3

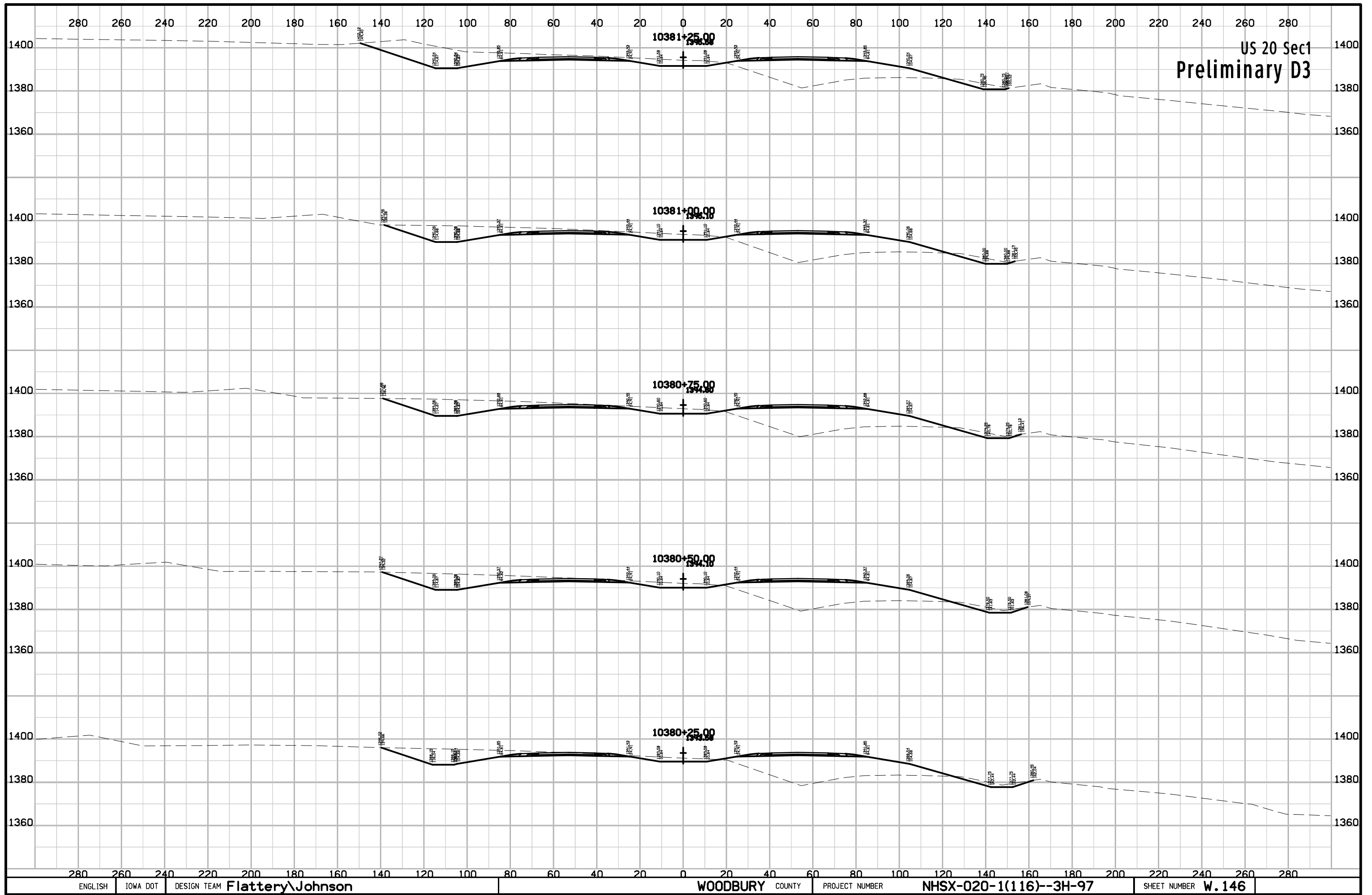


US 20 Sec1
Preliminary D3



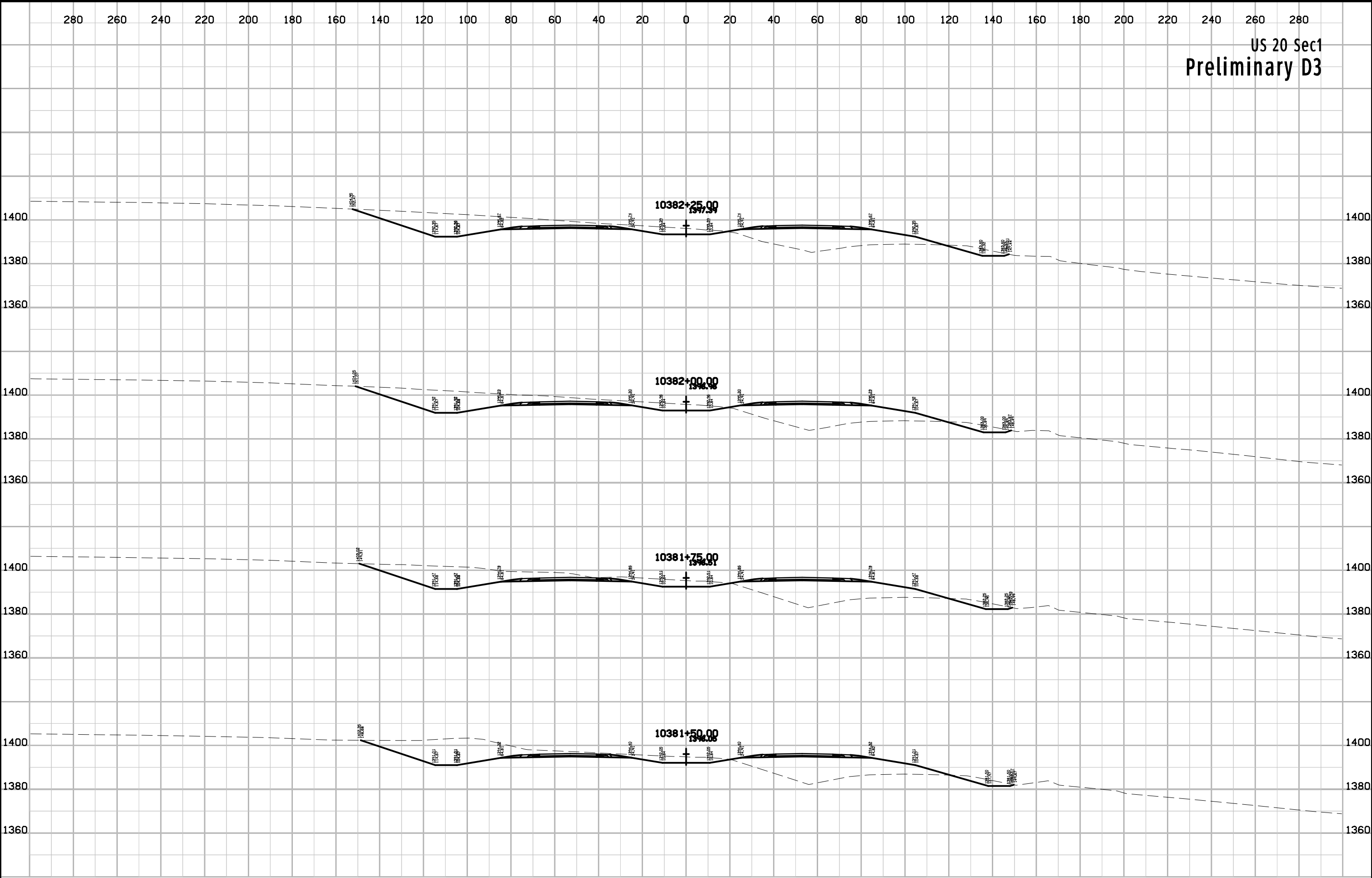


US 20 Sec1
Preliminary D3

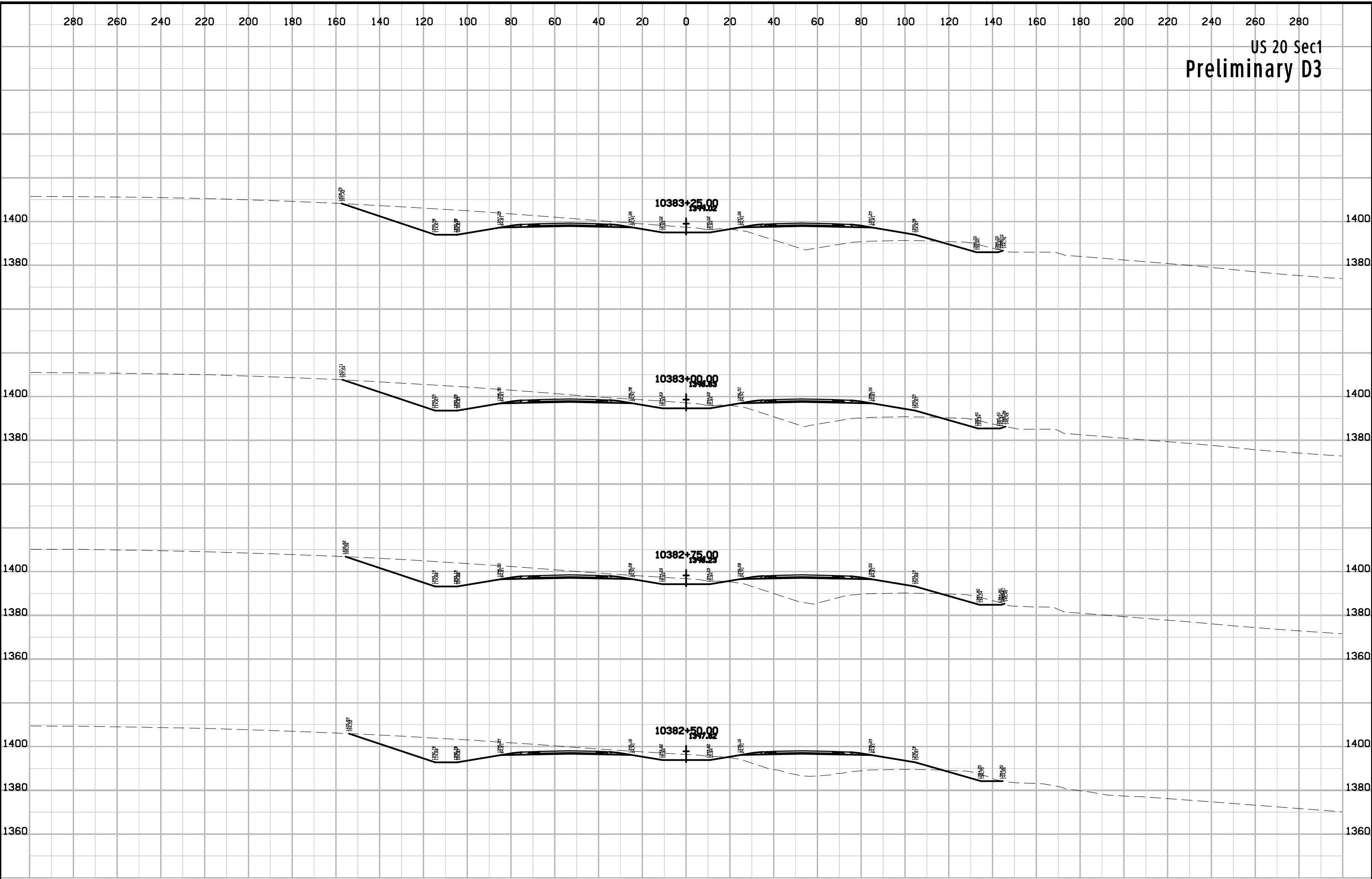


US 20 Sec1
Preliminary D3

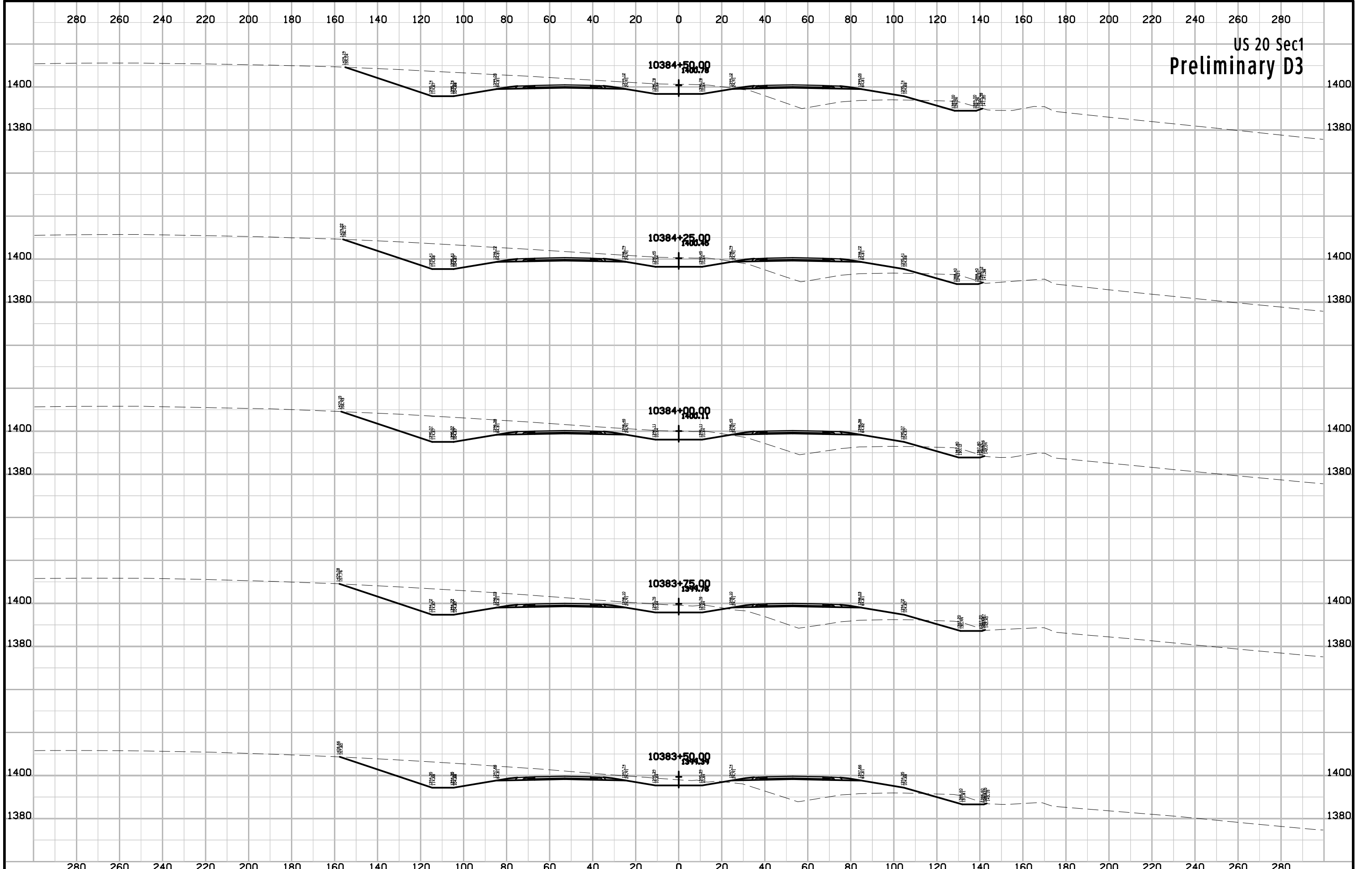
US 20 Sec1
Preliminary D3



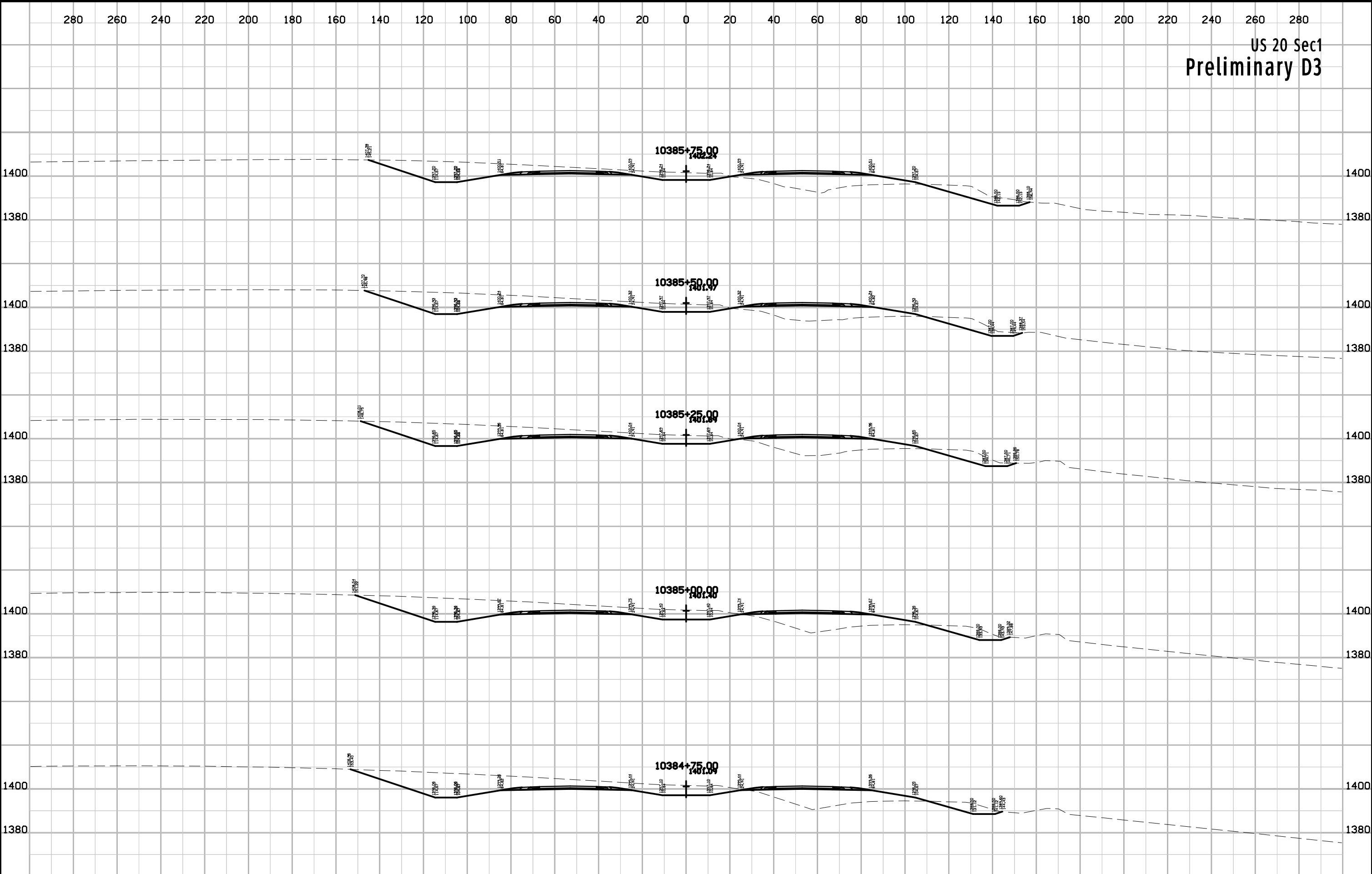
US 20 Sec1
Preliminary D3



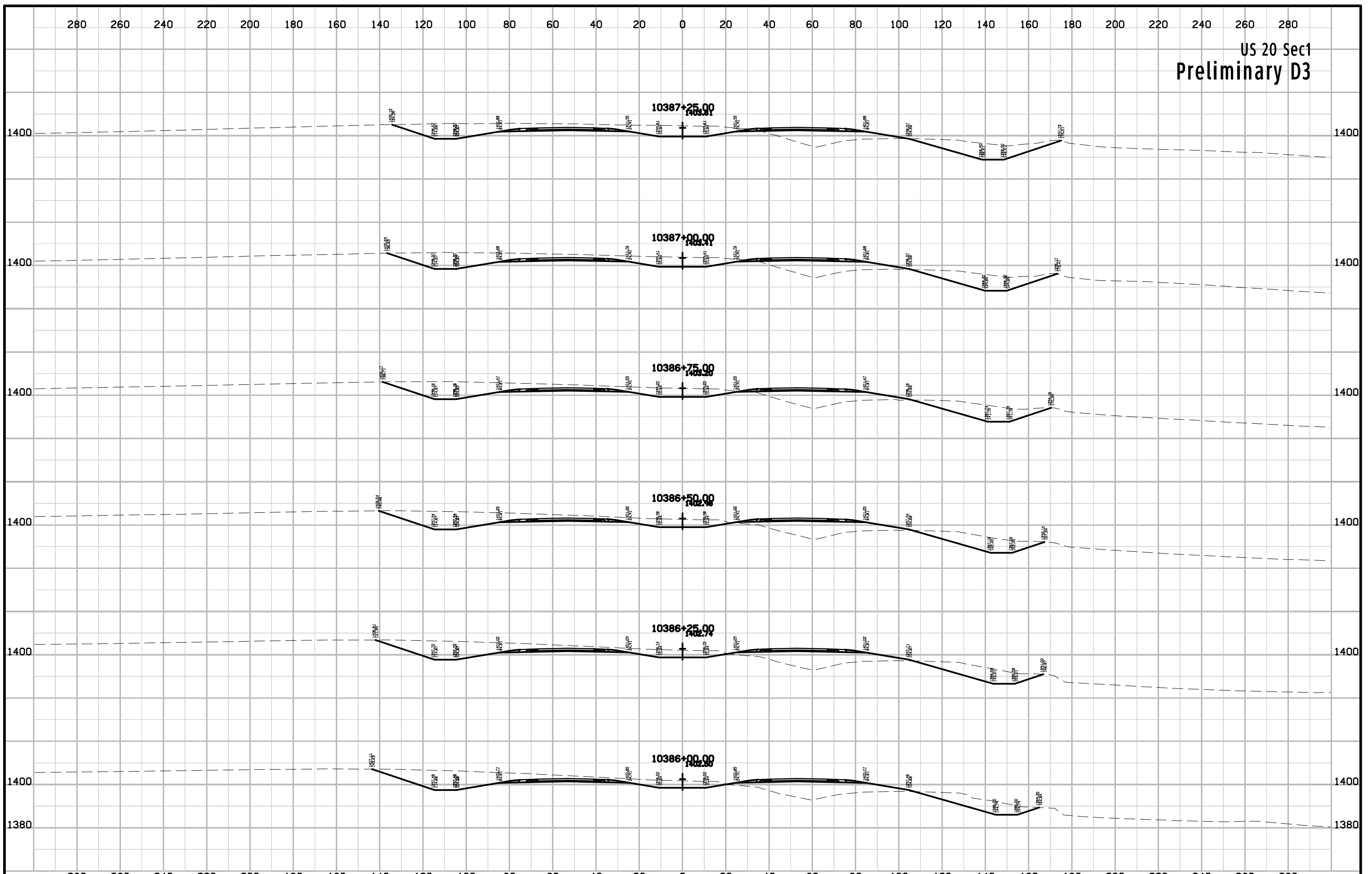
US 20 Sec1
Preliminary D3



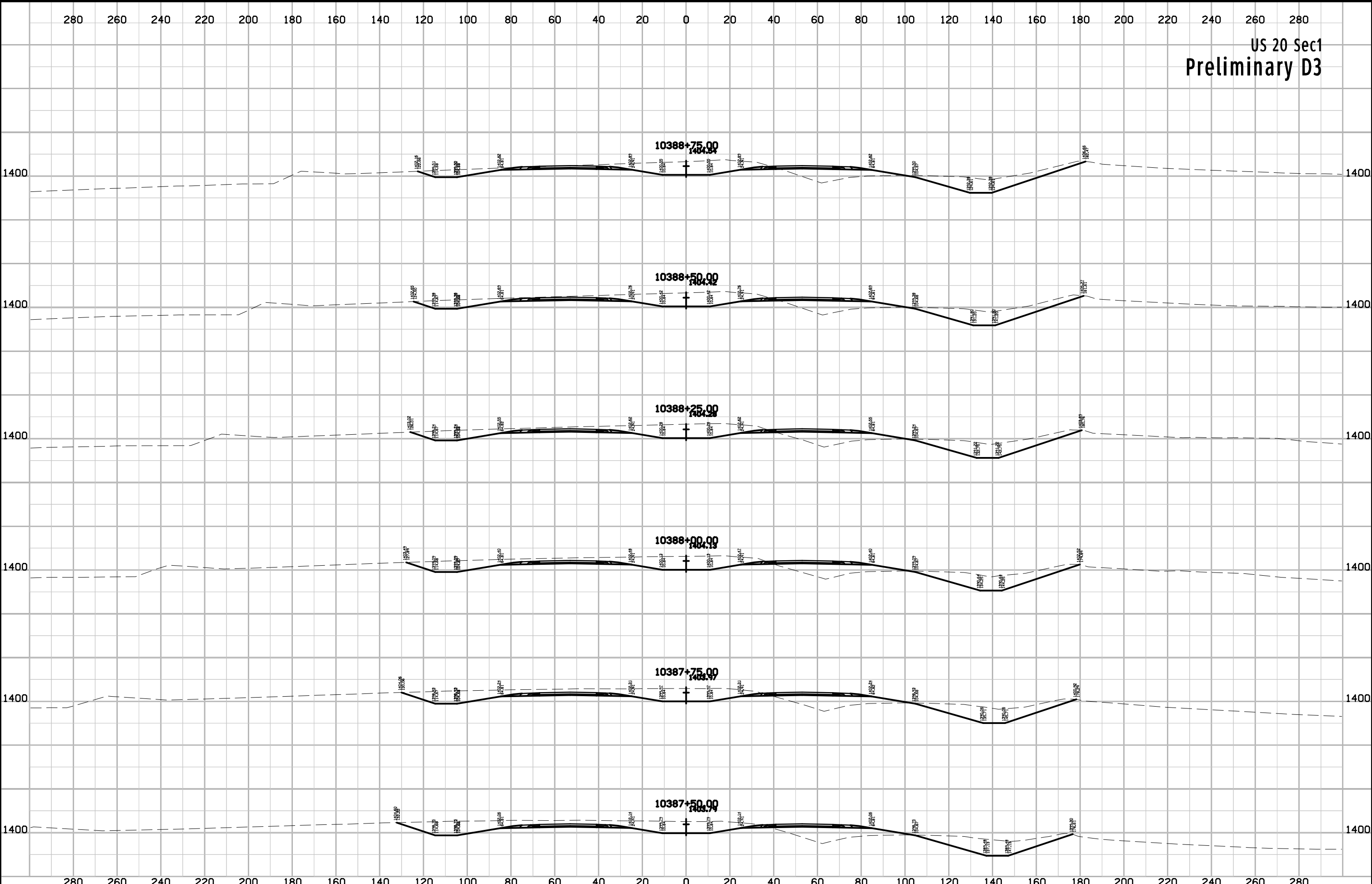
US 20 Sec1
Preliminary D3



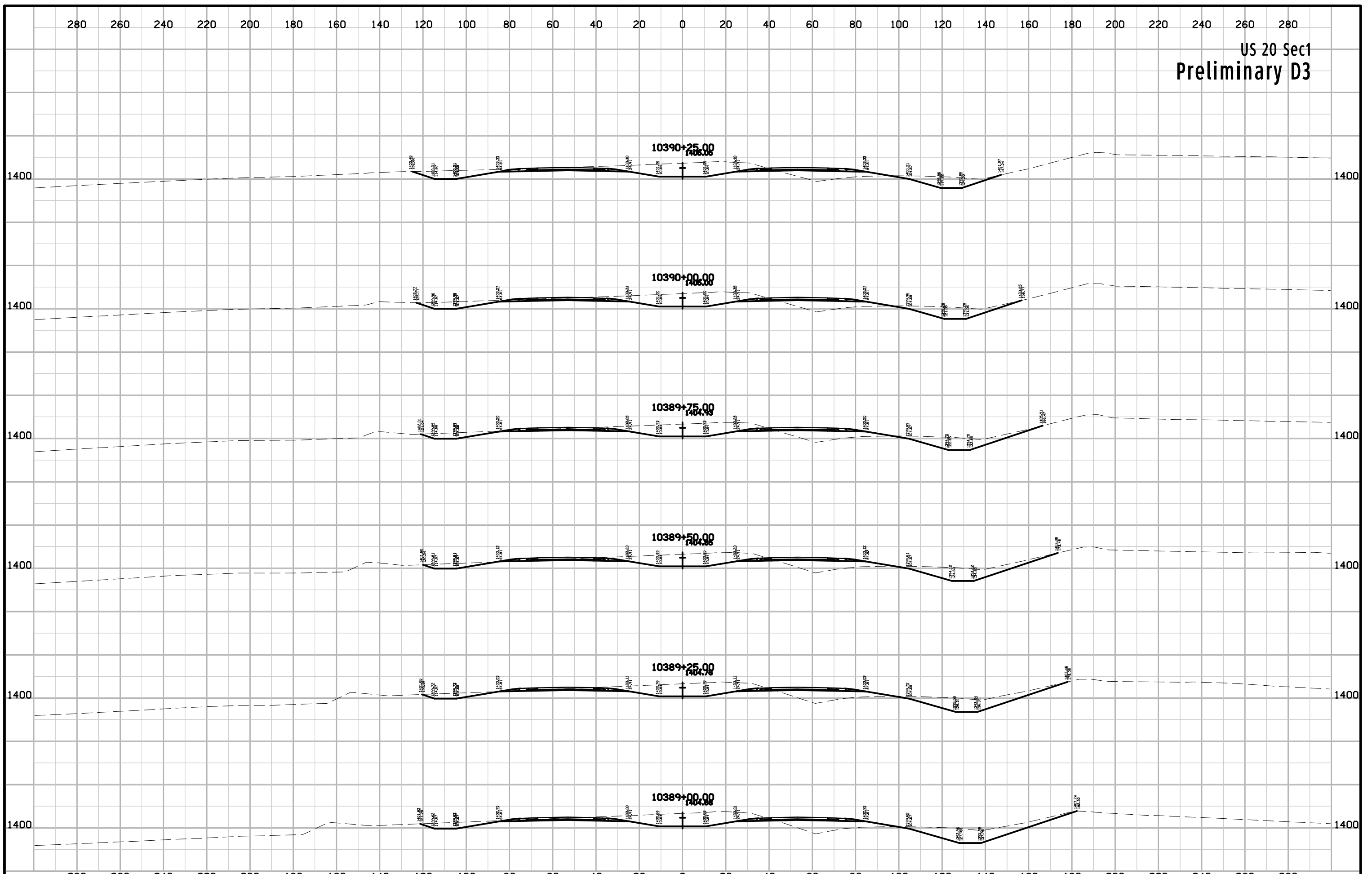
US 20 Sec1
Preliminary D3

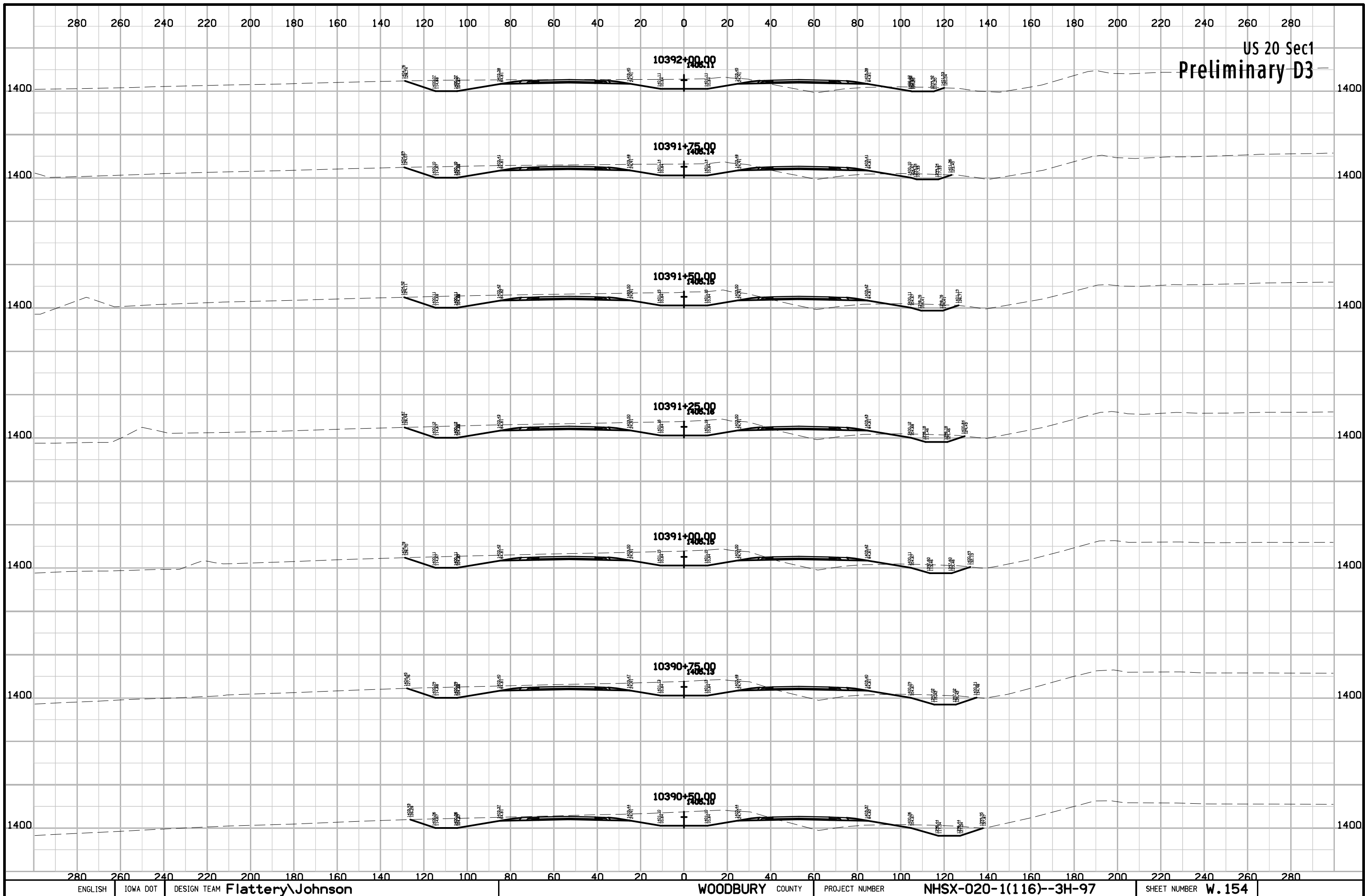


US 20 Sec1
Preliminary D3



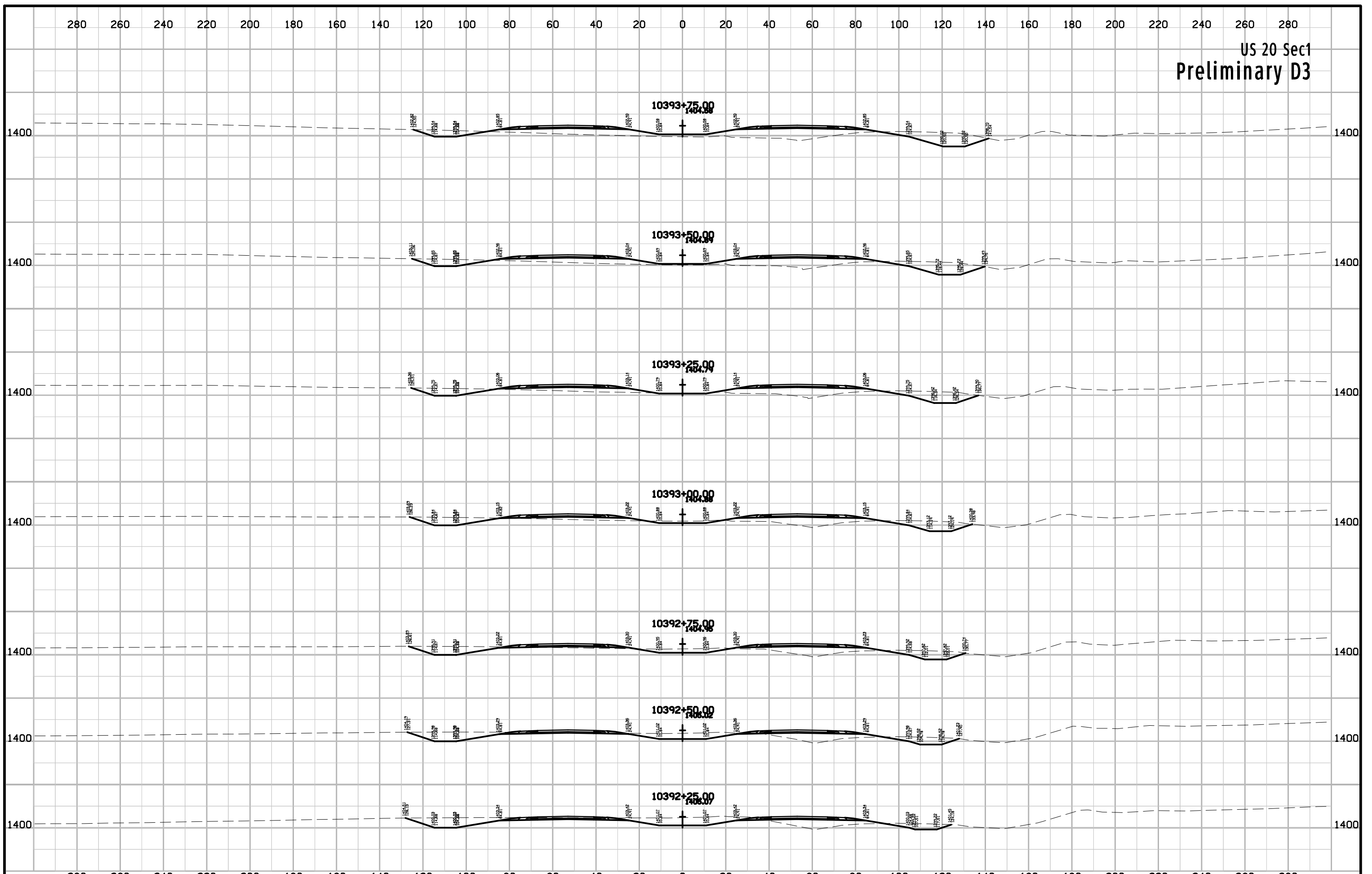
US 20 Sec1
Preliminary D3



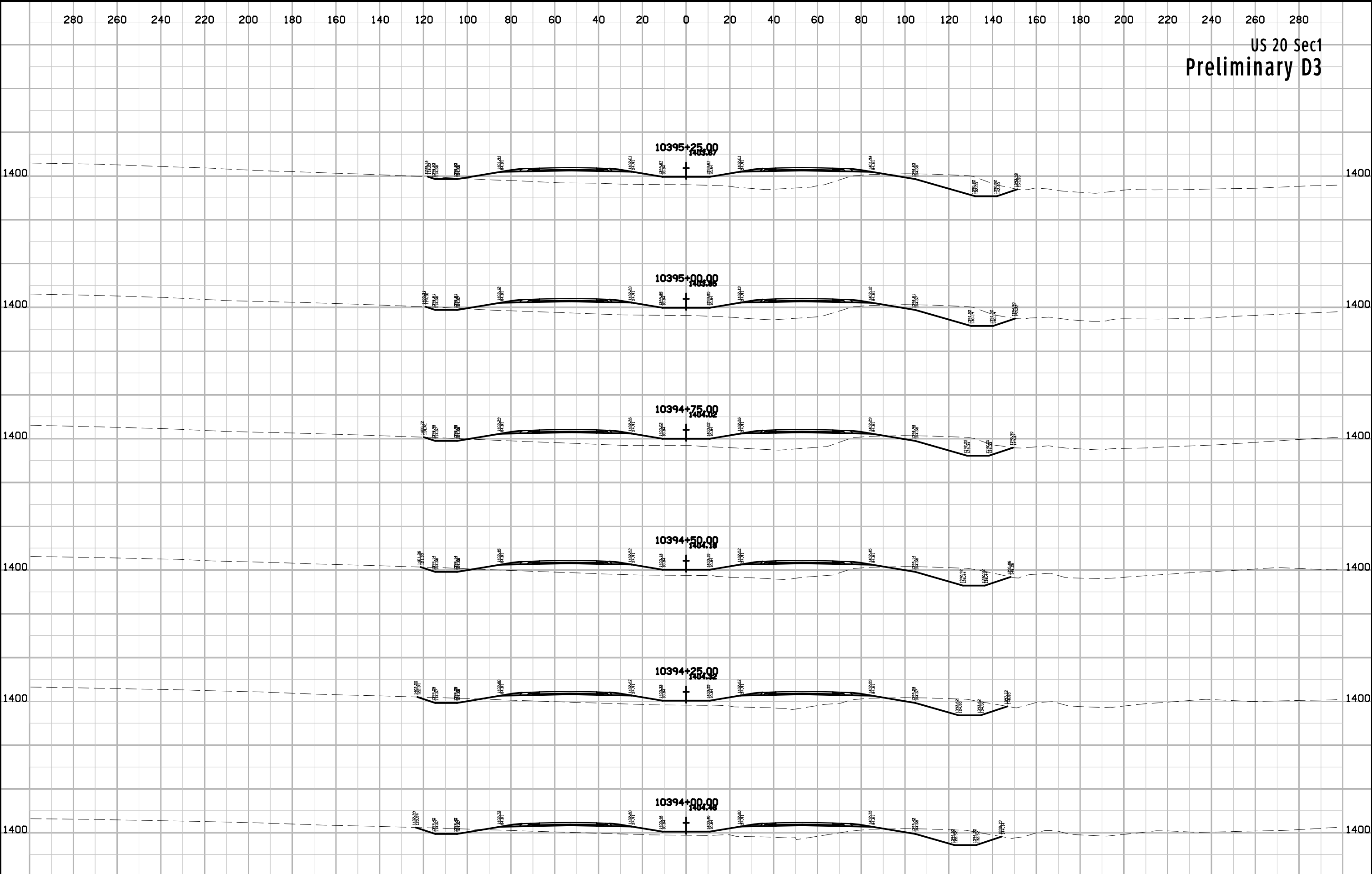


US 20 Sec1
Preliminary D3

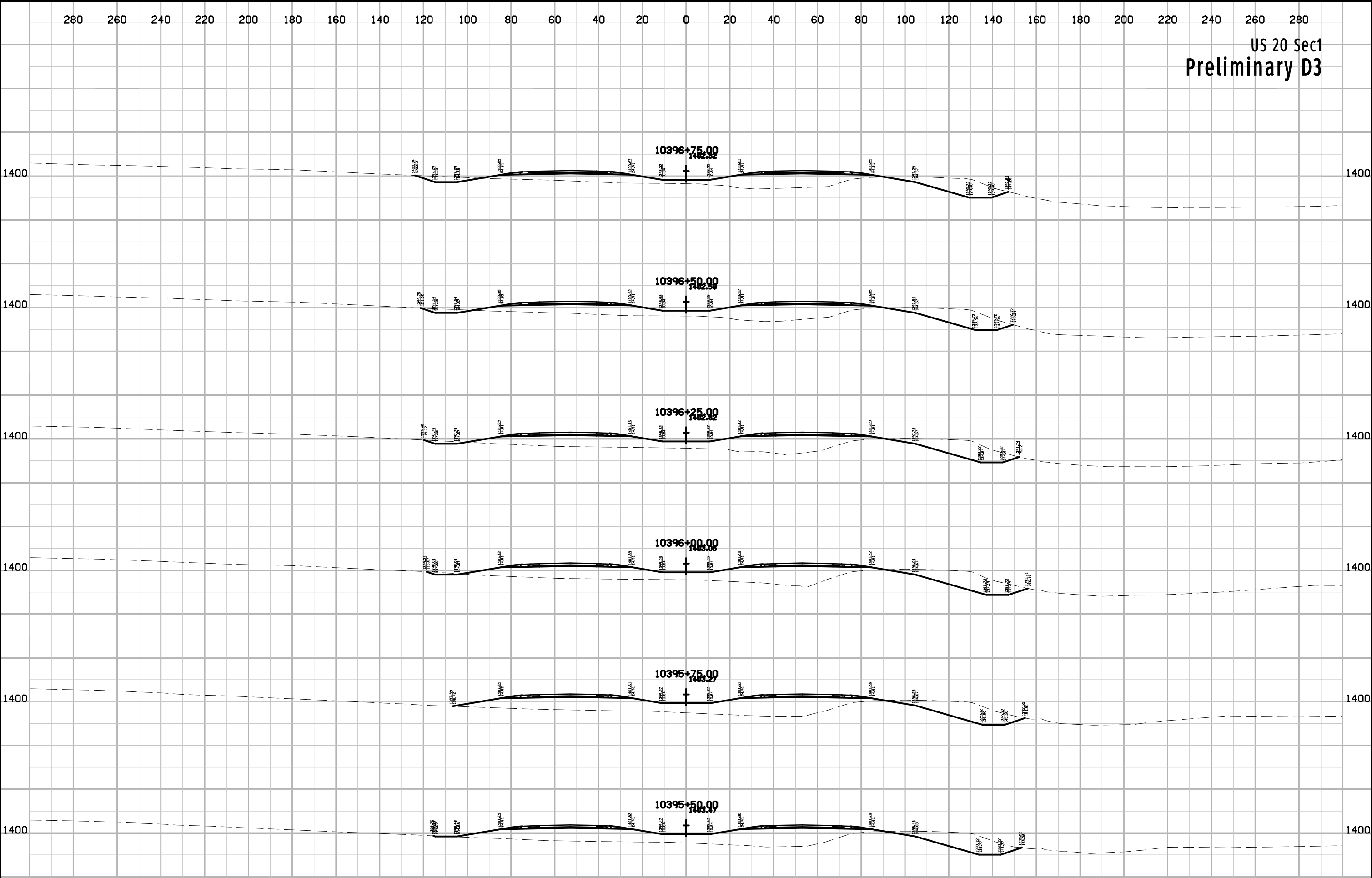
US 20 Sec1
Preliminary D3



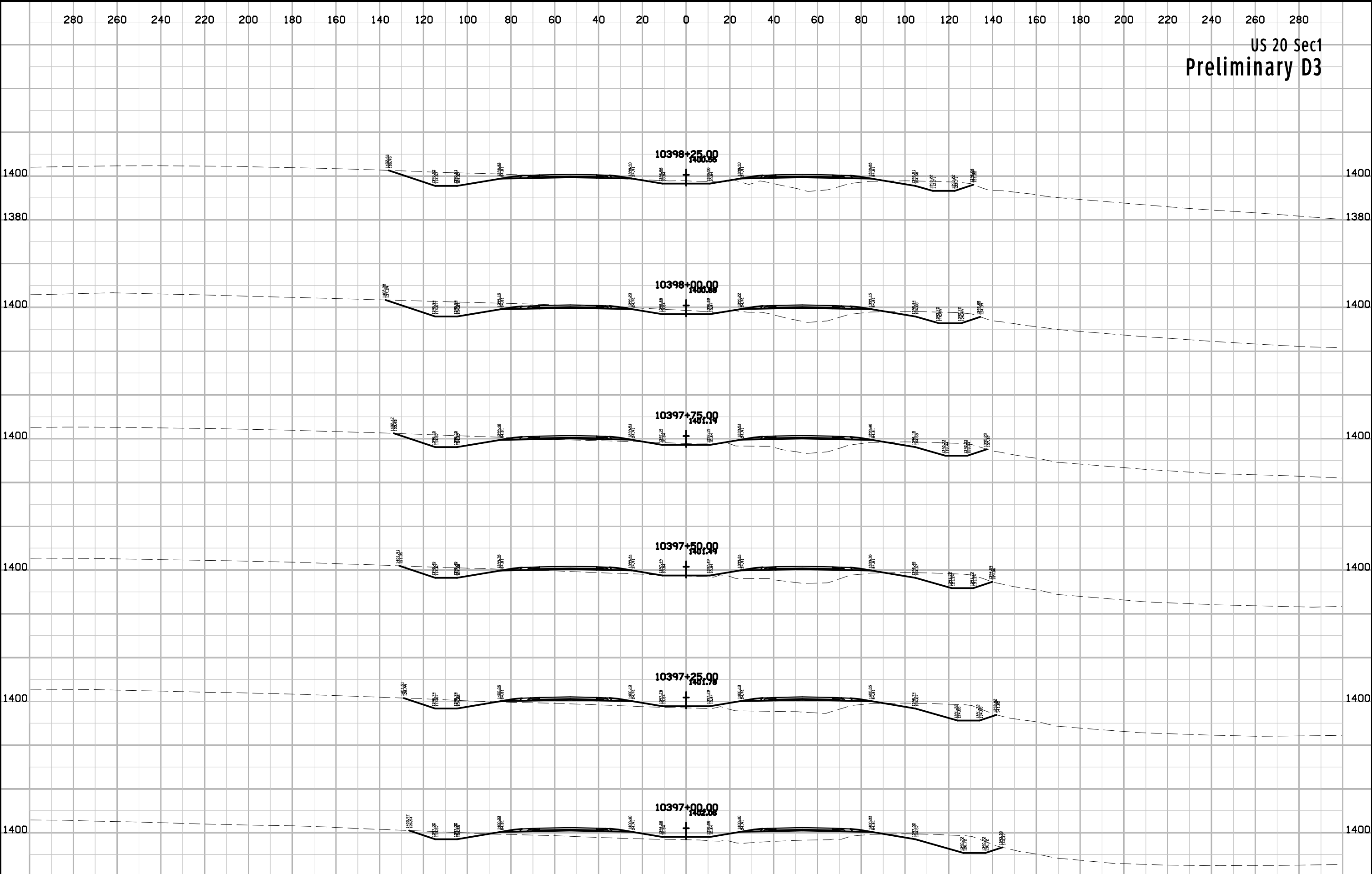
US 20 Sec1
Preliminary D3



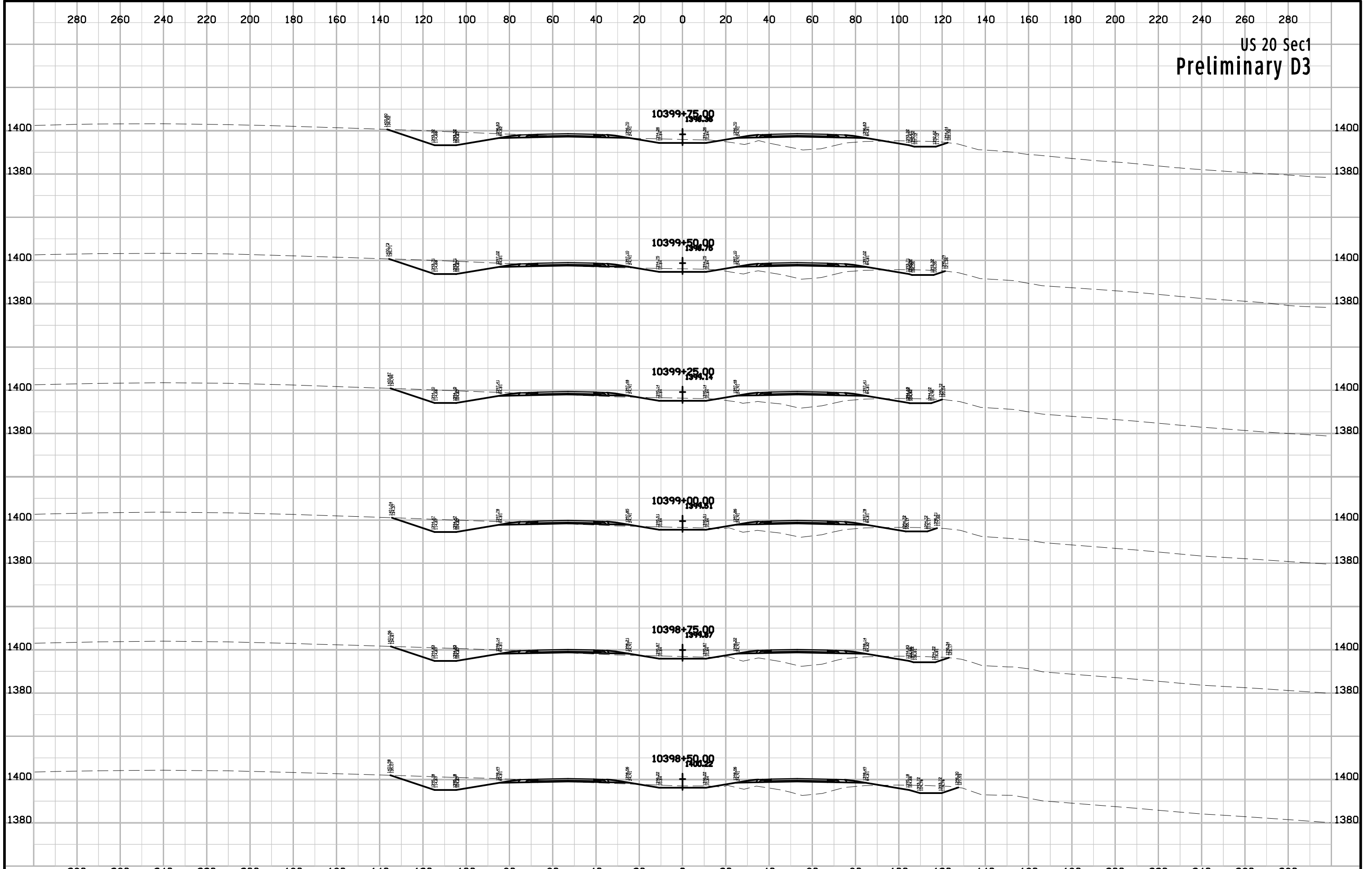
US 20 Sec1
Preliminary D3



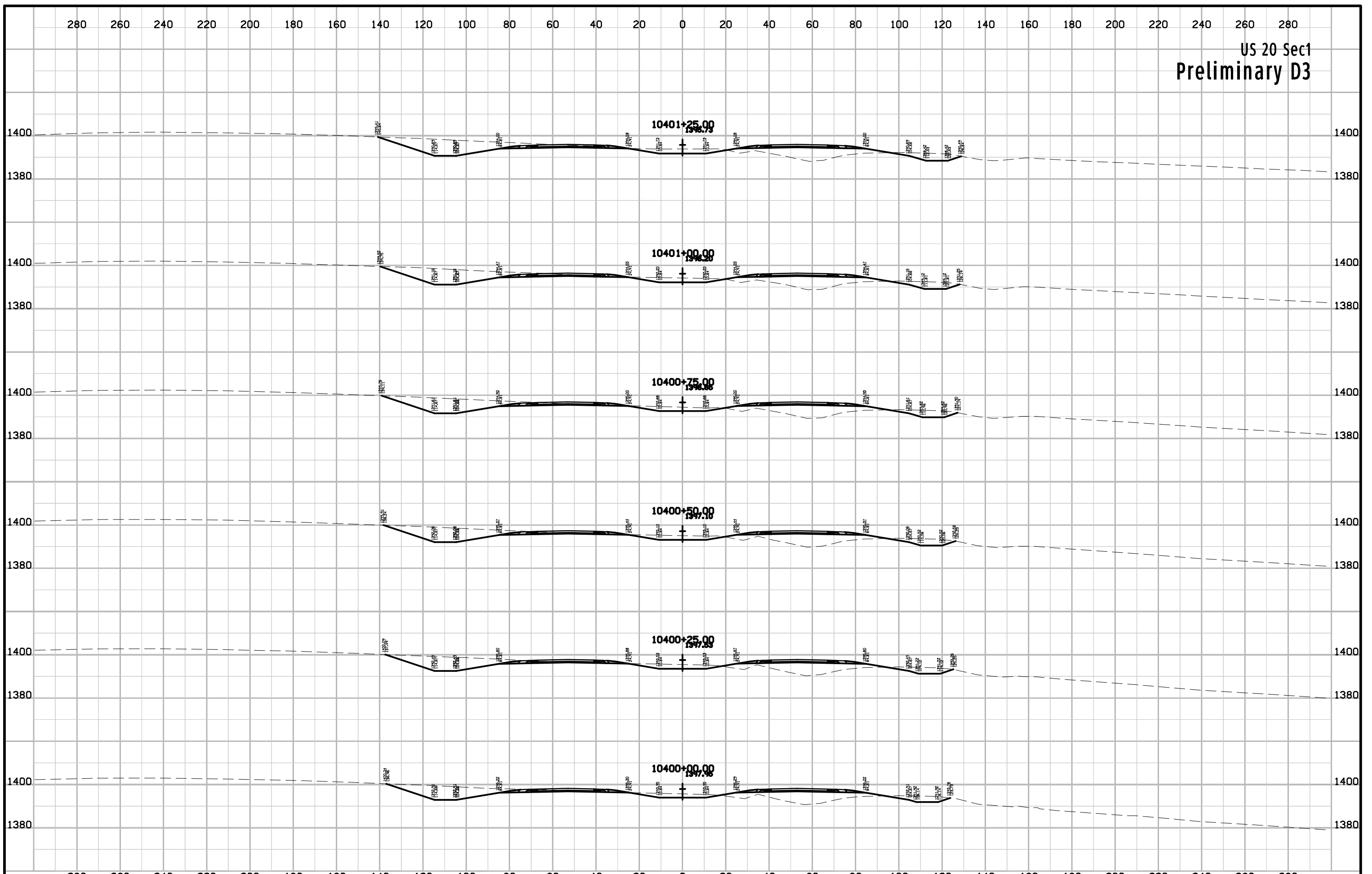
US 20 Sec1
Preliminary D3



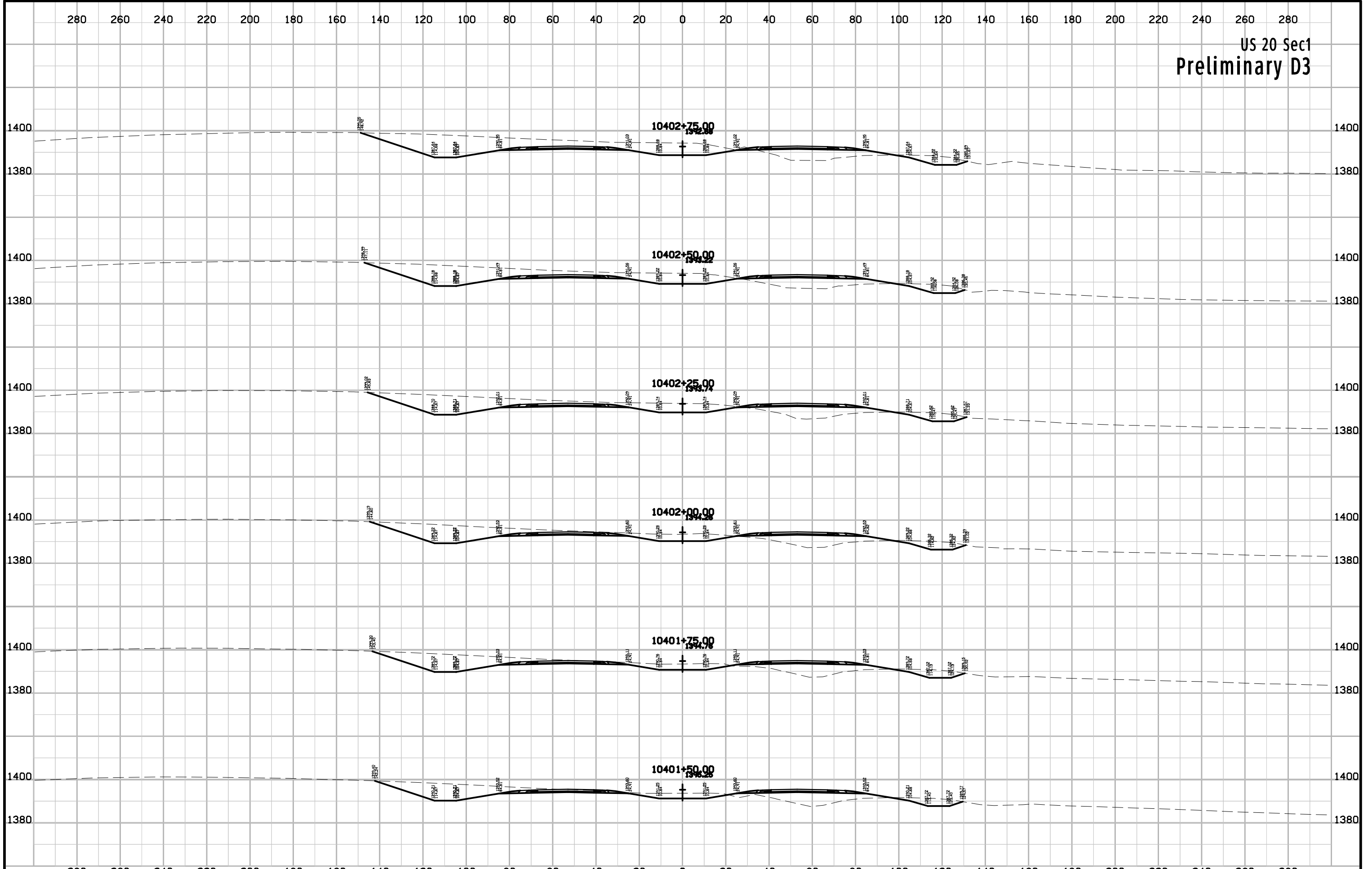
US 20 Sec1
Preliminary D3



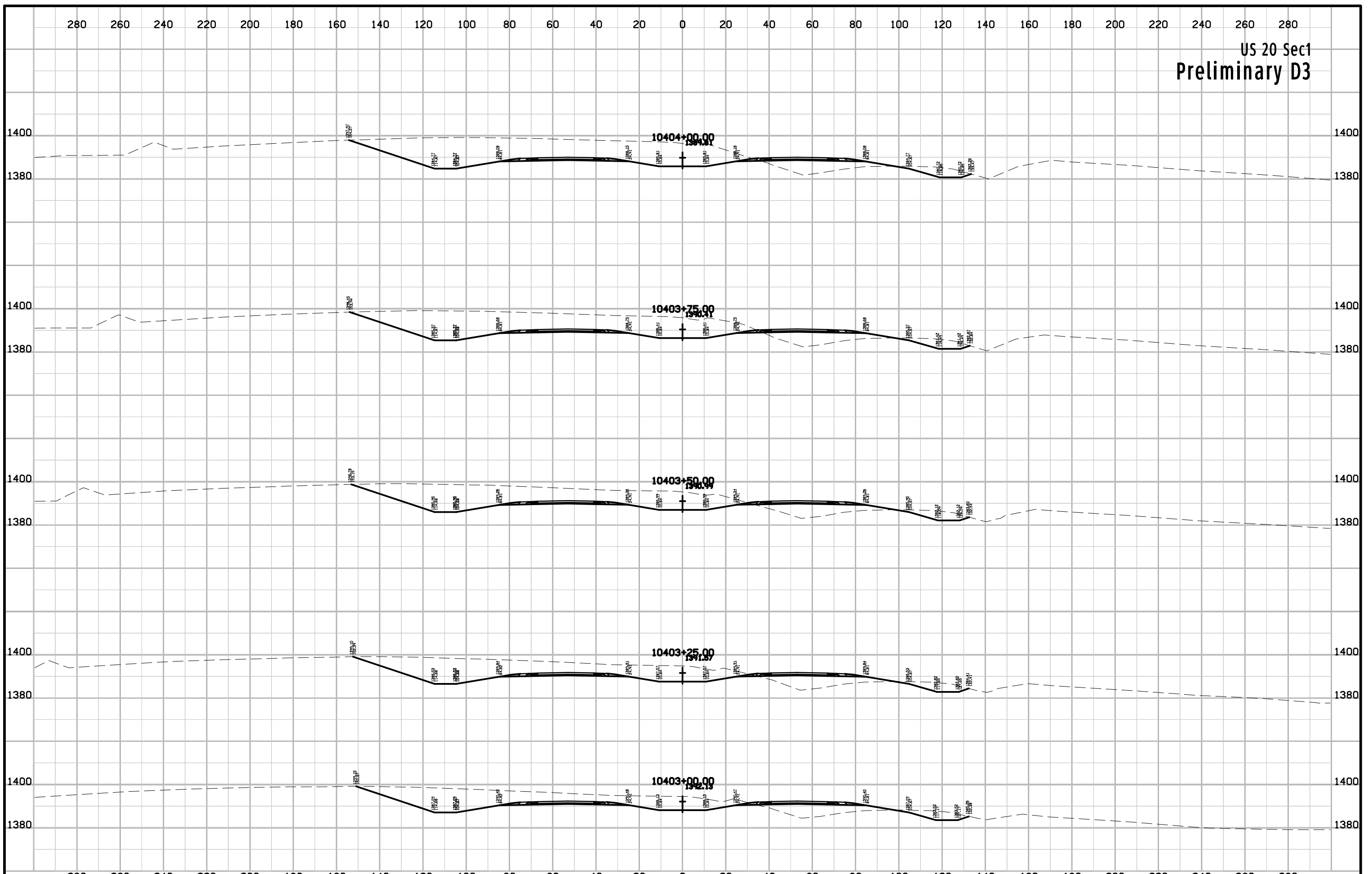
US 20 Sec1
Preliminary D3



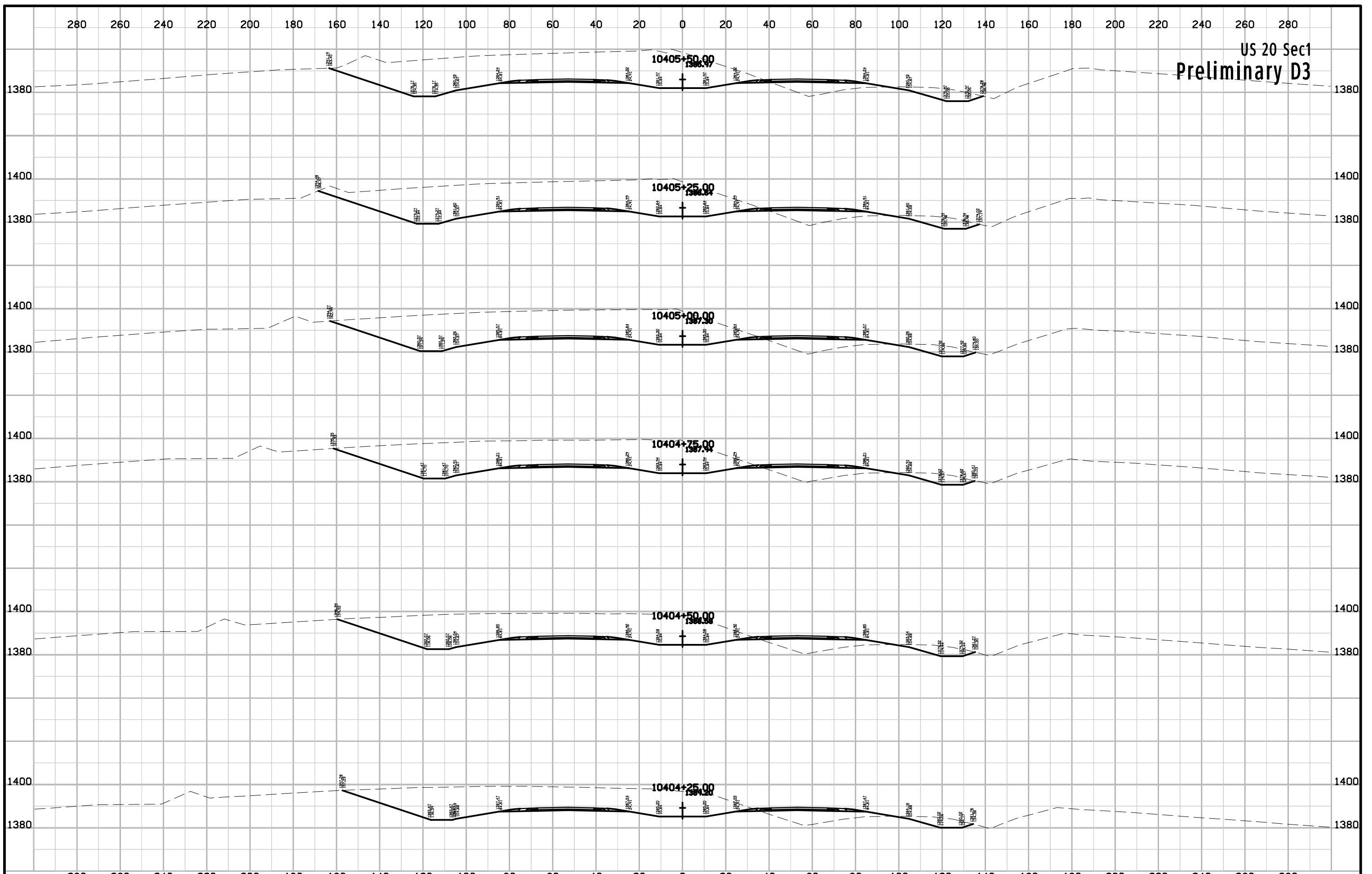
US 20 Sec1
Preliminary D3



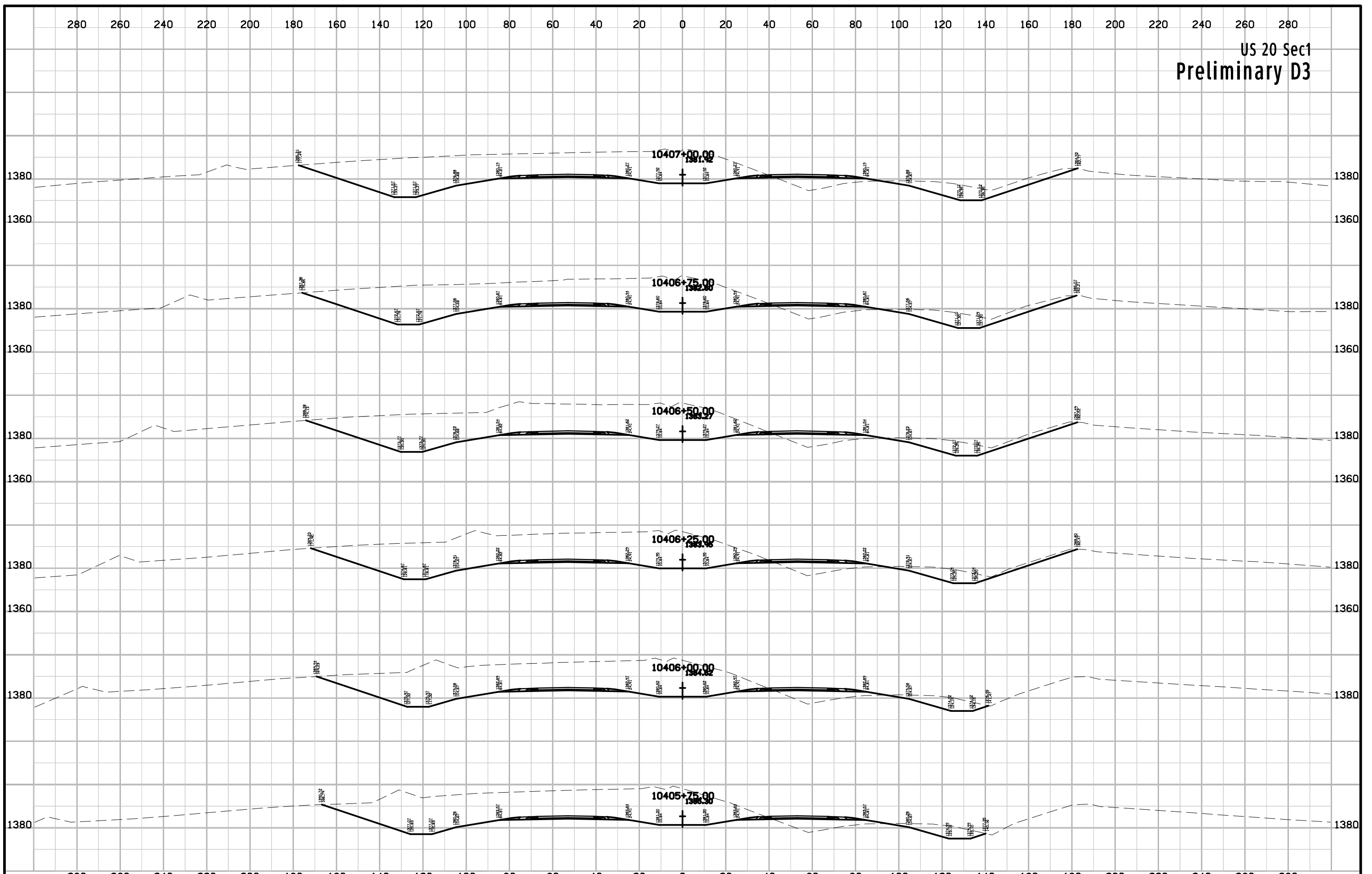
US 20 Sec1
Preliminary D3



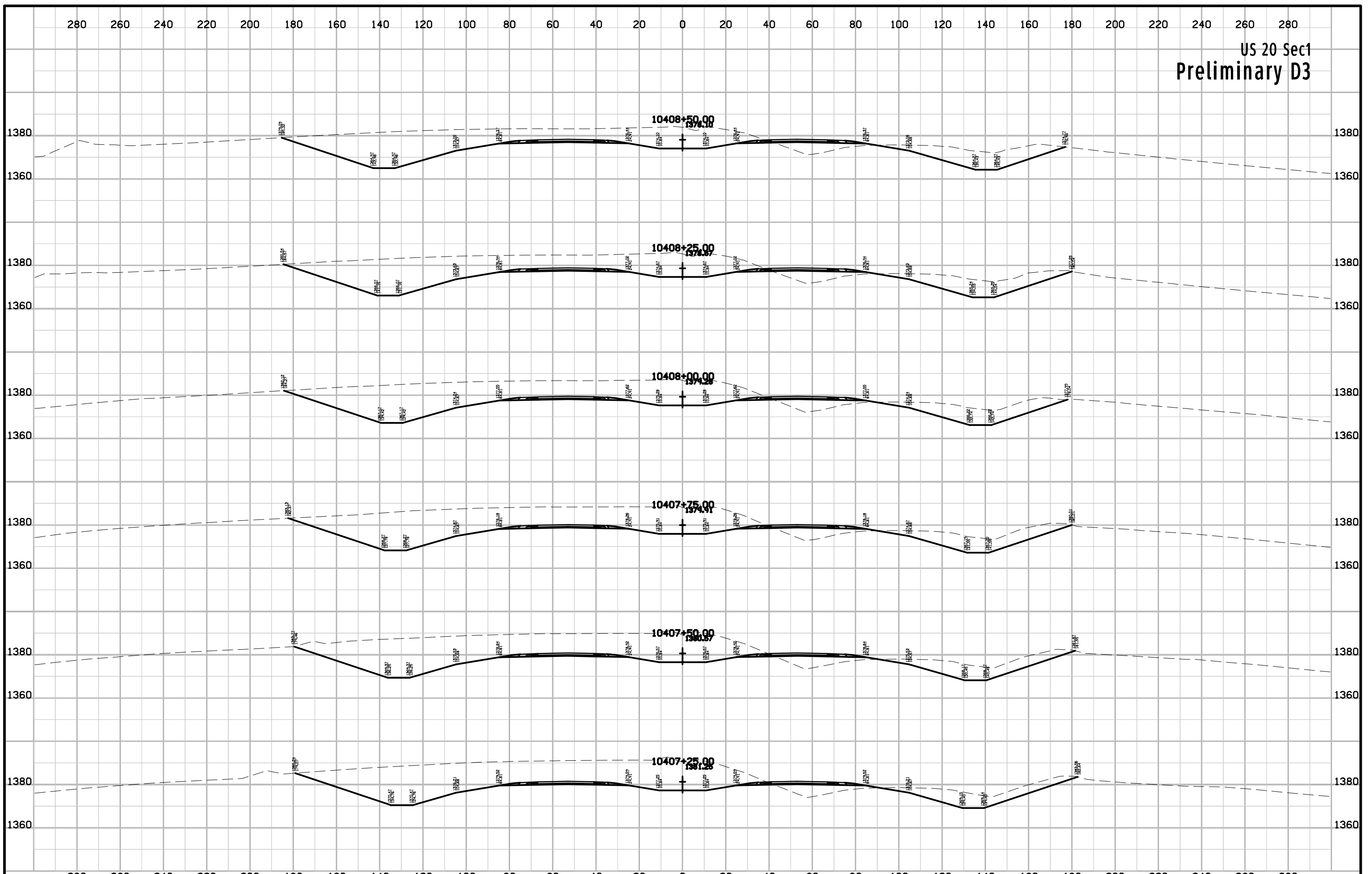
US 20 Sec1
Preliminary D3



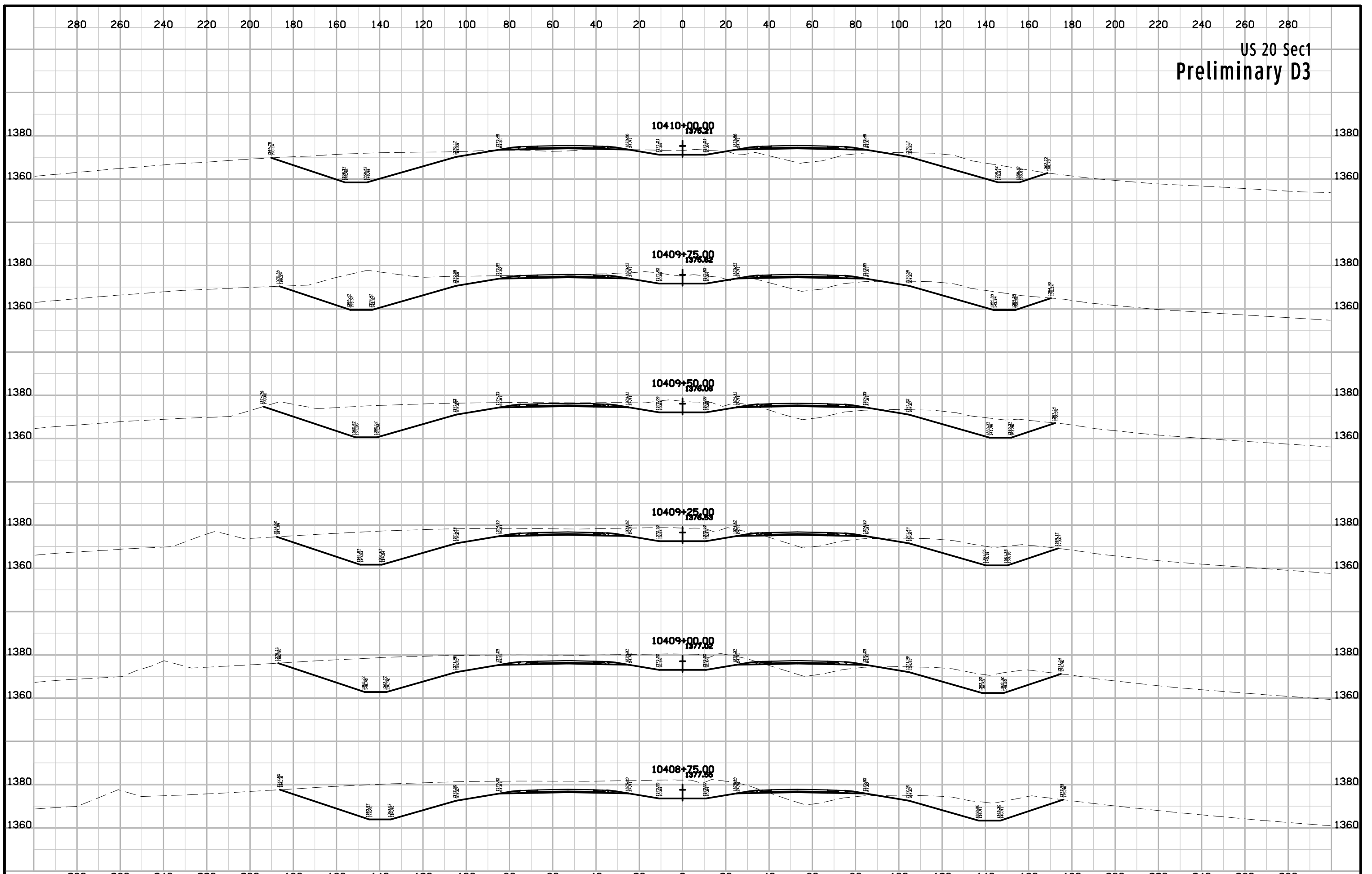
US 20 Sec1
Preliminary D3



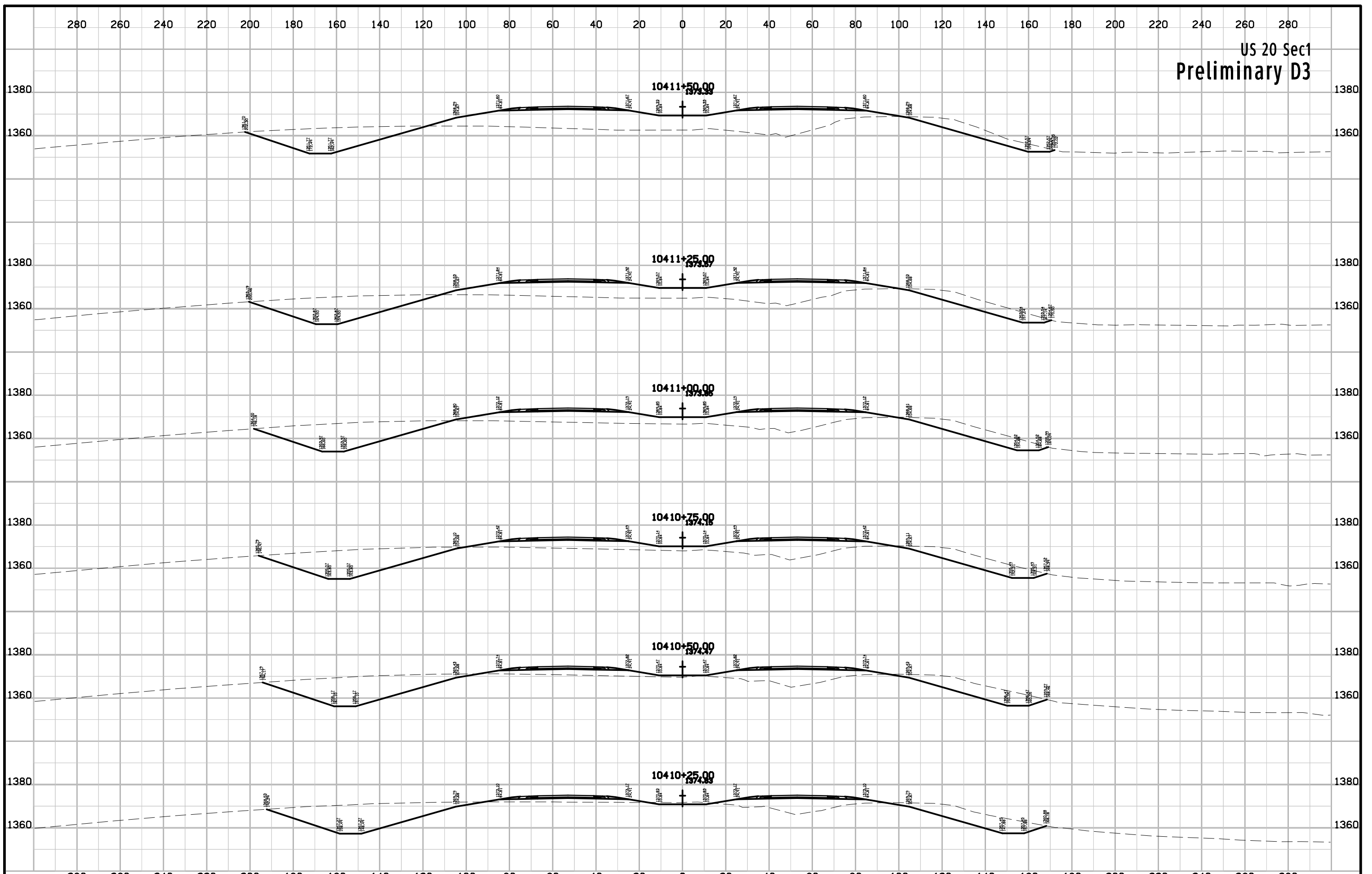
US 20 Sec1
Preliminary D3



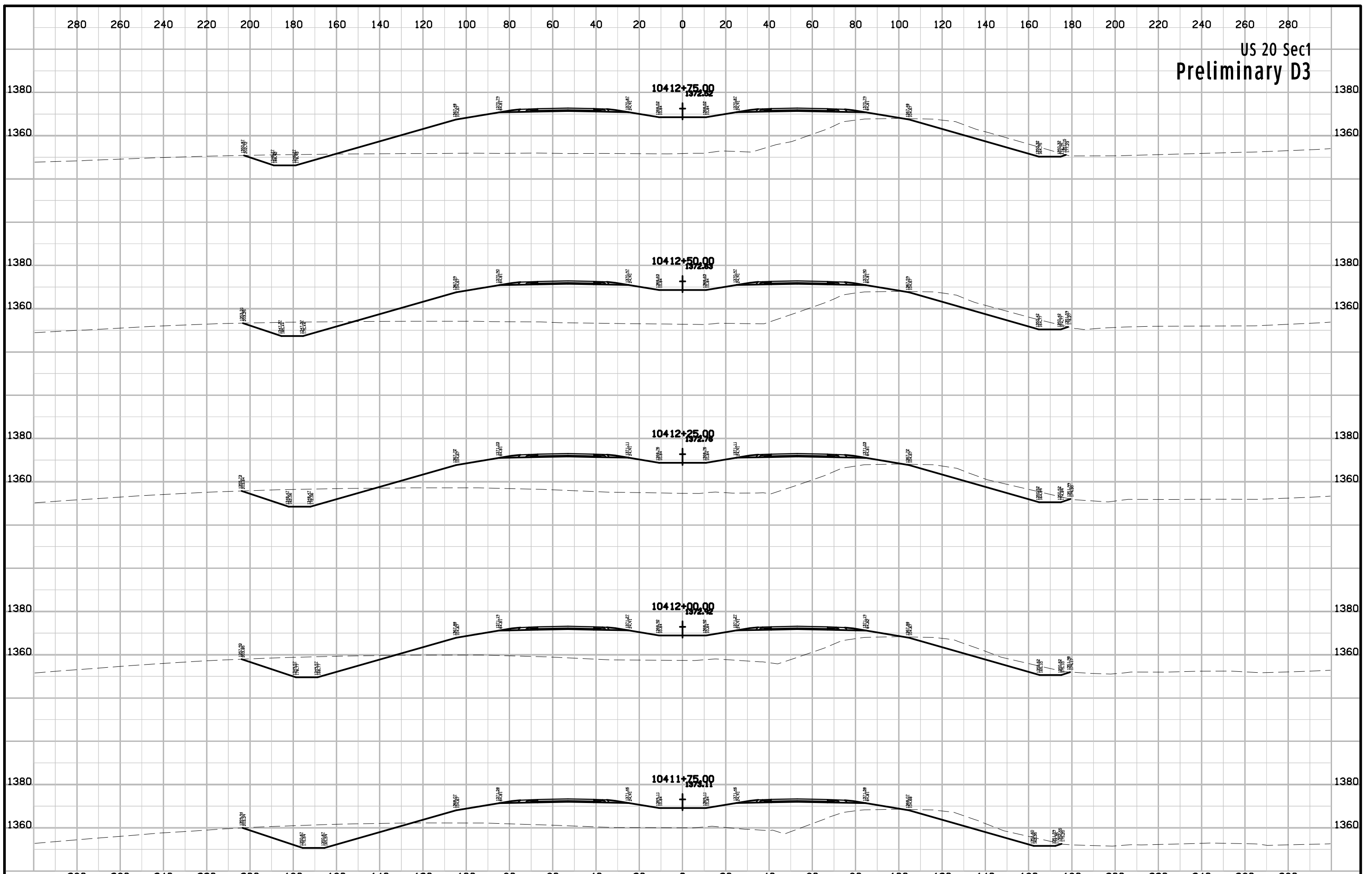
US 20 Sec1
Preliminary D3



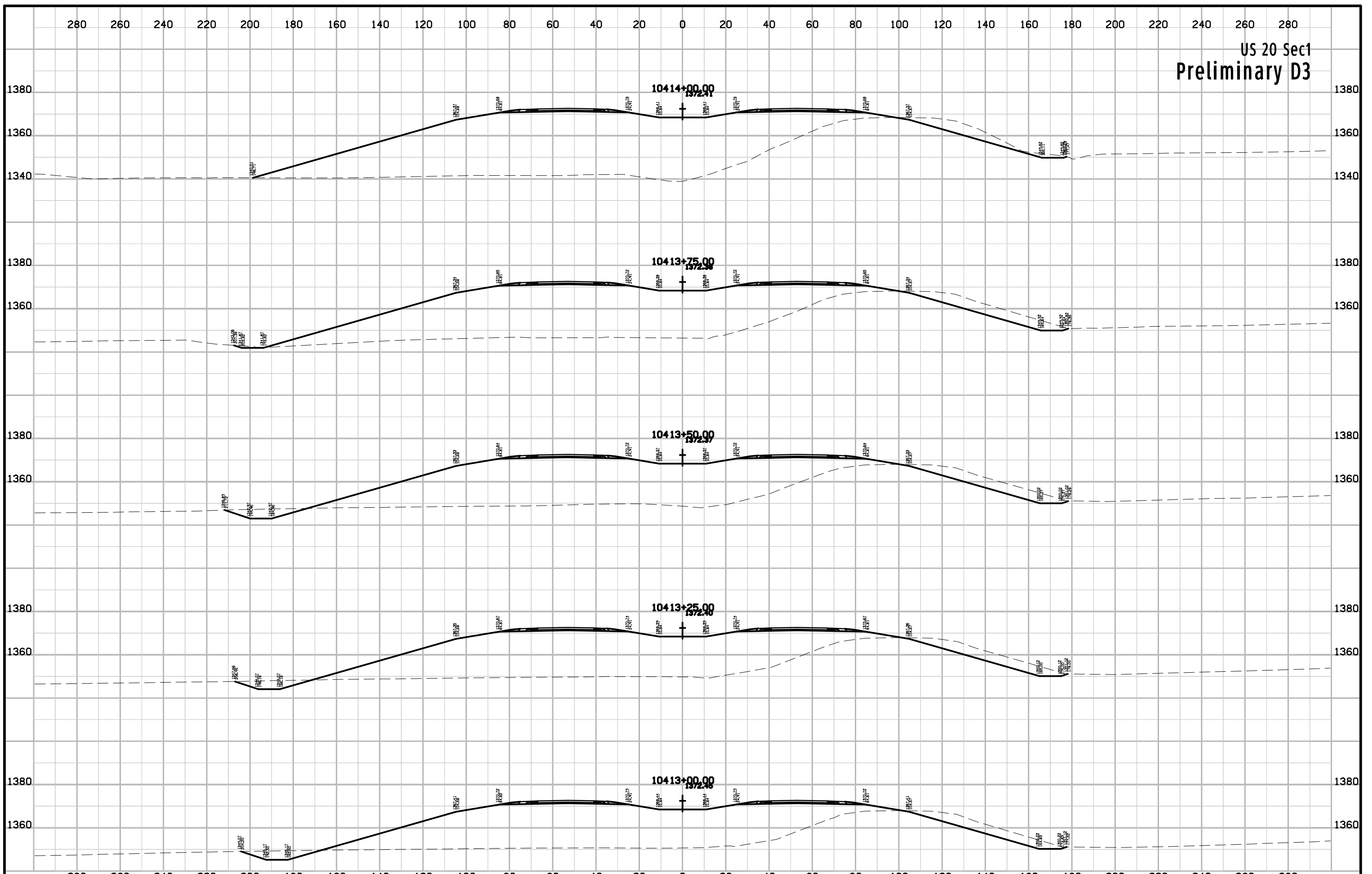
US 20 Sec1
Preliminary D3

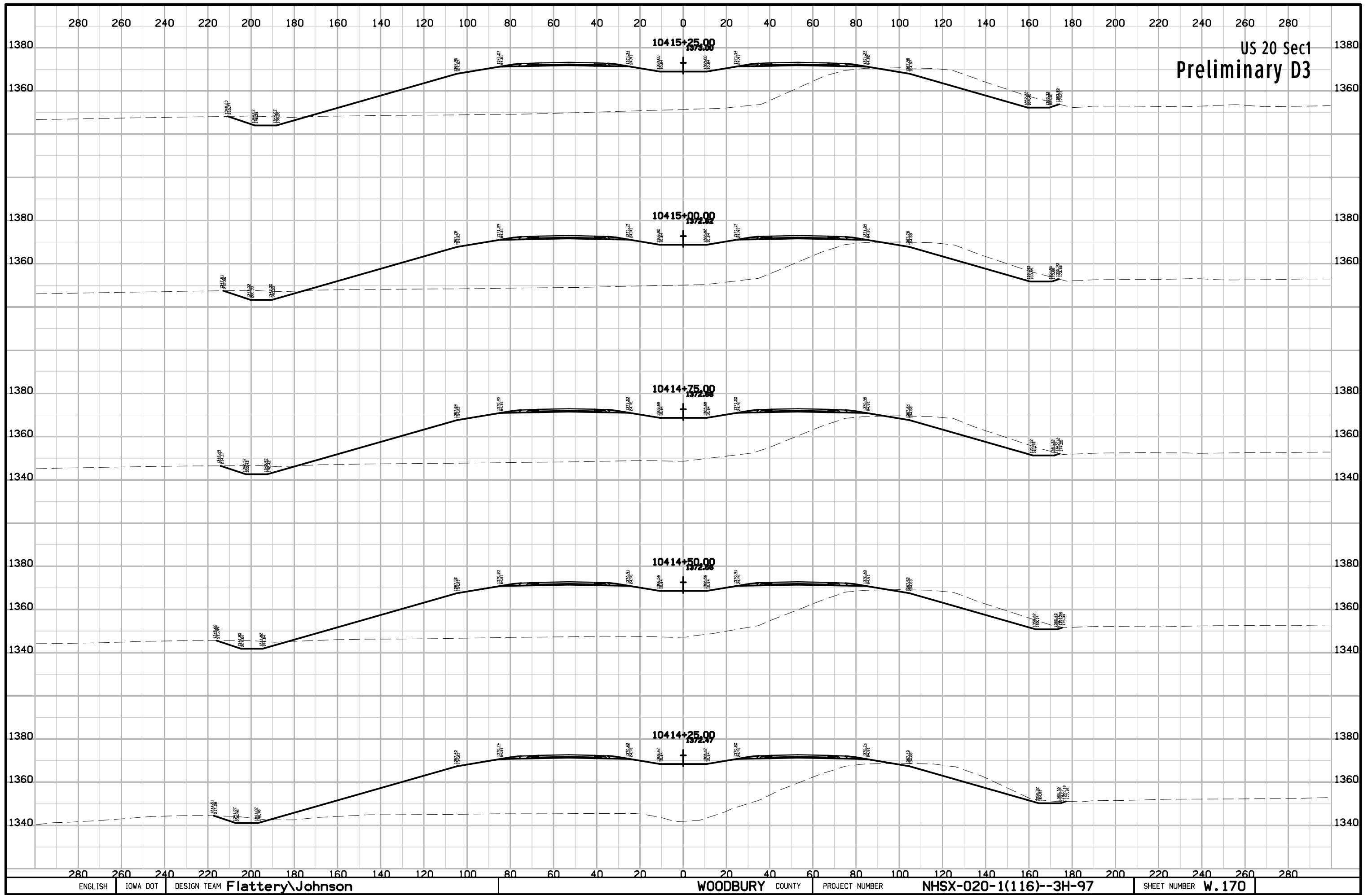


US 20 Sec1
Preliminary D3



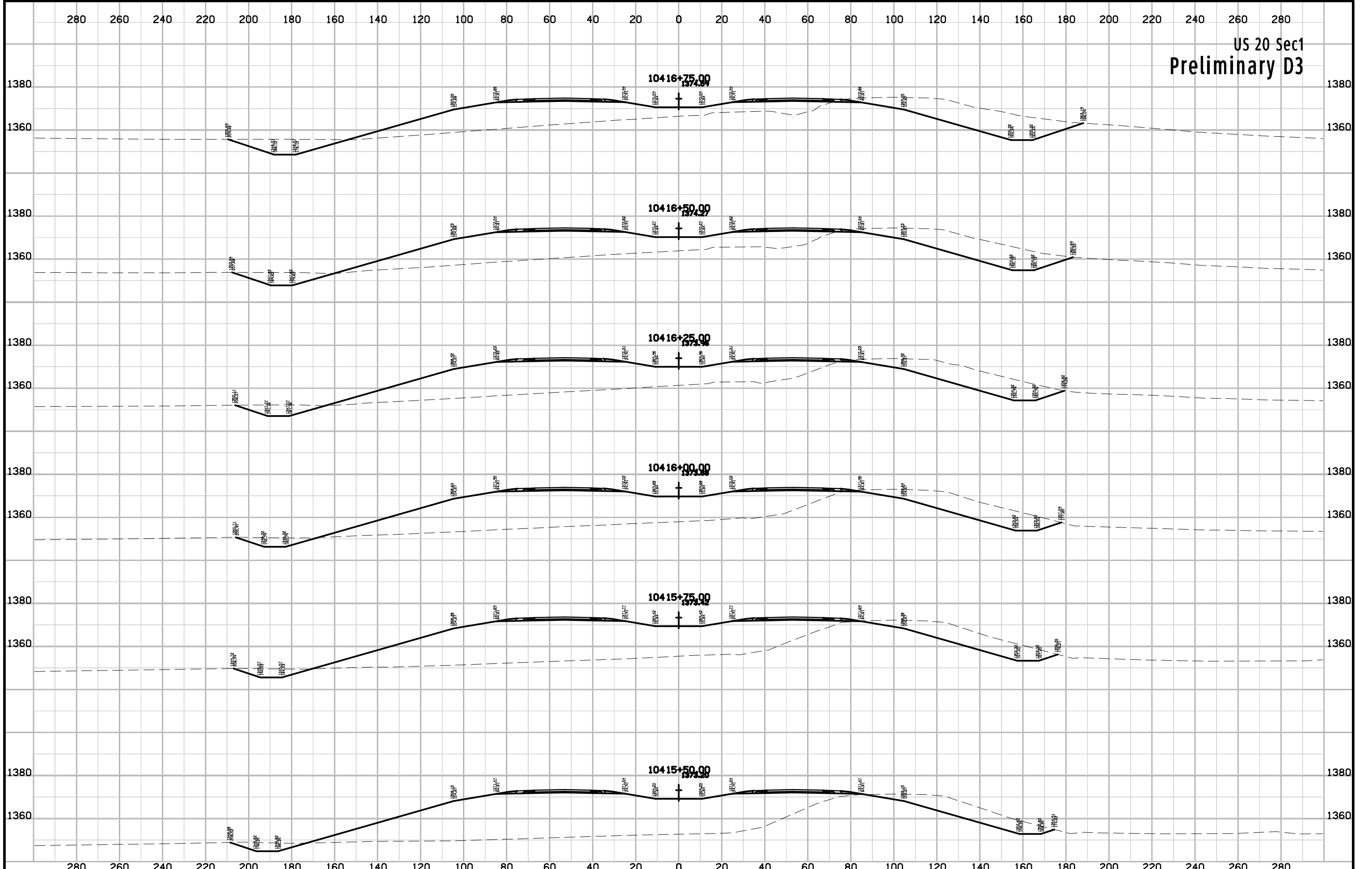
US 20 Sec1
Preliminary D3



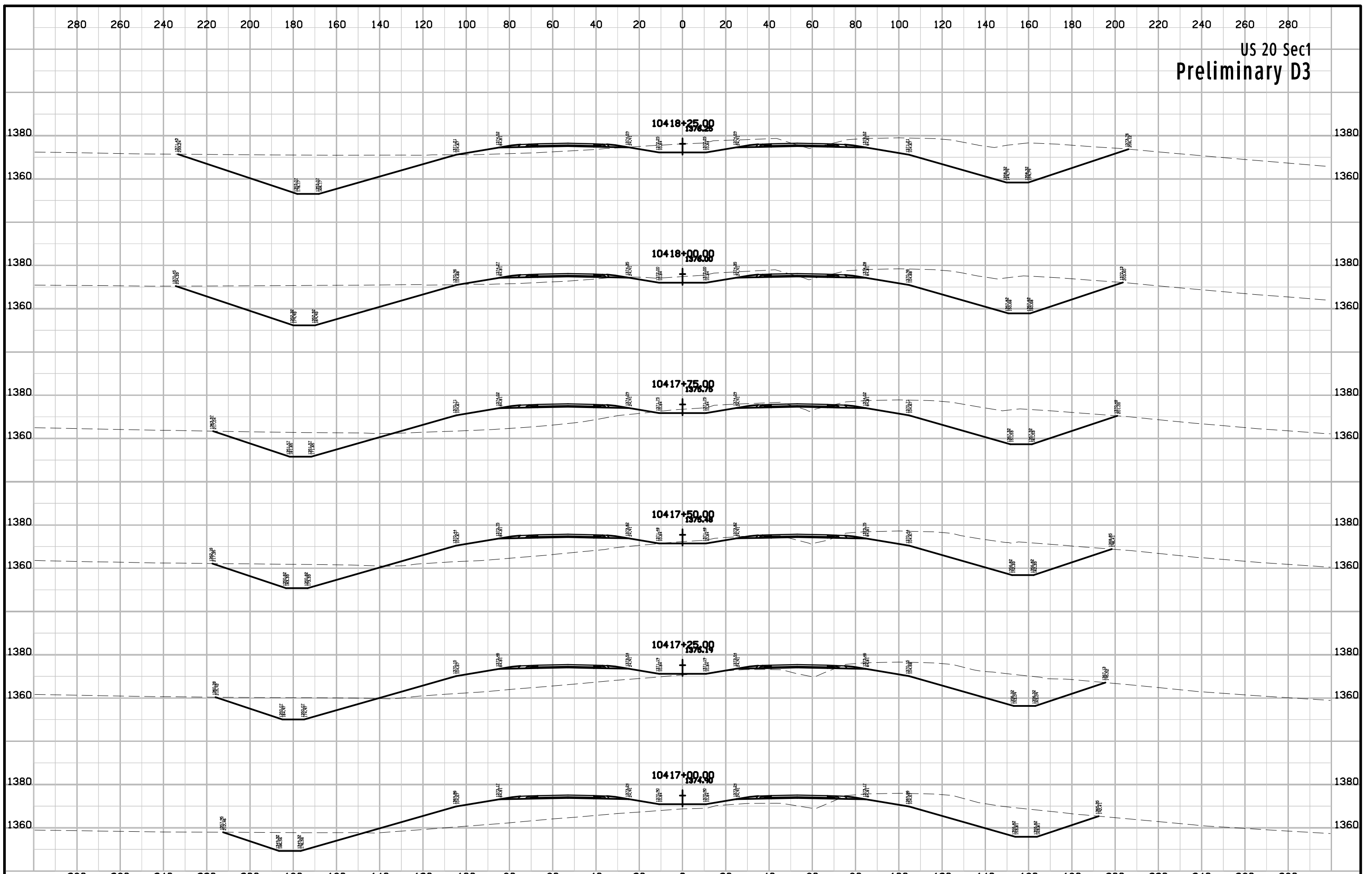


US 20 Sec1
Preliminary D3

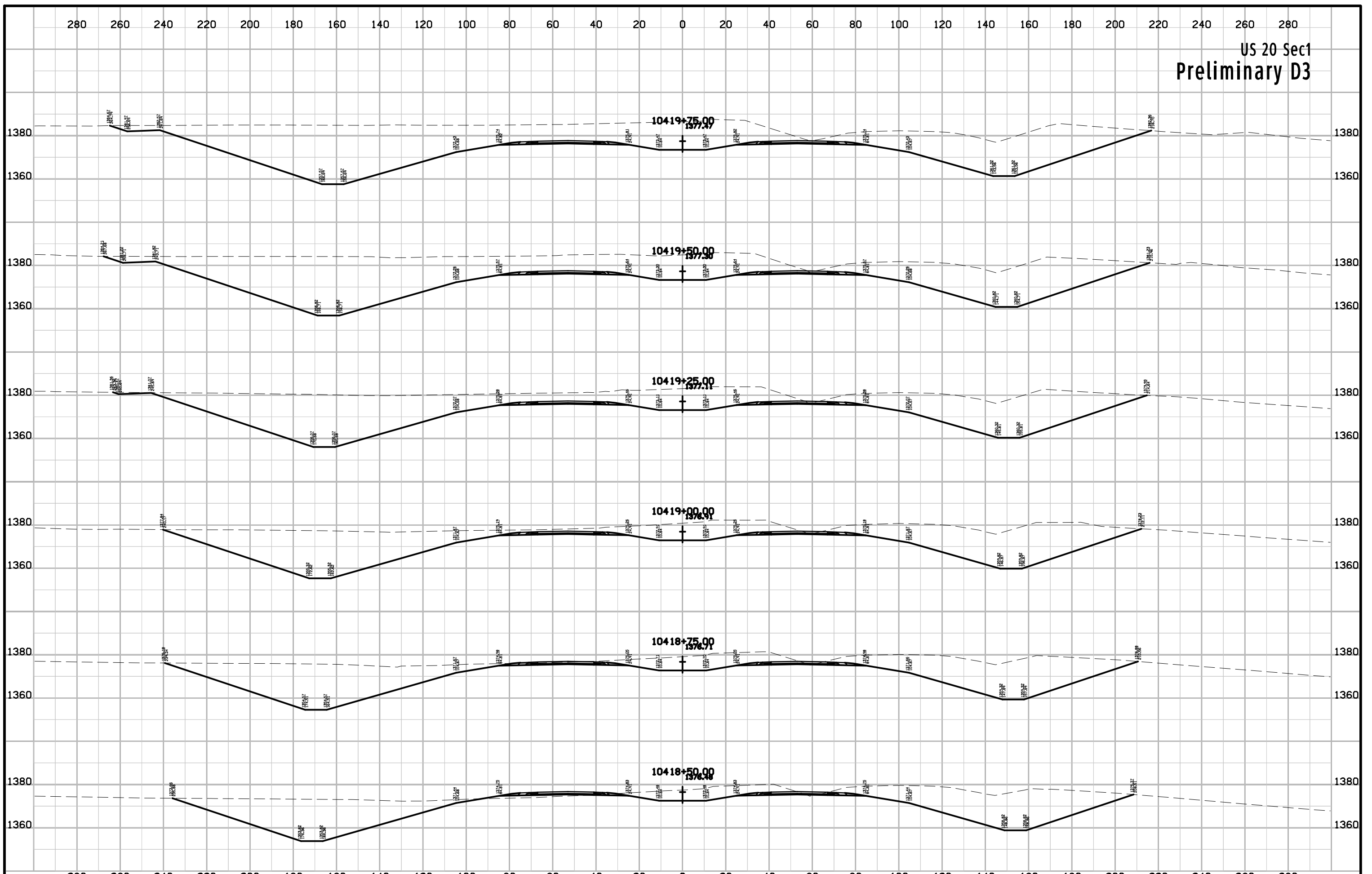
US 20 Sec1
Preliminary D3

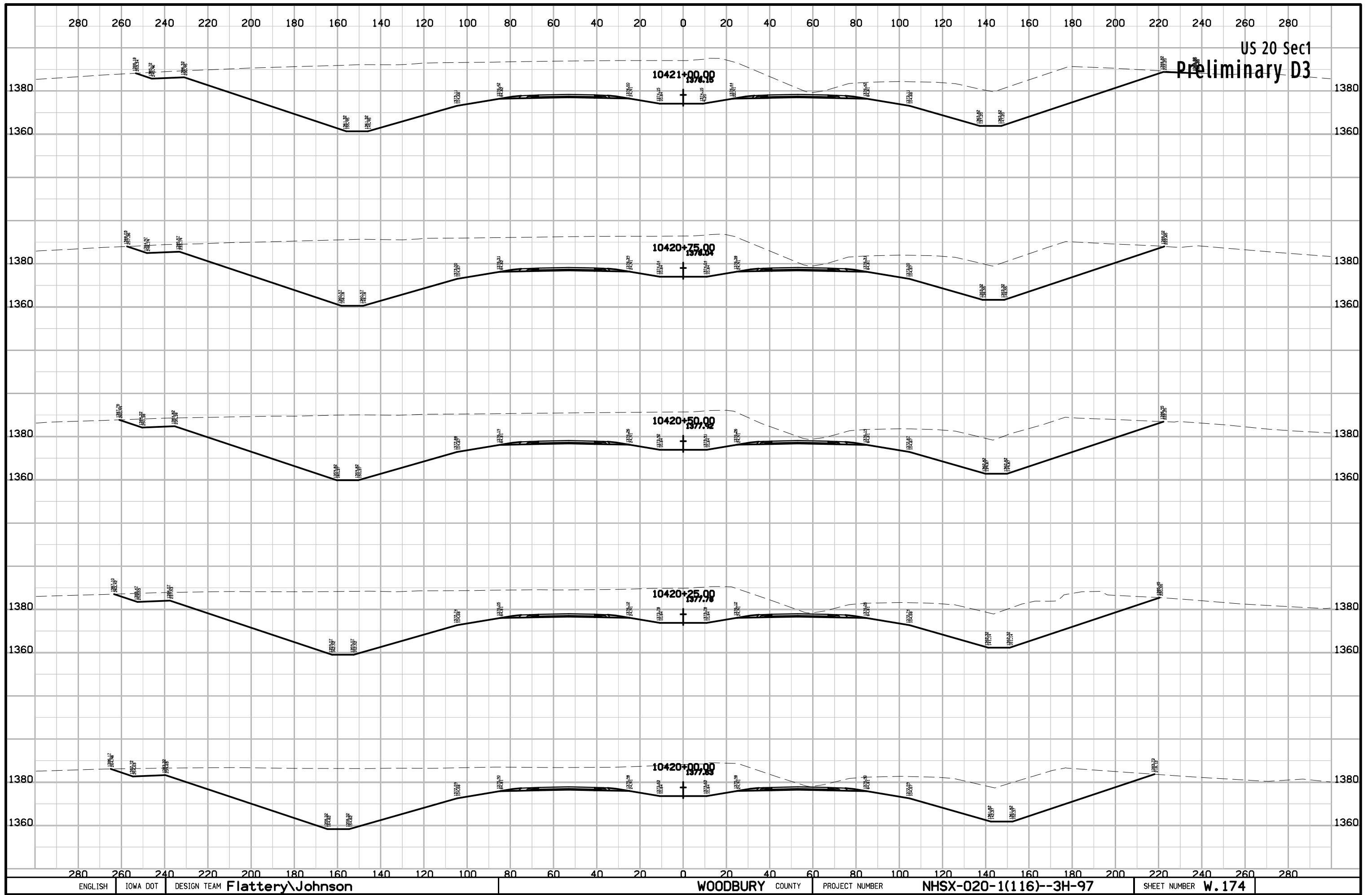


US 20 Sec1
Preliminary D3

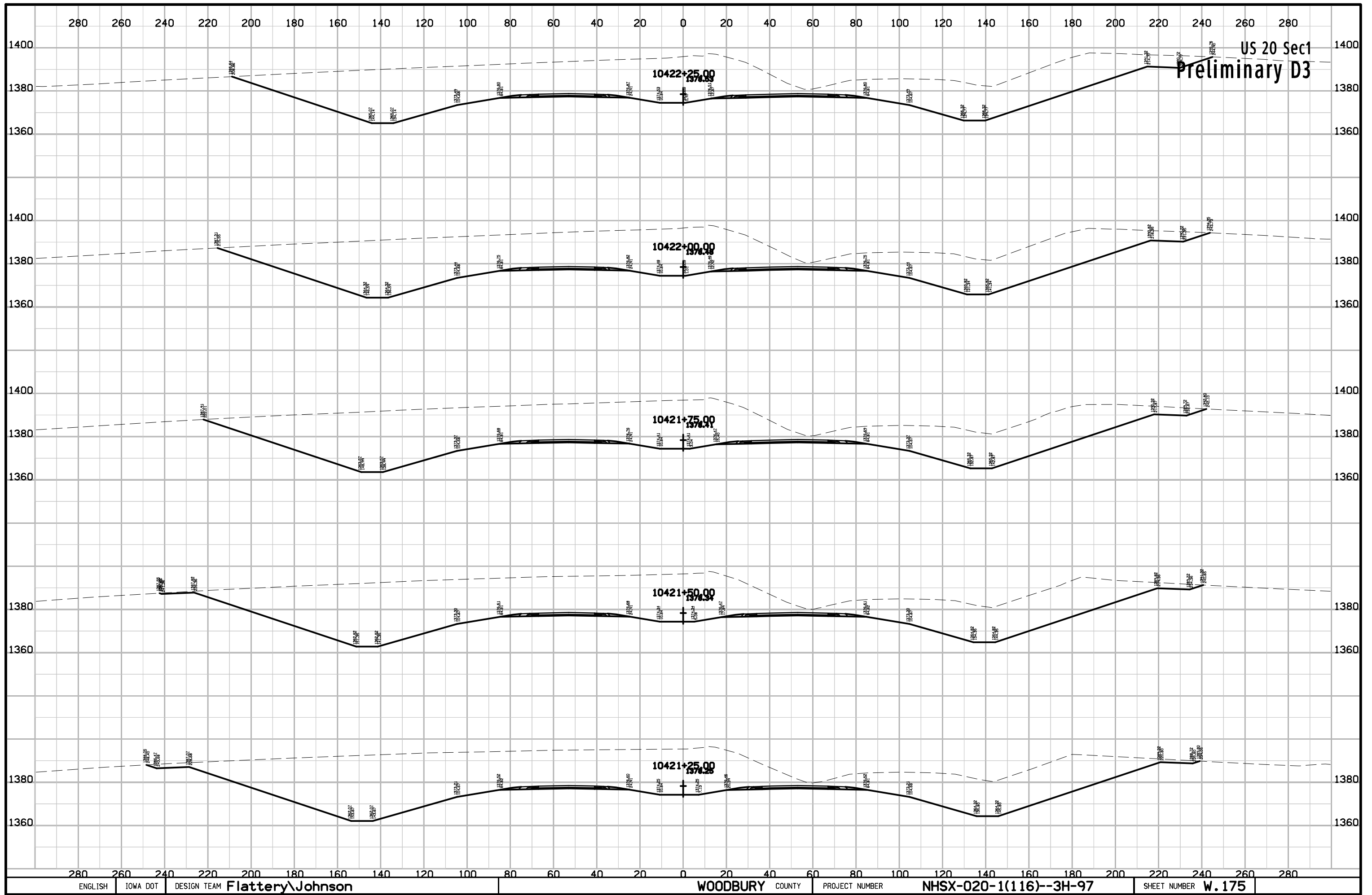


US 20 Sec1
Preliminary D3

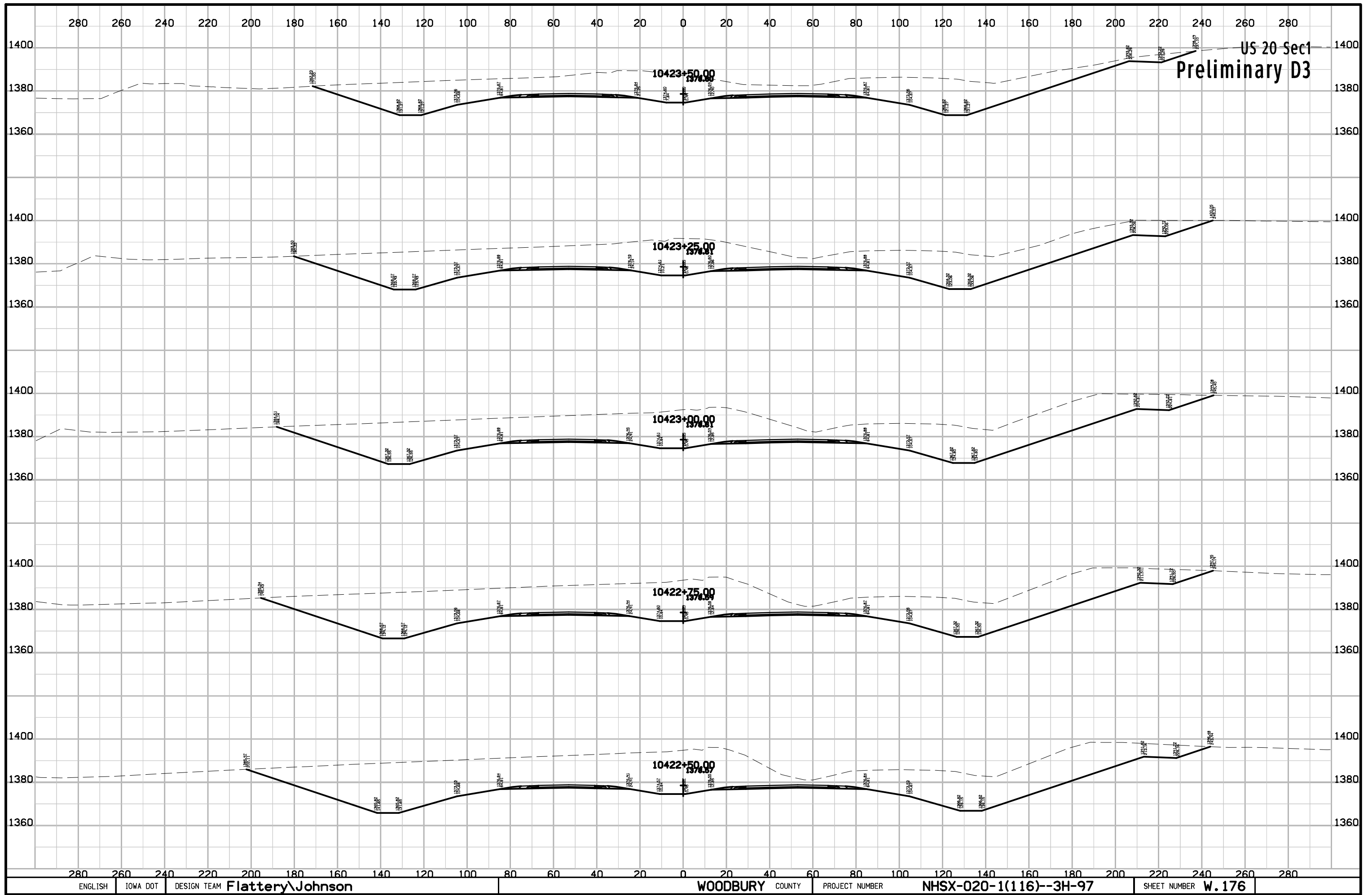




US 20 Sec1
Preliminary D3

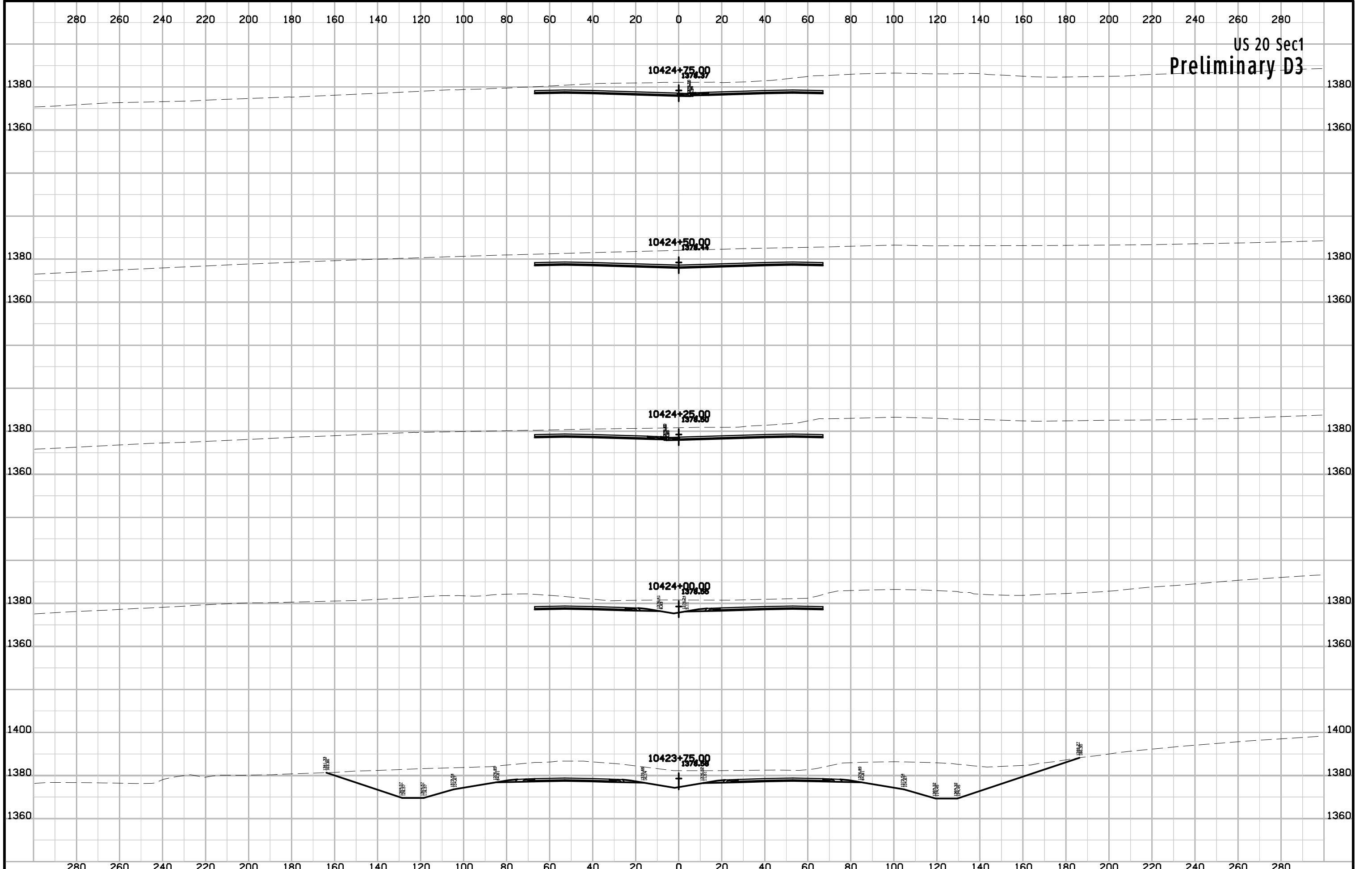


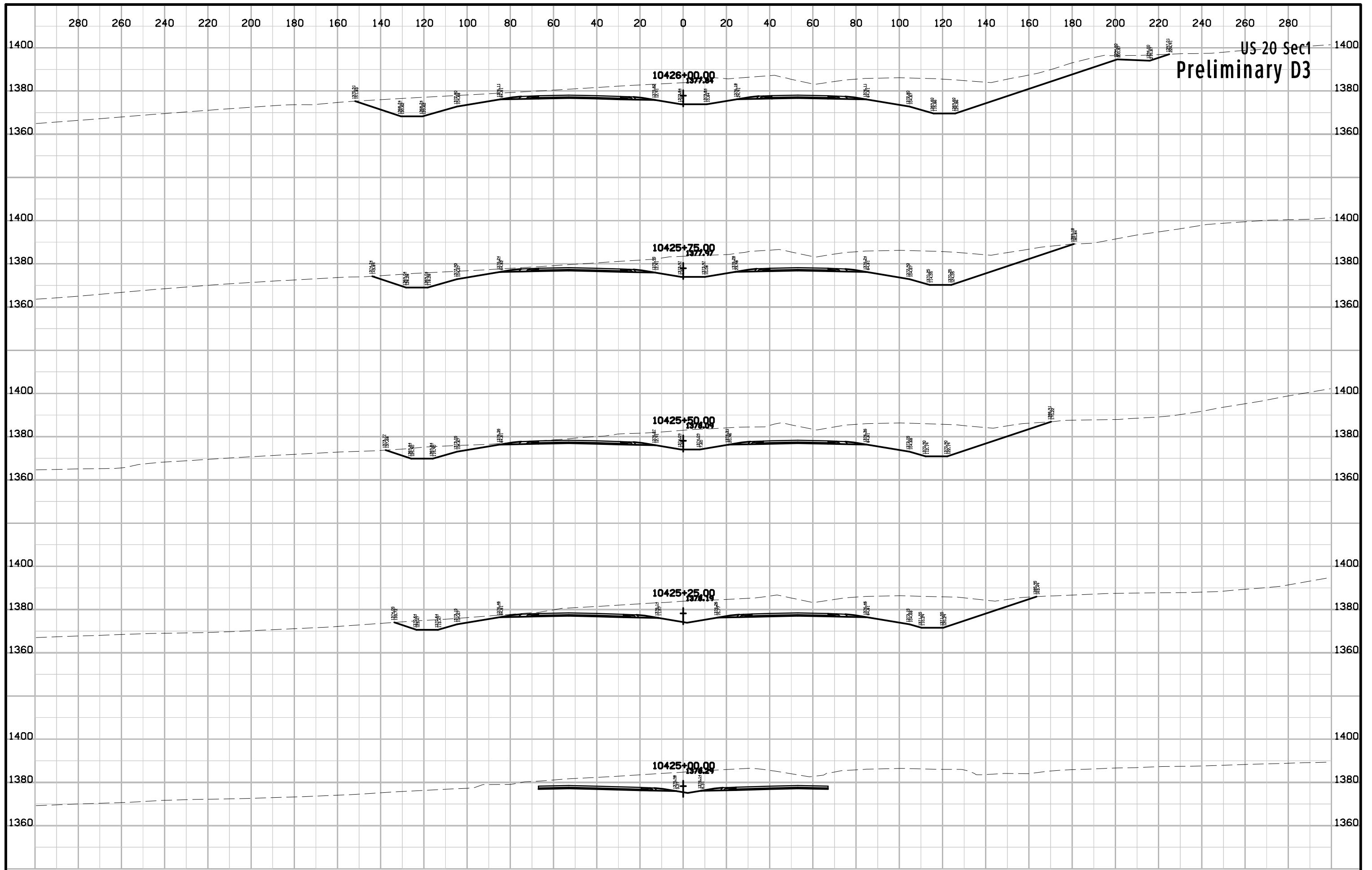
US 20 Sec1
Preliminary D3



US 20 Sec1
Preliminary D3

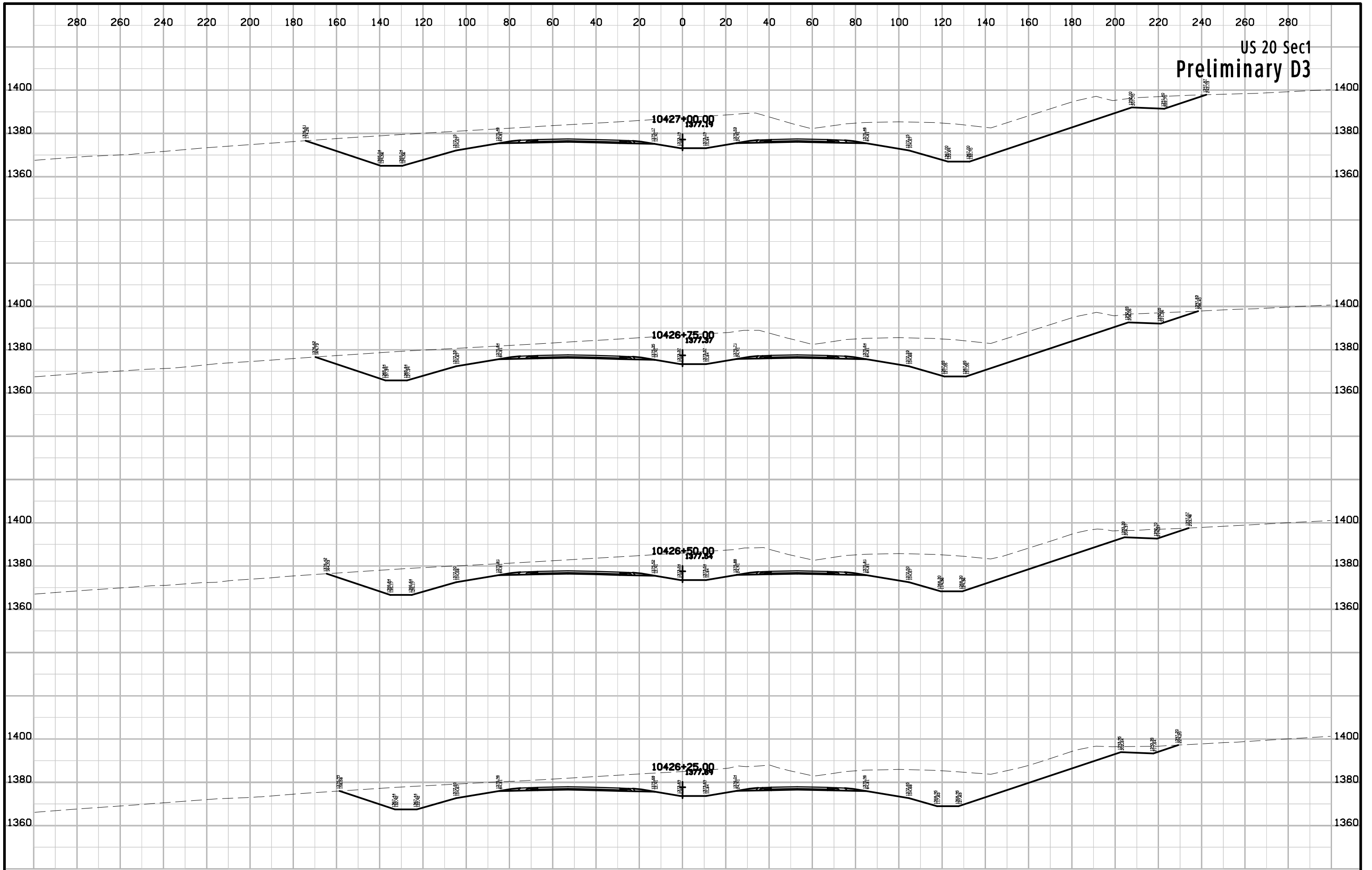
US 20 Sec1
Preliminary D3



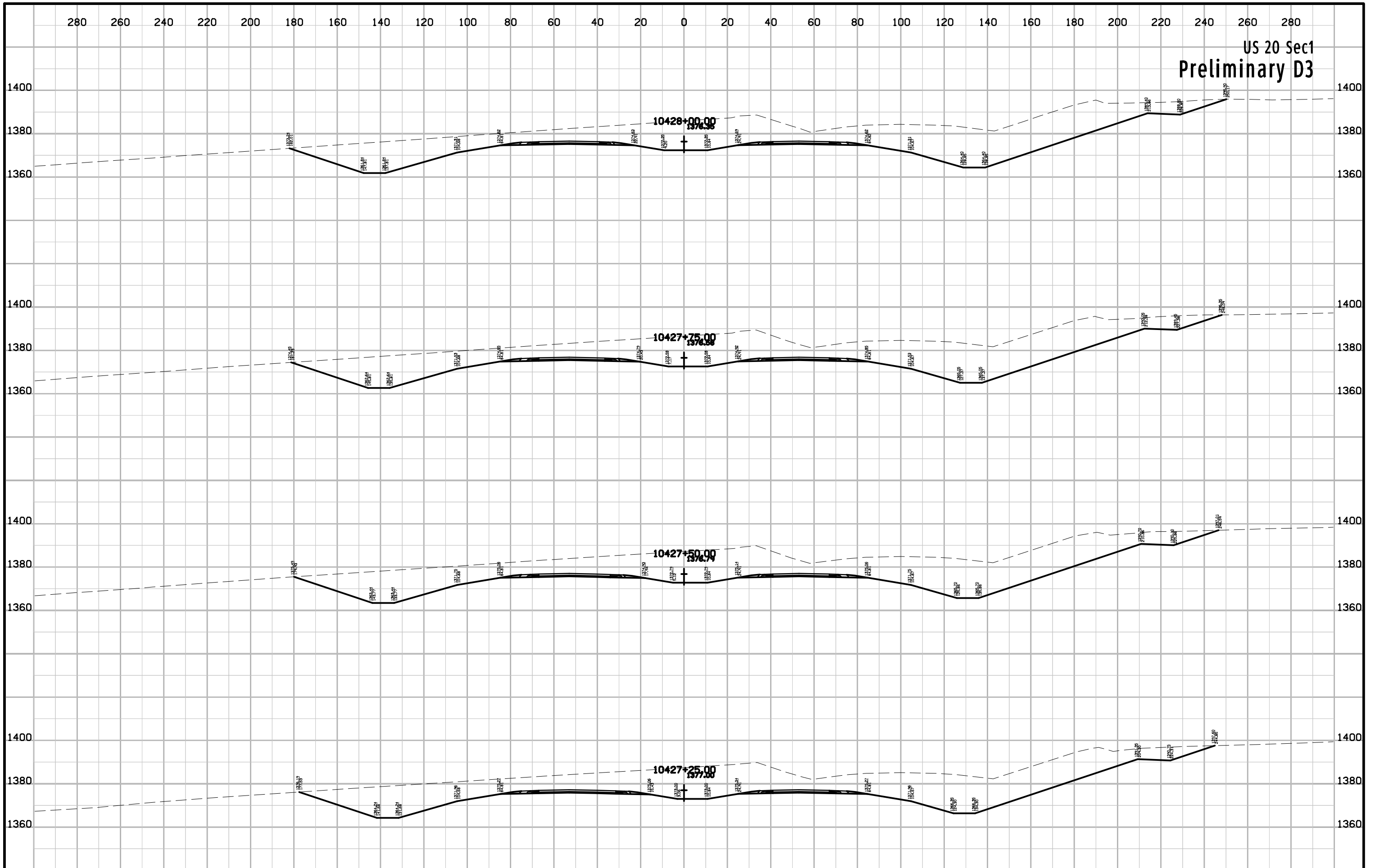


US-20 Sec 1
Preliminary D3

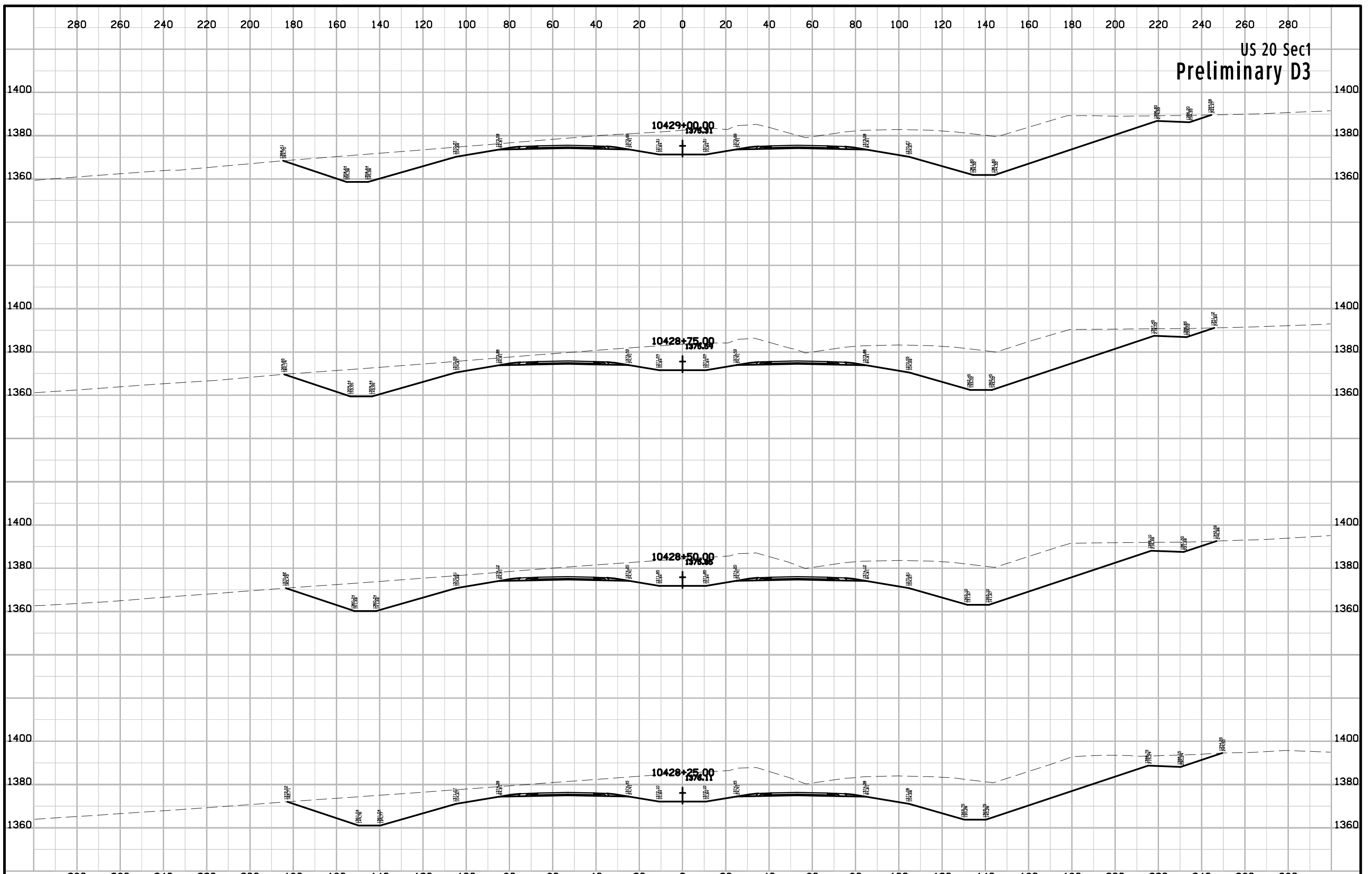
US 20 Sec1
Preliminary D3



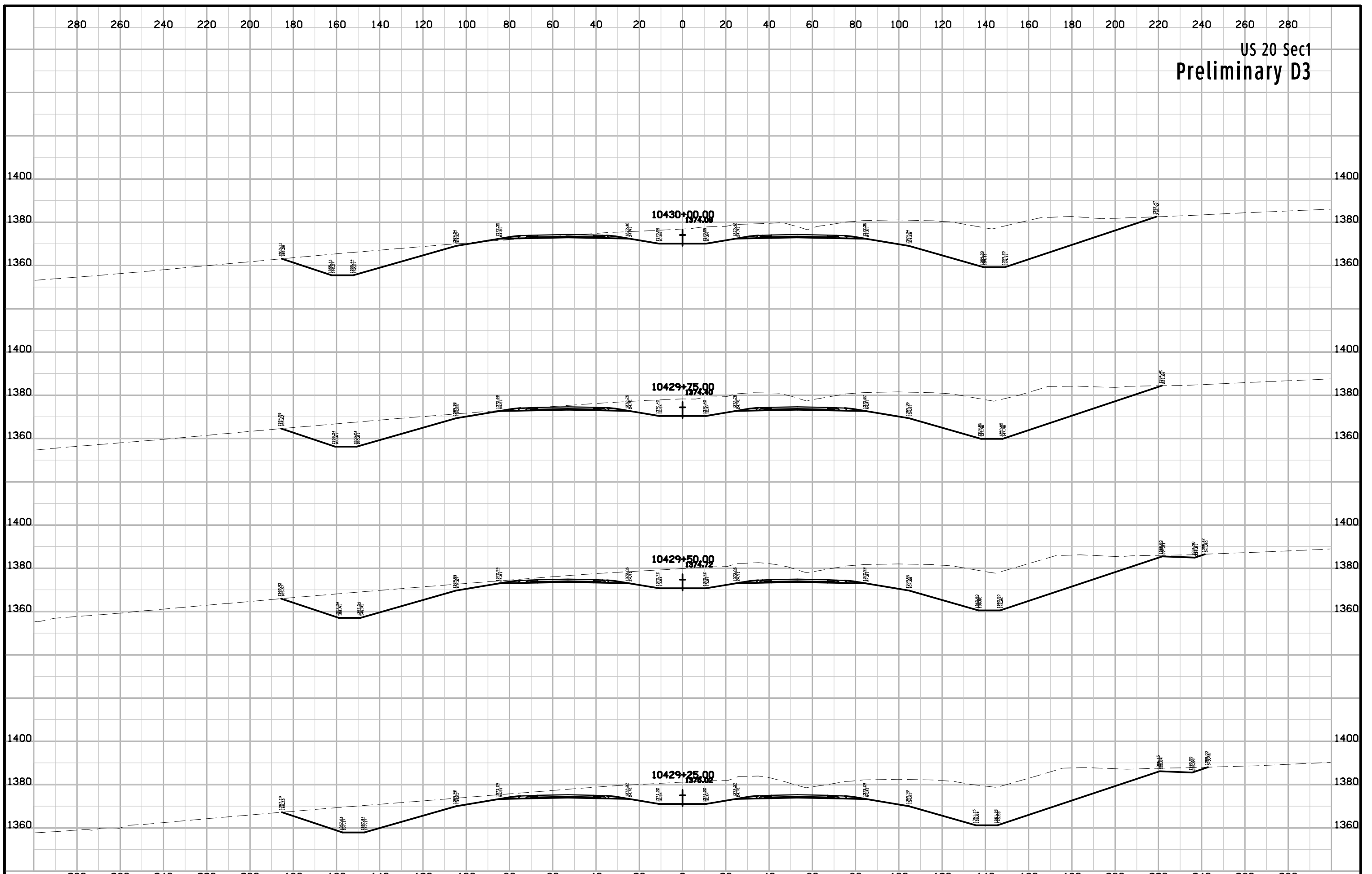
US 20 Sec1
Preliminary D3



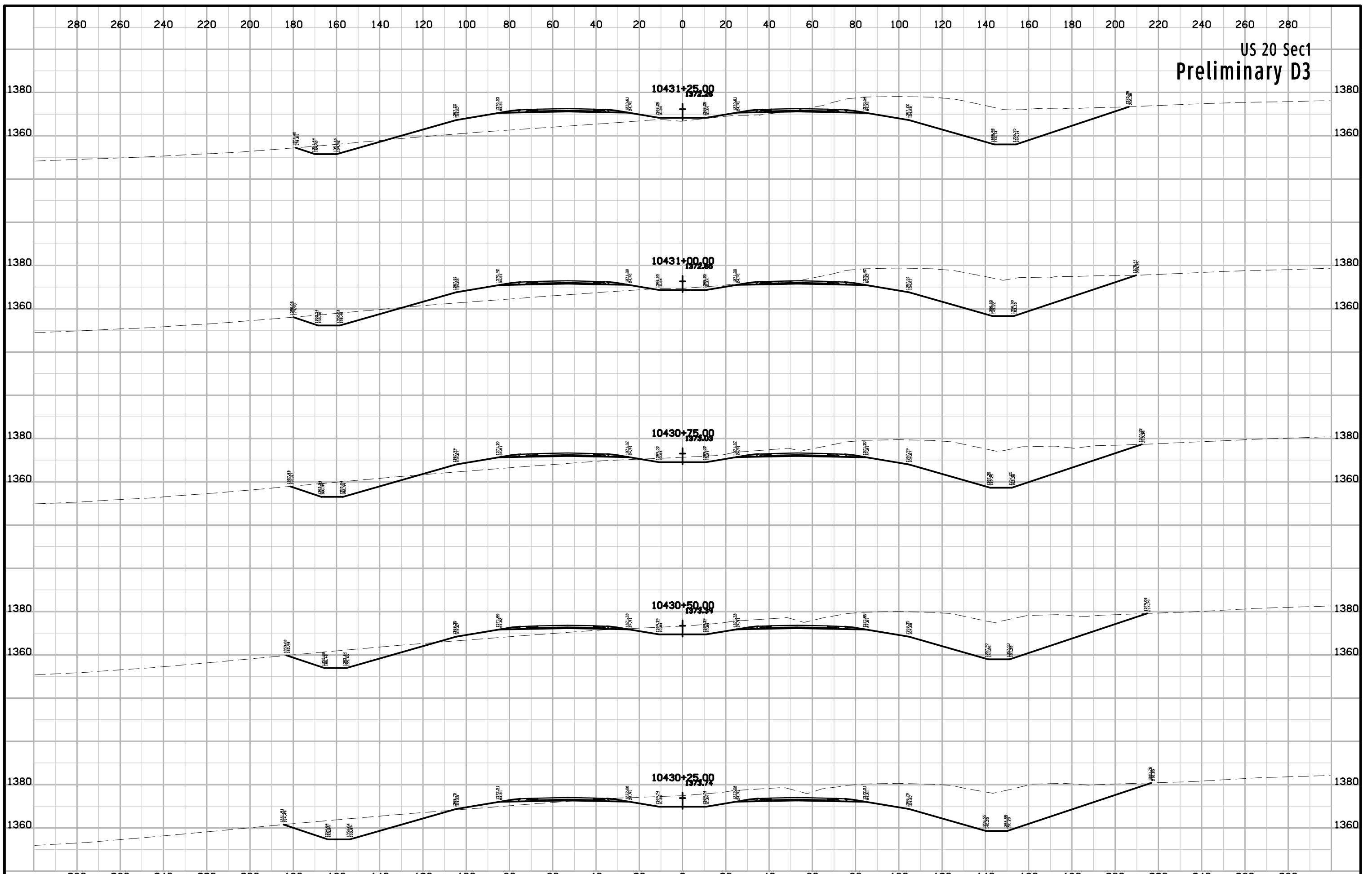
US 20 Sec1
Preliminary D3



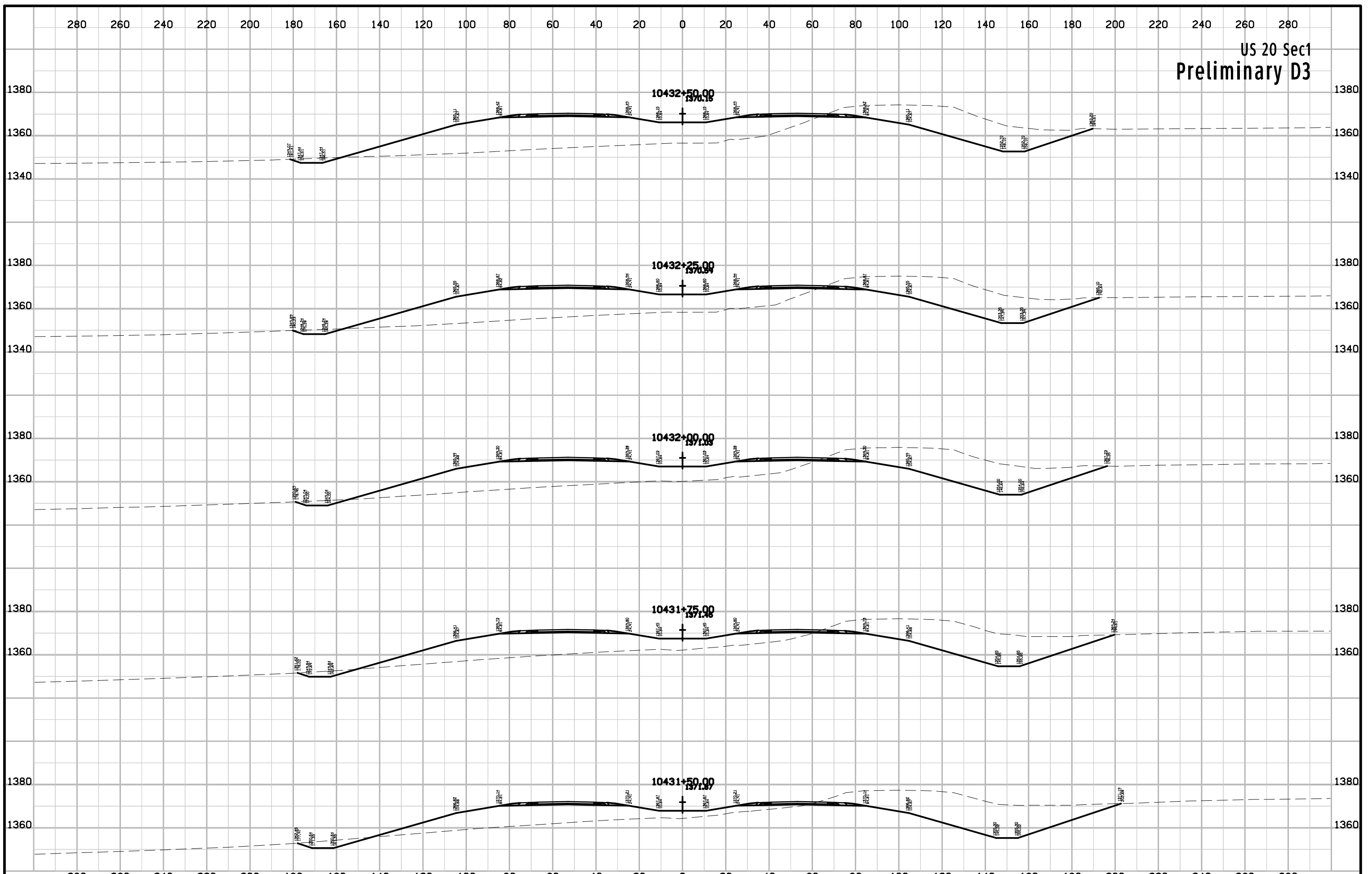
US 20 Sec1
Preliminary D3



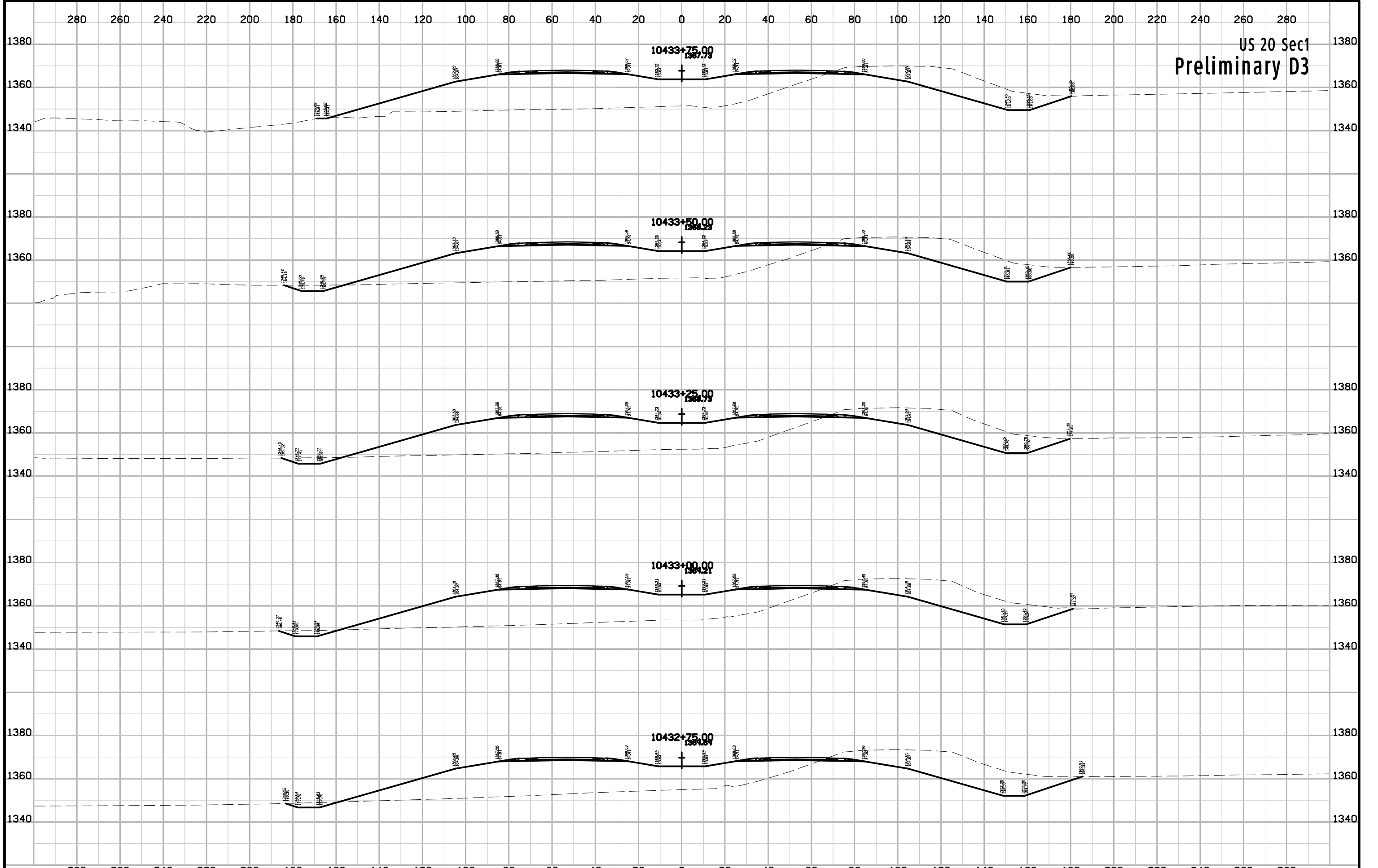
US 20 Sec1
Preliminary D3



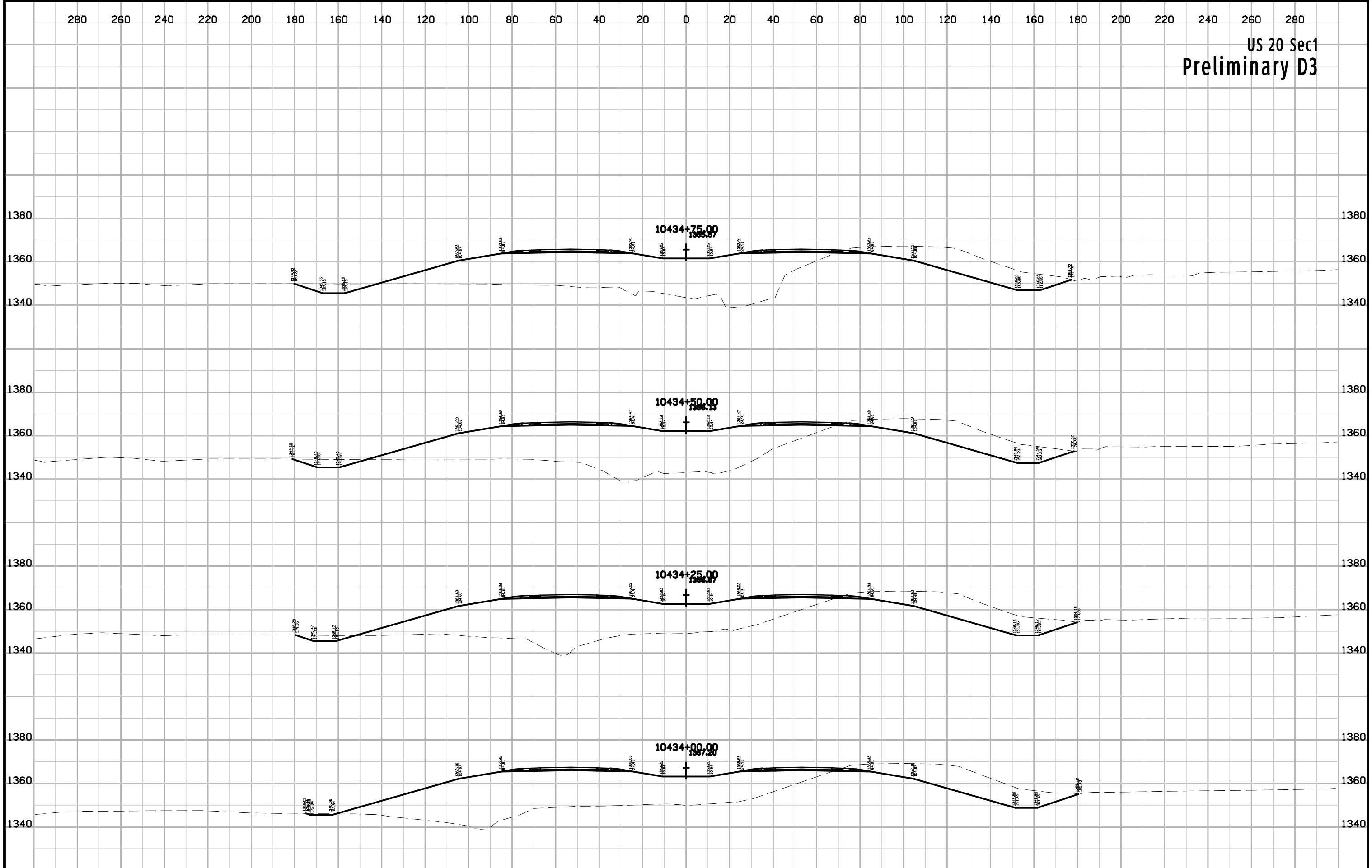
US 20 Sec1
Preliminary D3



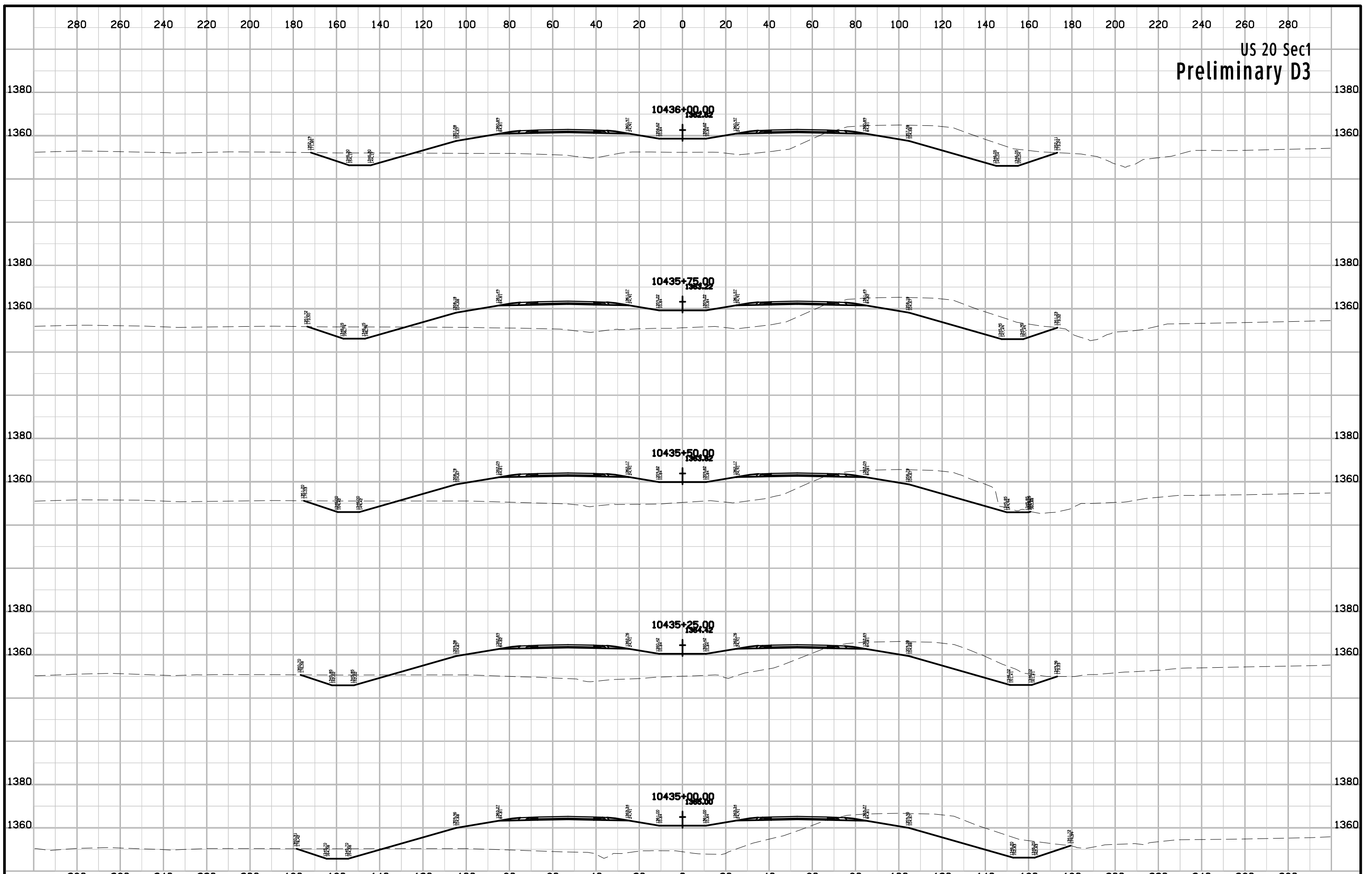
US 20 Sec1
Preliminary D3



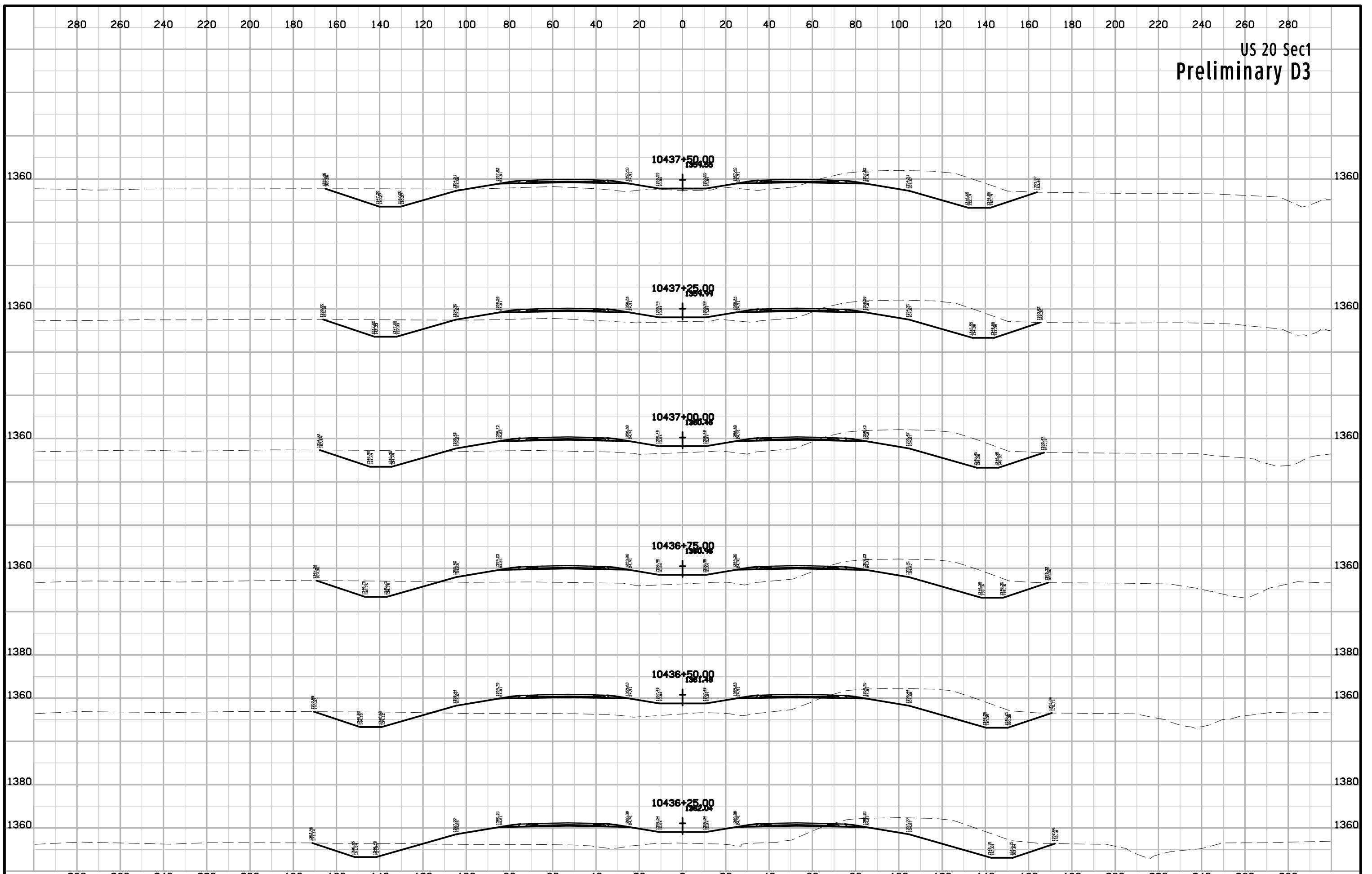
US 20 Sec1
Preliminary D3



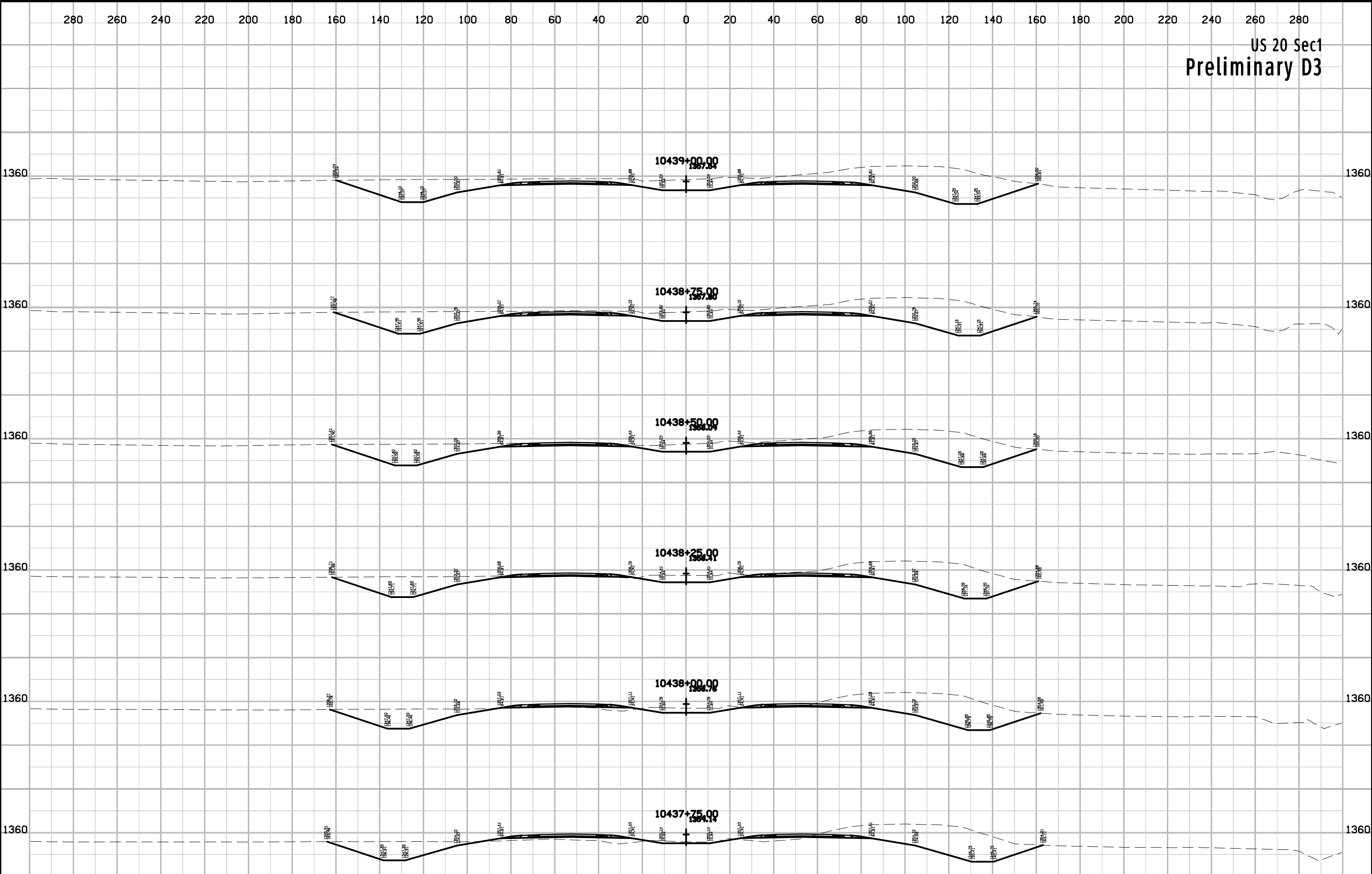
US 20 Sec1
Preliminary D3



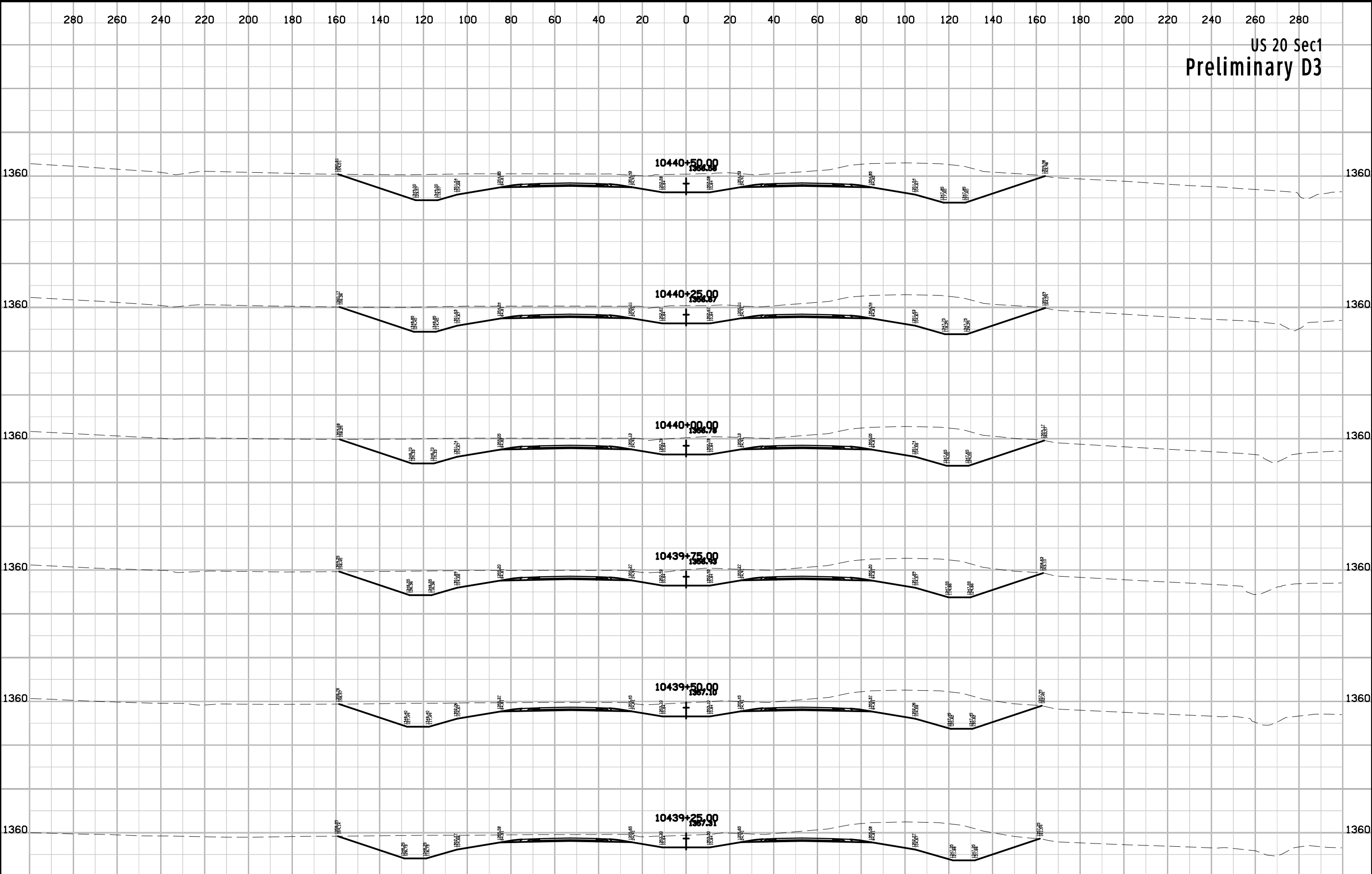
US 20 Sec1
Preliminary D3



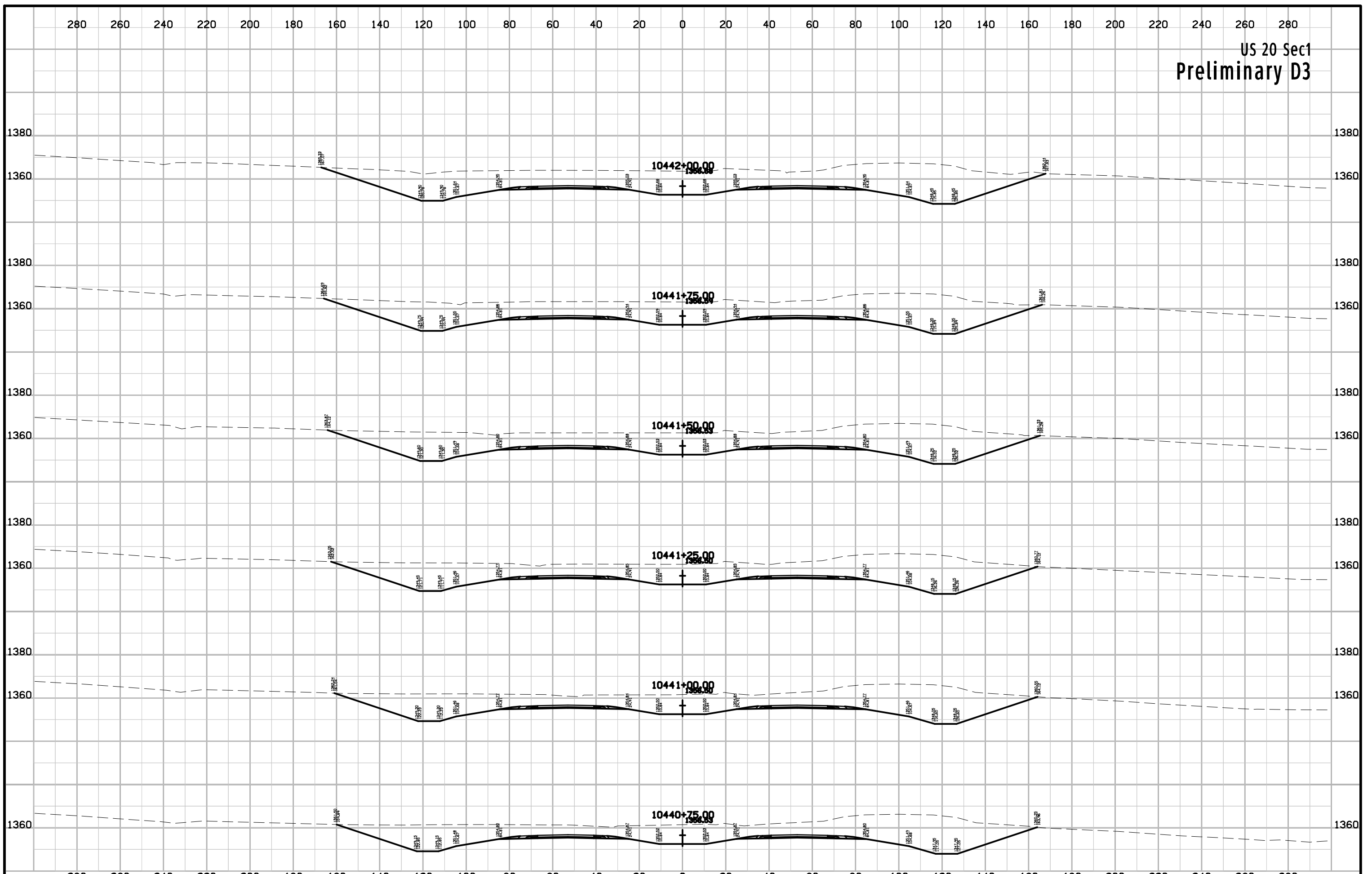
US 20 Sec1
Preliminary D3



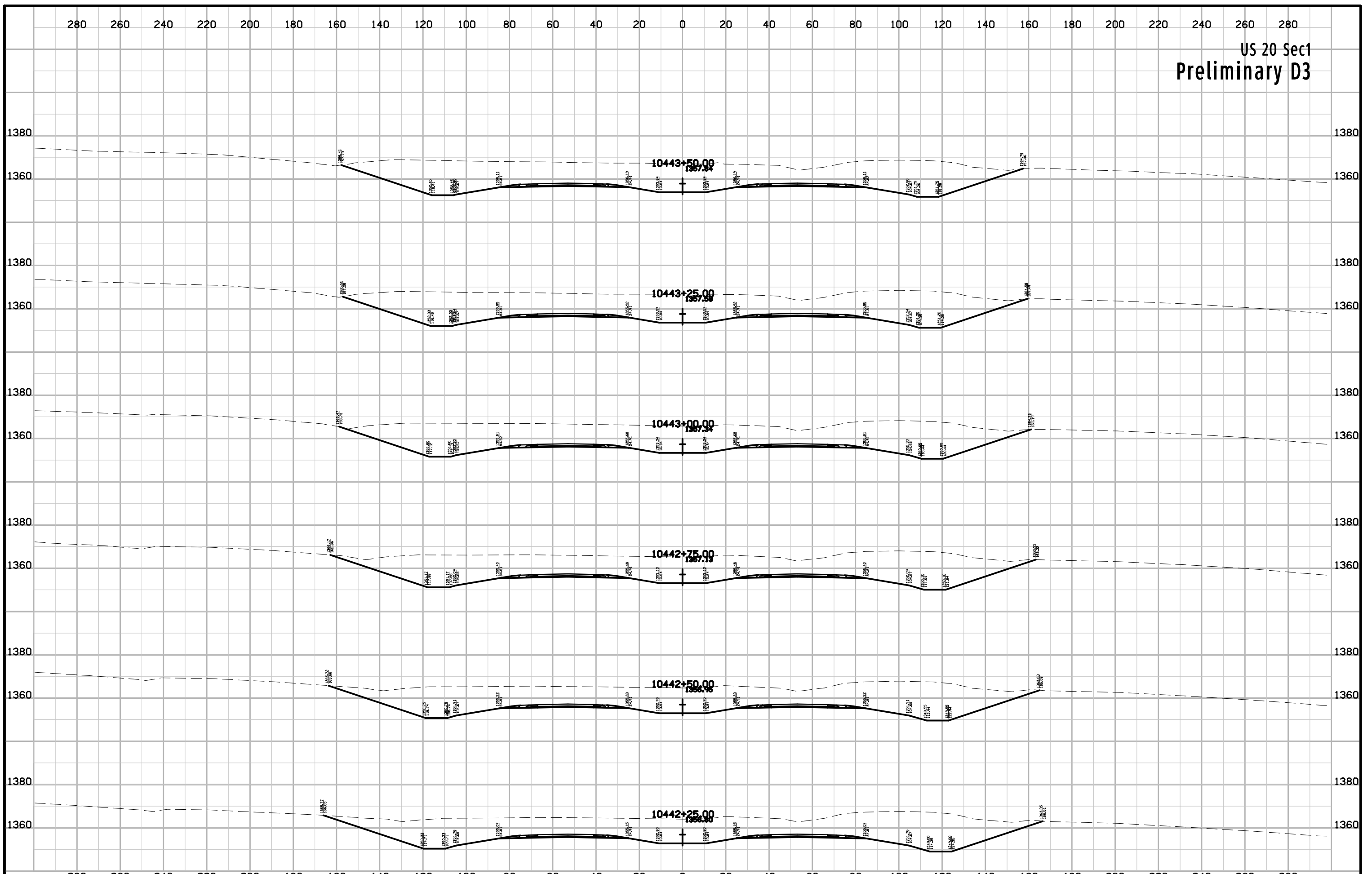
US 20 Sec1
Preliminary D3



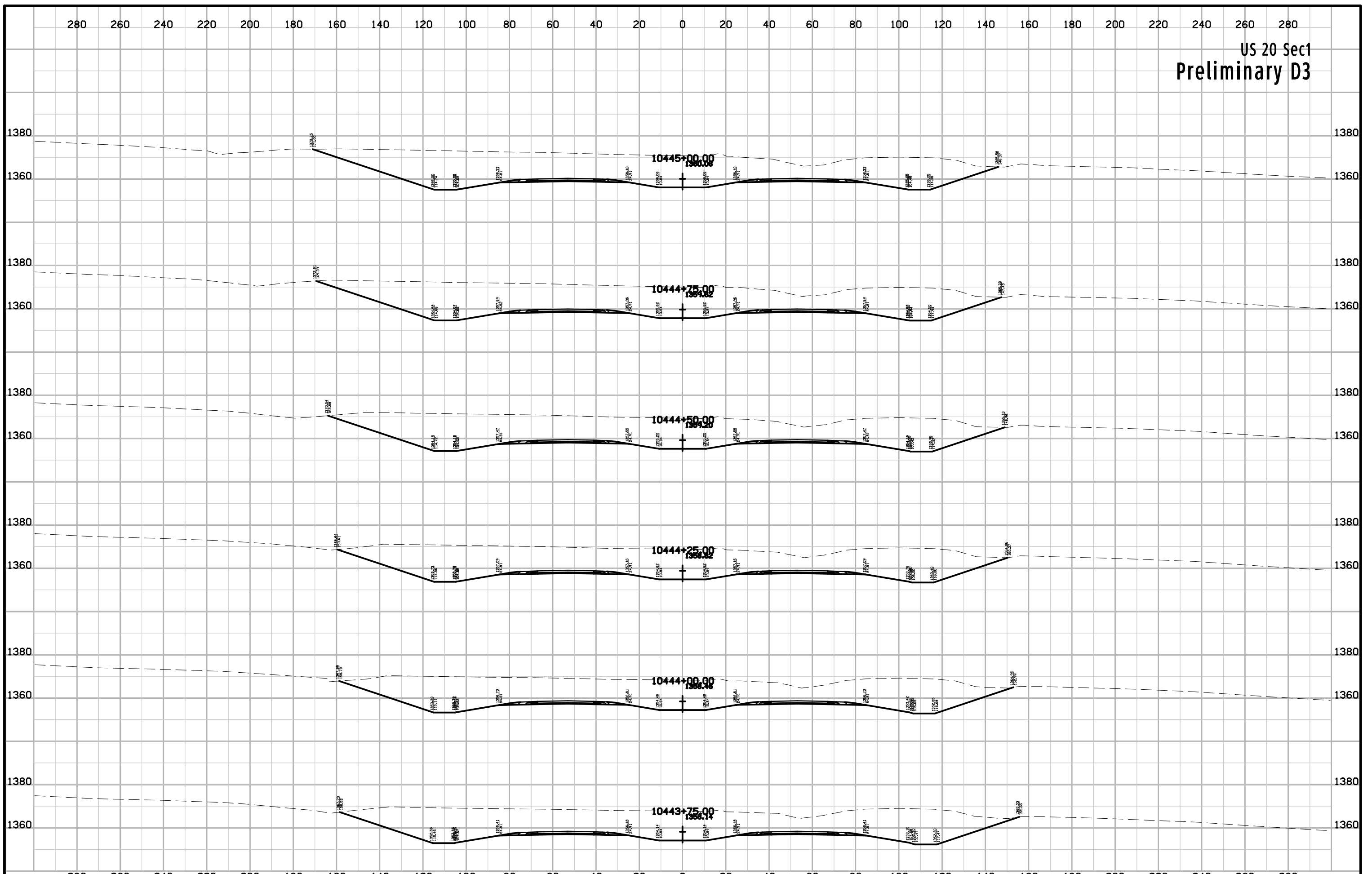
US 20 Sec1
Preliminary D3



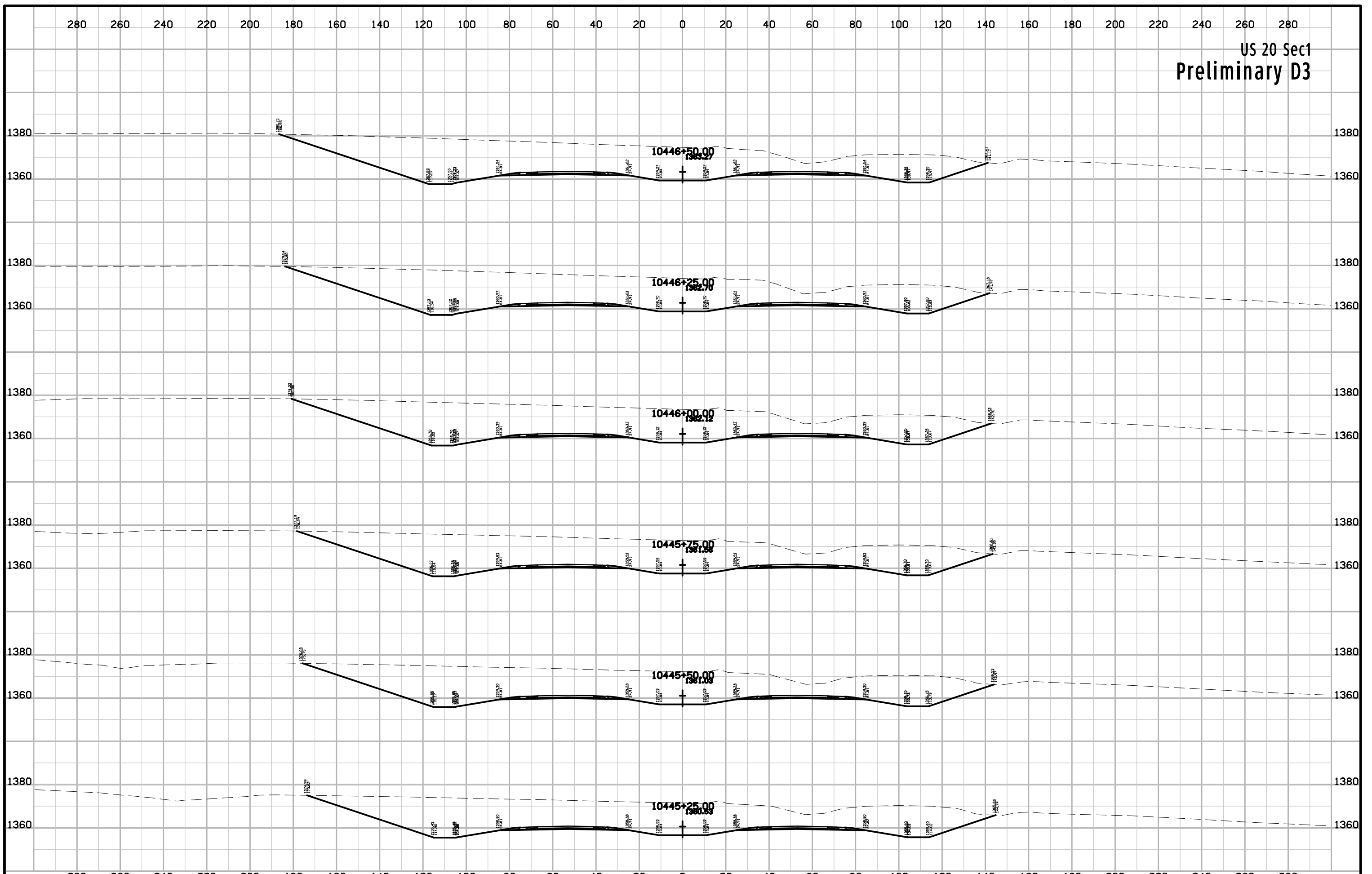
US 20 Sec1
Preliminary D3



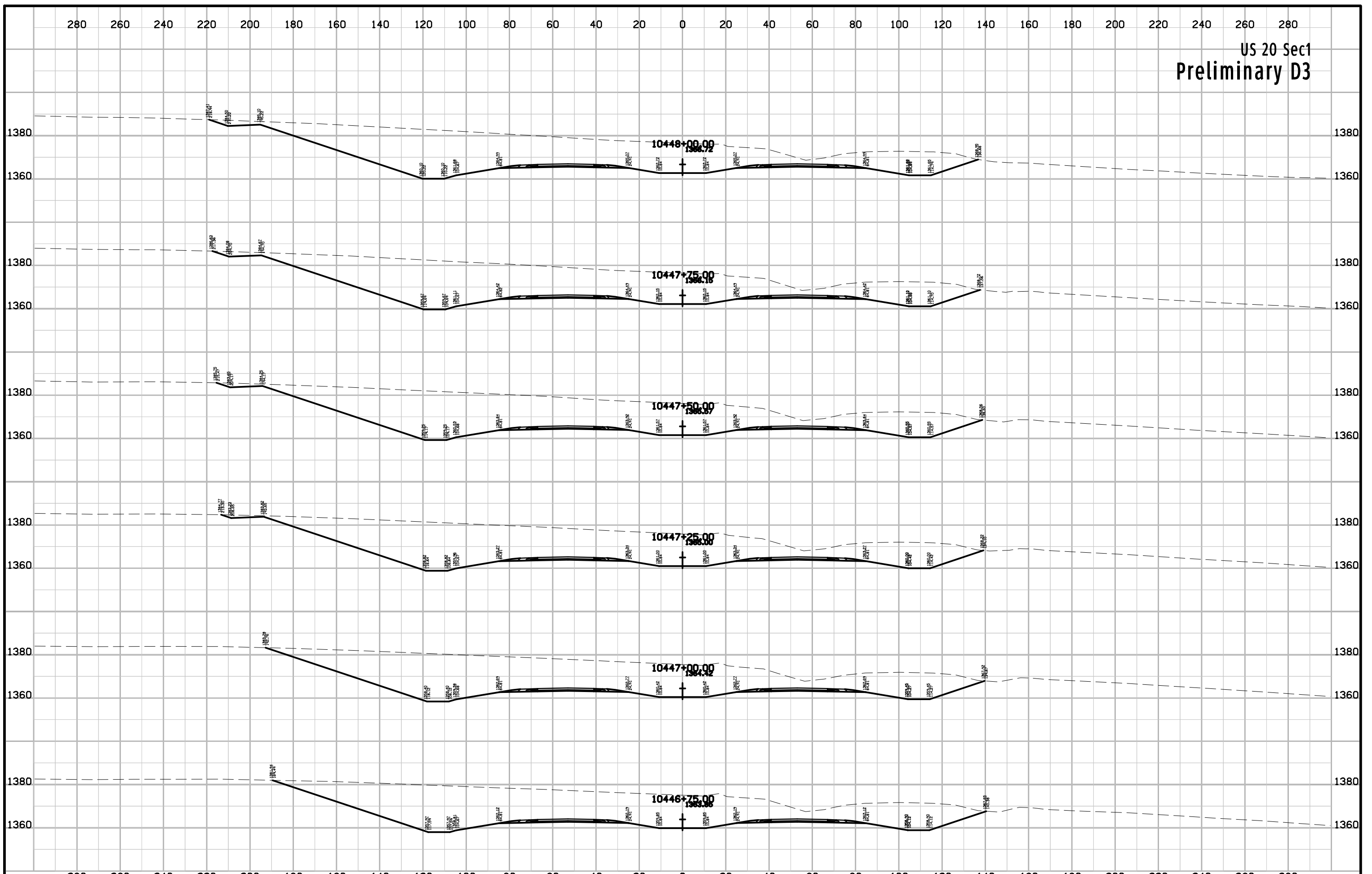
US 20 Sec1
Preliminary D3



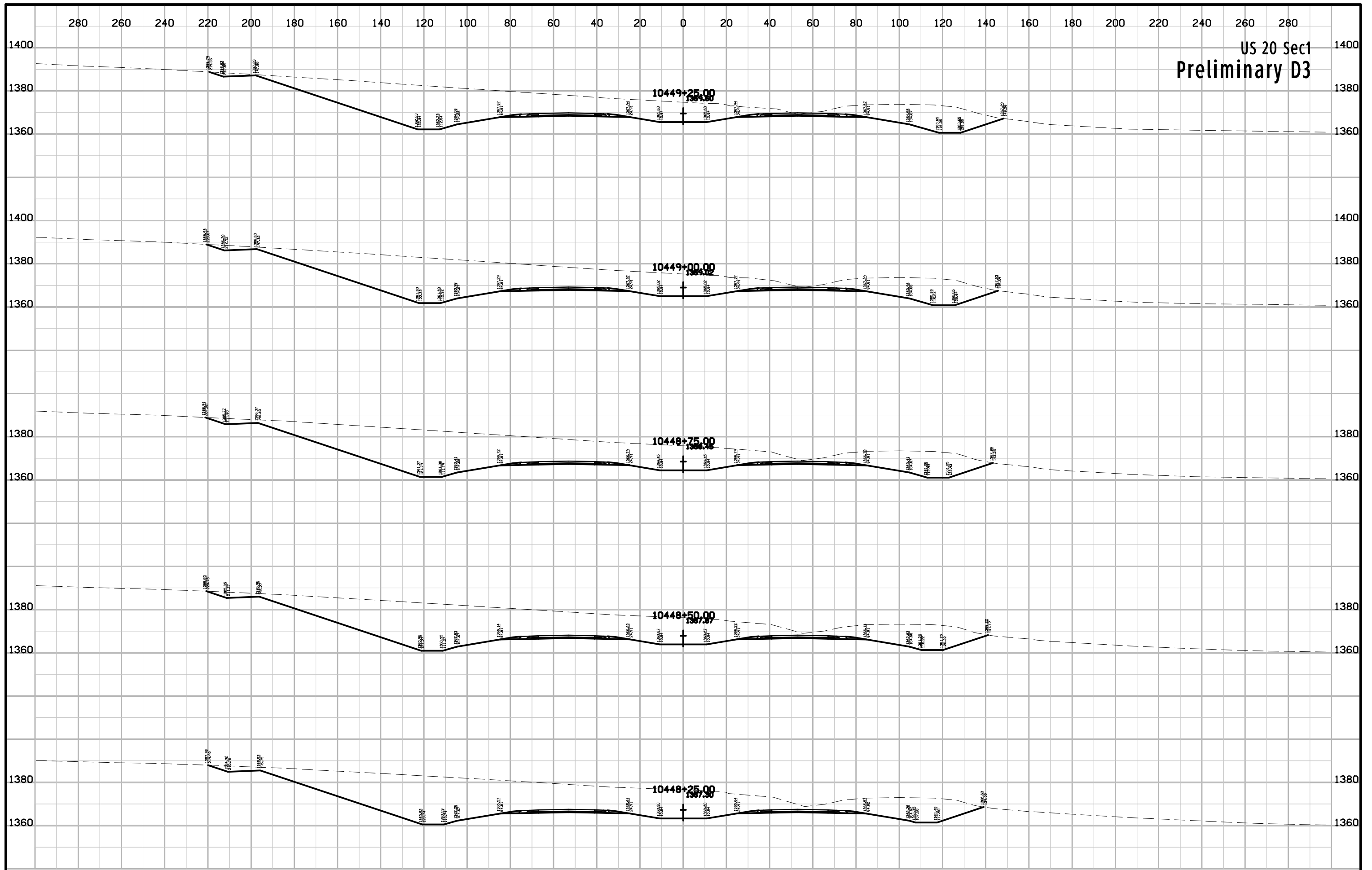
US 20 Sec1
Preliminary D3



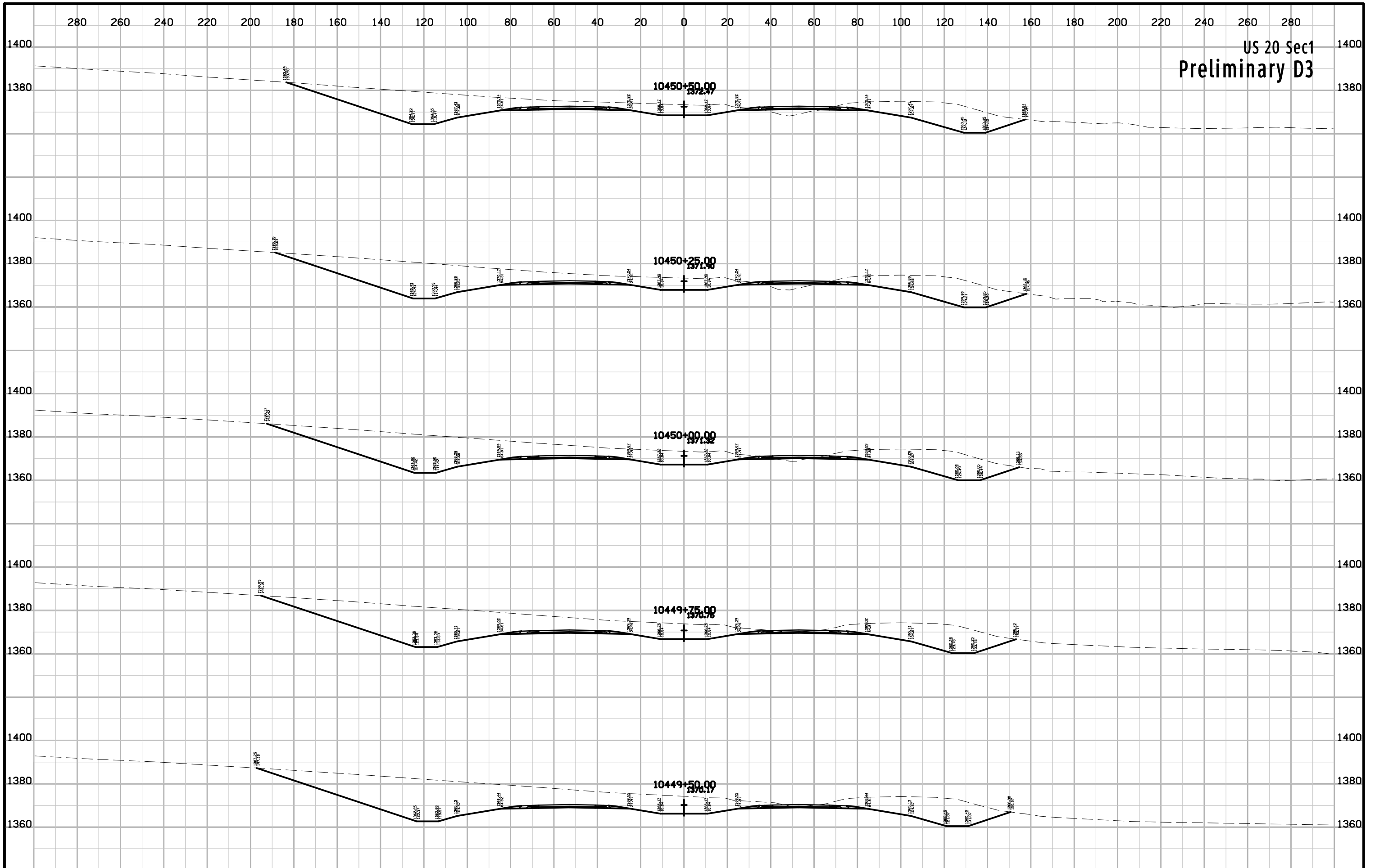
US 20 Sec1
Preliminary D3



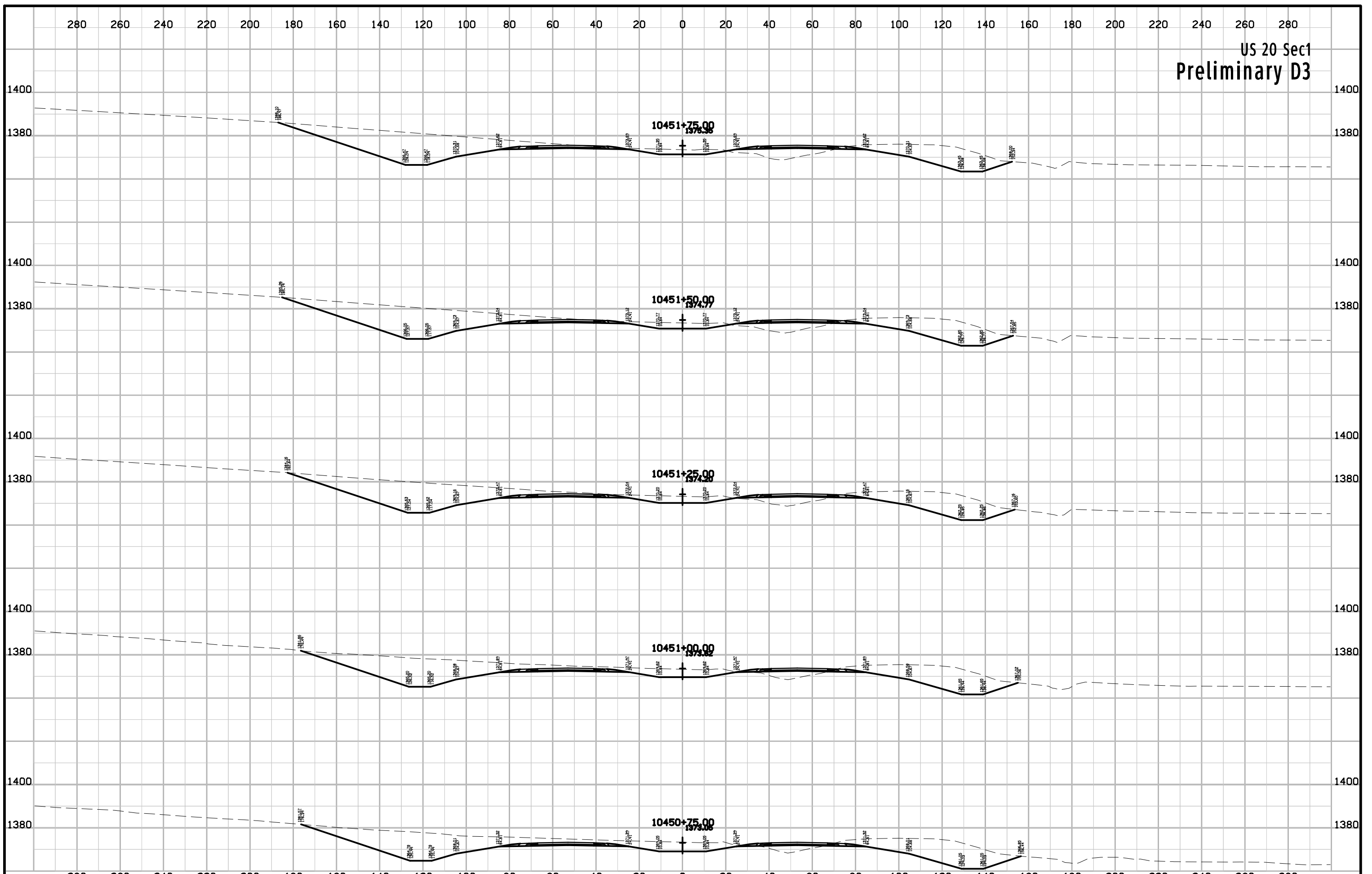
US 20 Sec1
Preliminary D3



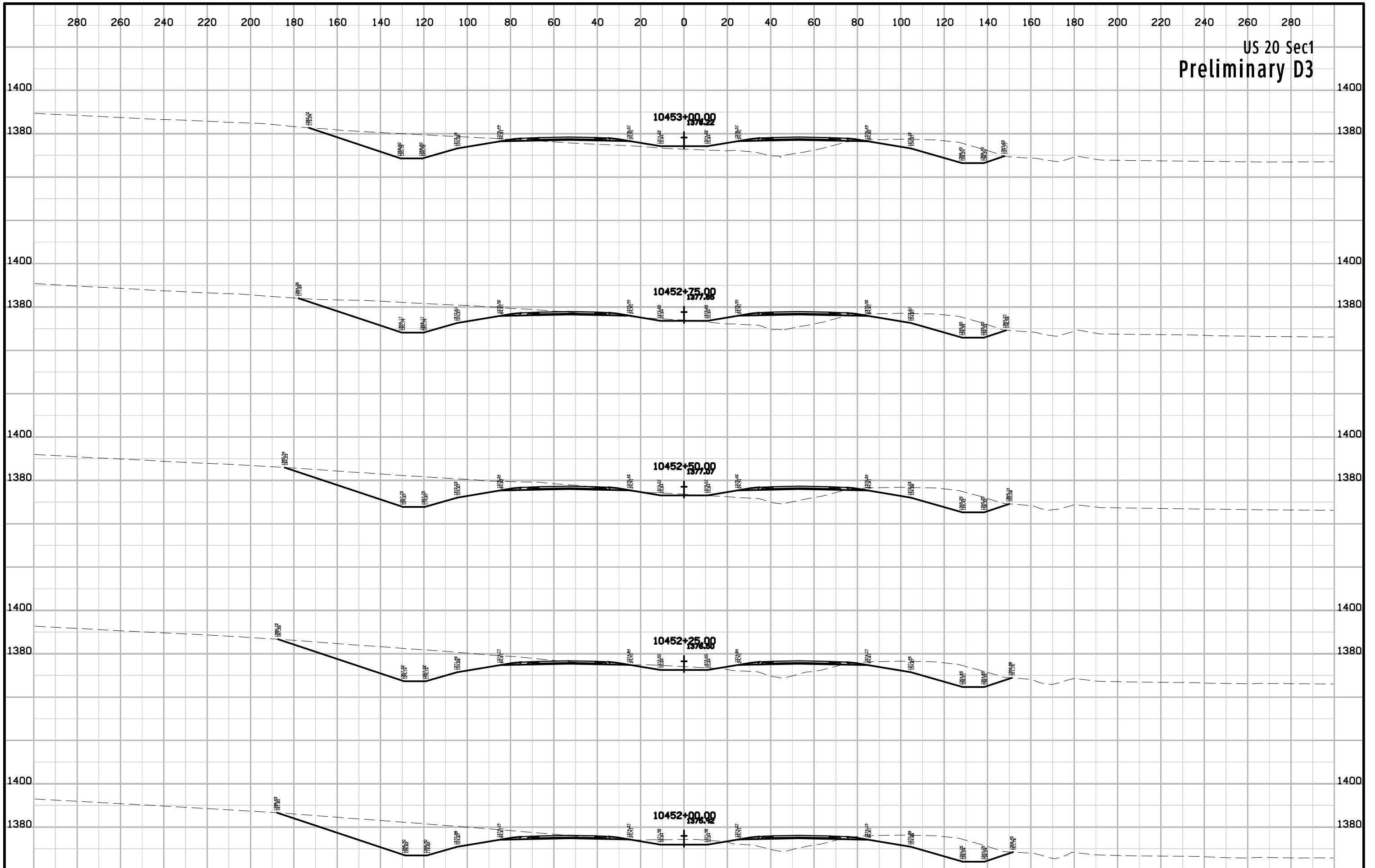
US 20 Sec1
Preliminary D3



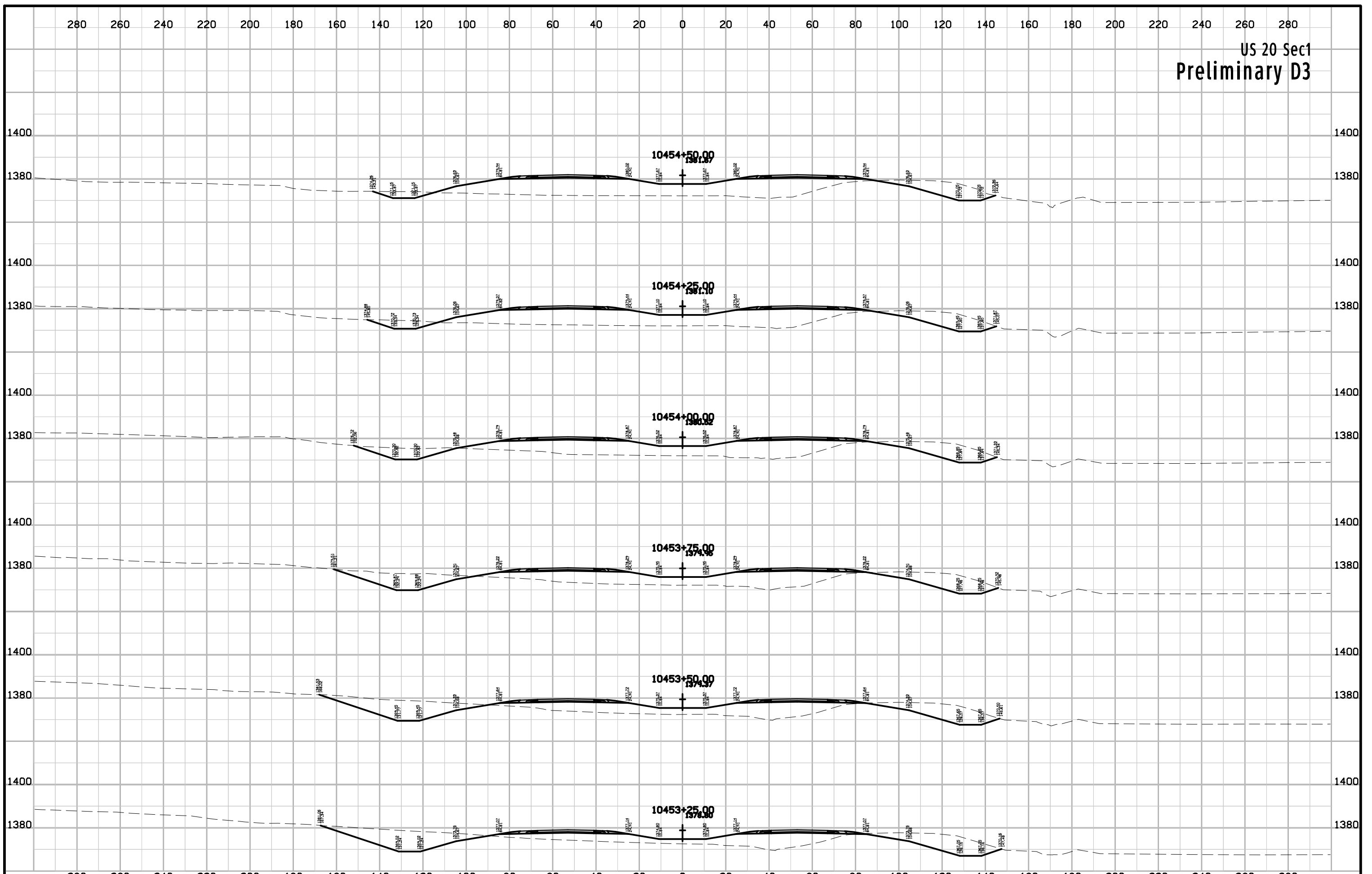
US 20 Sec1
Preliminary D3



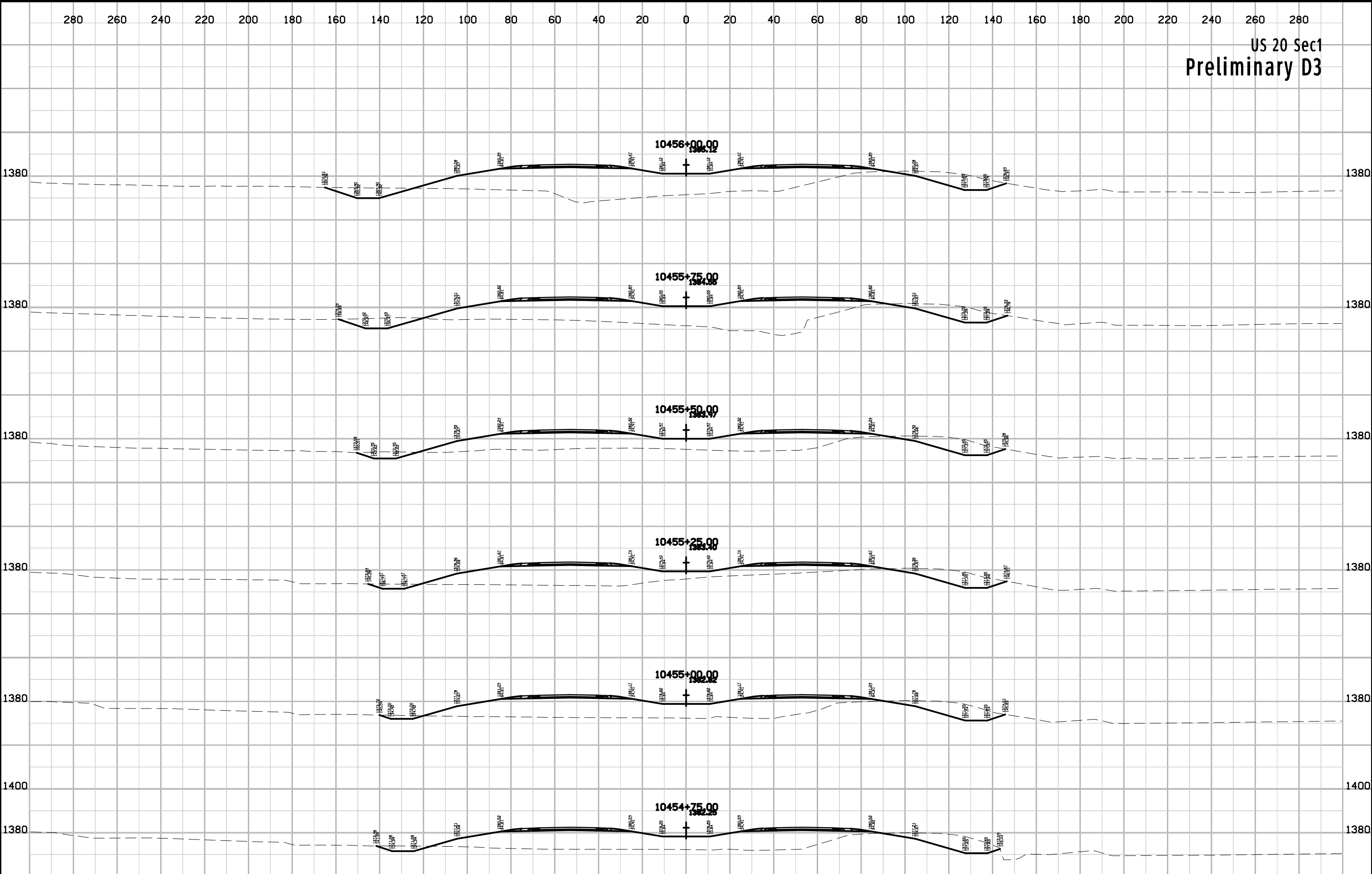
US 20 Sec1
Preliminary D3



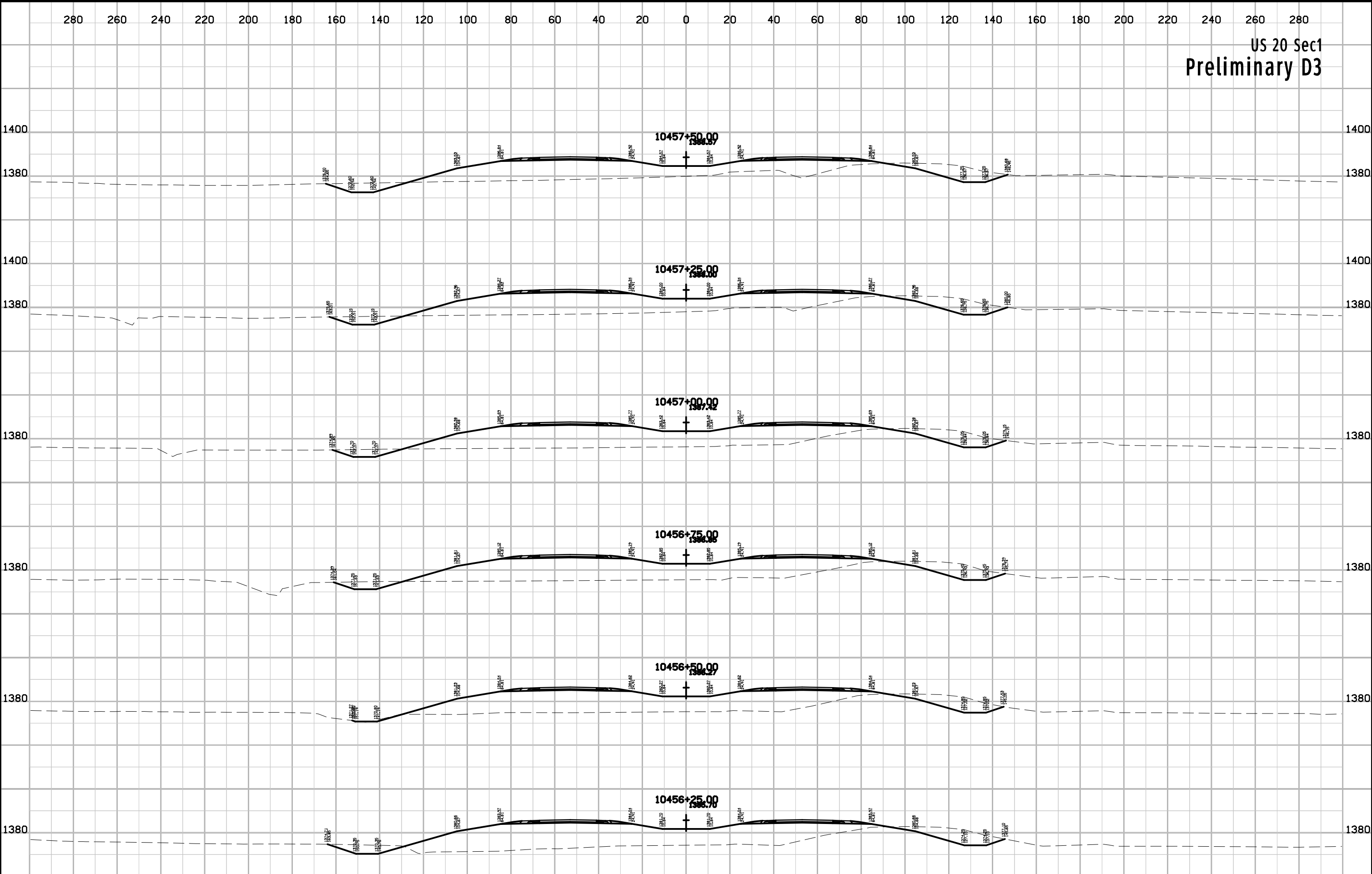
US 20 Sec1
Preliminary D3



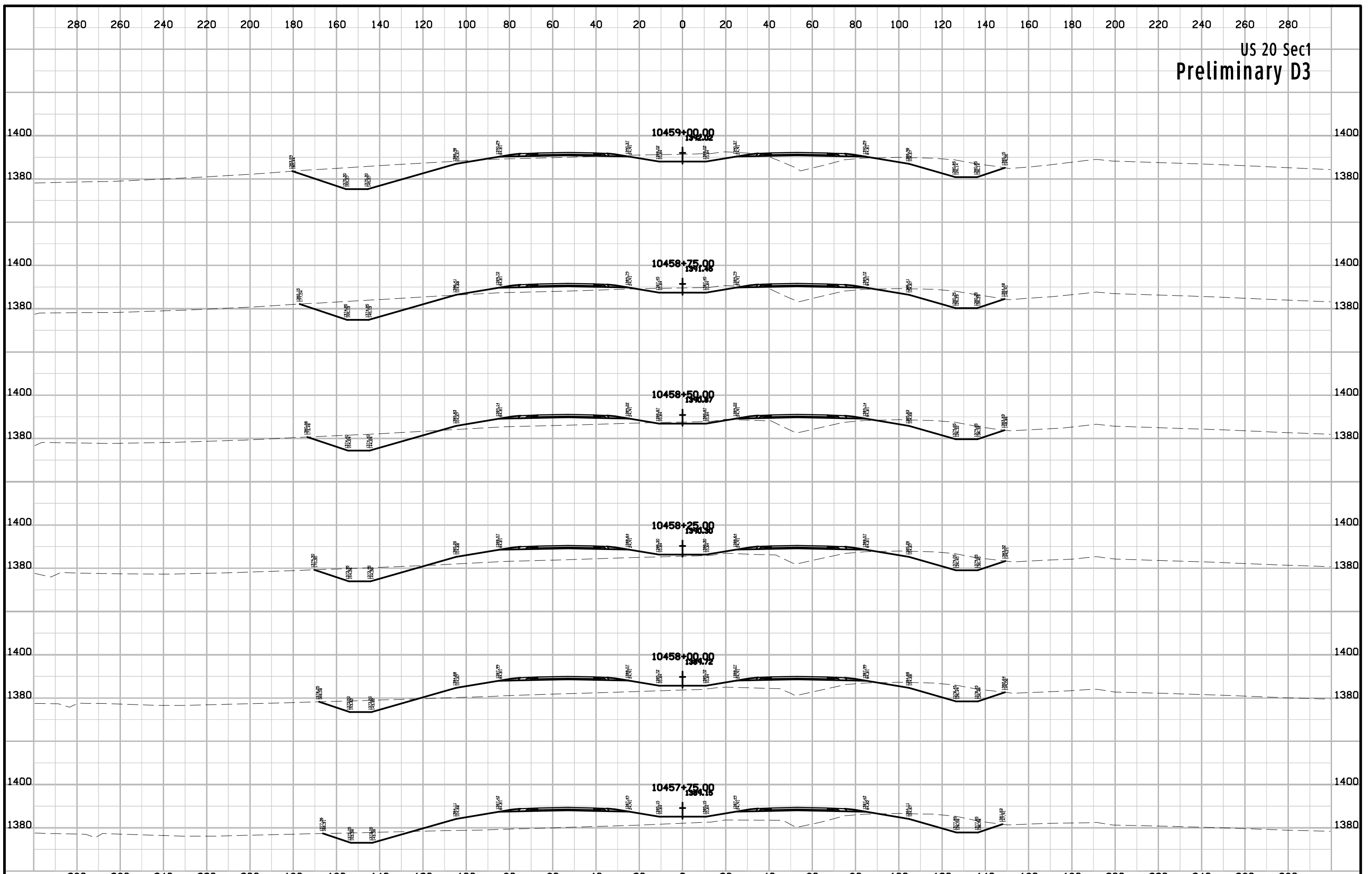
US 20 Sec1
Preliminary D3



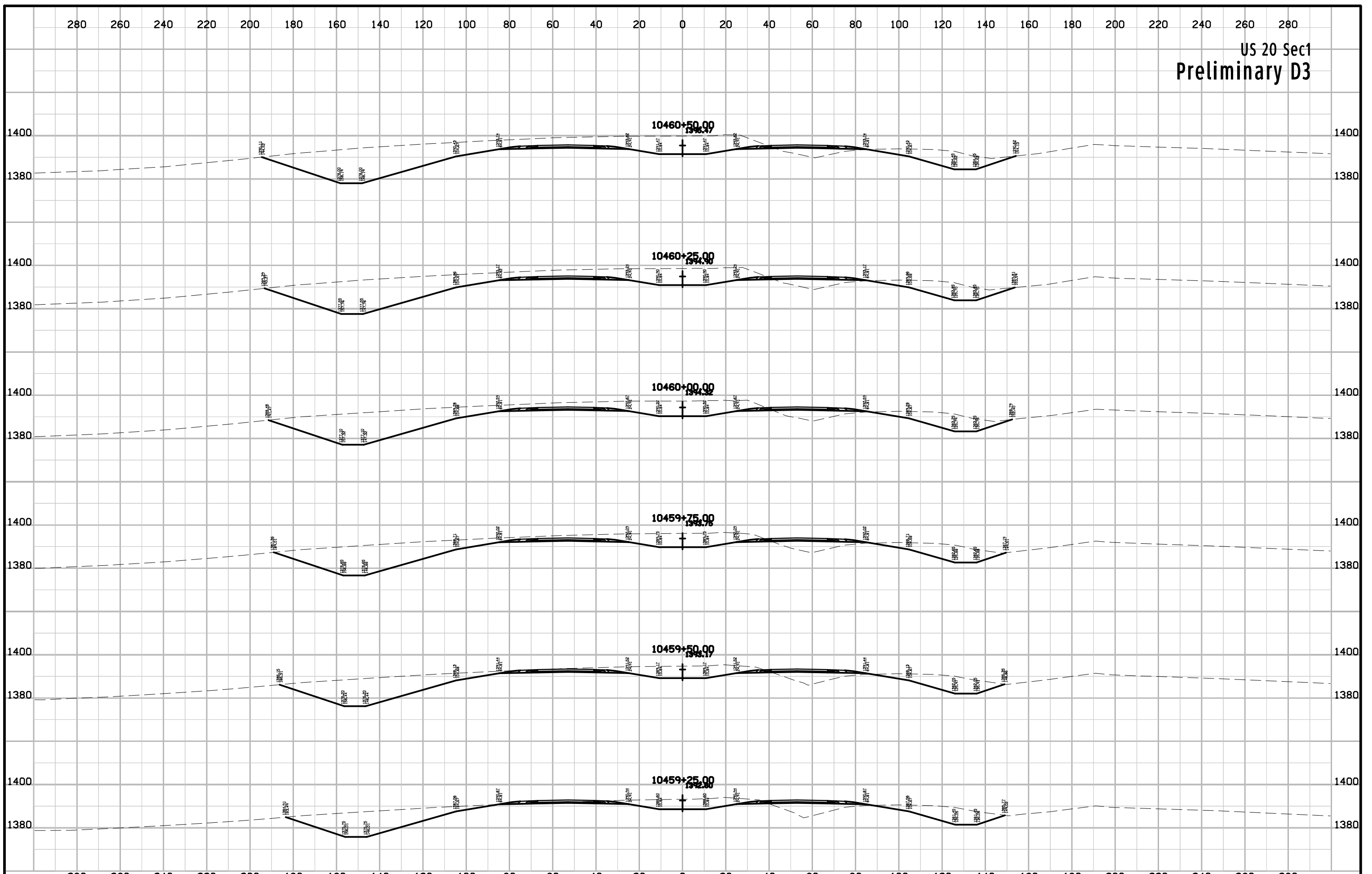
US 20 Sec1
Preliminary D3



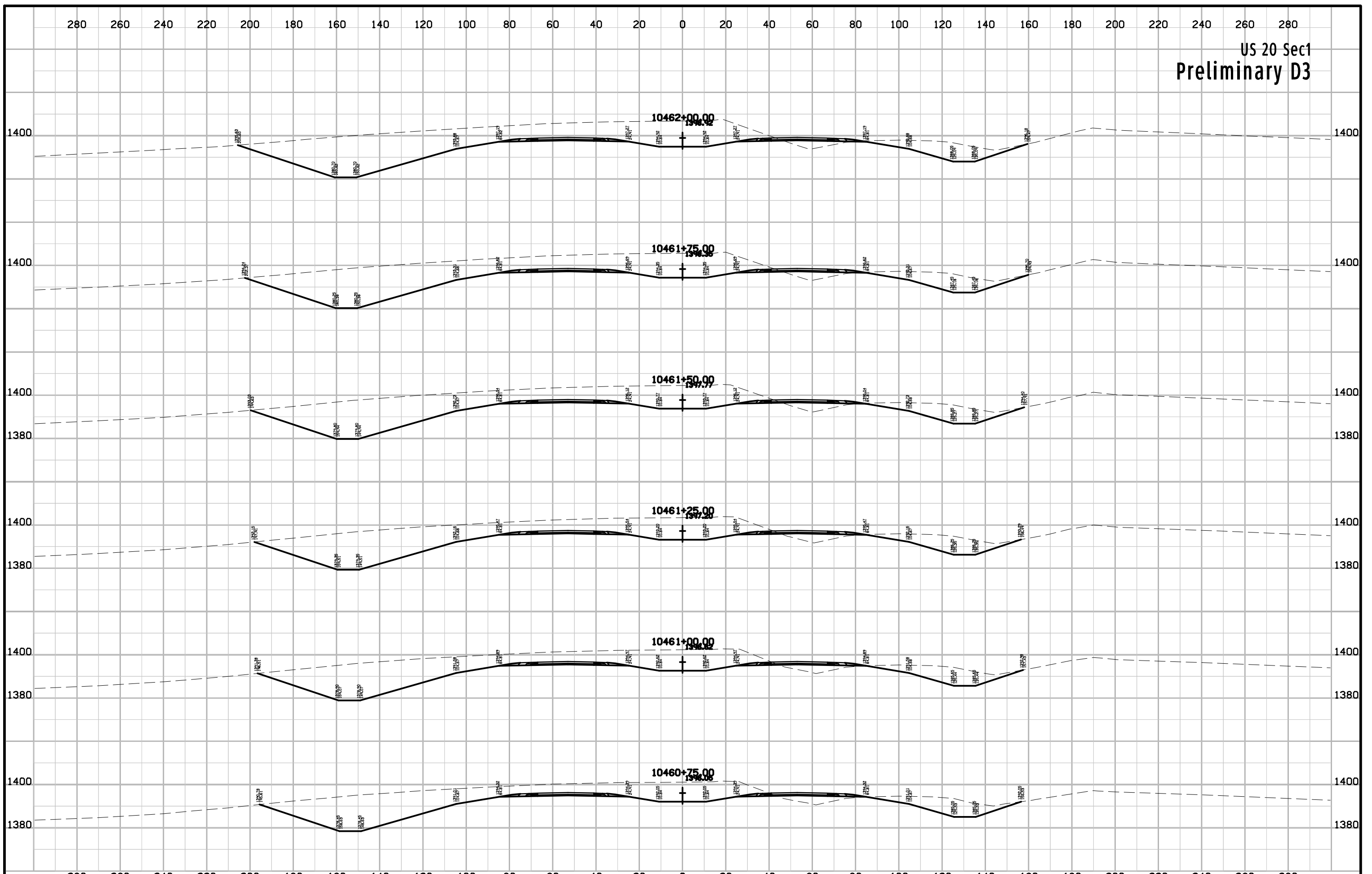
US 20 Sec1
Preliminary D3



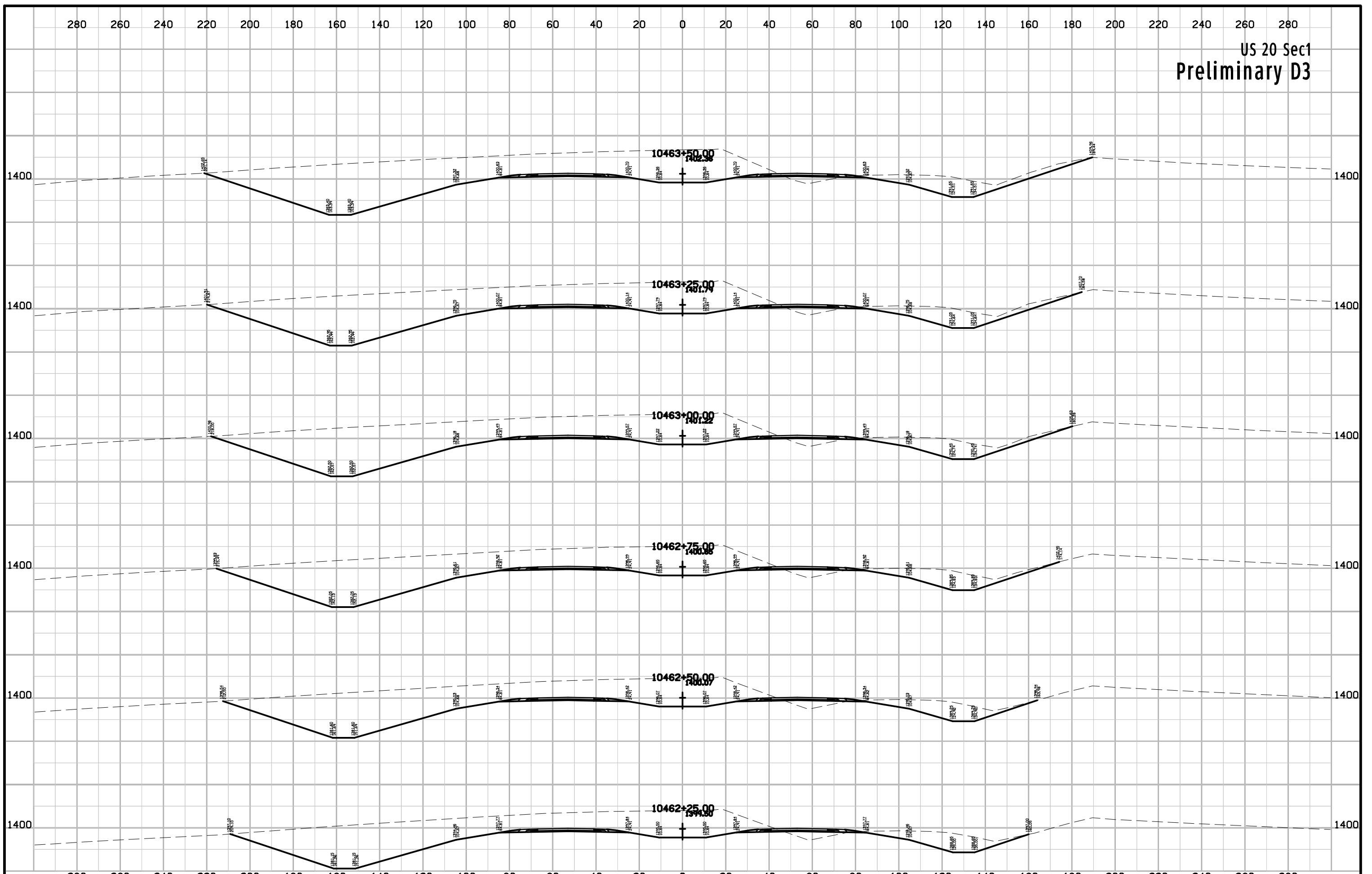
US 20 Sec1
Preliminary D3



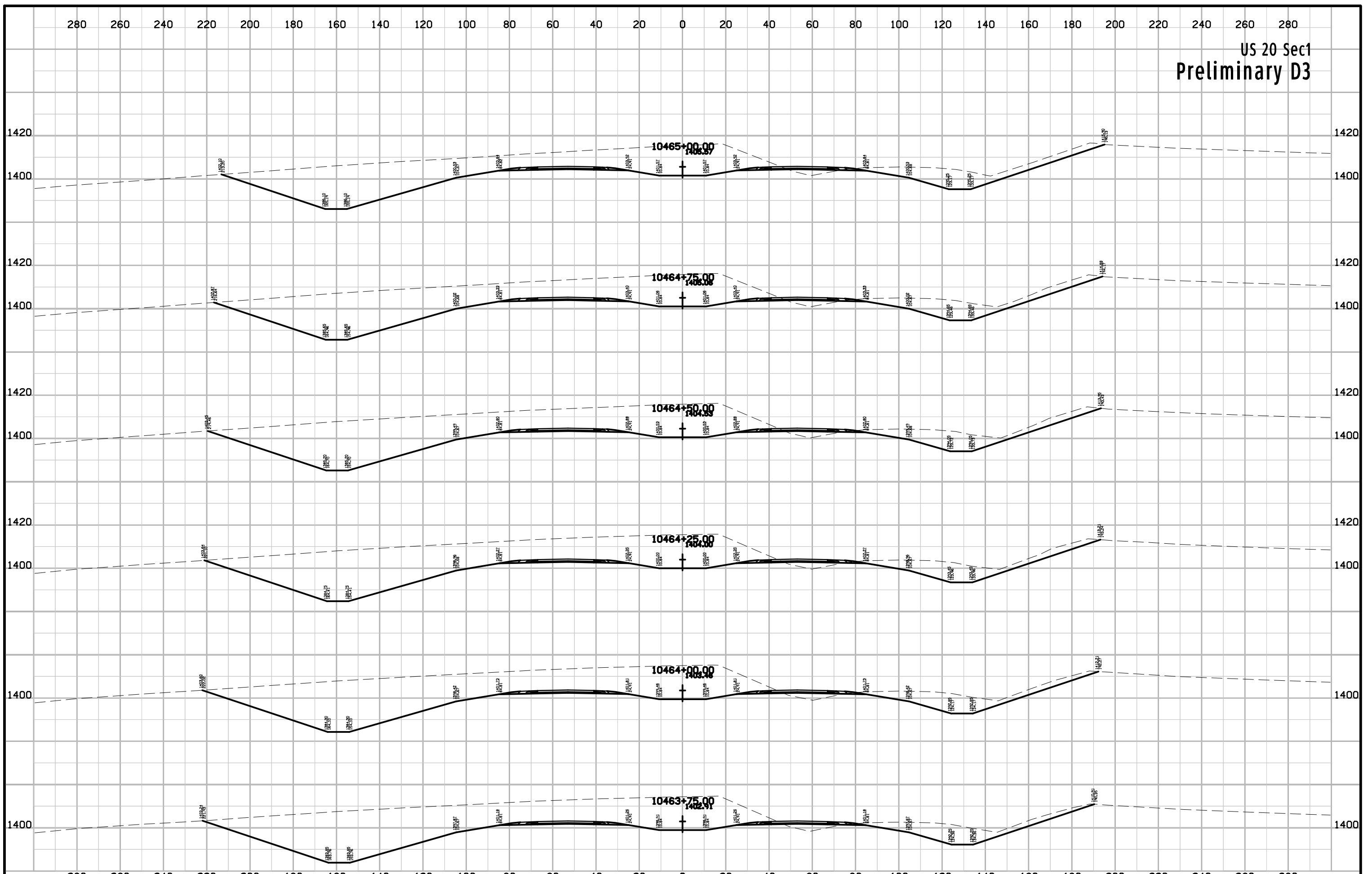
US 20 Sec1
Preliminary D3

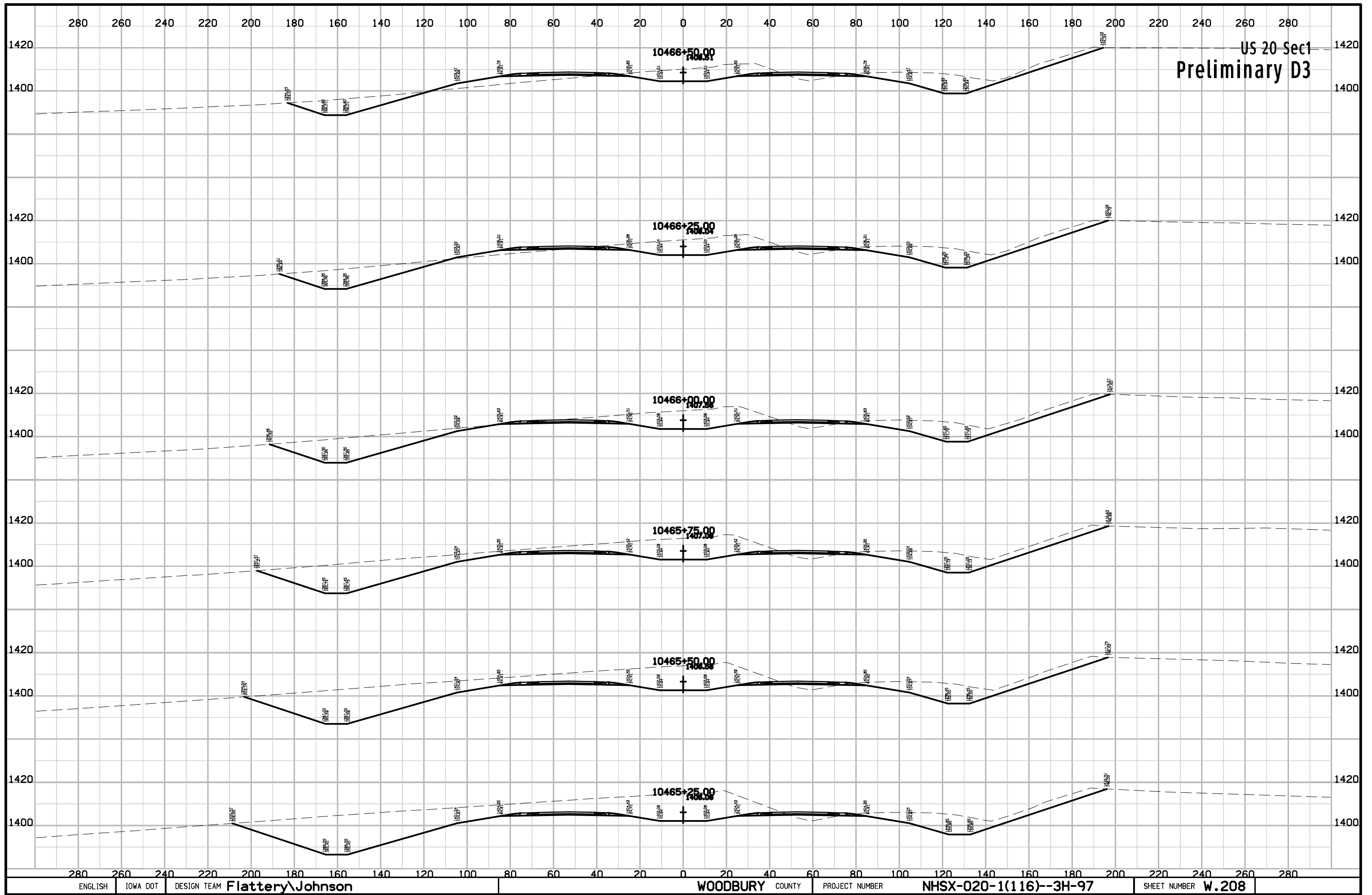


US 20 Sec1
Preliminary D3

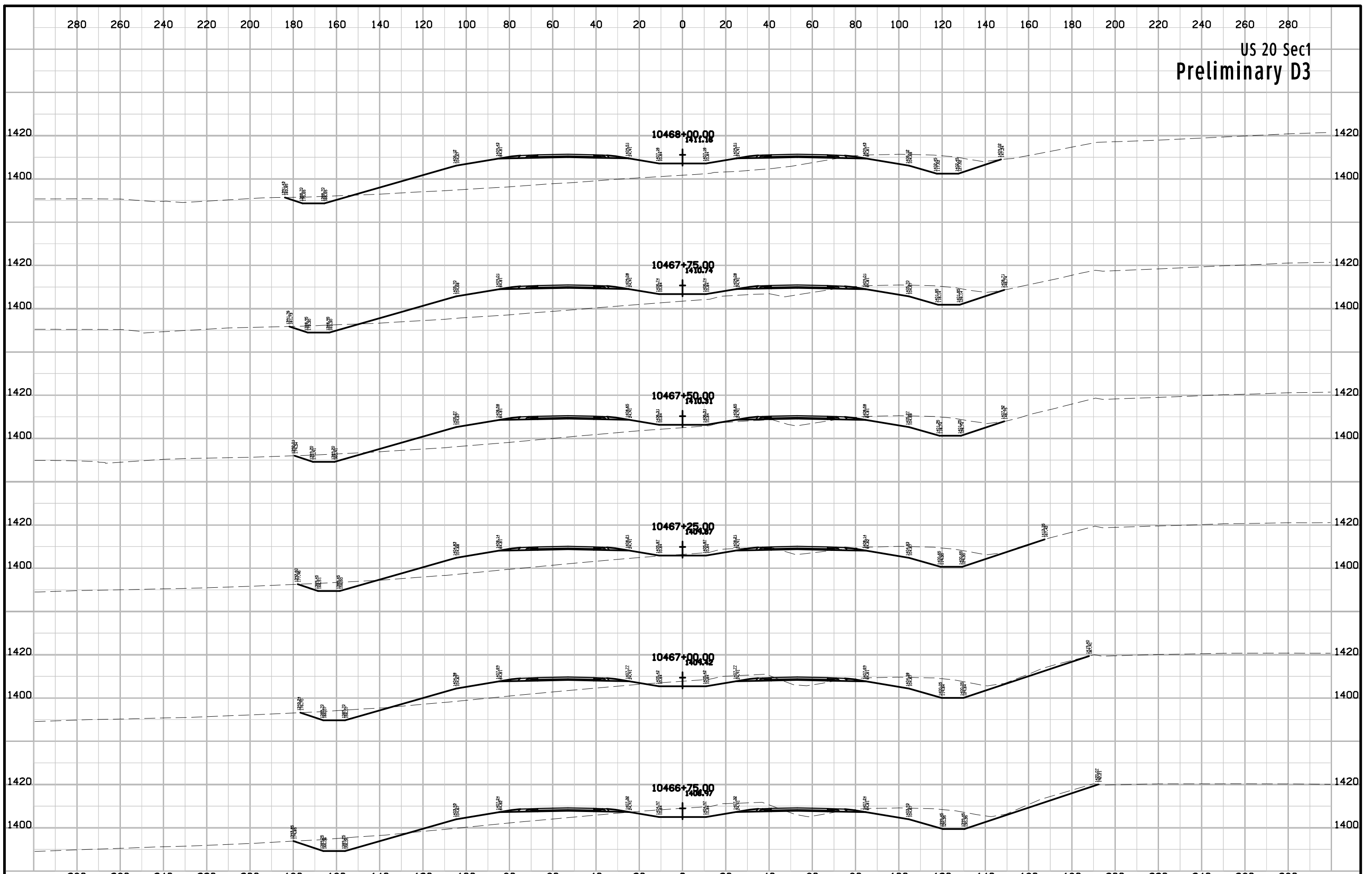


US 20 Sec1
Preliminary D3

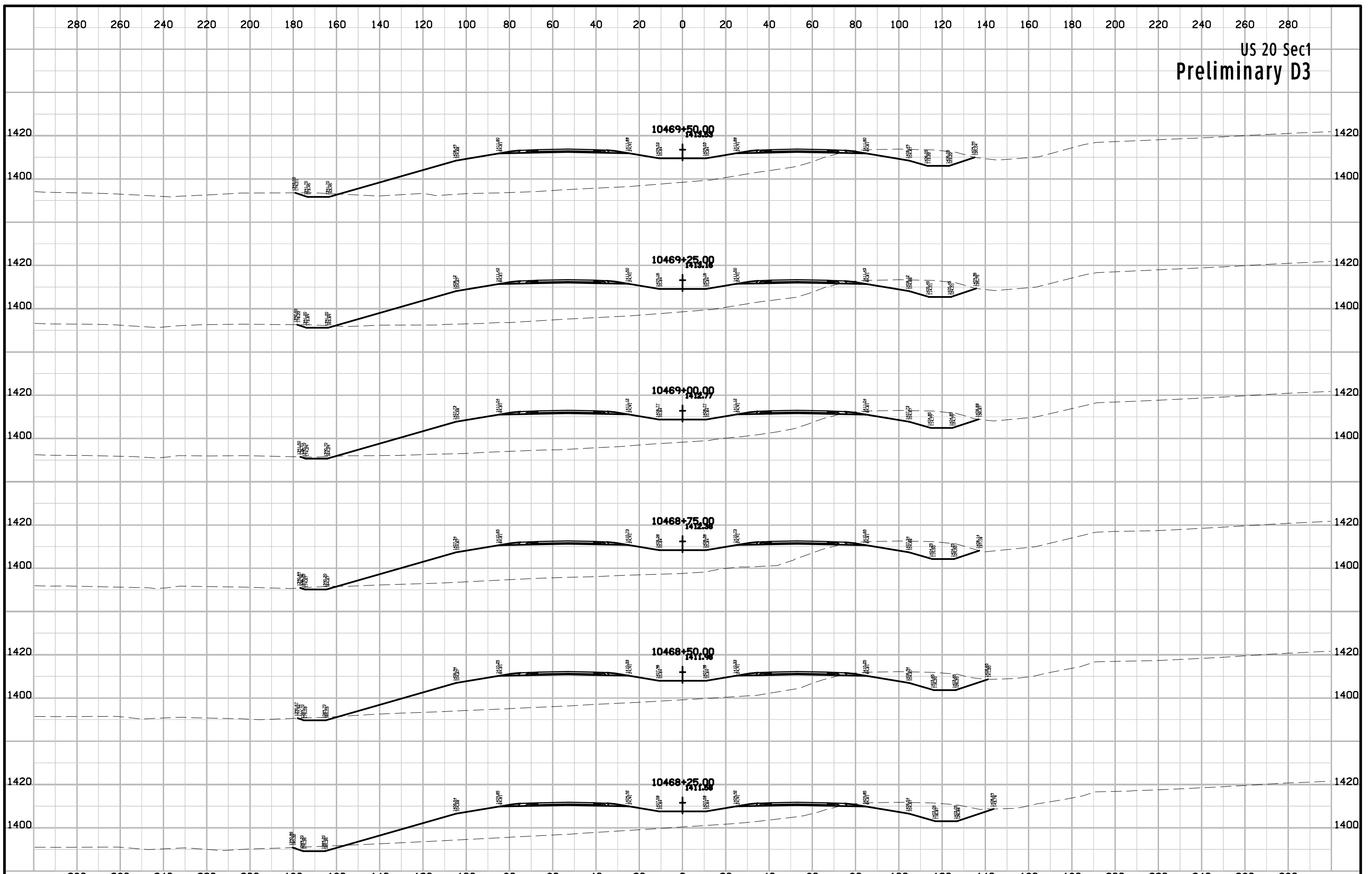




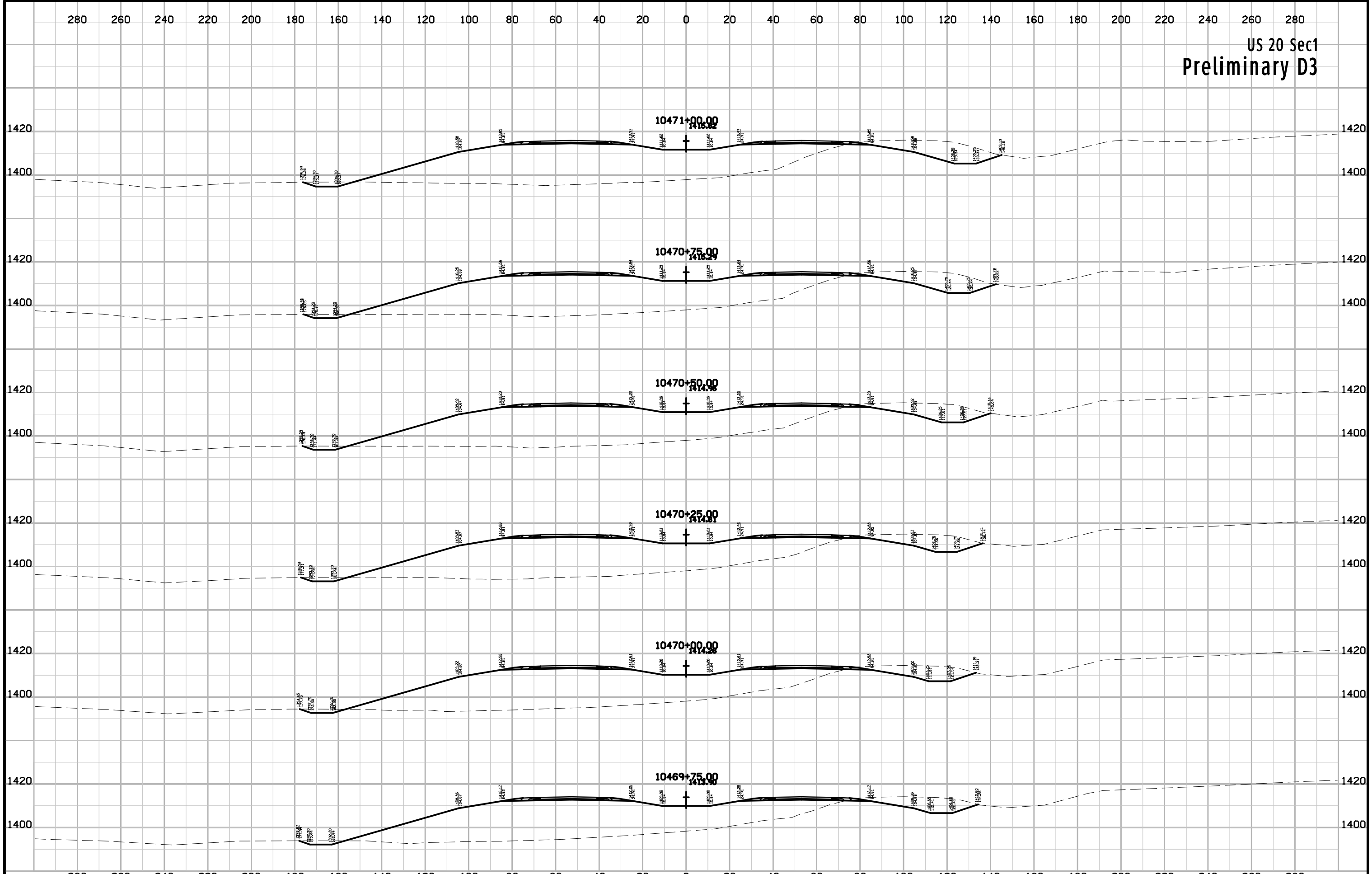
US 20 Sec1
Preliminary D3



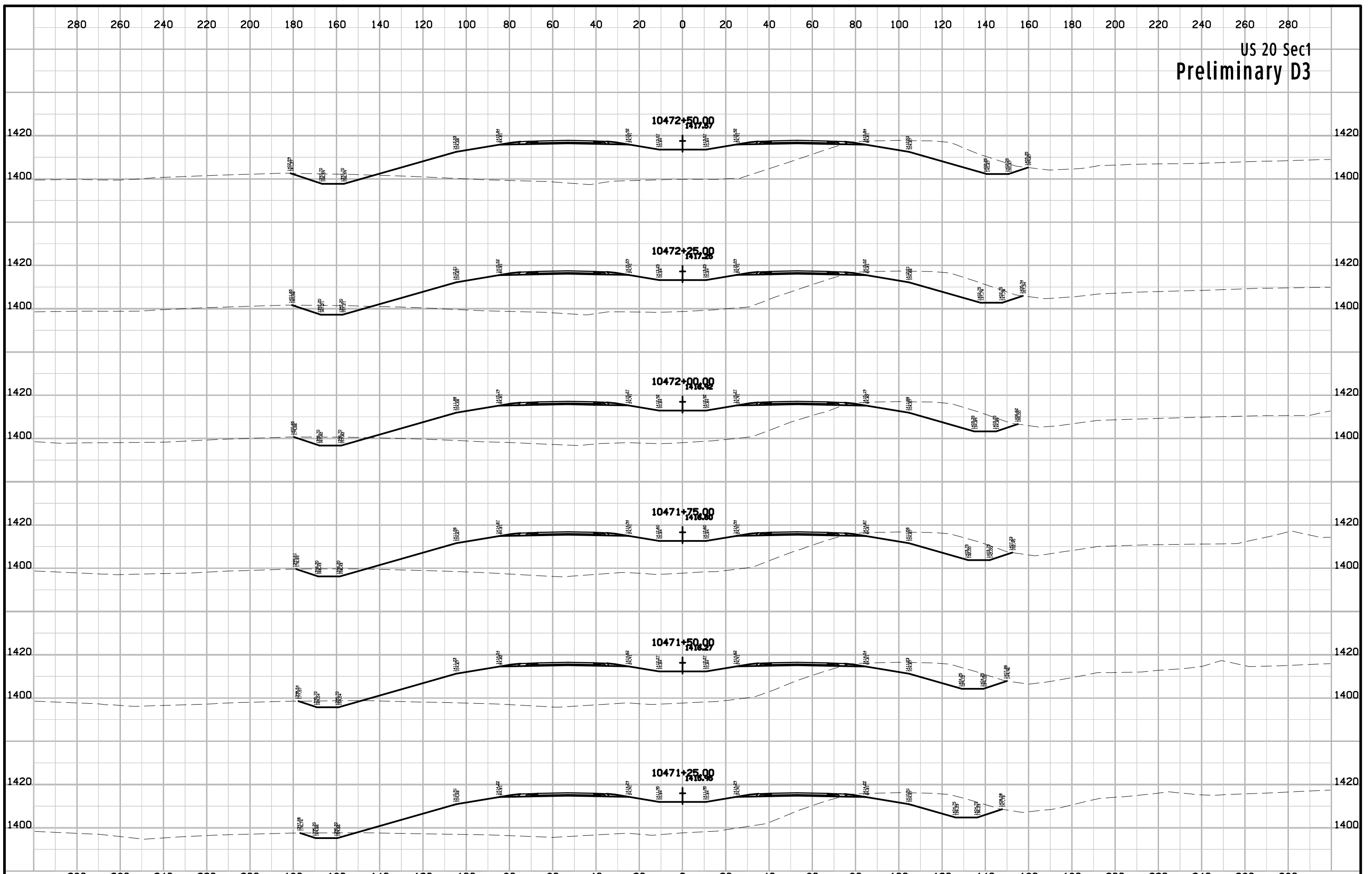
US 20 Sec1
Preliminary D3



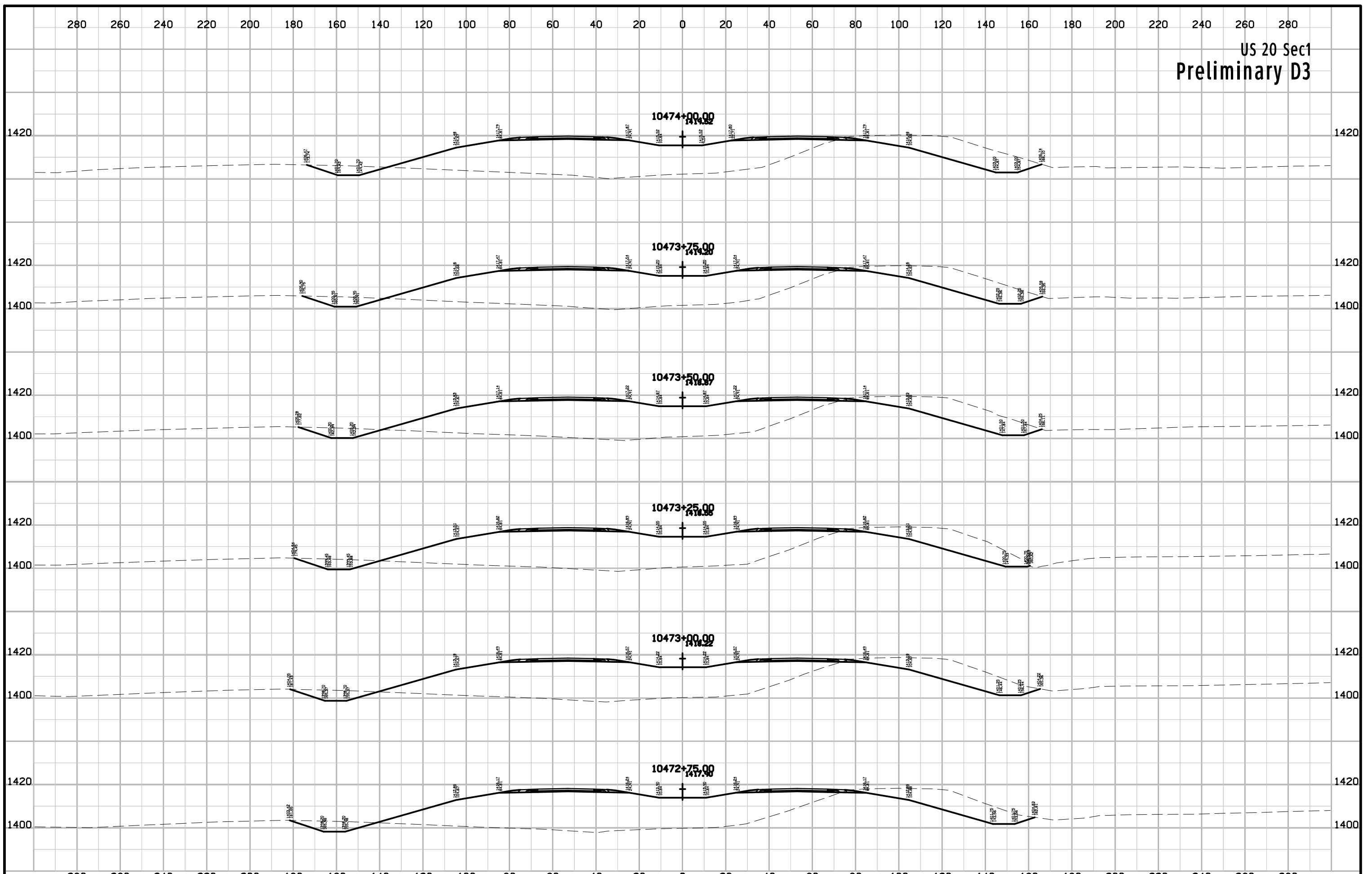
US 20 Sec1
Preliminary D3



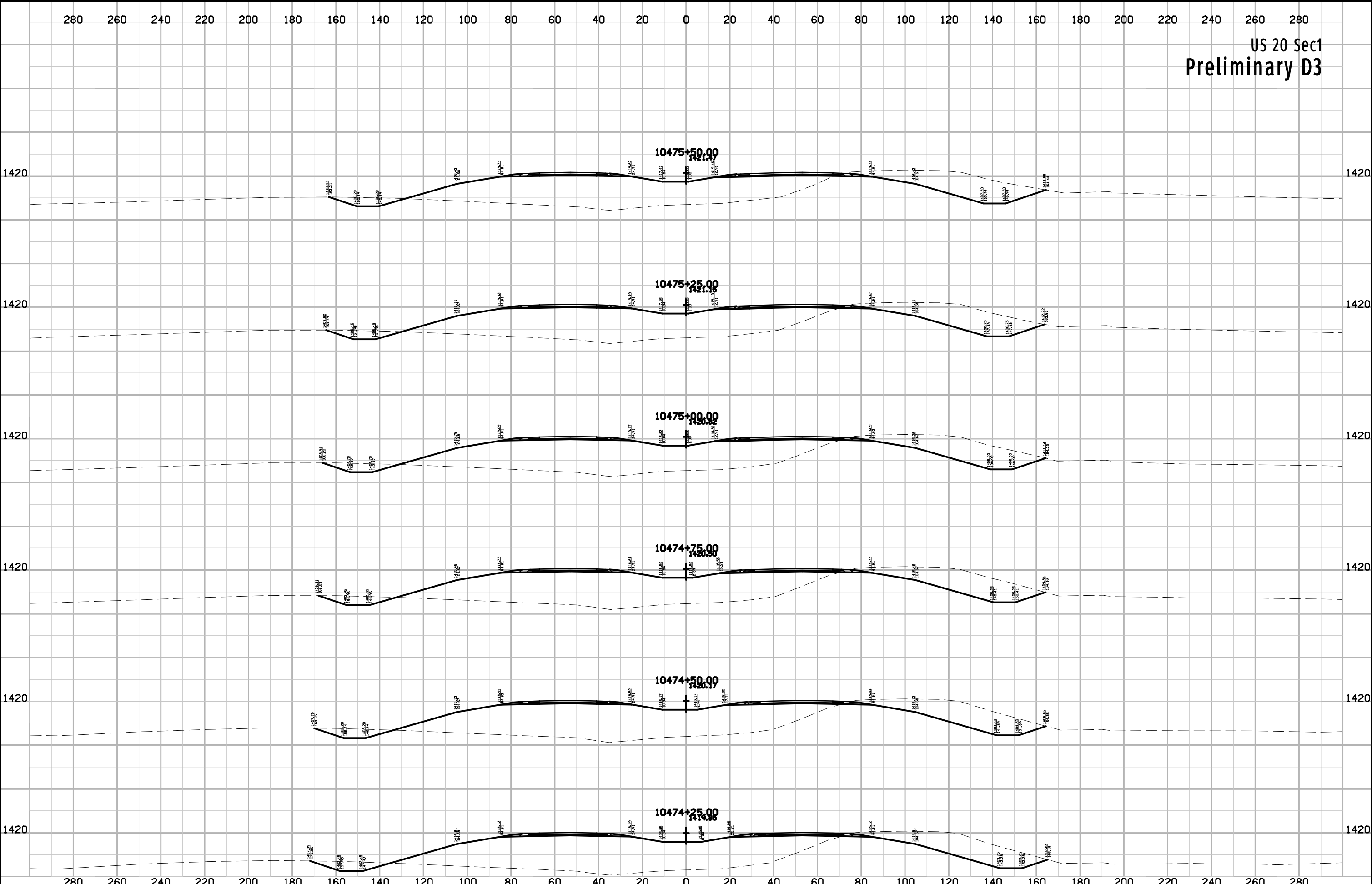
US 20 Sec1
Preliminary D3



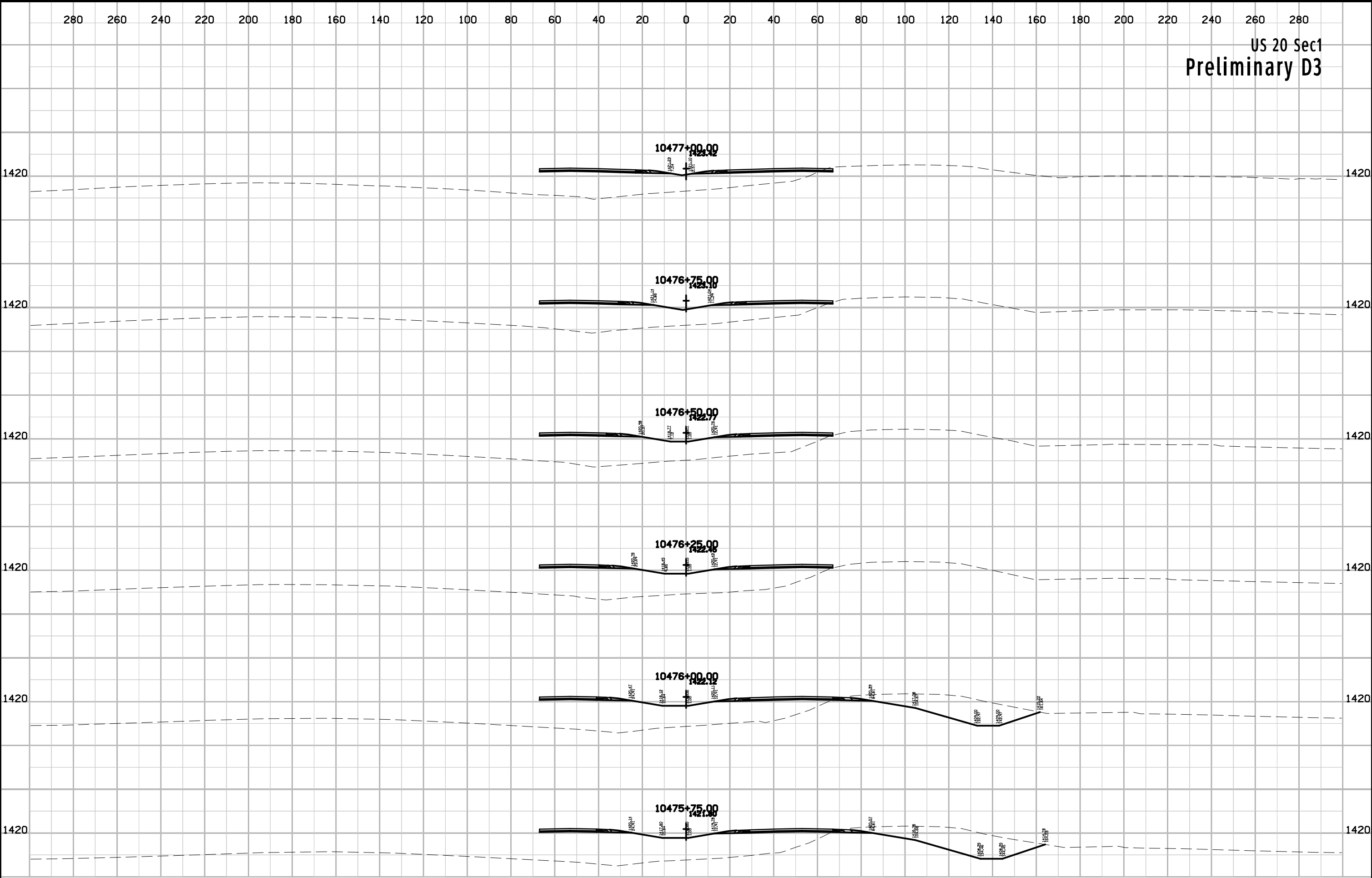
US 20 Sec1
Preliminary D3

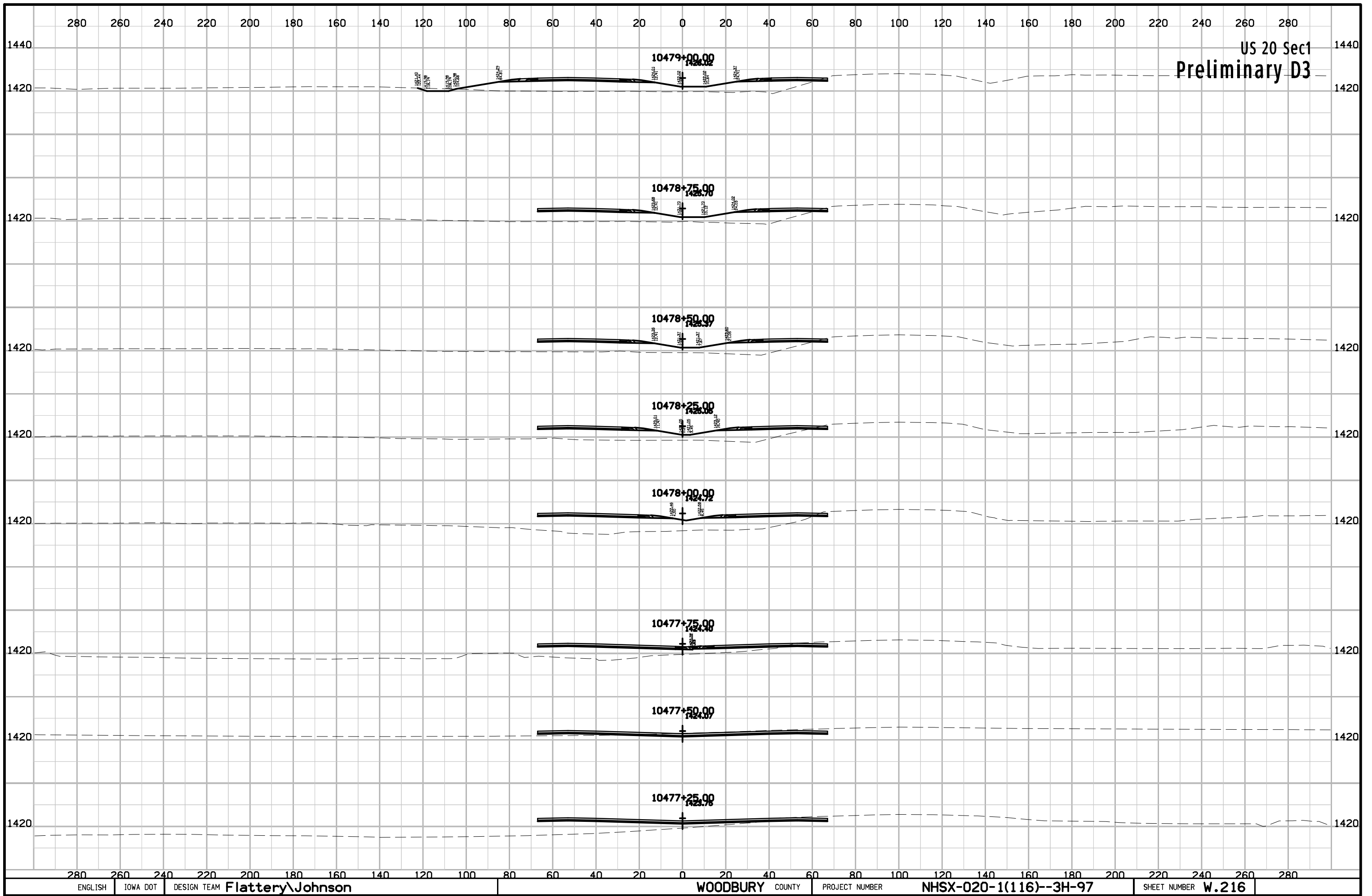


US 20 Sec1
Preliminary D3



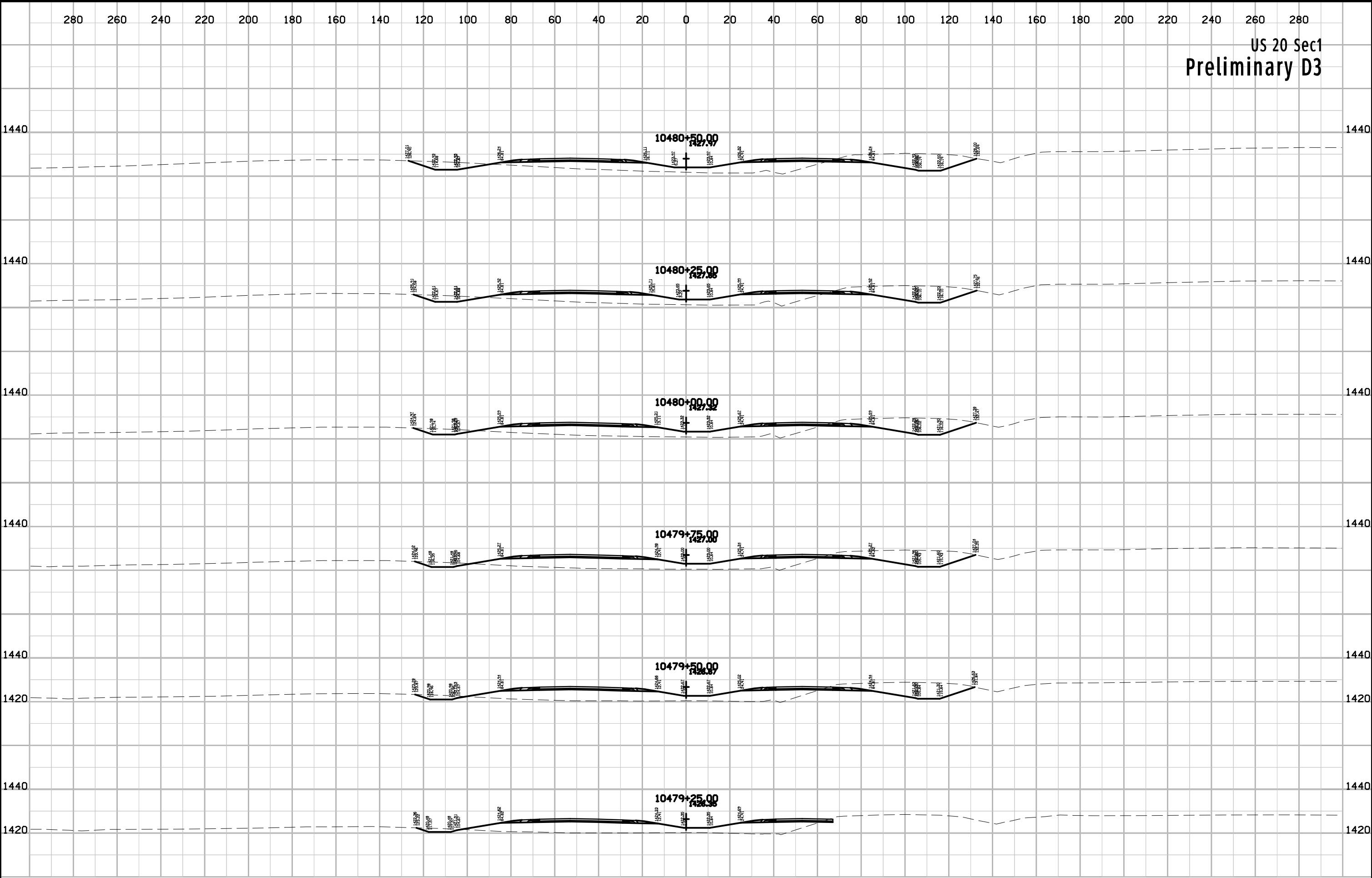
US 20 Sec1
Preliminary D3



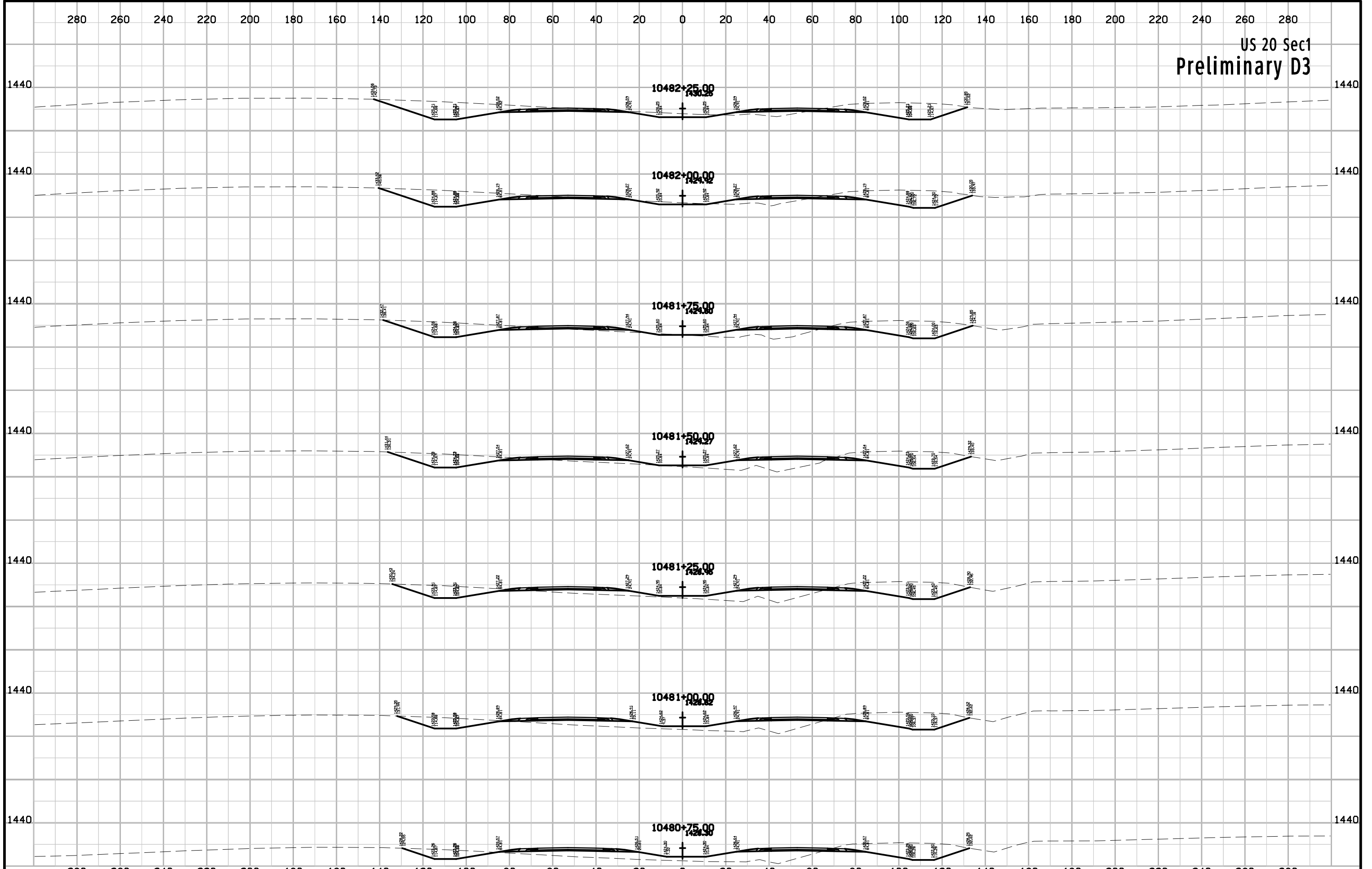


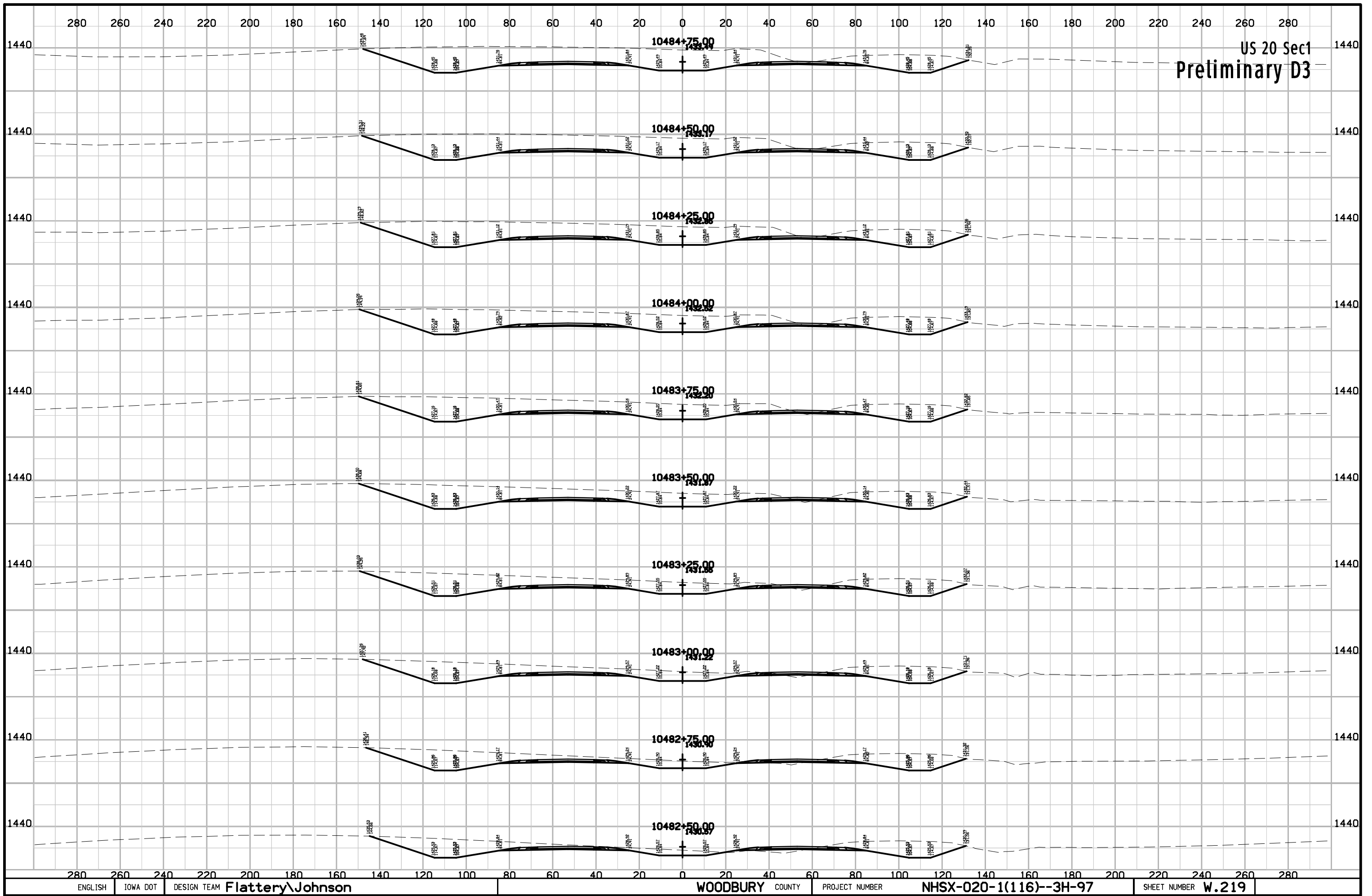
US 20 Sec1
Preliminary D3

US 20 Sec1
Preliminary D3

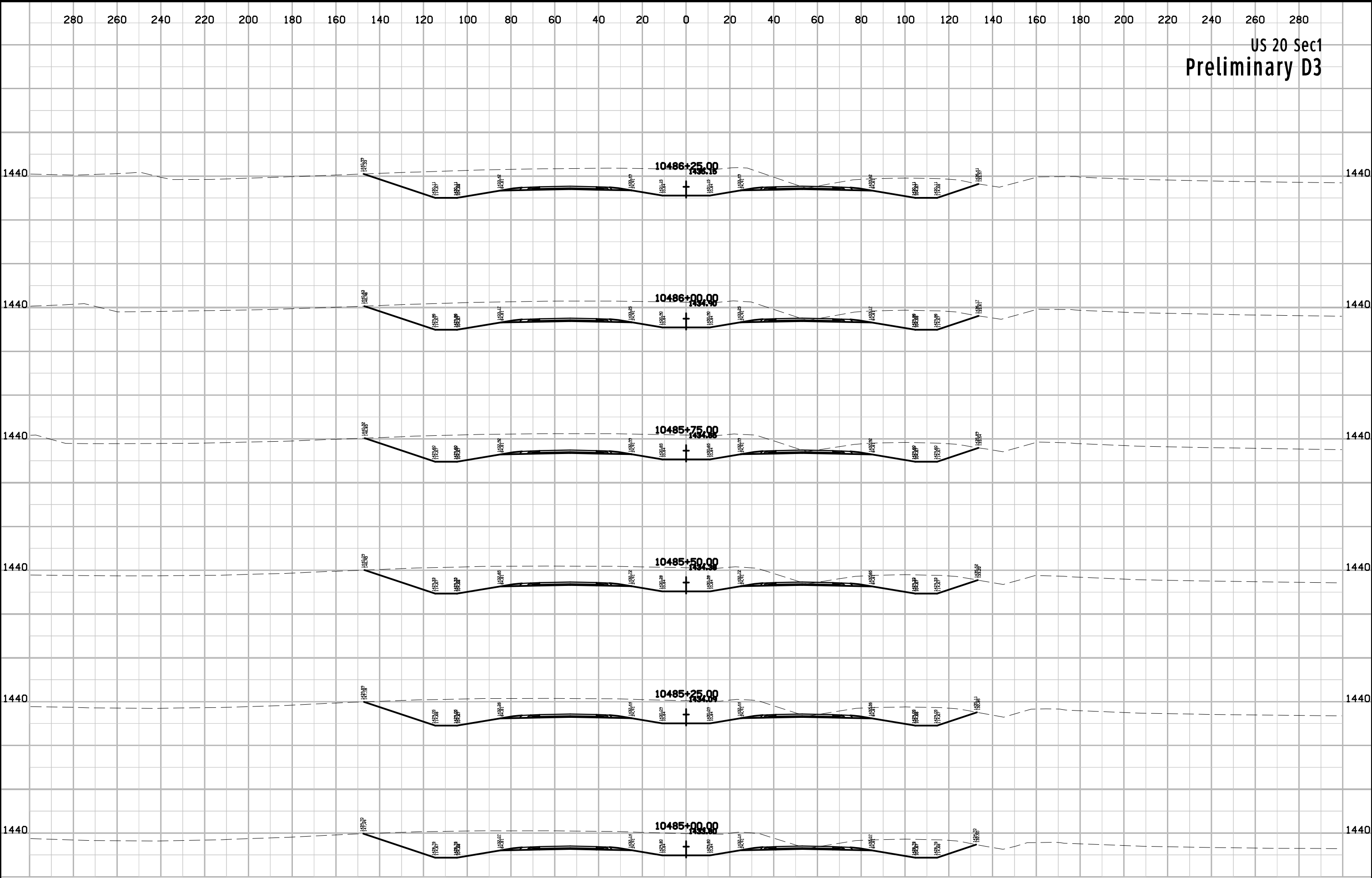


US 20 Sec1
Preliminary D3

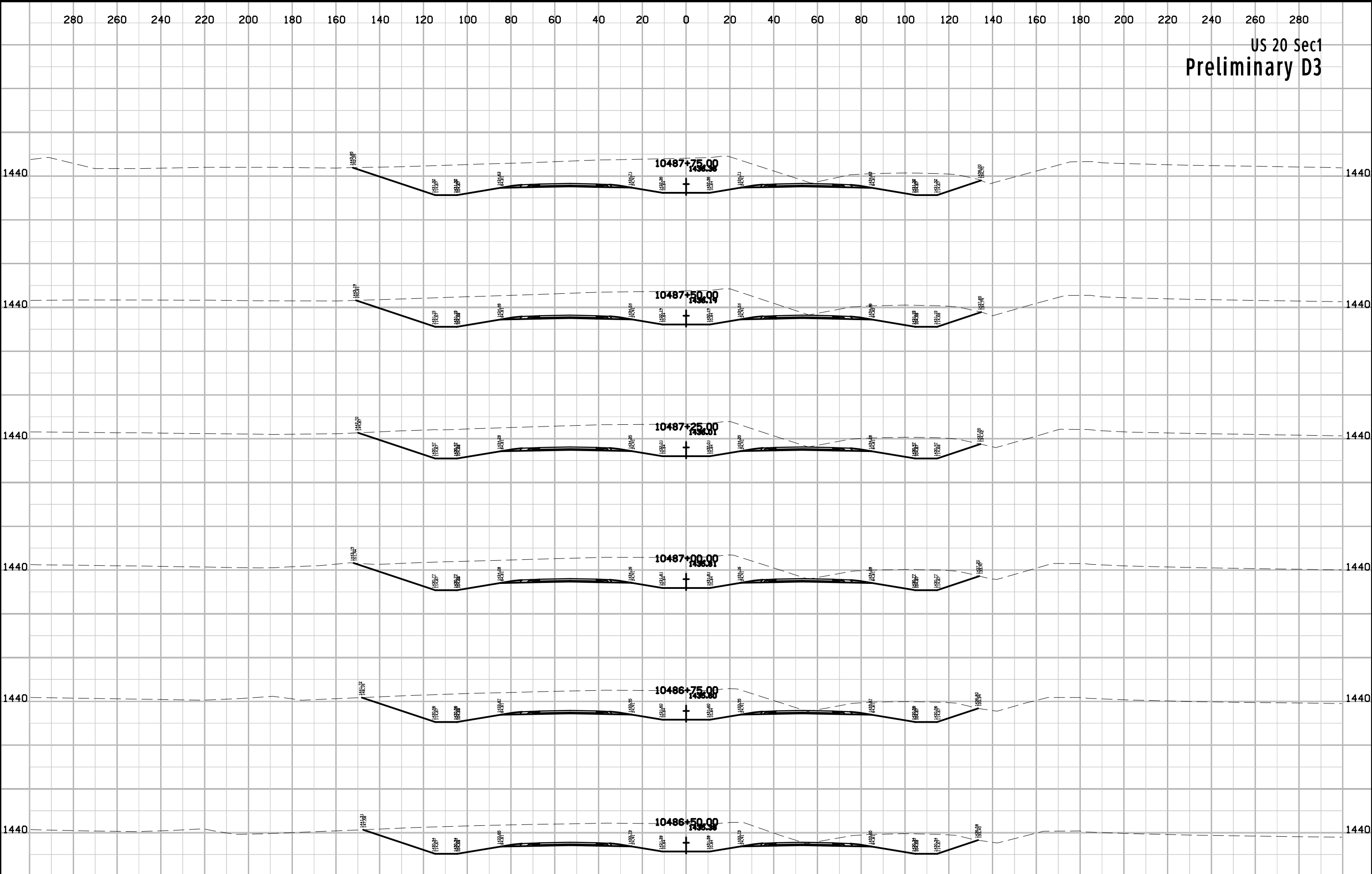




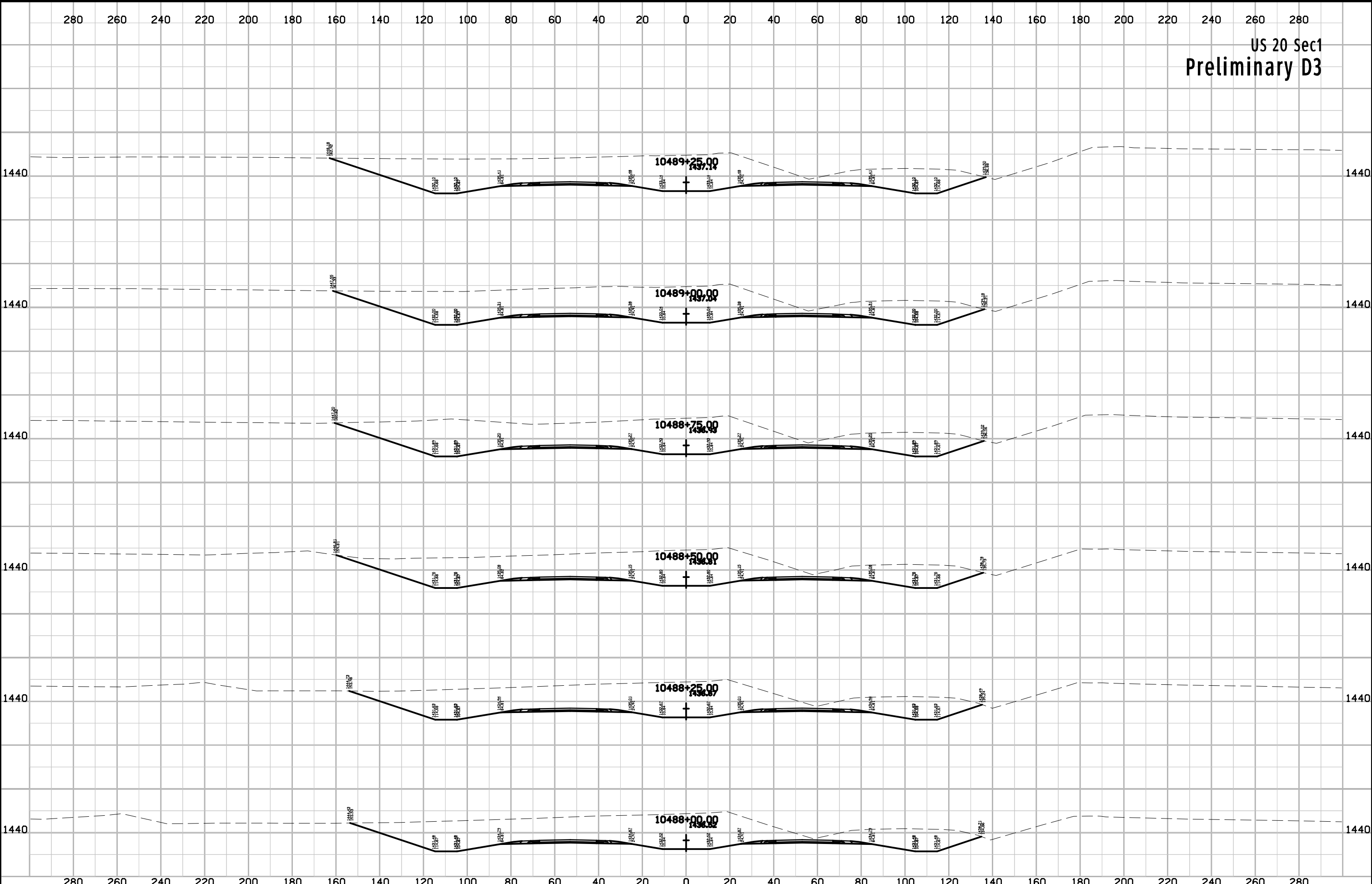
US 20 Sec1
Preliminary D3



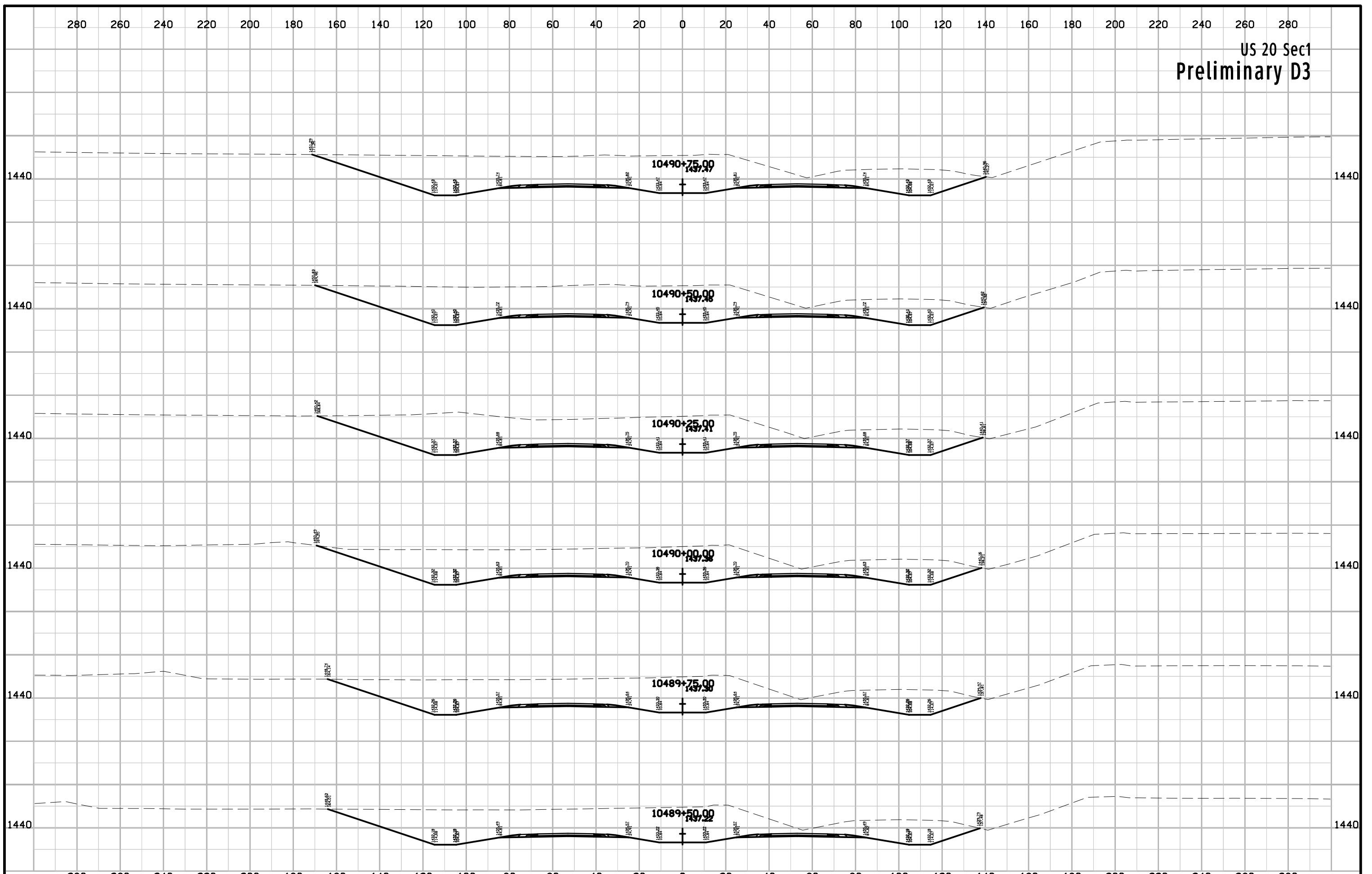
US 20 Sec1
Preliminary D3



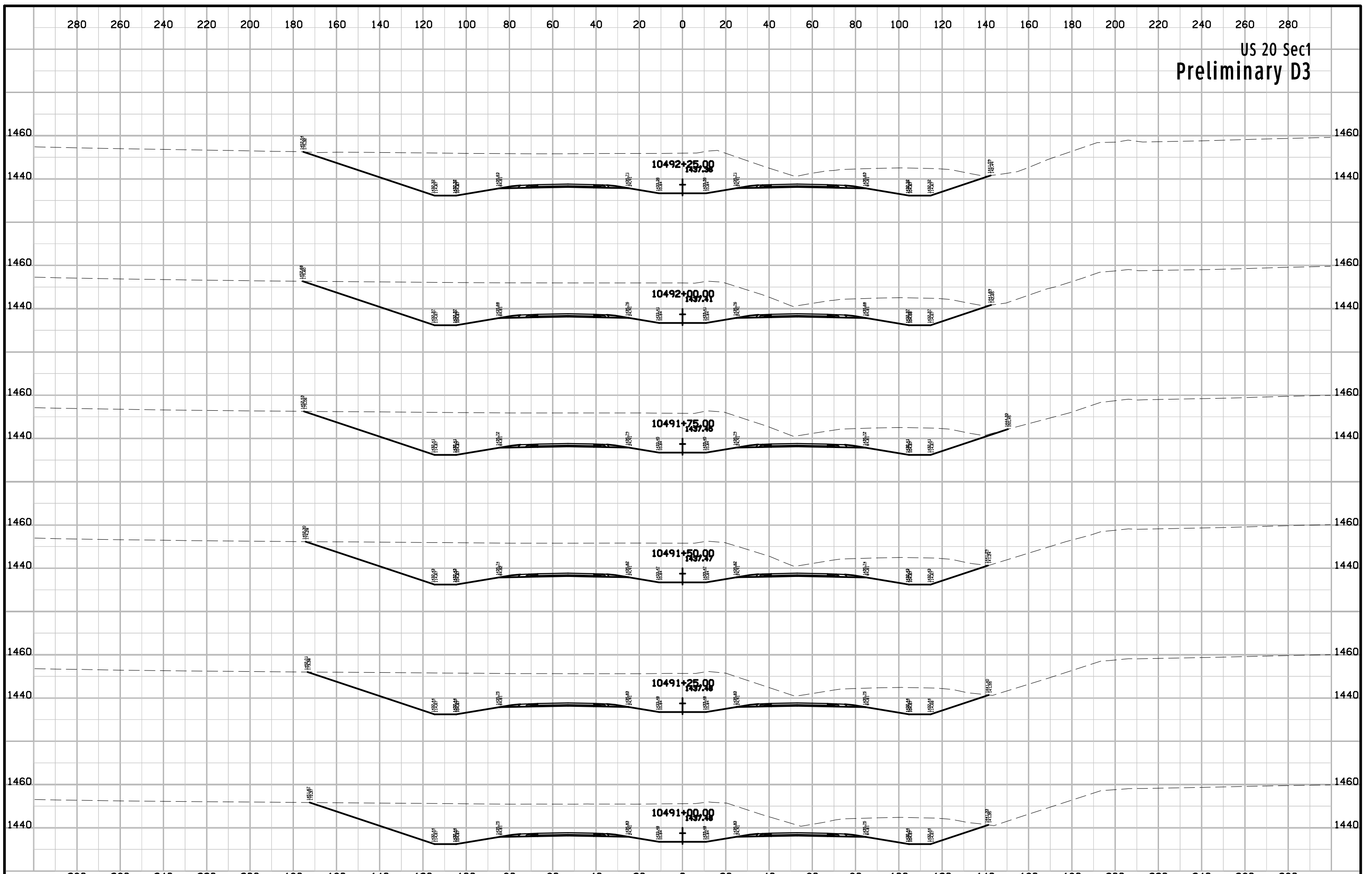
US 20 Sec1
Preliminary D3



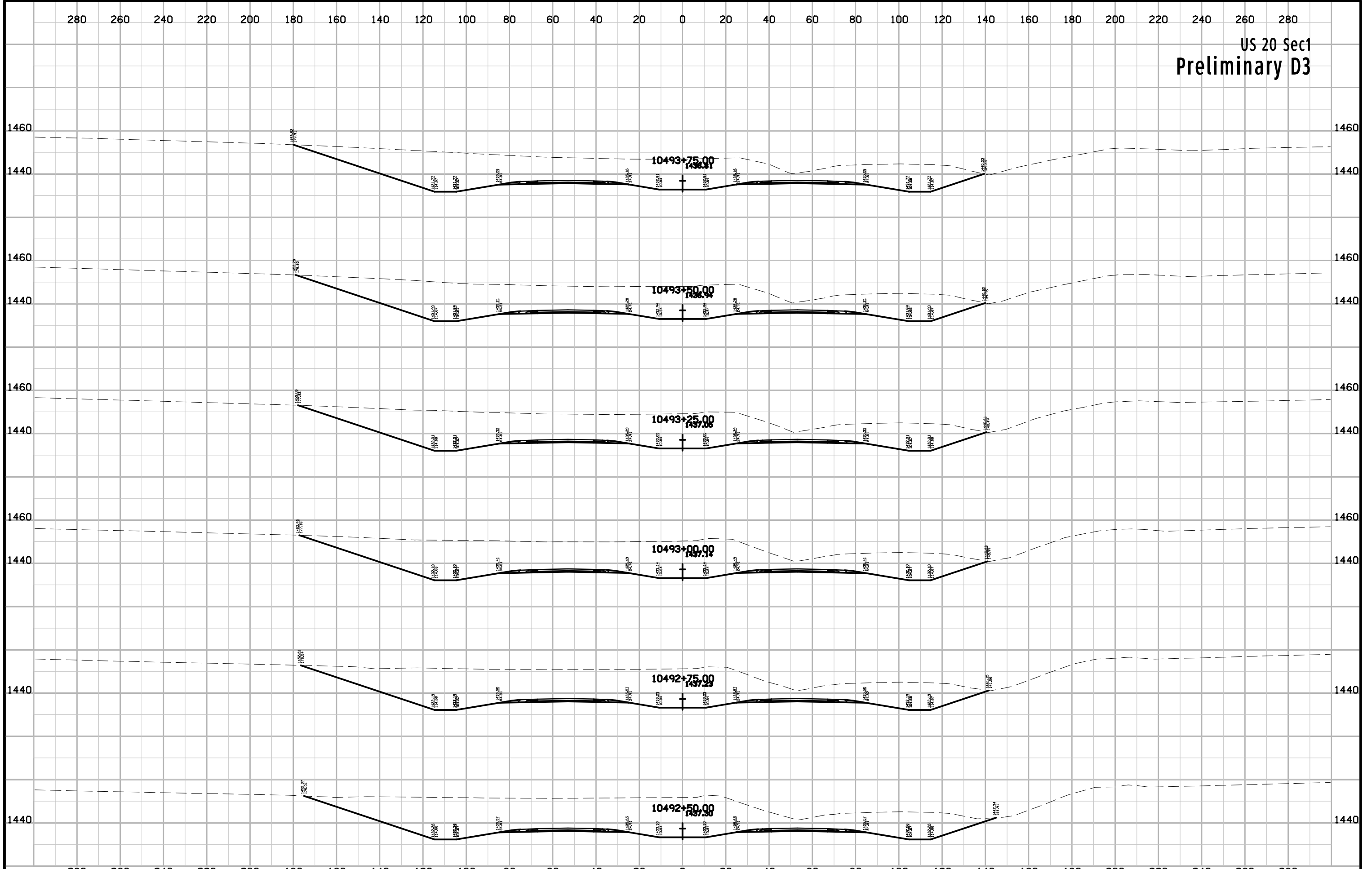
US 20 Sec1
Preliminary D3



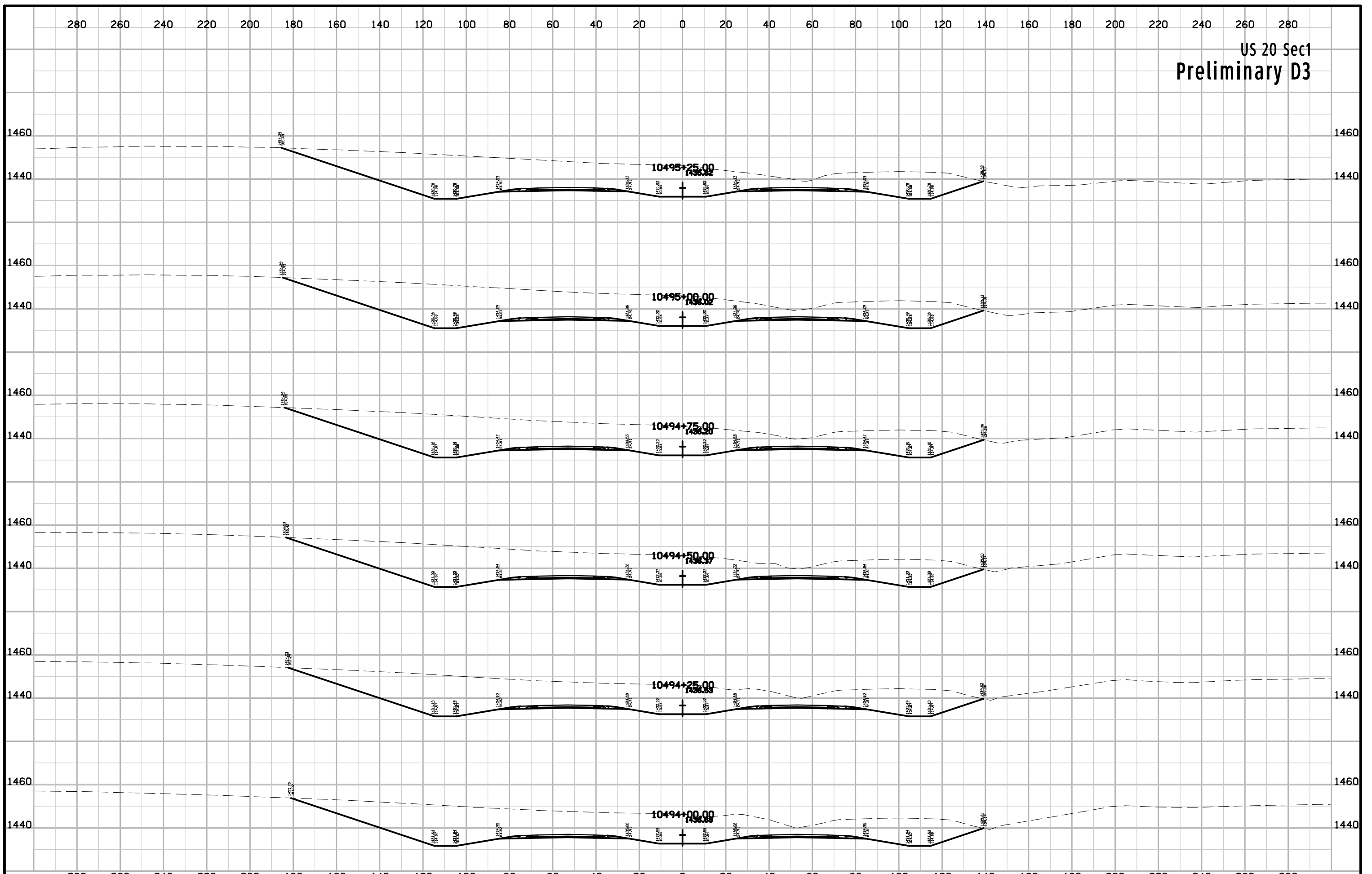
US 20 Sec1
Preliminary D3



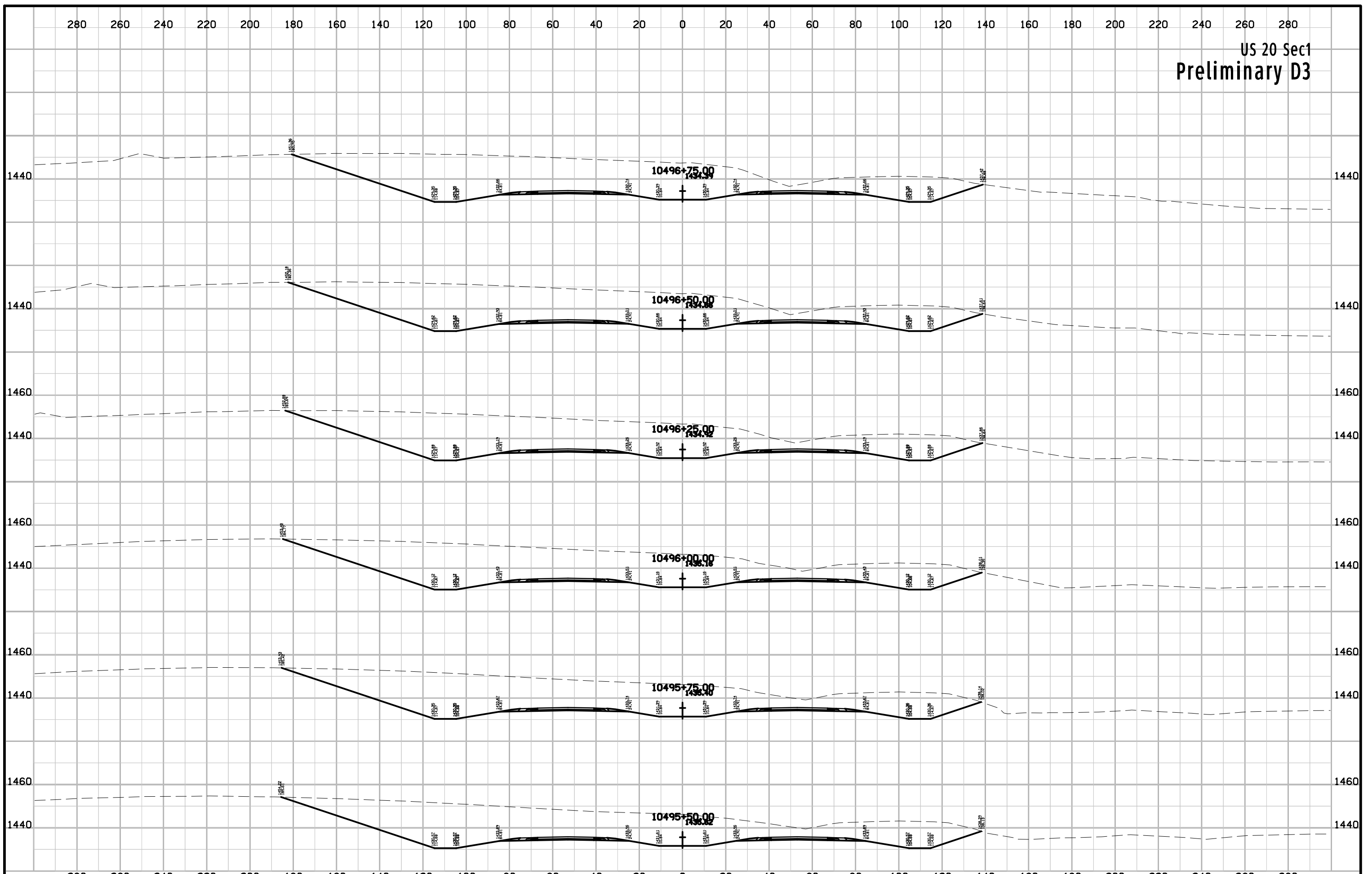
US 20 Sec1
Preliminary D3



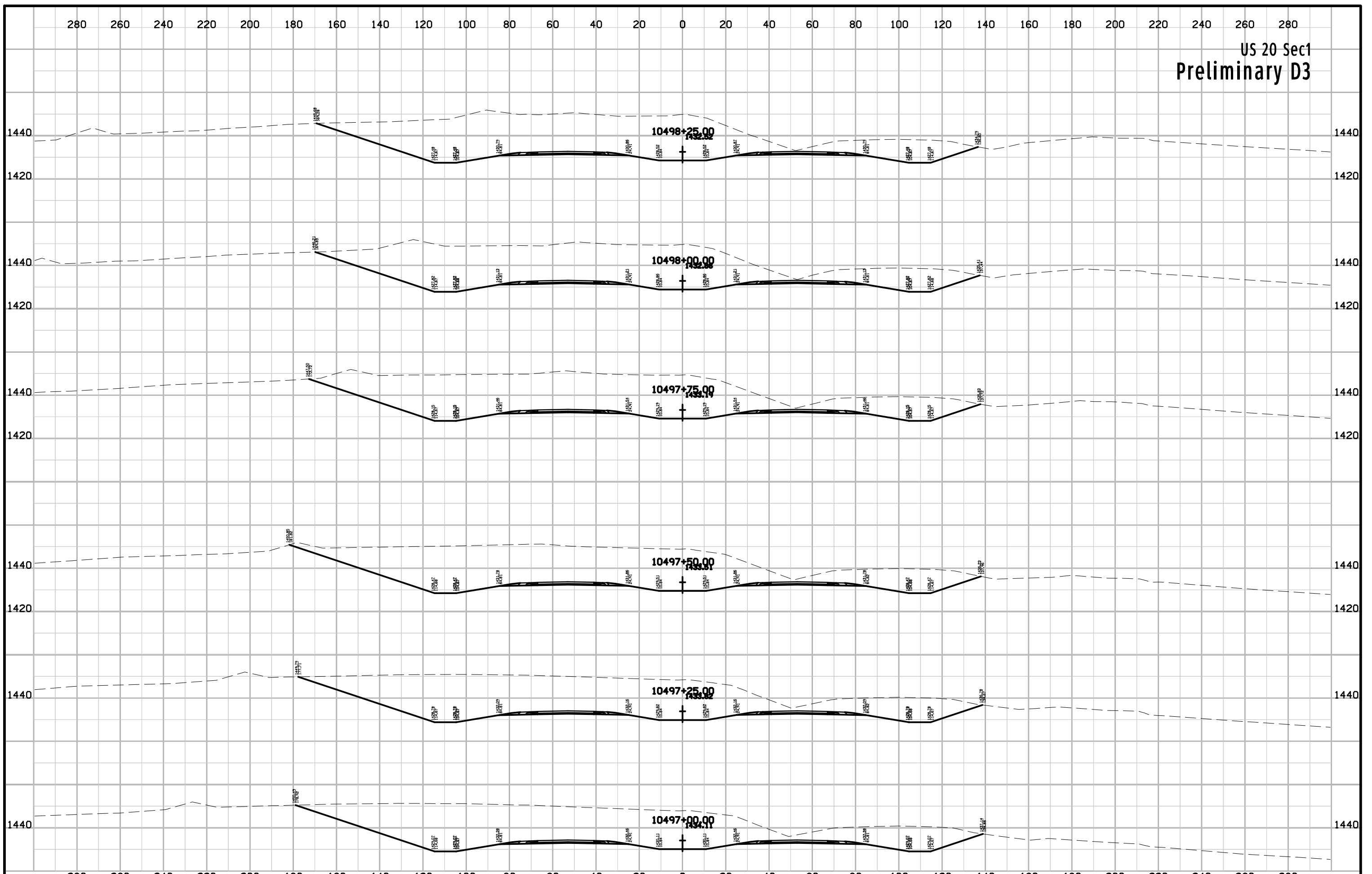
US 20 Sec1
Preliminary D3



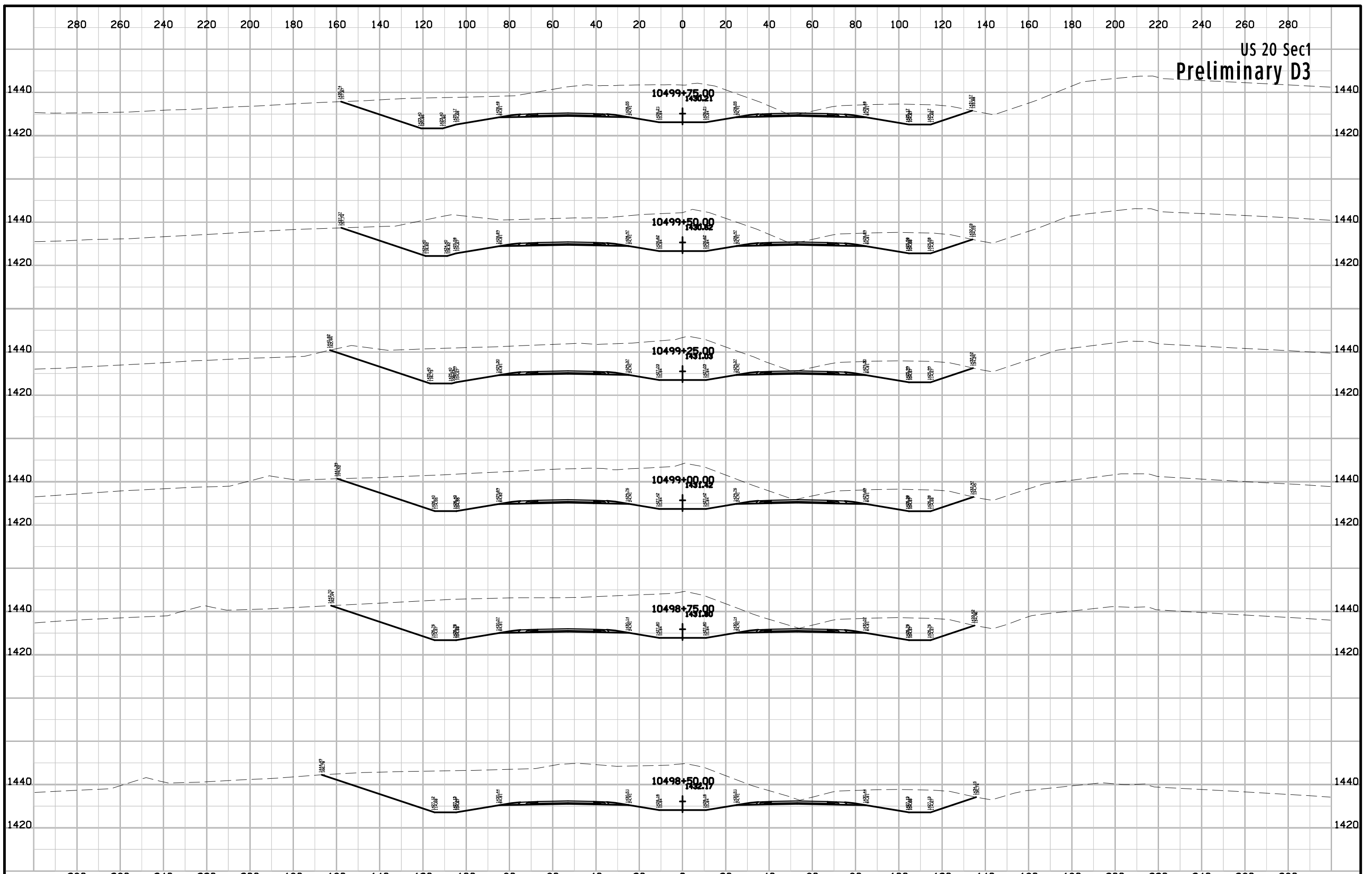
US 20 Sec1
Preliminary D3



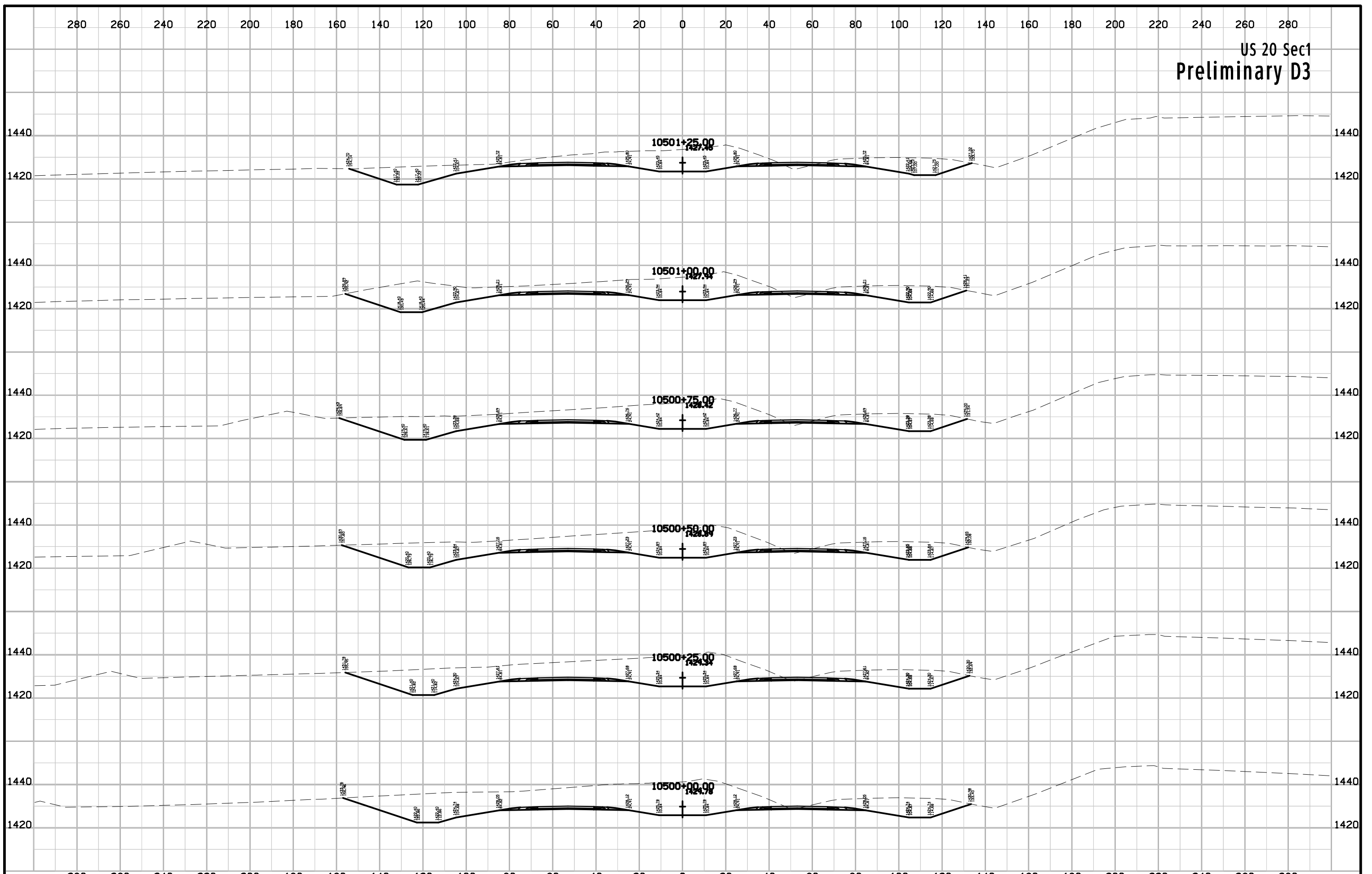
US 20 Sec1
Preliminary D3



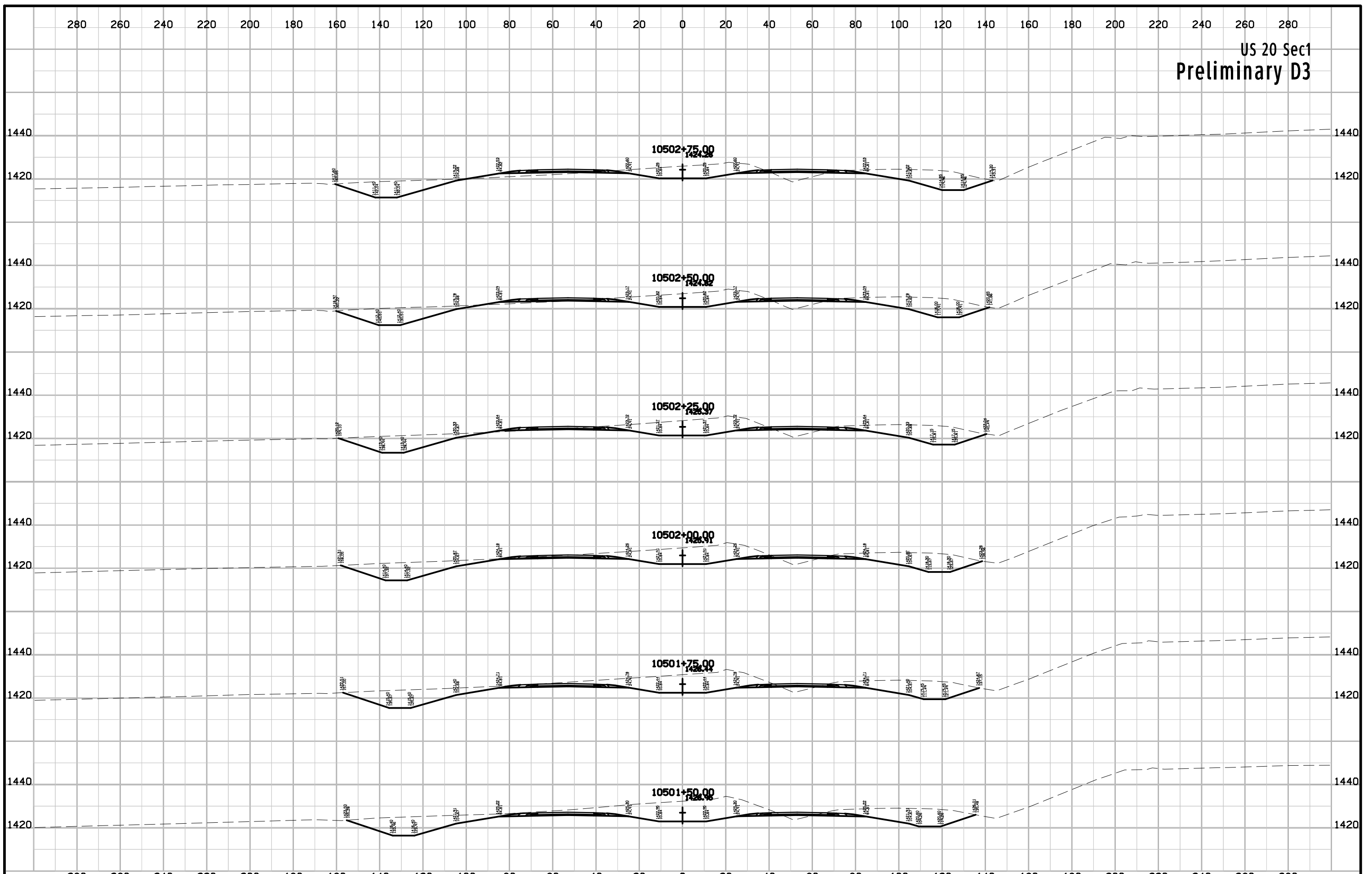
US 20 Sec1
Preliminary D3



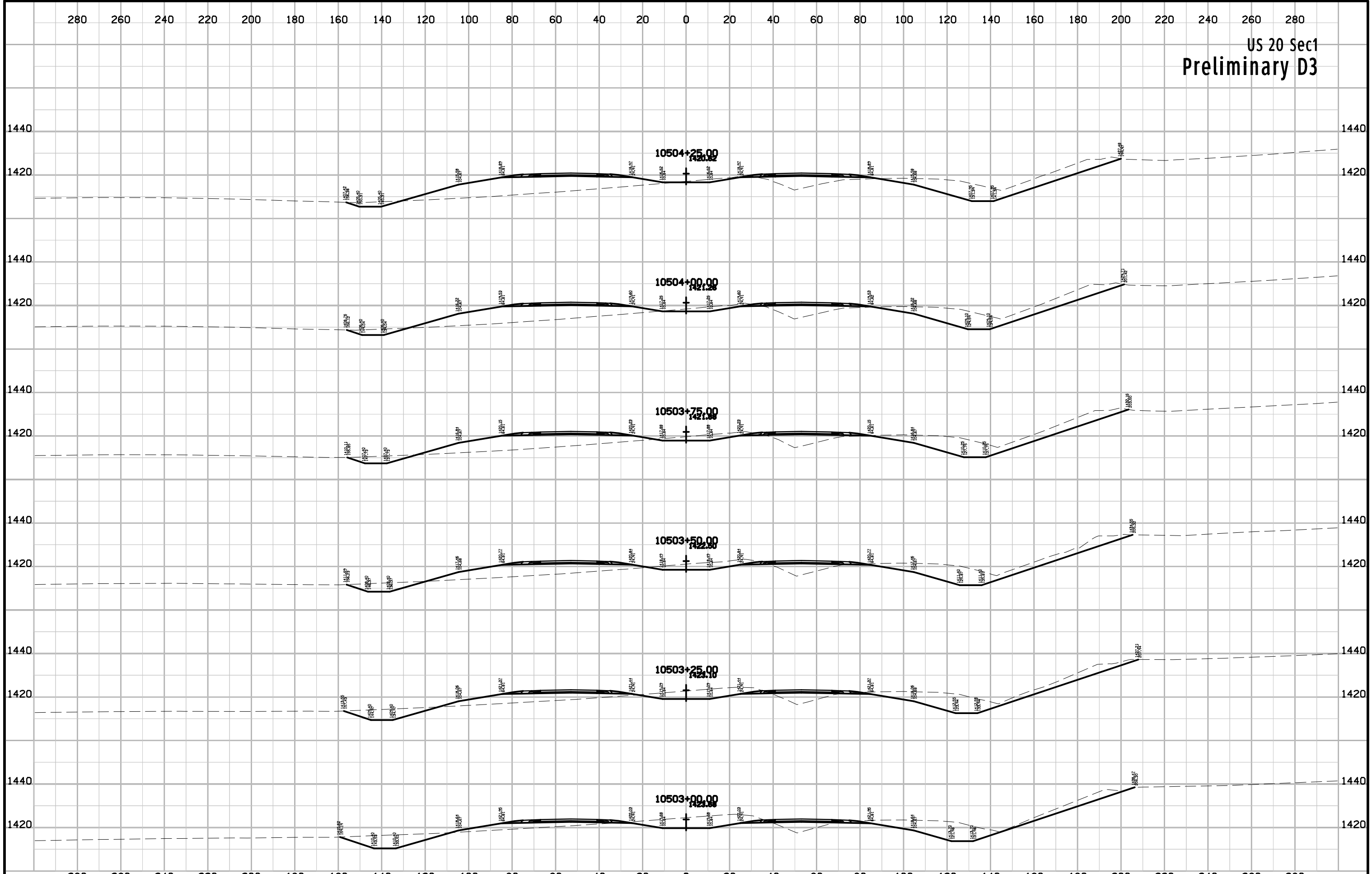
US 20 Sec1
Preliminary D3



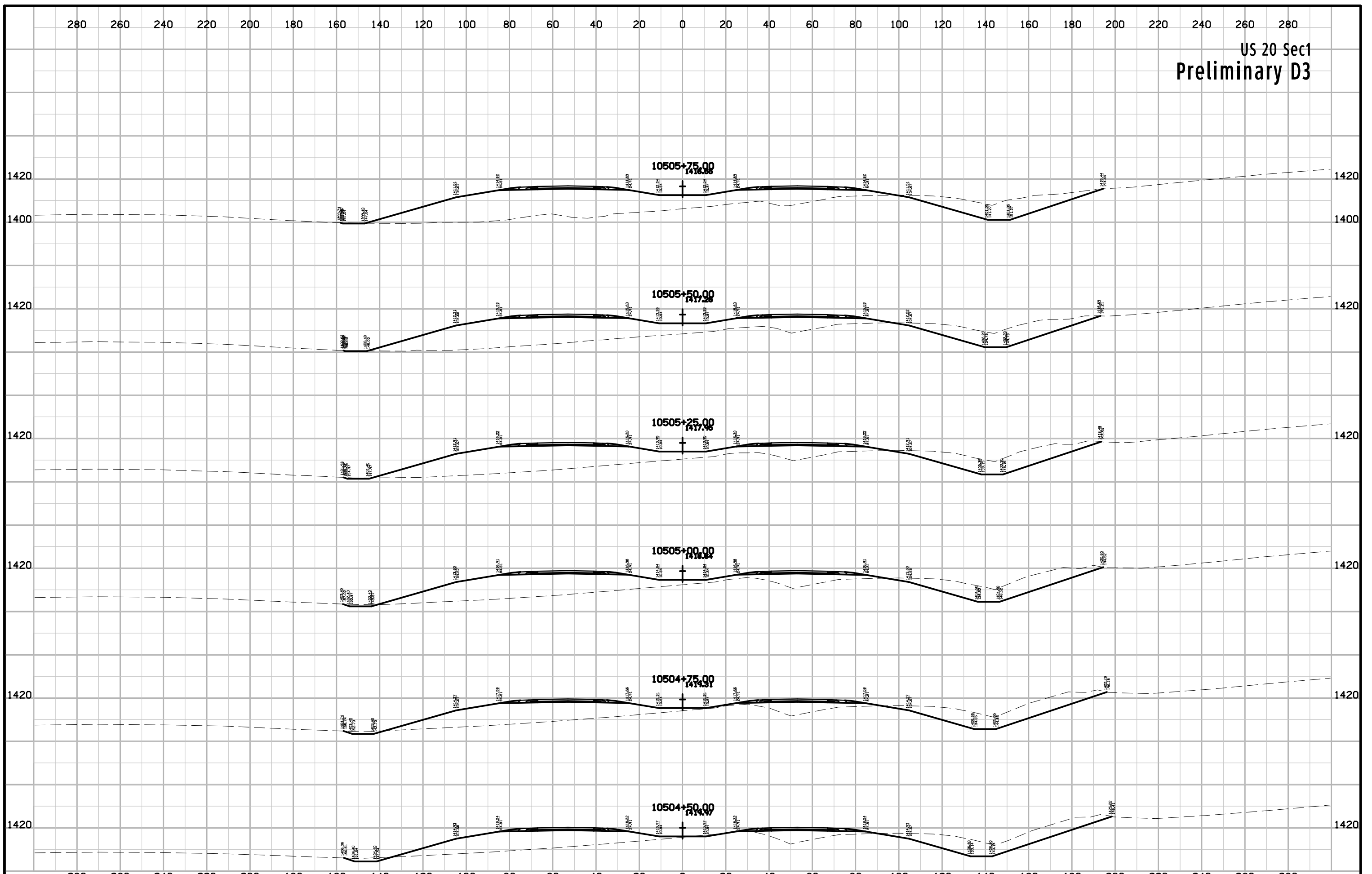
US 20 Sec1
Preliminary D3



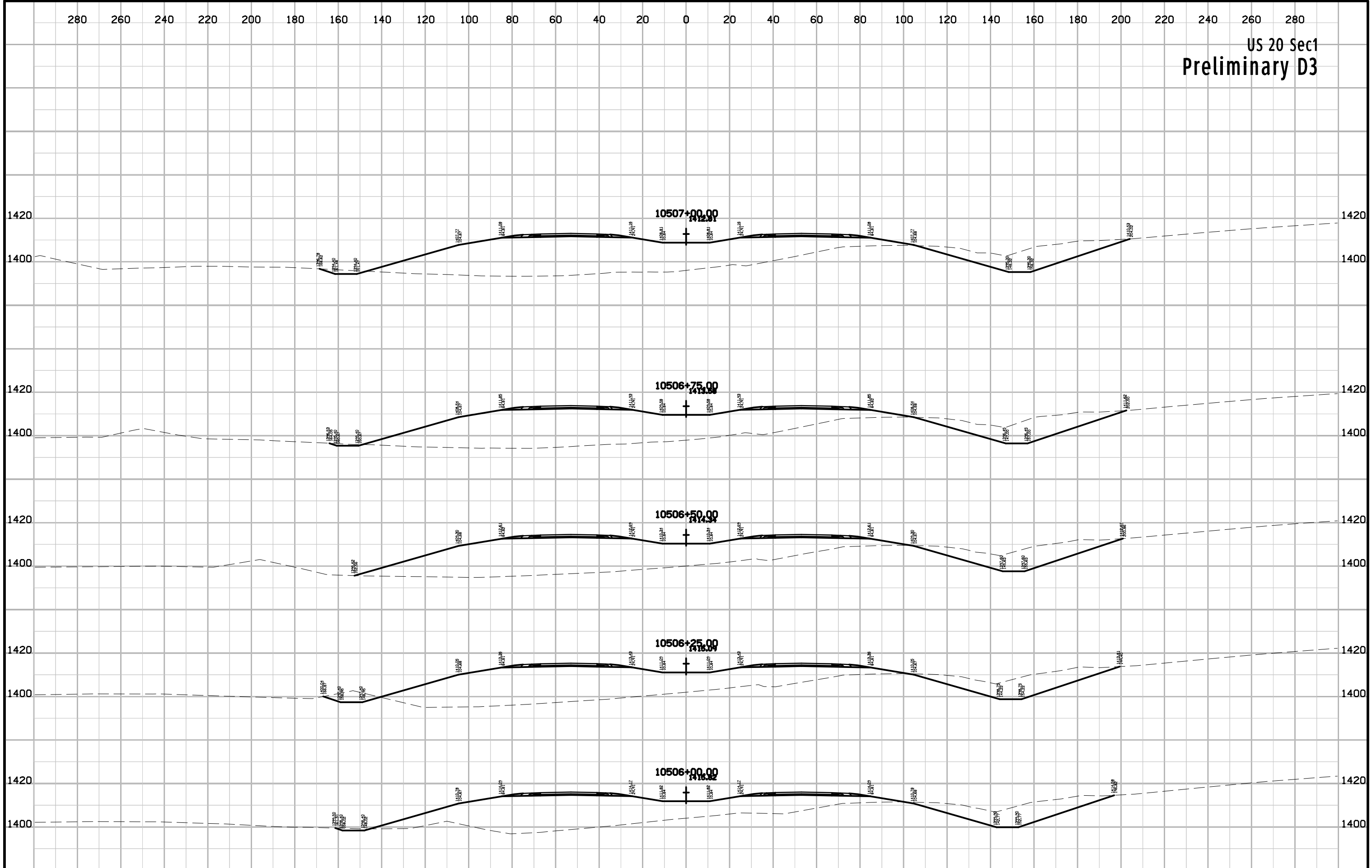
US 20 Sec1
Preliminary D3



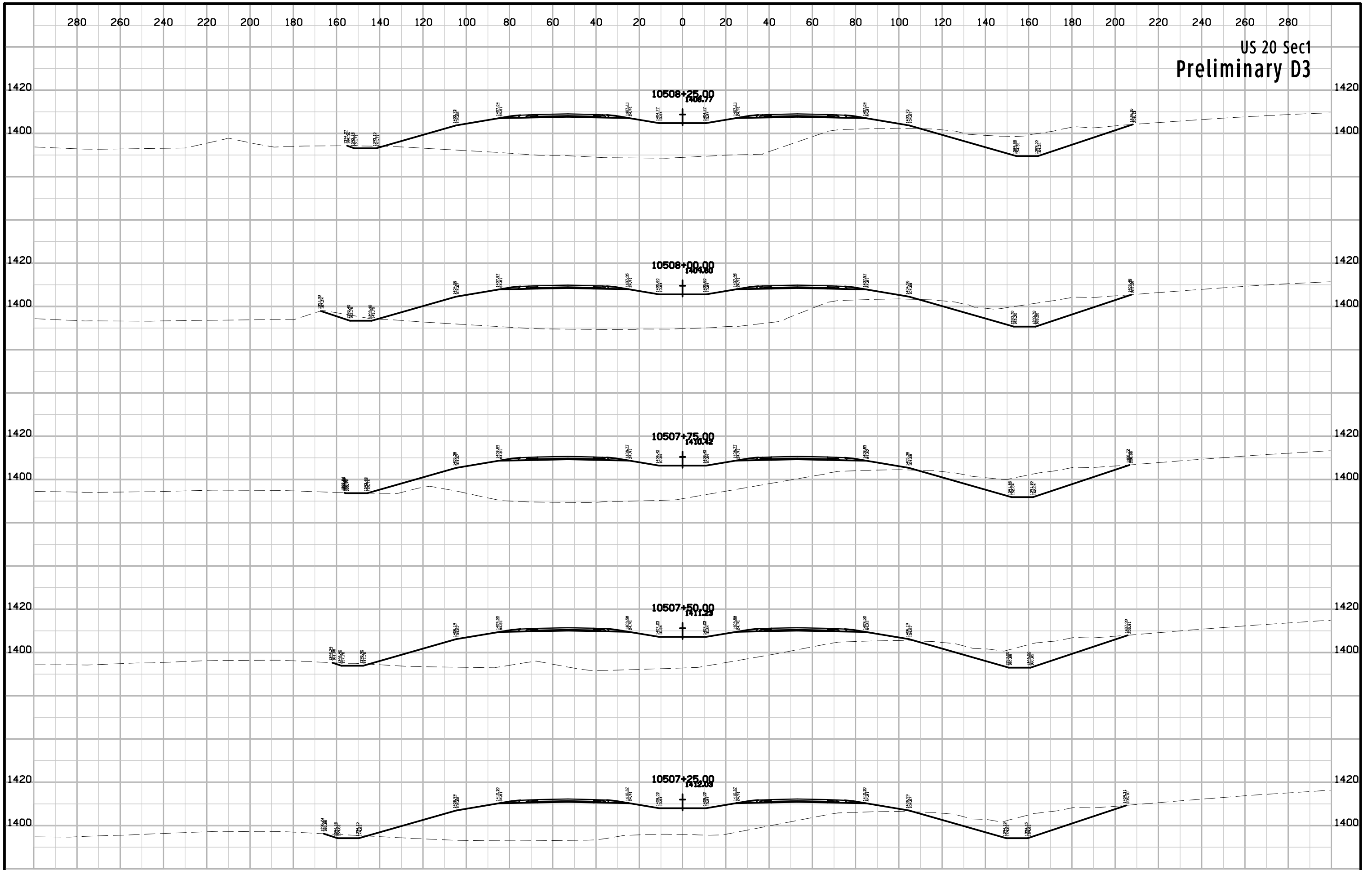
US 20 Sec1
Preliminary D3



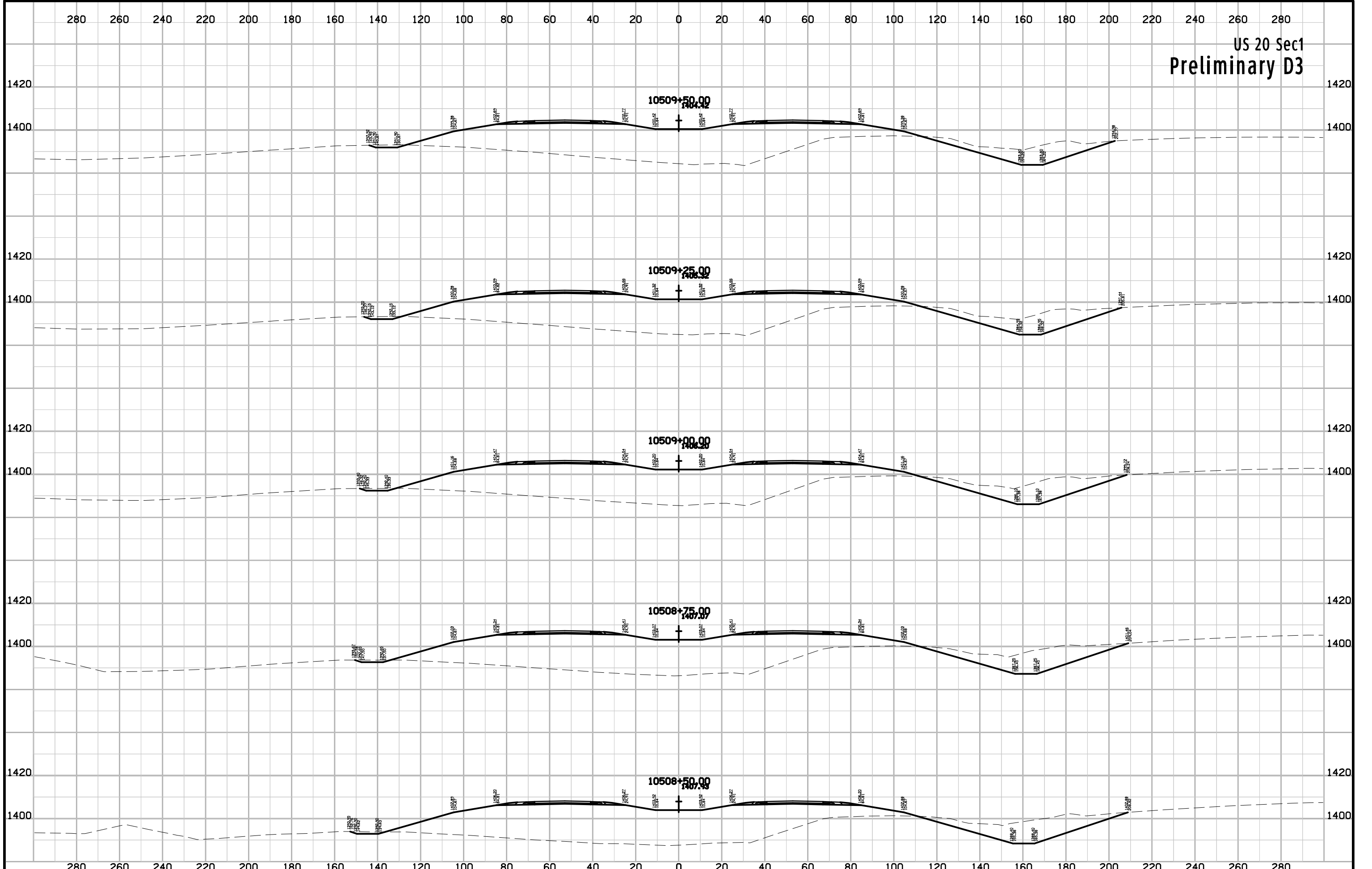
US 20 Sec1
Preliminary D3



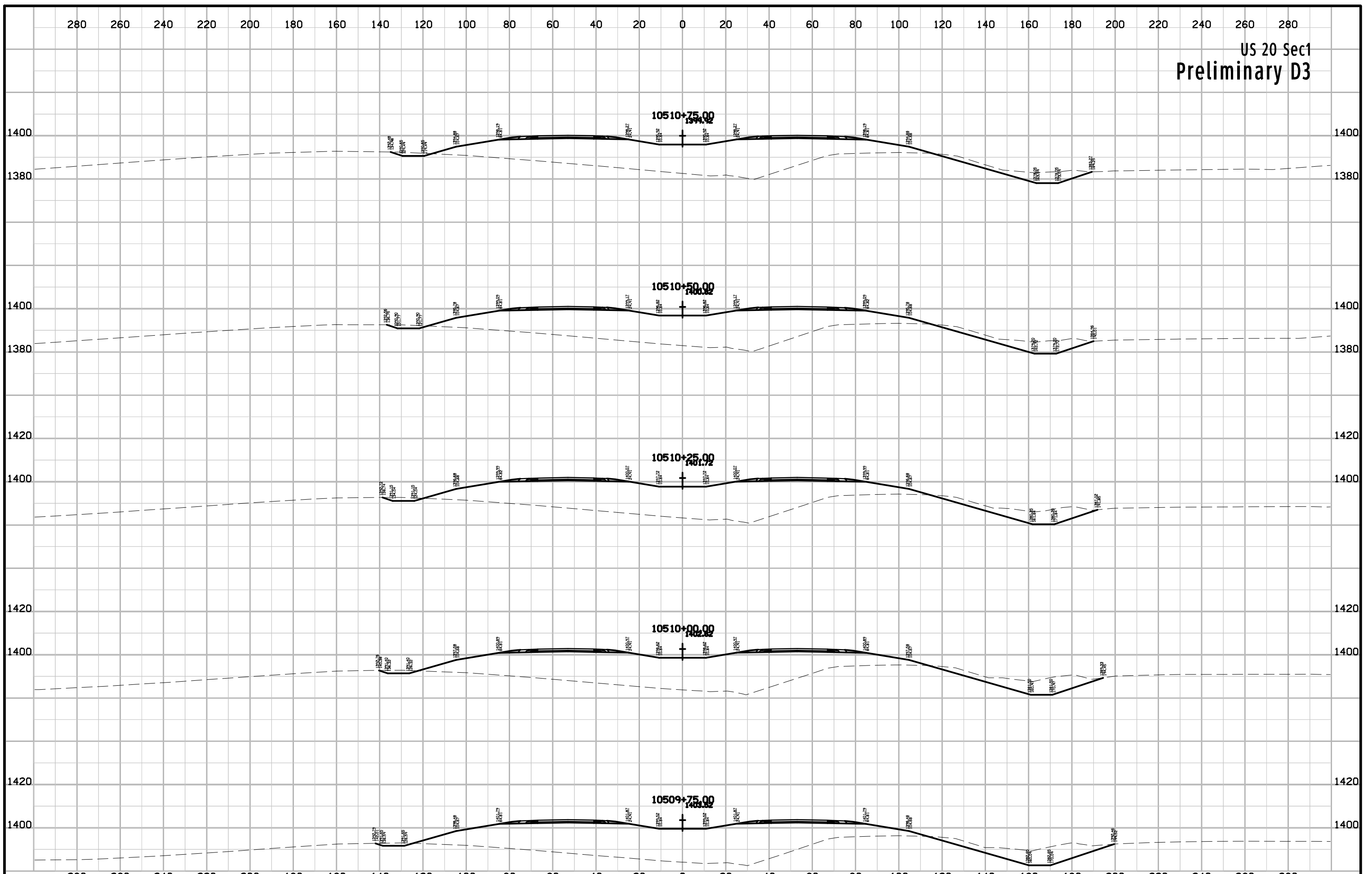
US 20 Sec1
Preliminary D3



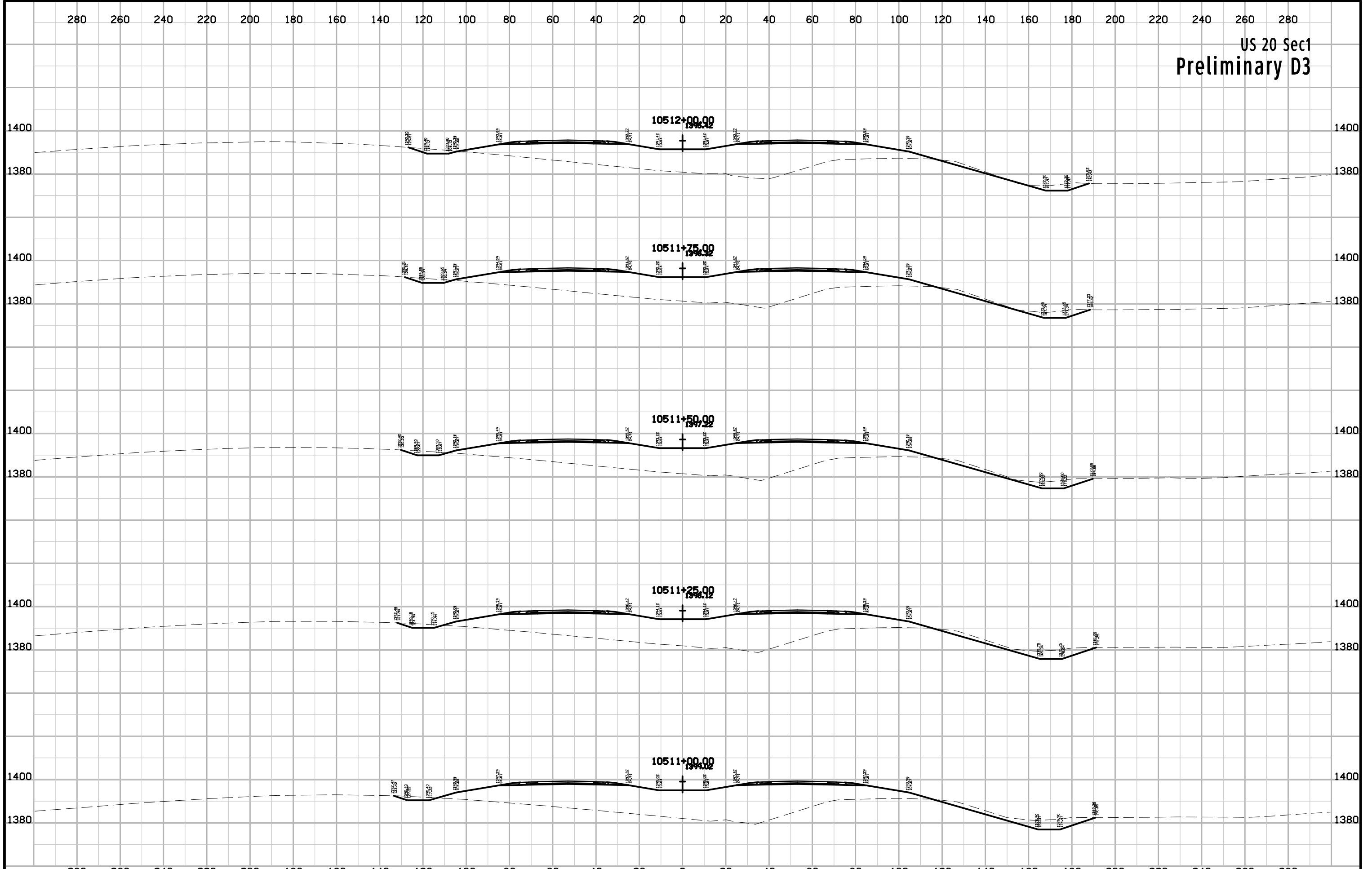
US 20 Sec1
Preliminary D3



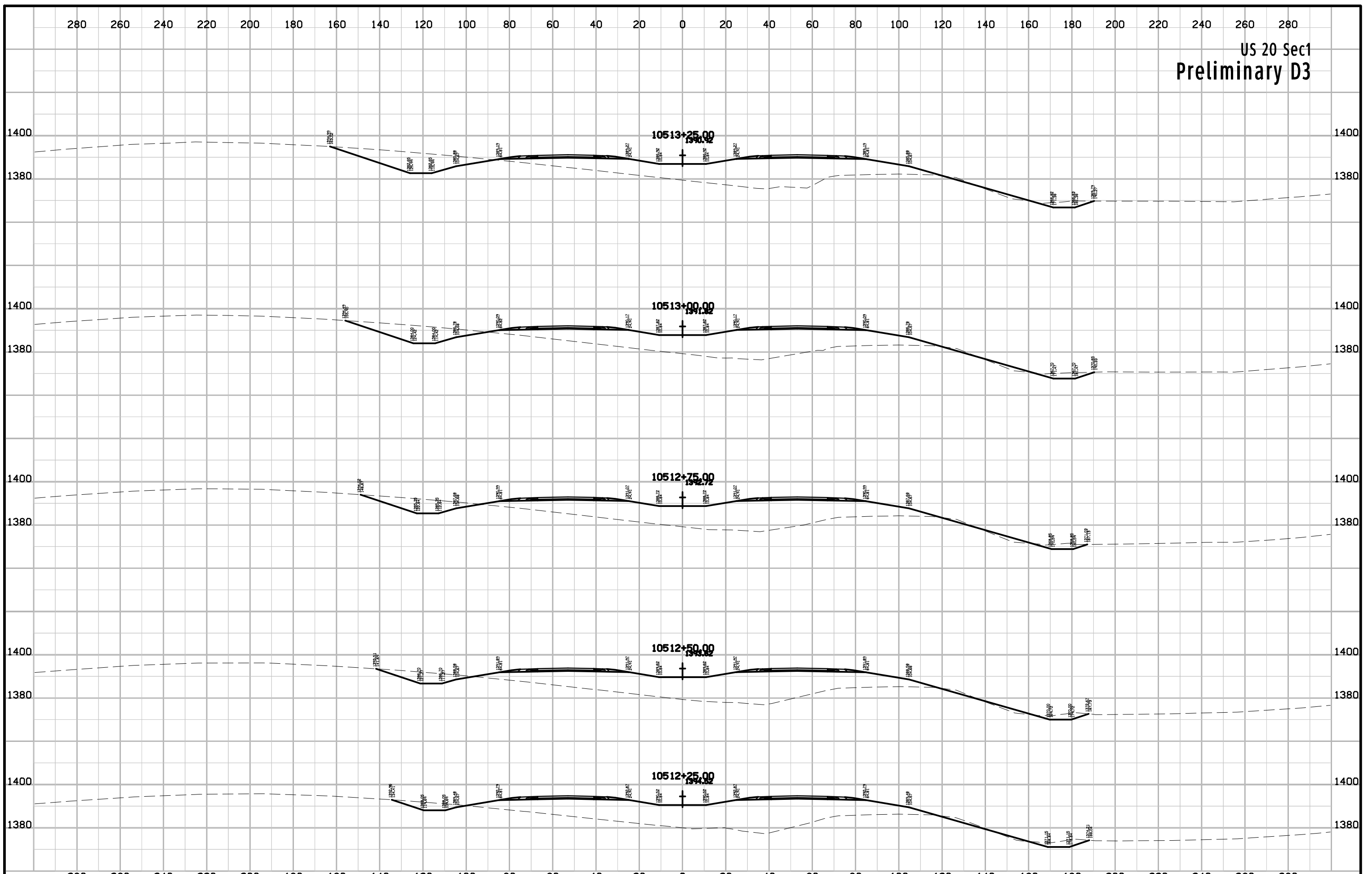
US 20 Sec1
Preliminary D3



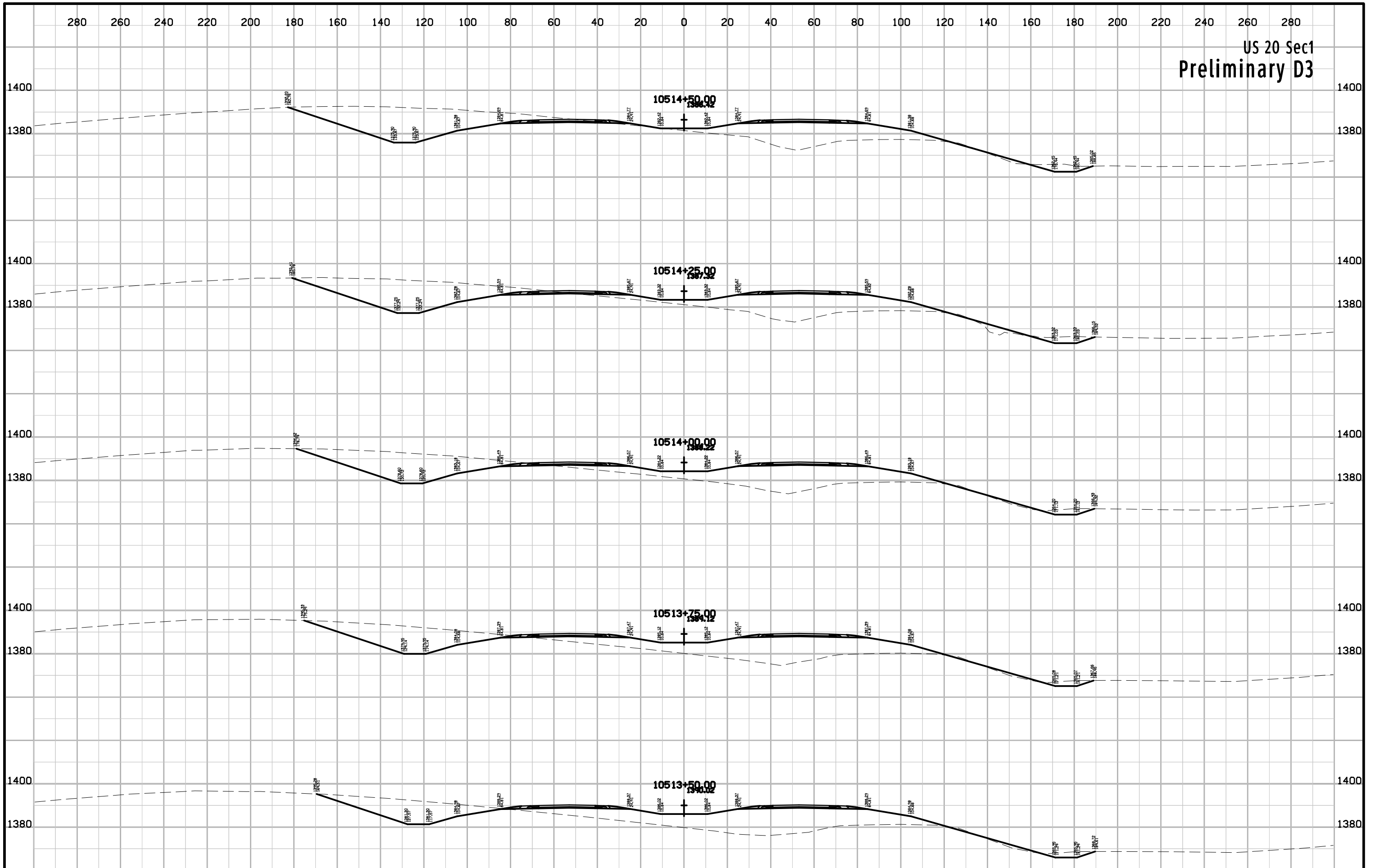
US 20 Sec1
Preliminary D3



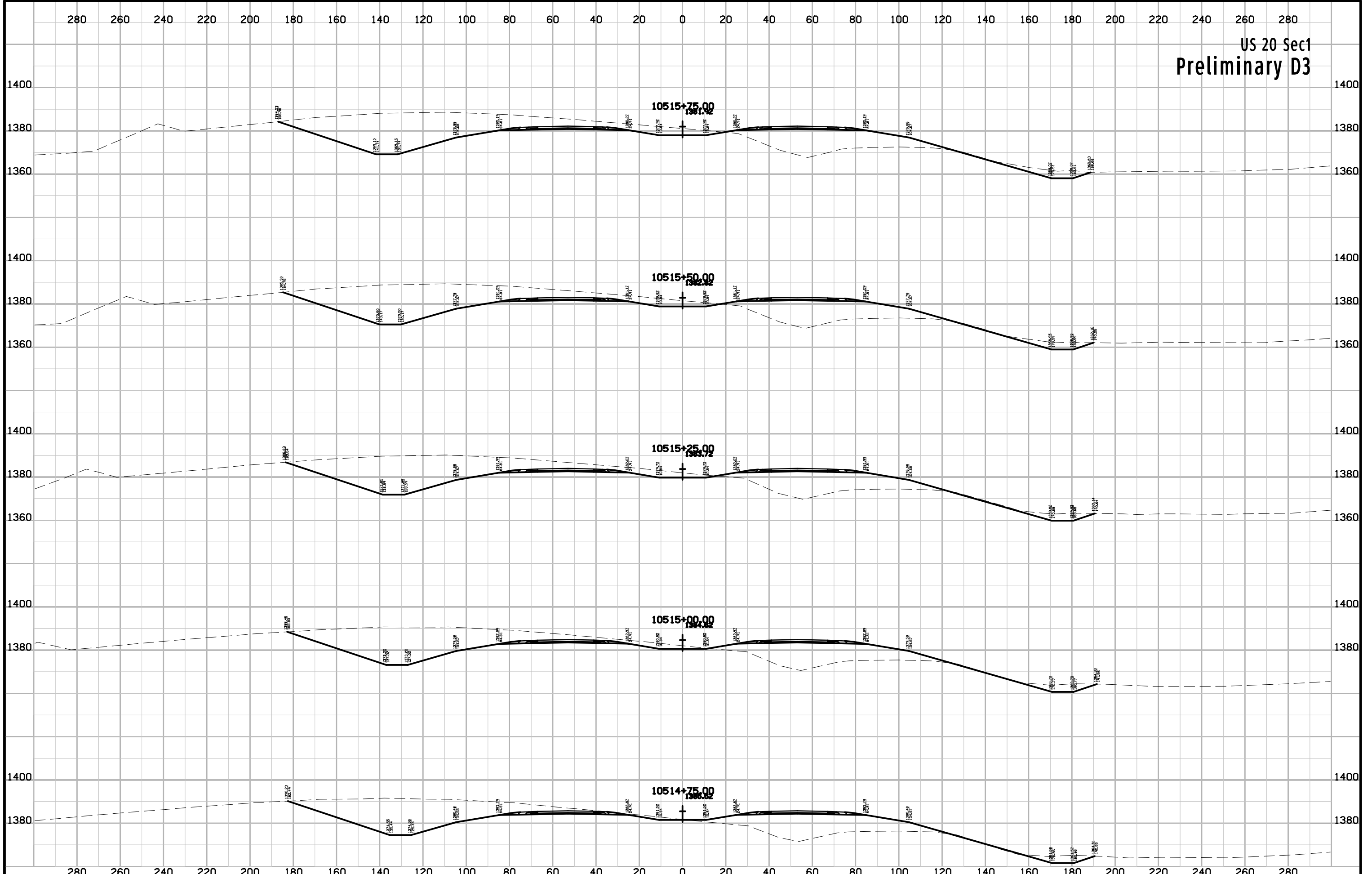
US 20 Sec1
Preliminary D3



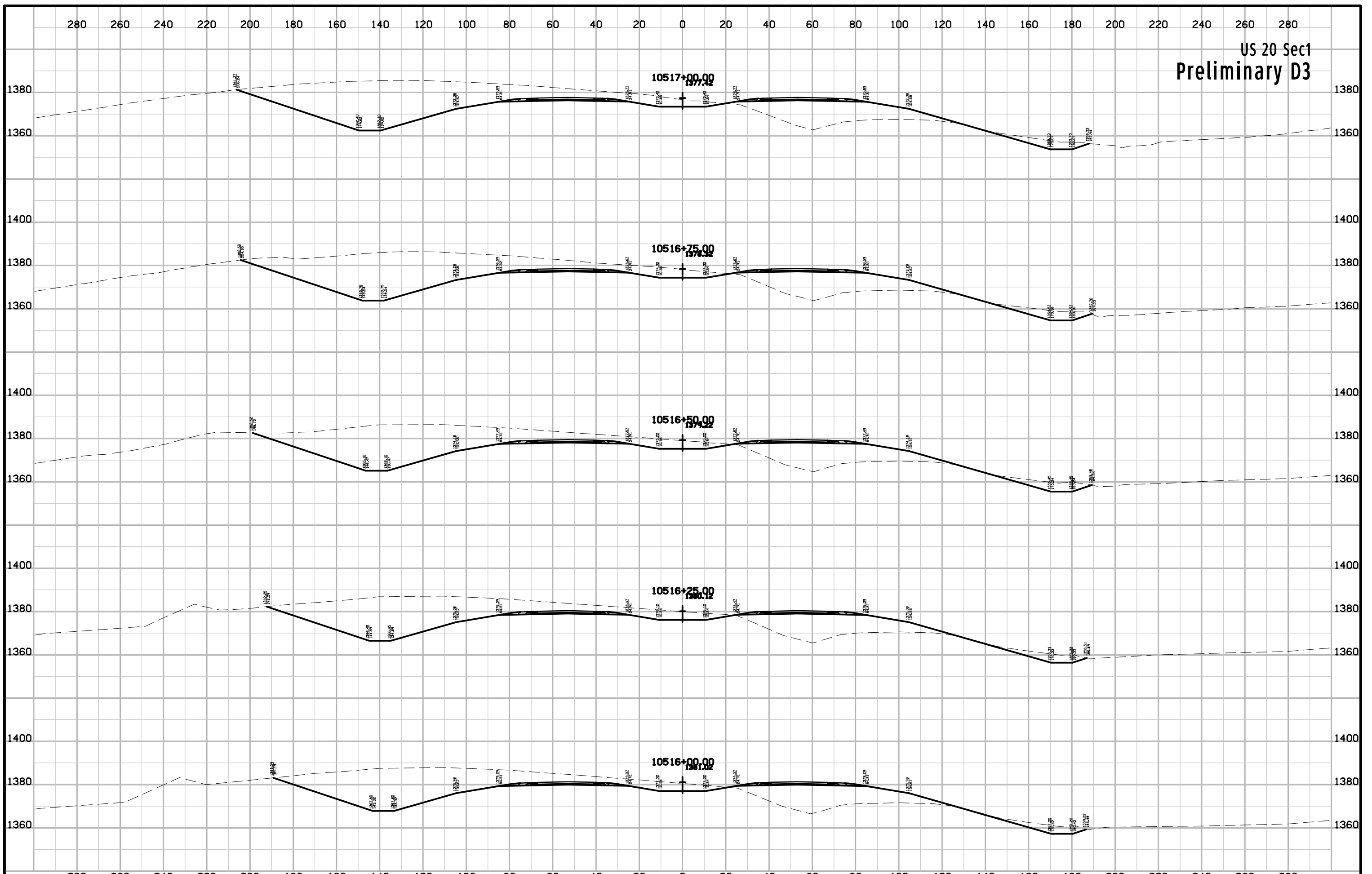
US 20 Sec1
Preliminary D3



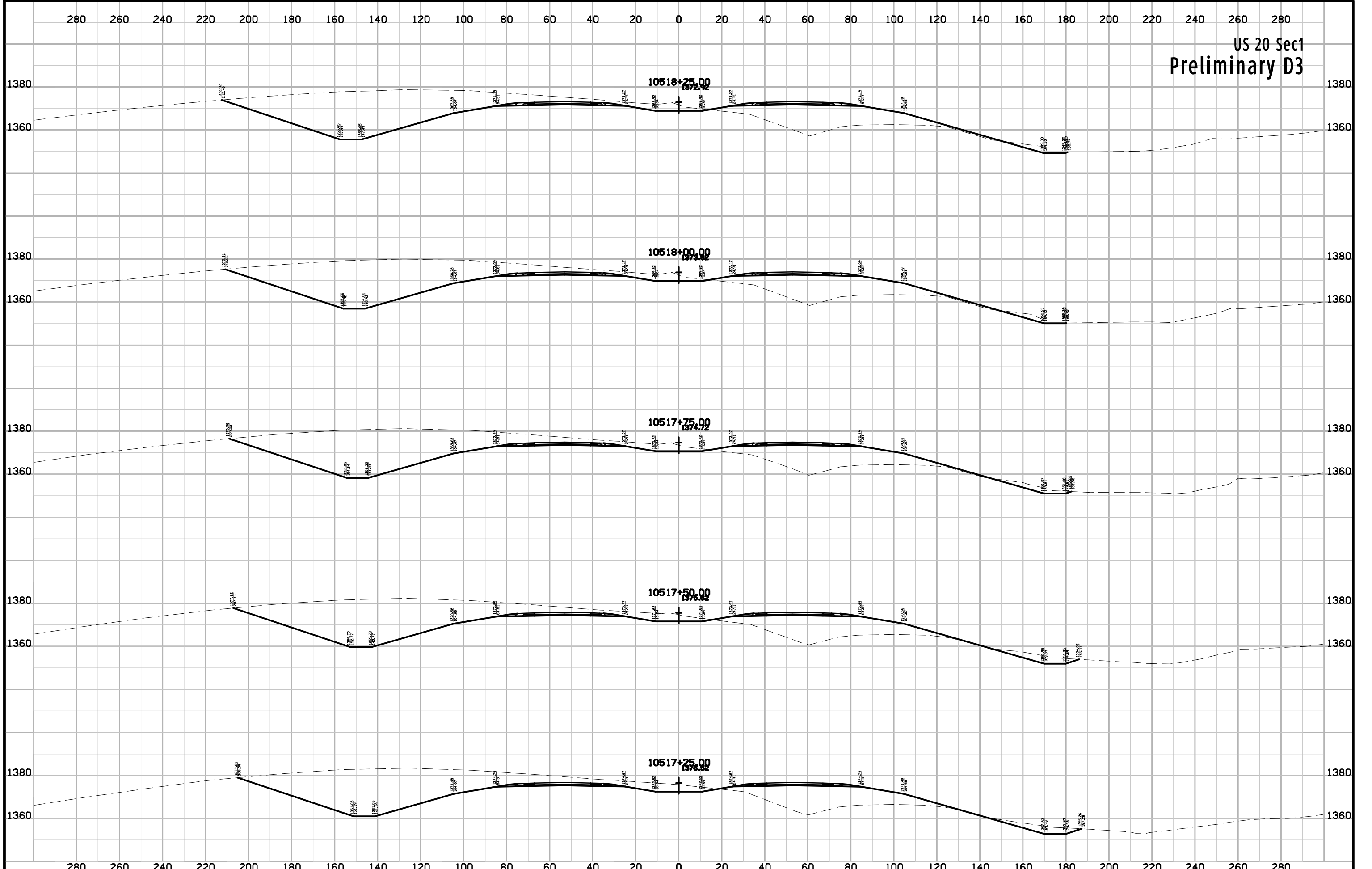
US 20 Sec1
Preliminary D3



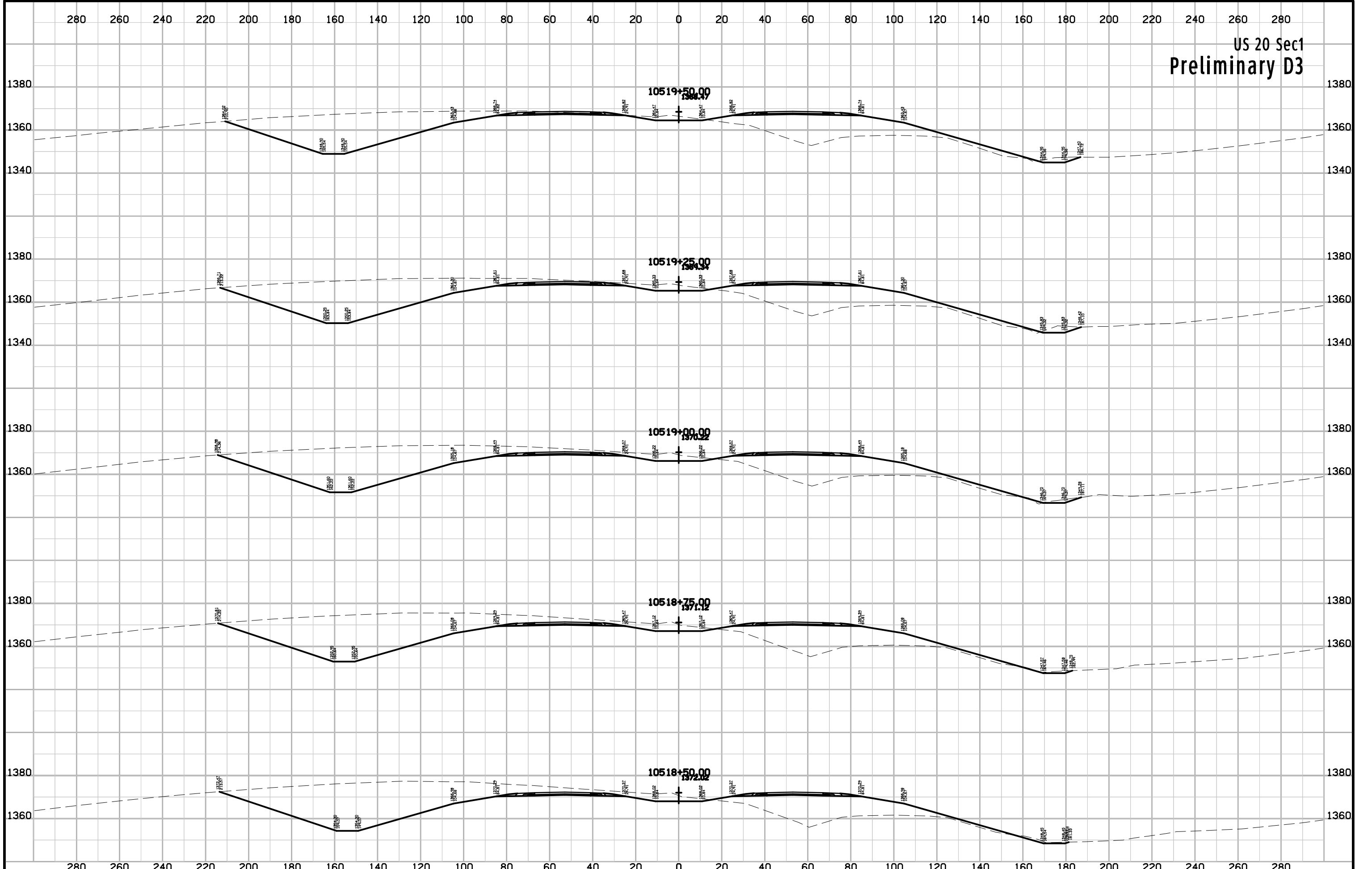
US 20 Sec1
Preliminary D3



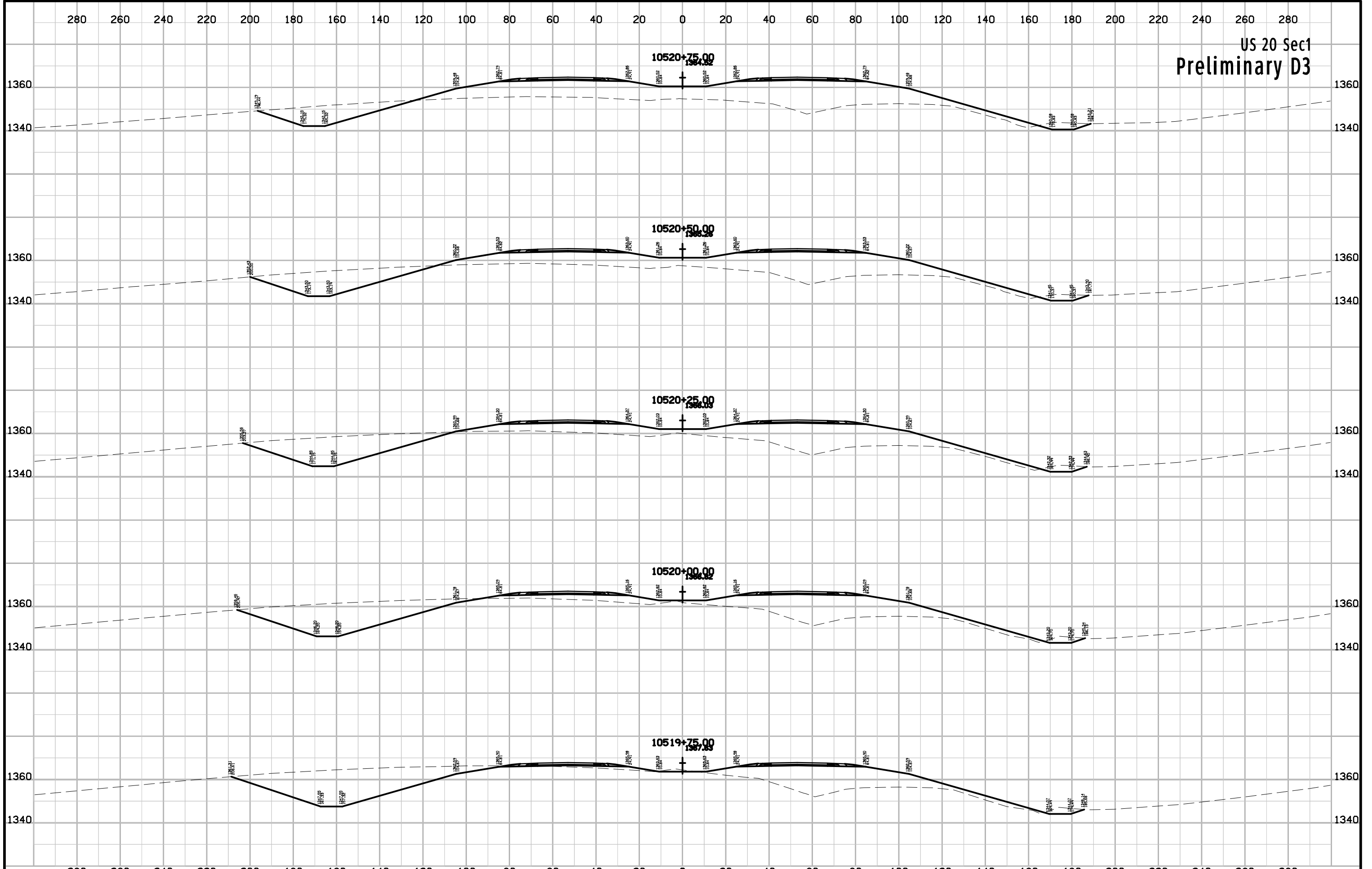
US 20 Sec1
Preliminary D3



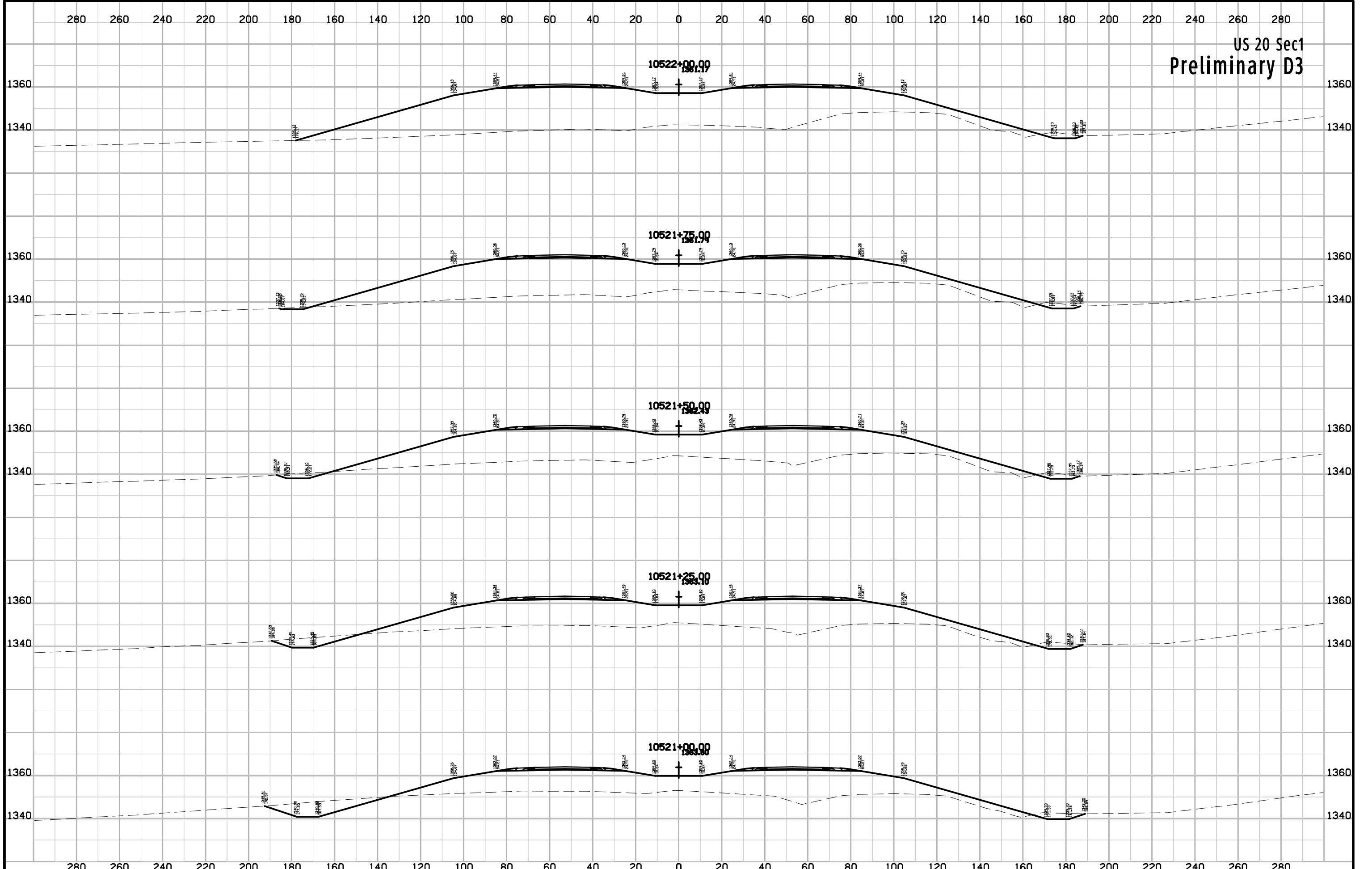
US 20 Sec1
Preliminary D3



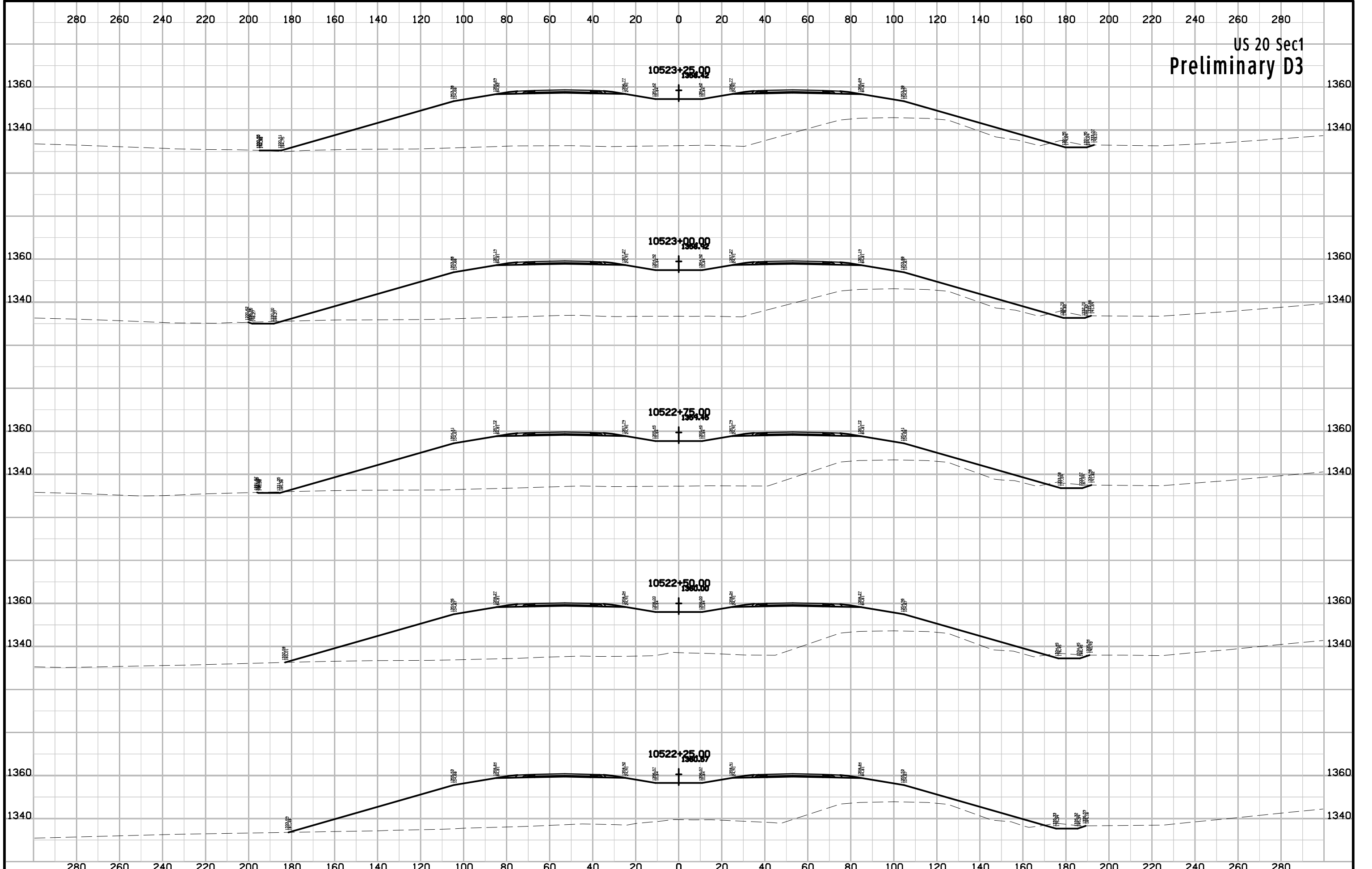
US 20 Sec1
Preliminary D3



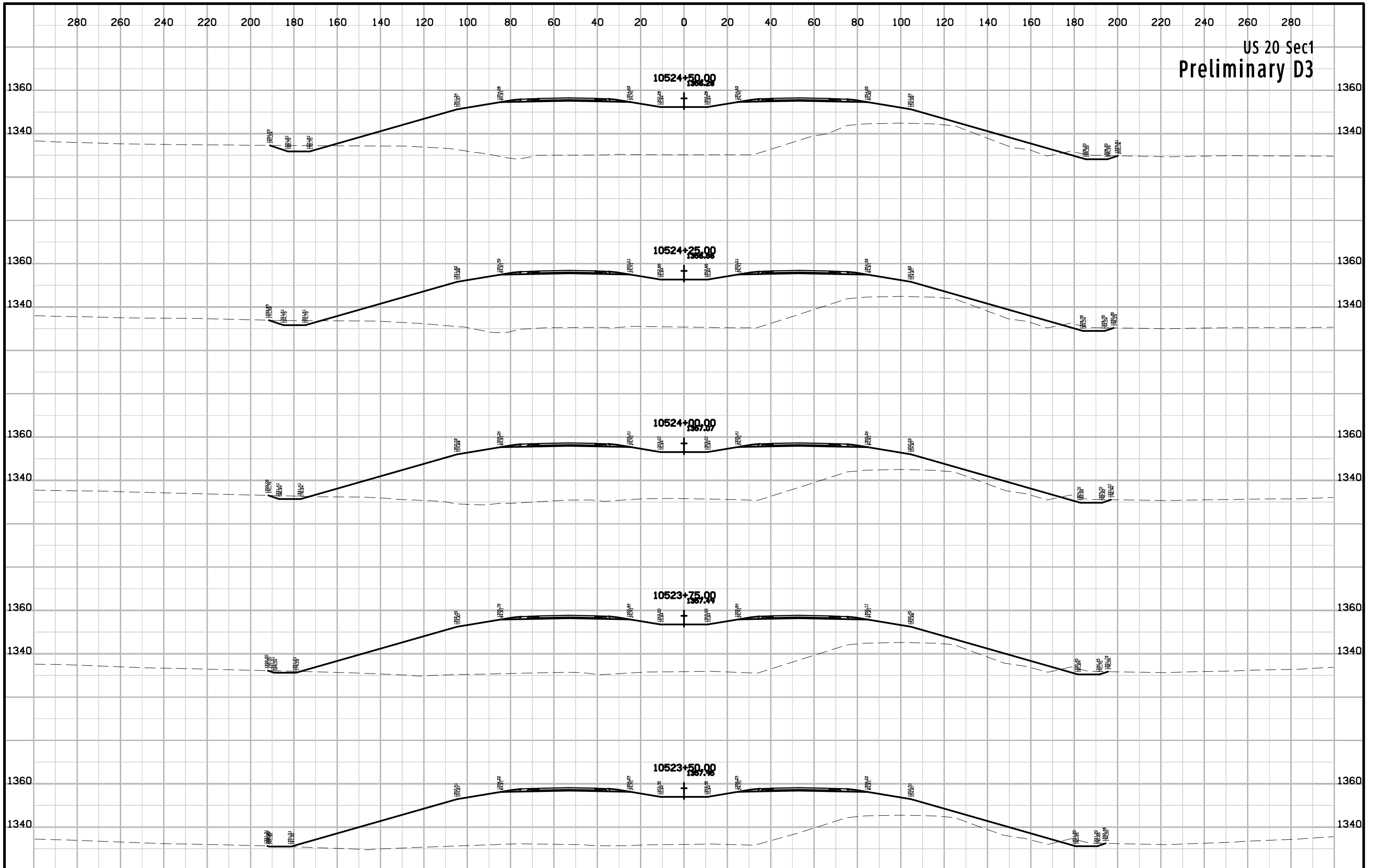
US 20 Sec1
Preliminary D3



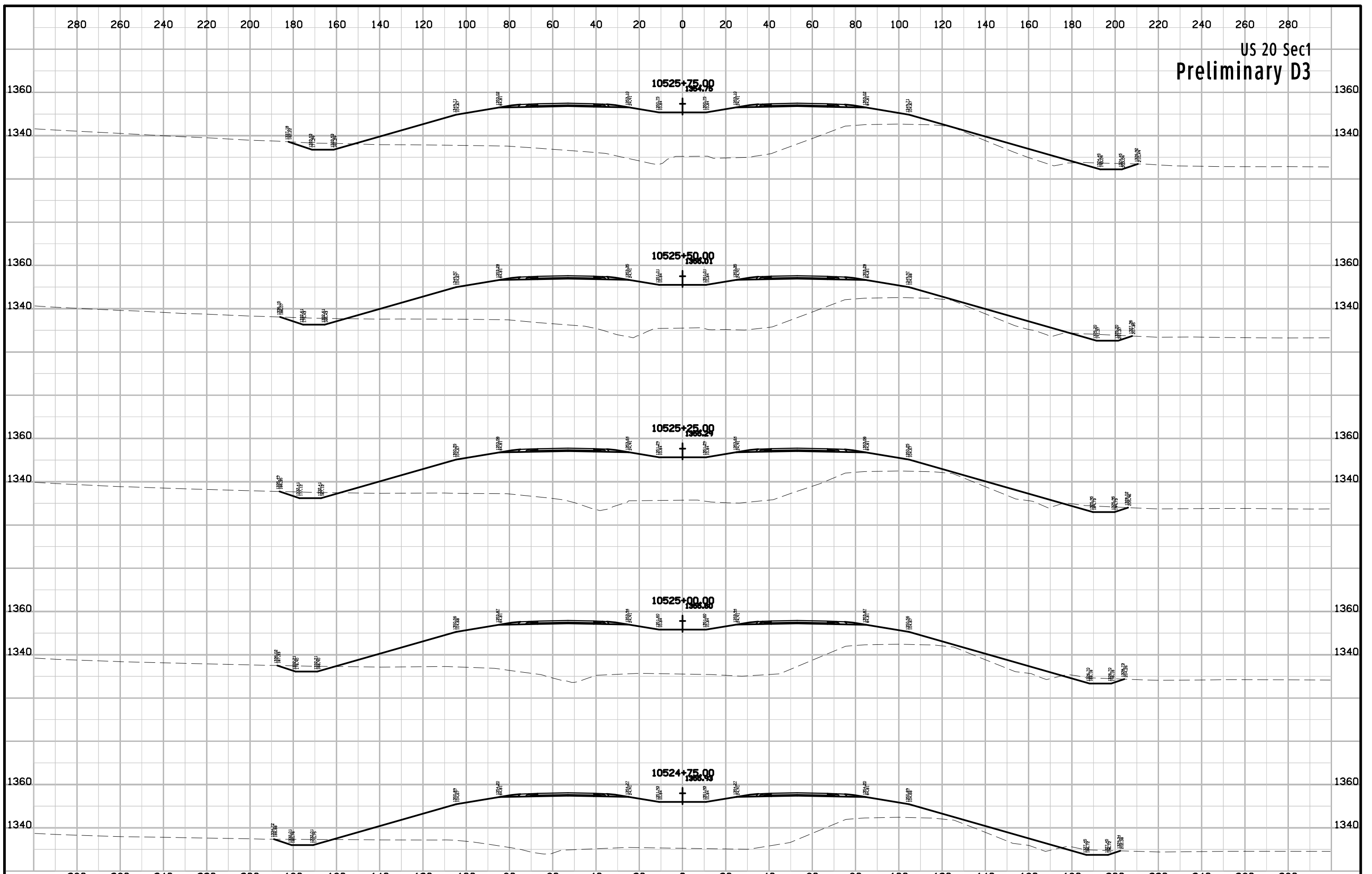
US 20 Sec1
Preliminary D3



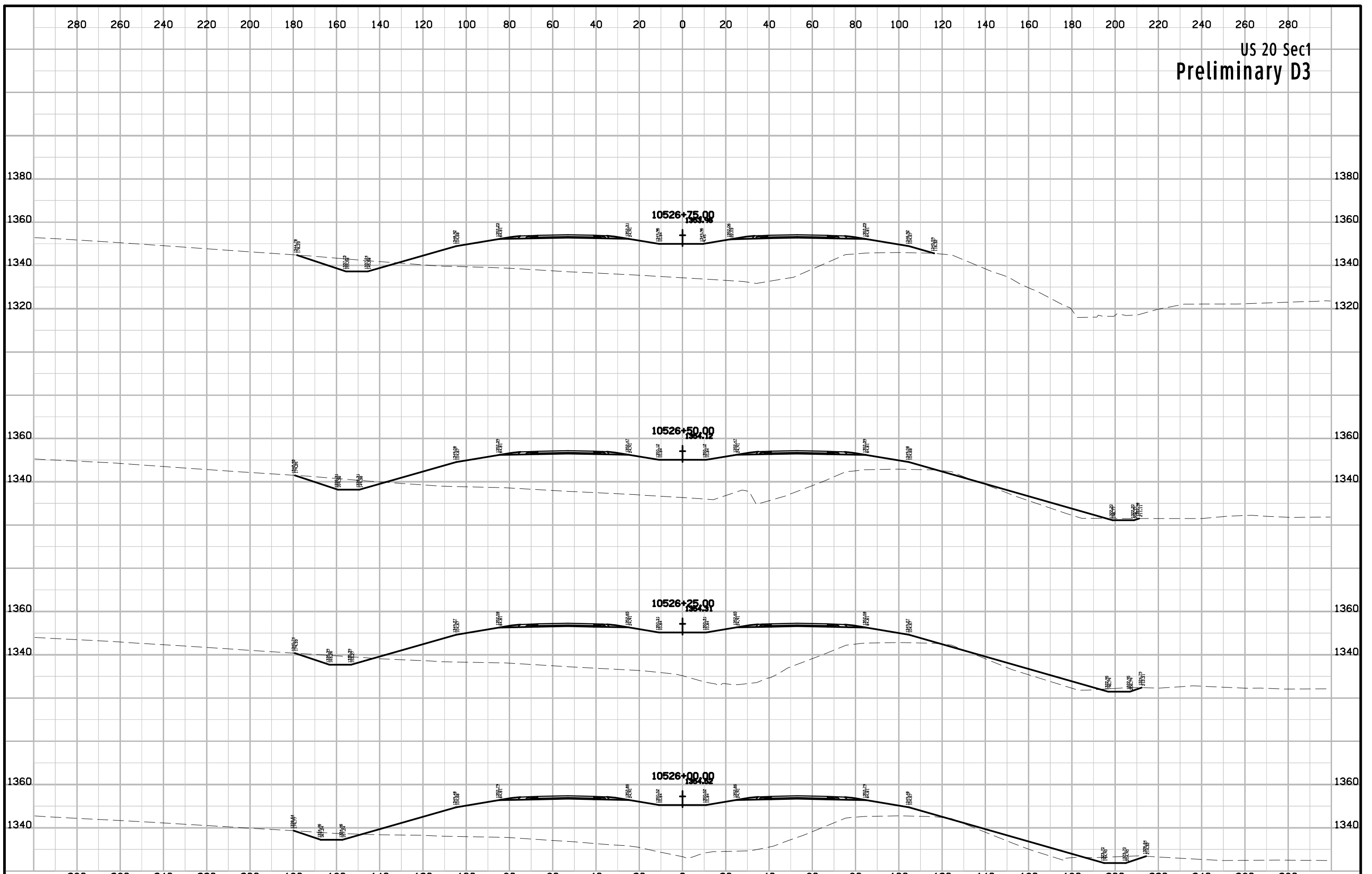
US 20 Sec1
Preliminary D3



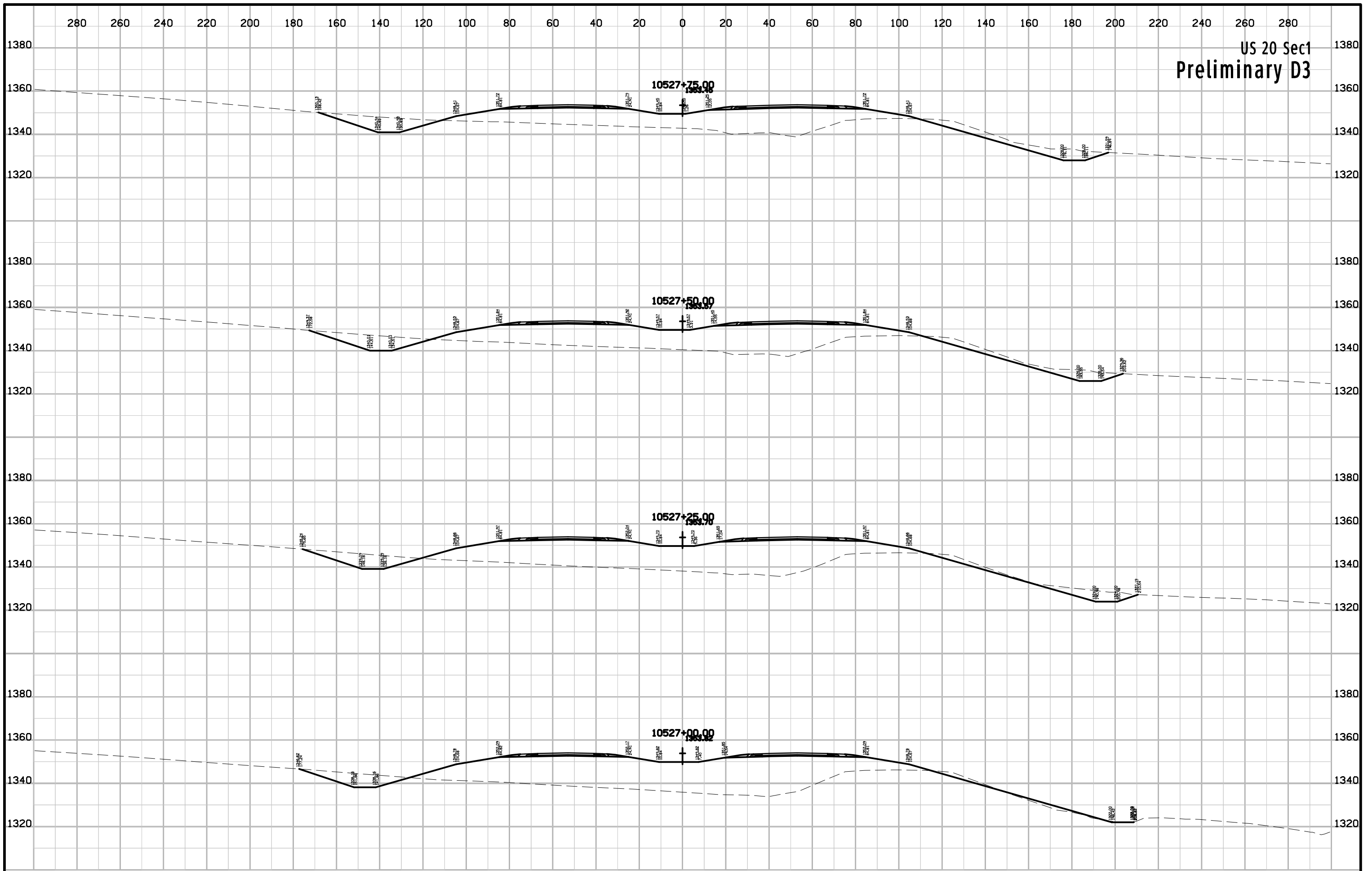
US 20 Sec1
Preliminary D3



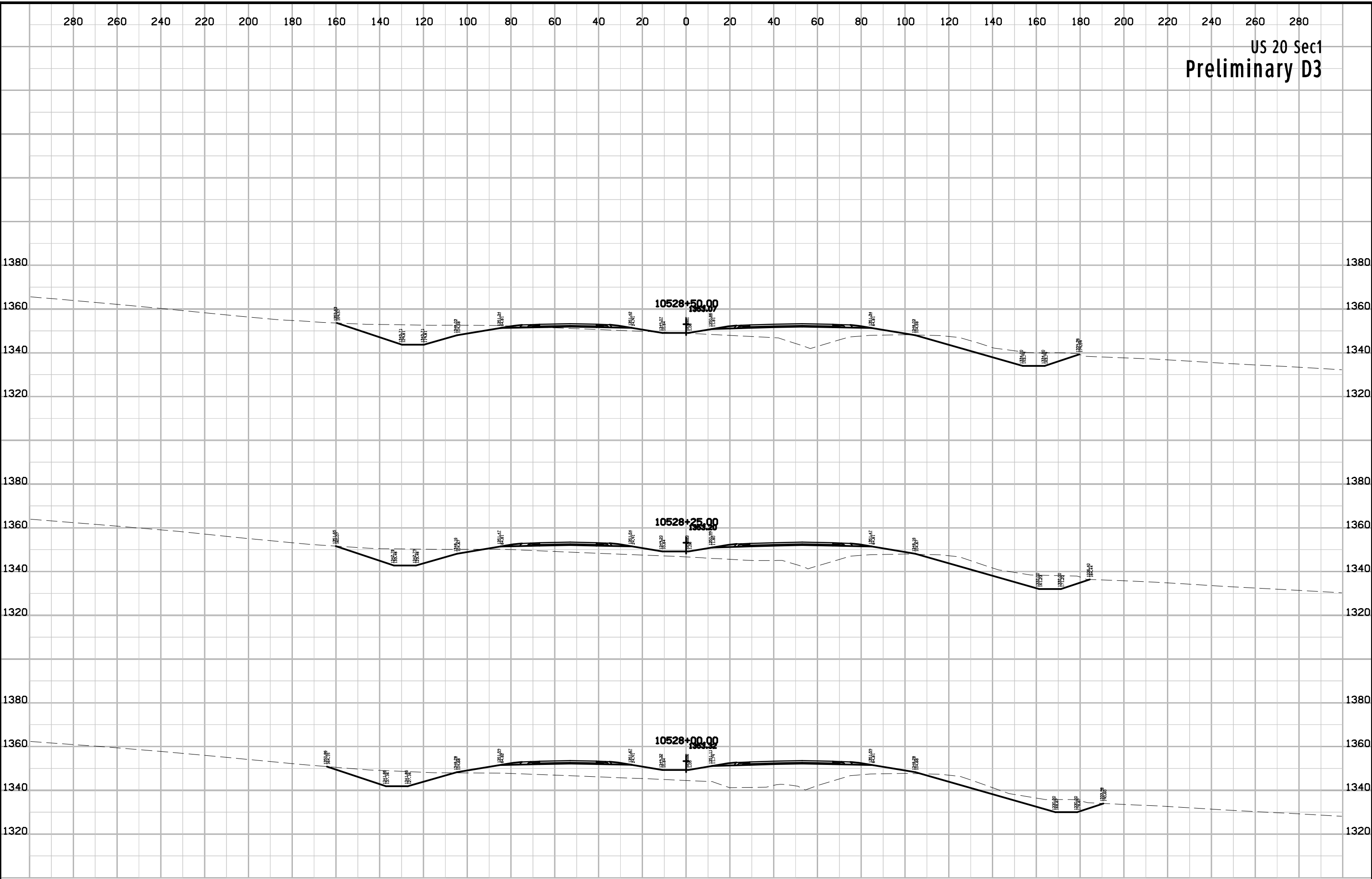
US 20 Sec1
Preliminary D3



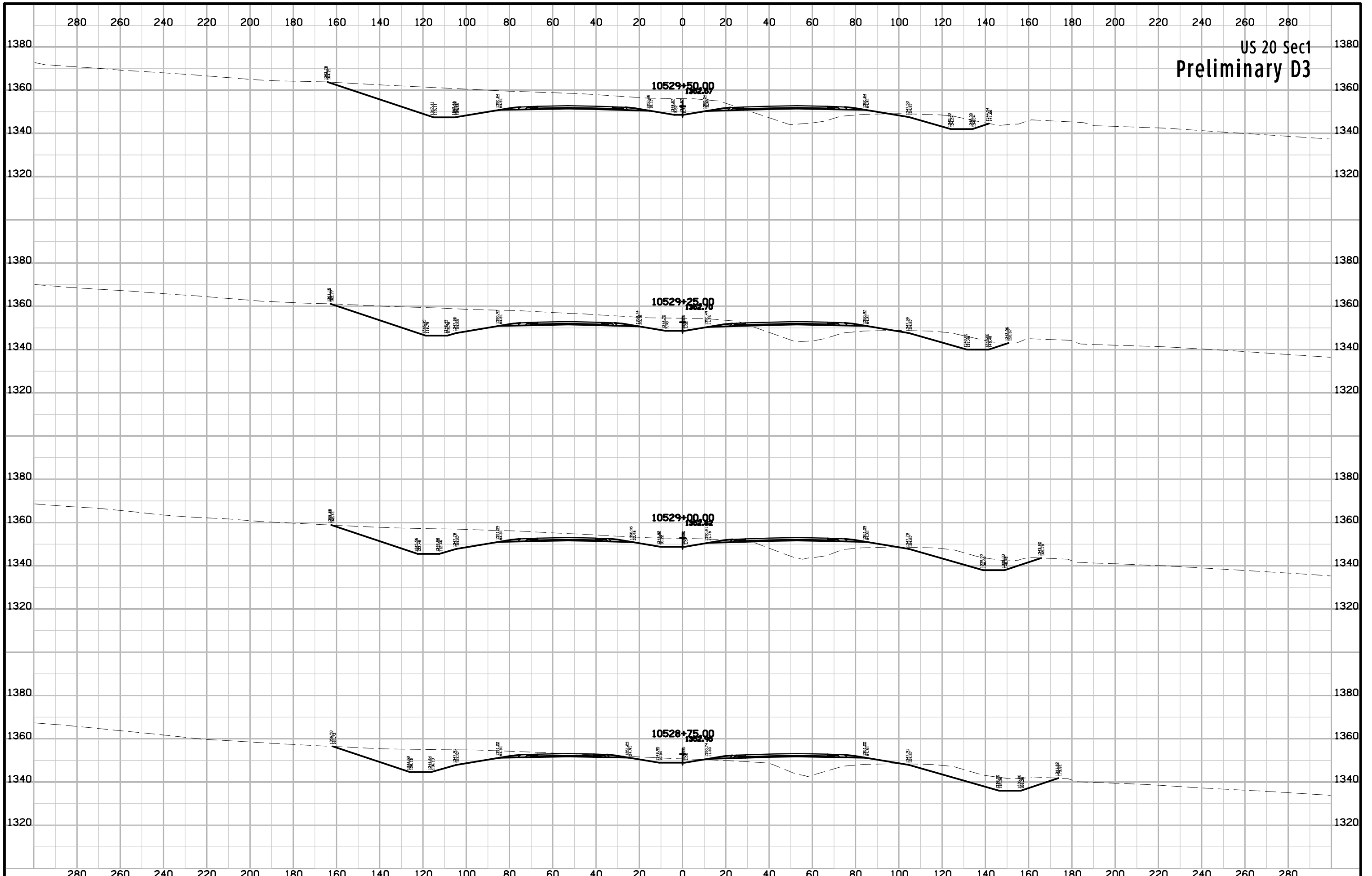
US 20 Sec1
Preliminary D3



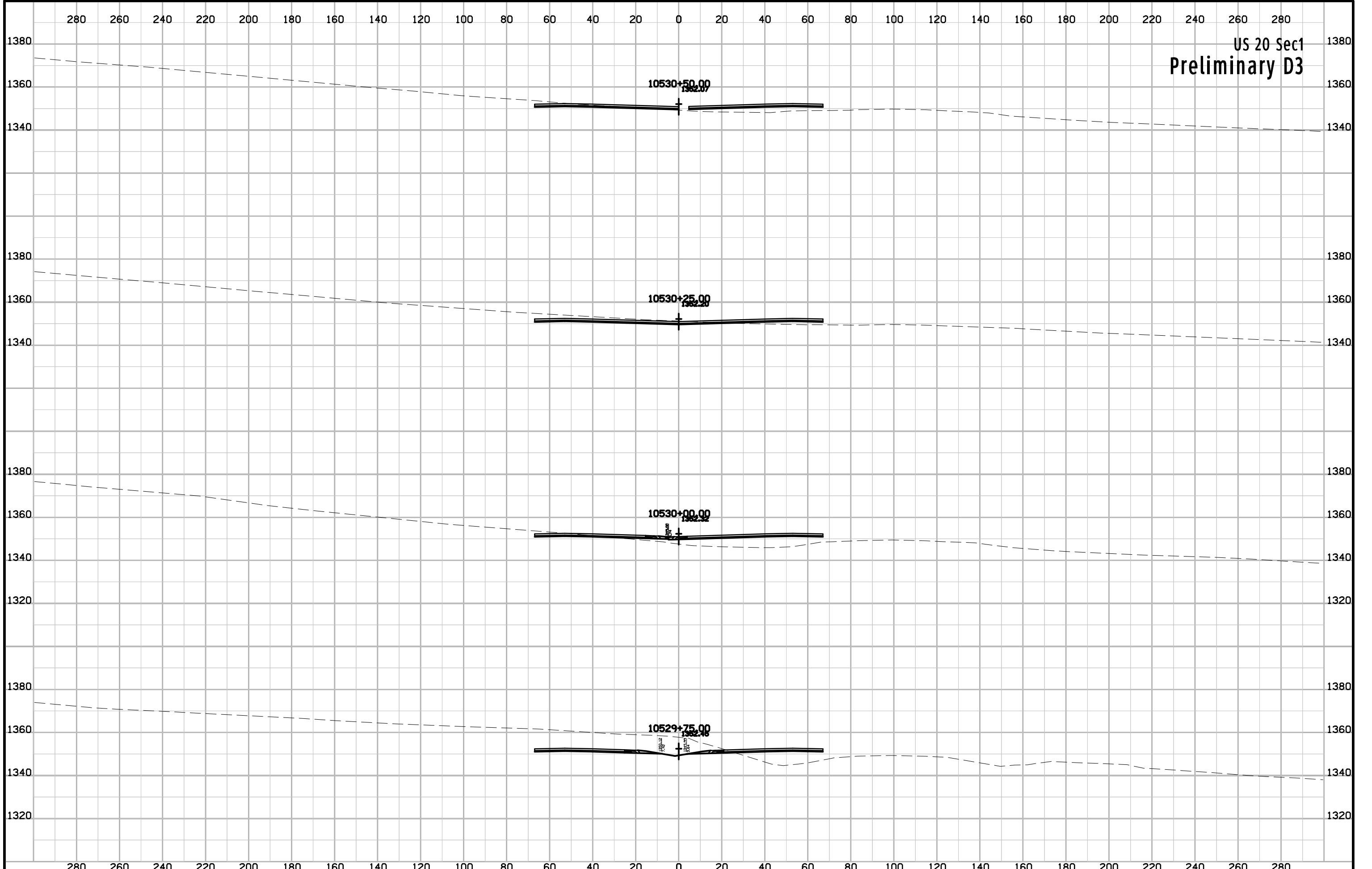
US 20 Sec1
Preliminary D3



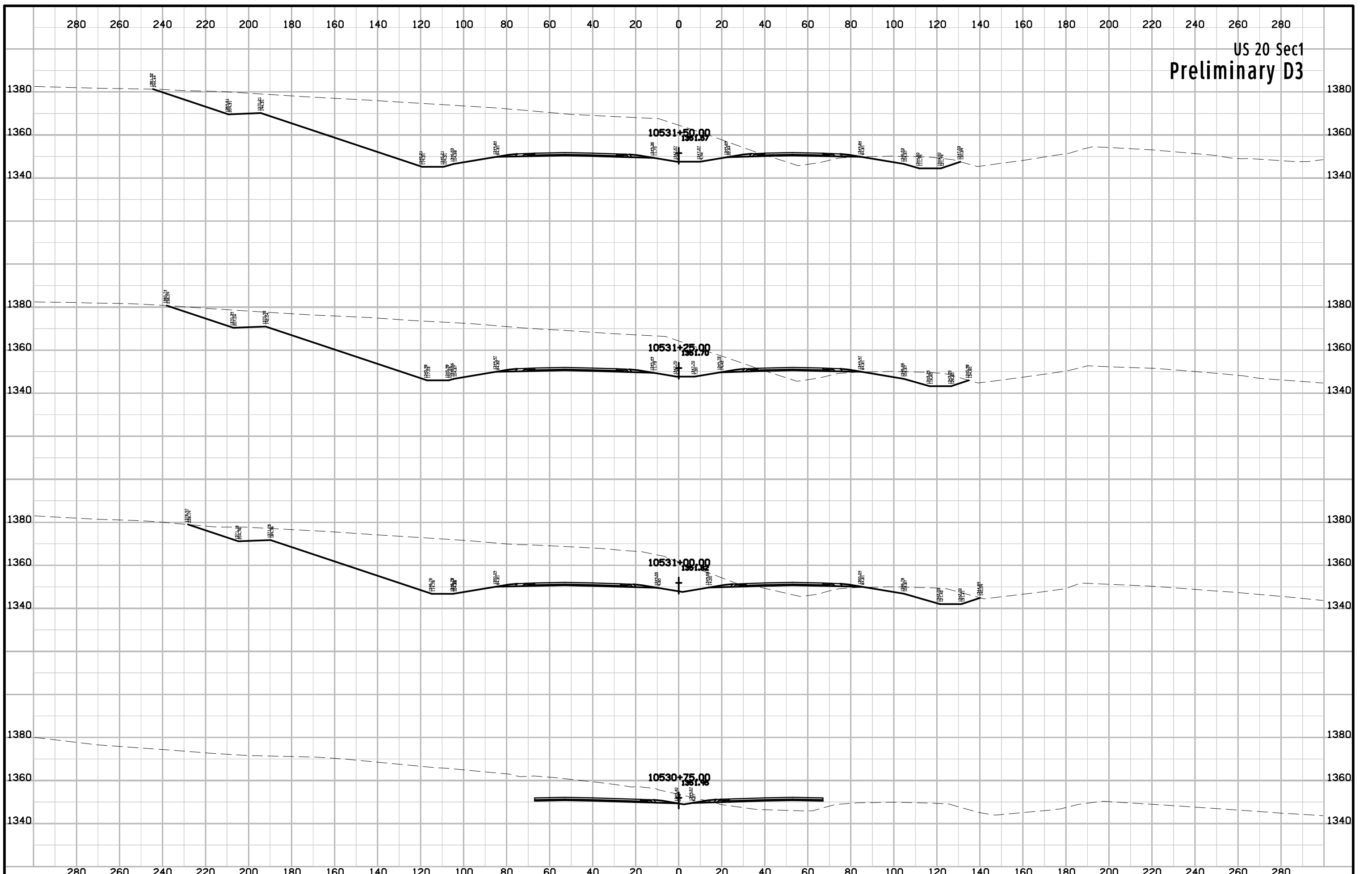
US 20 Sec1
Preliminary D3



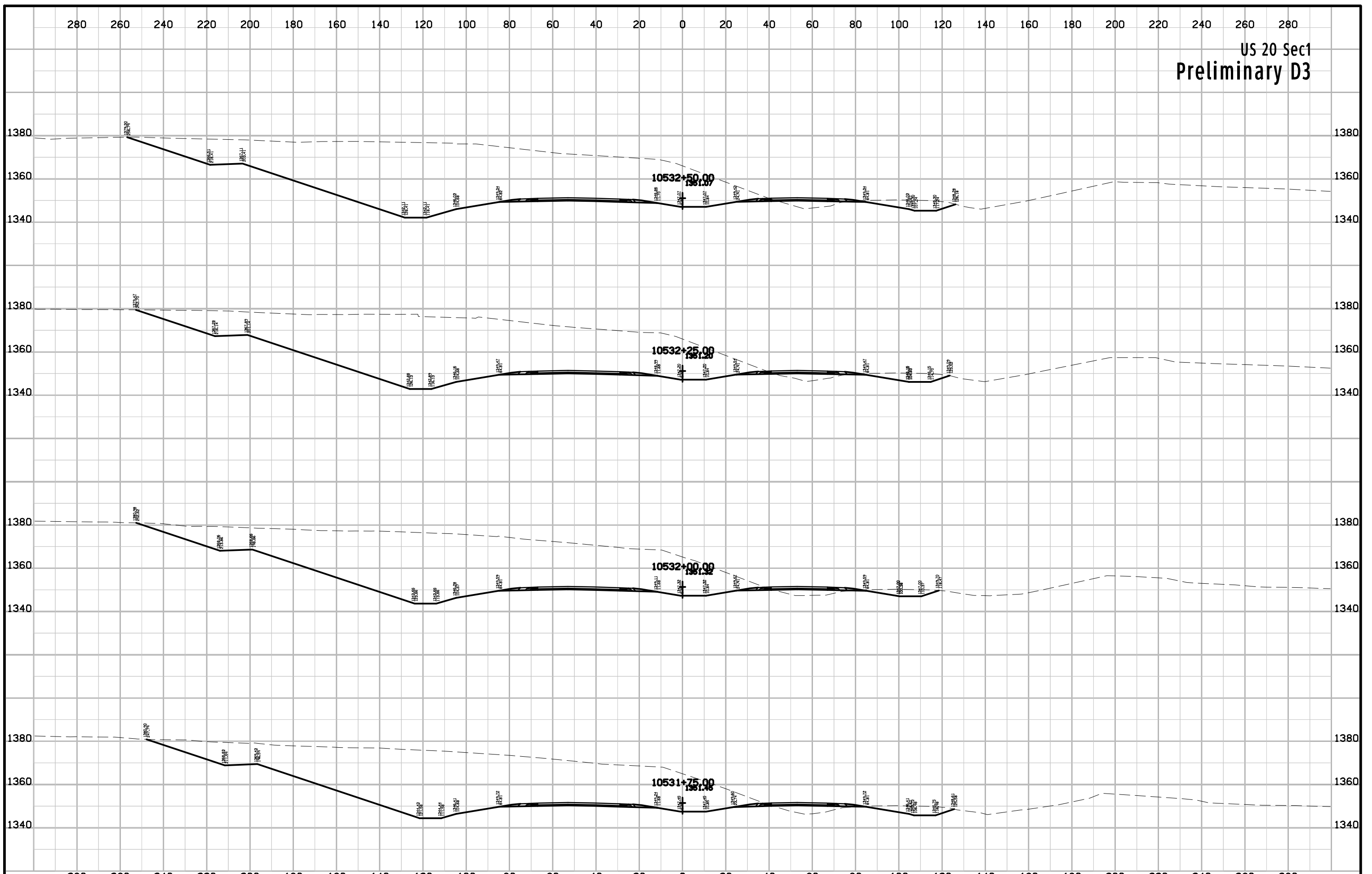
US 20 Sec1
Preliminary D3



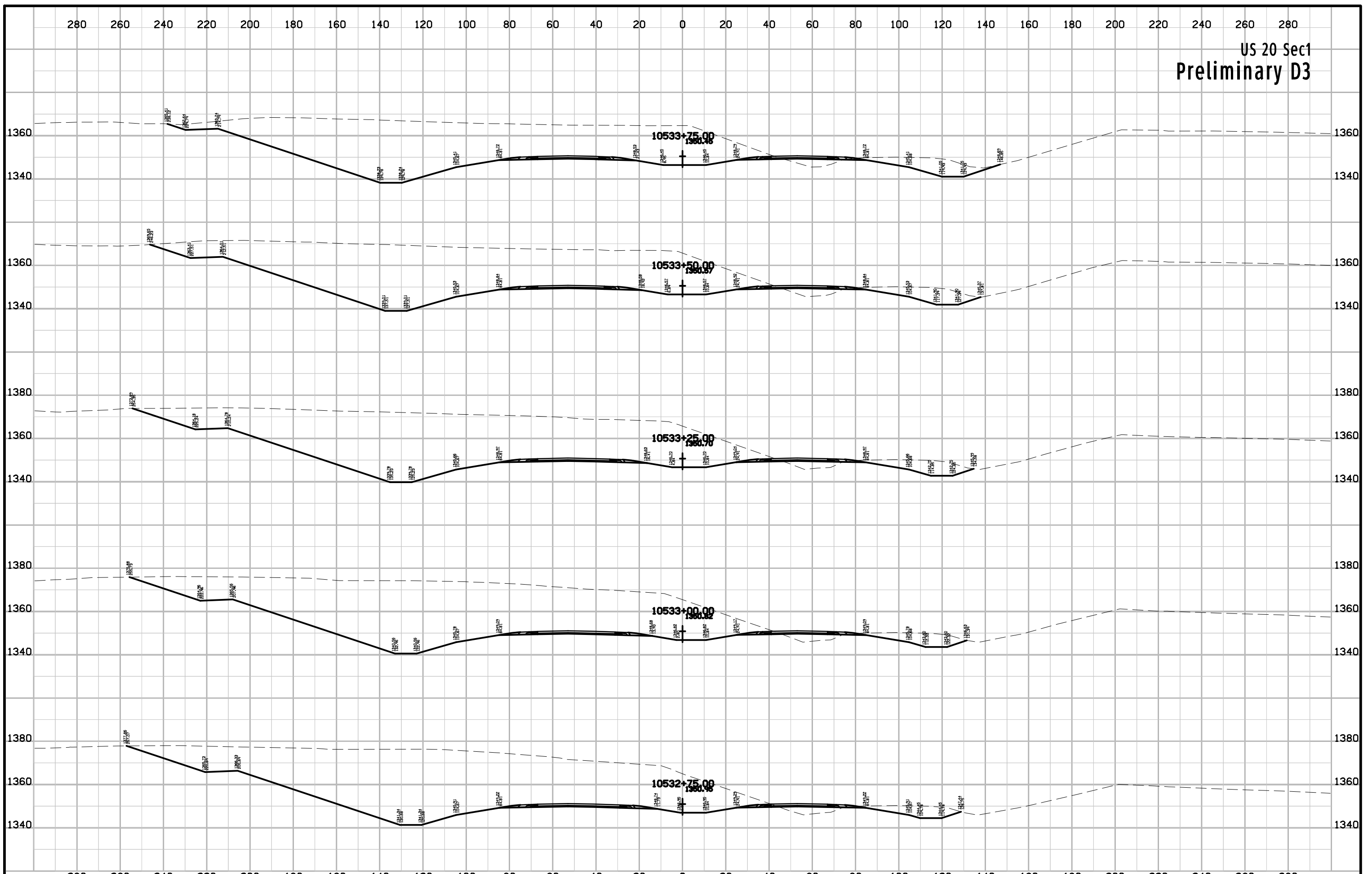
US 20 Sec1
Preliminary D3



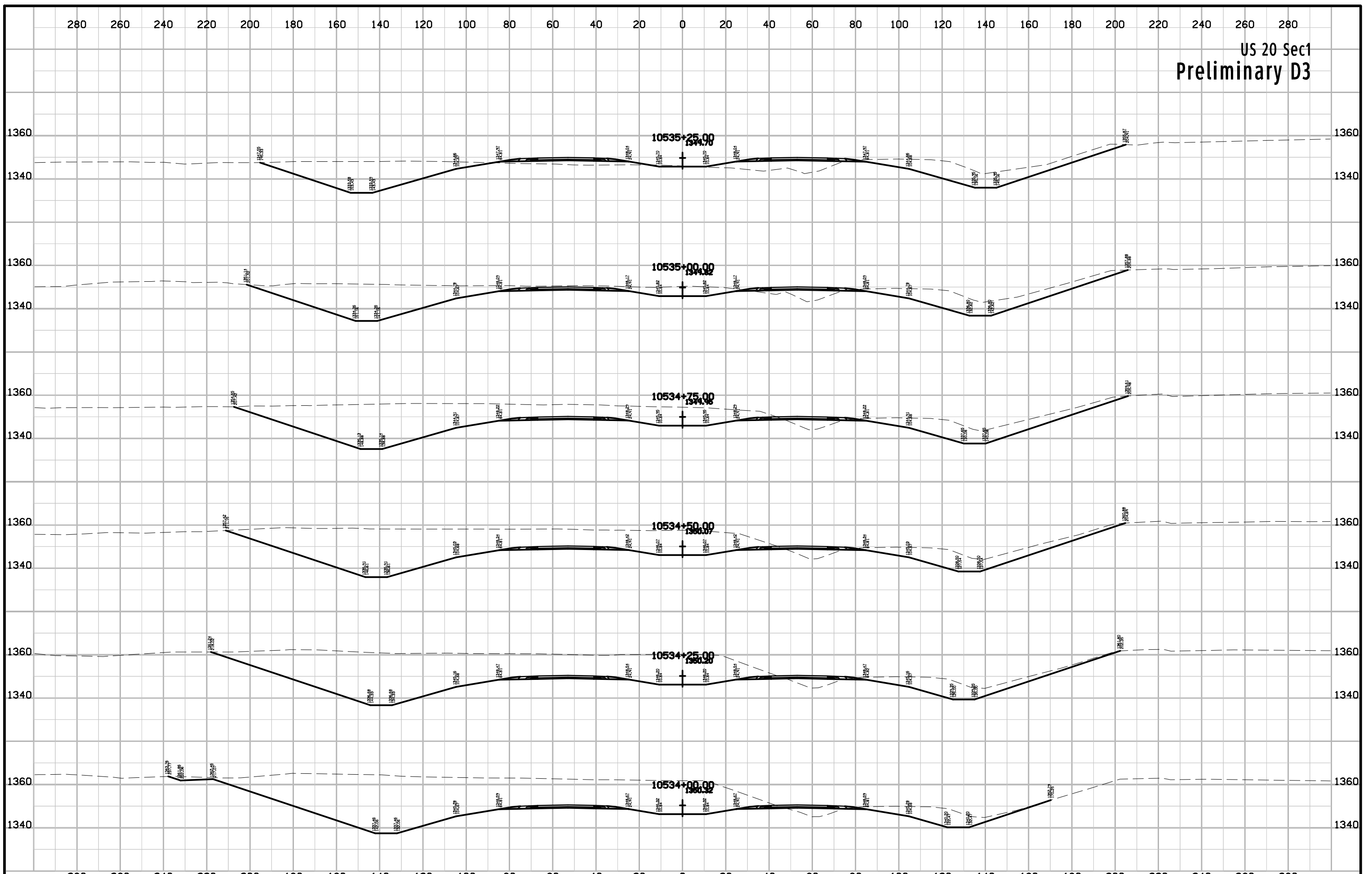
US 20 Sec1
Preliminary D3



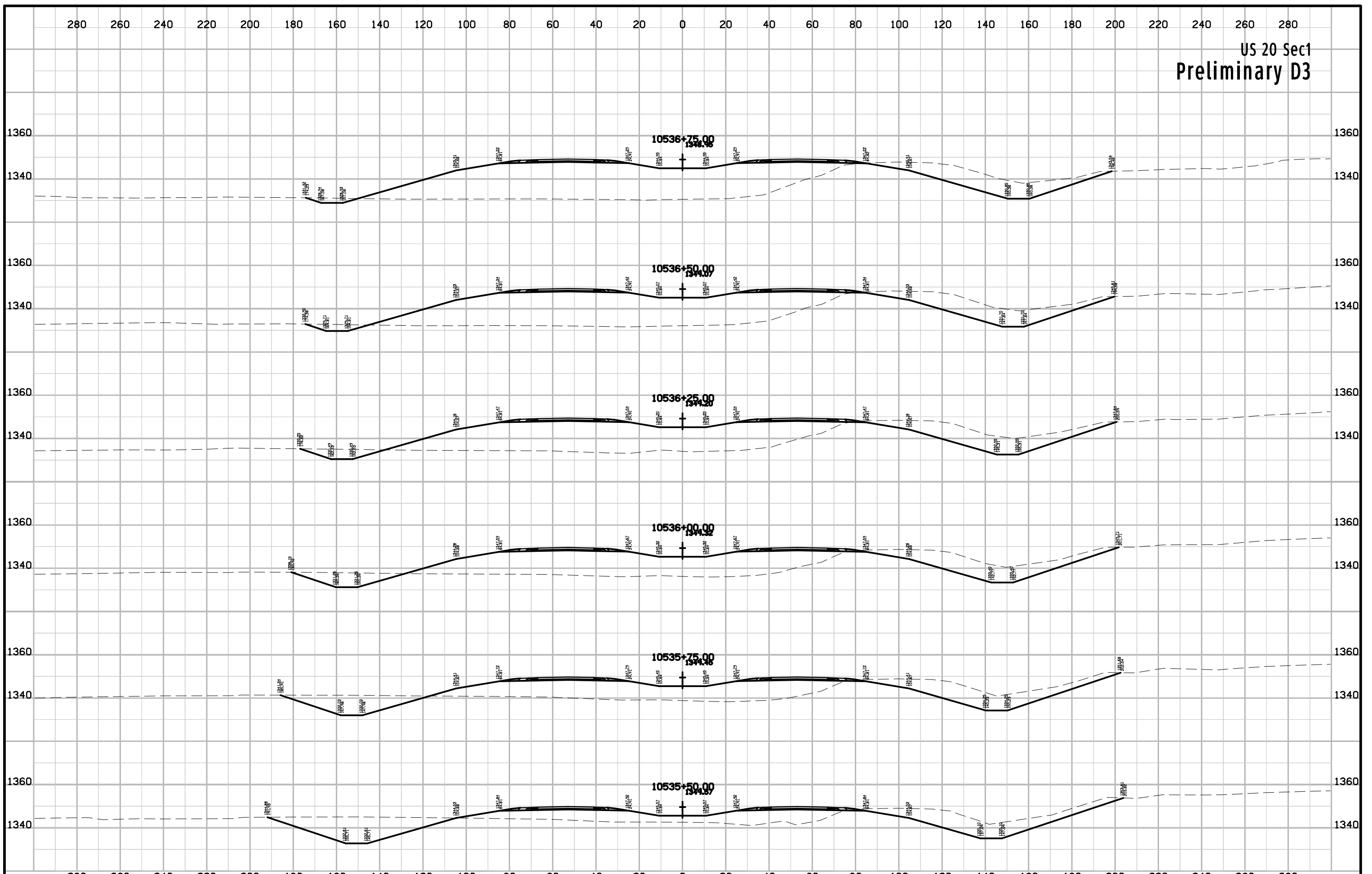
US 20 Sec1
Preliminary D3



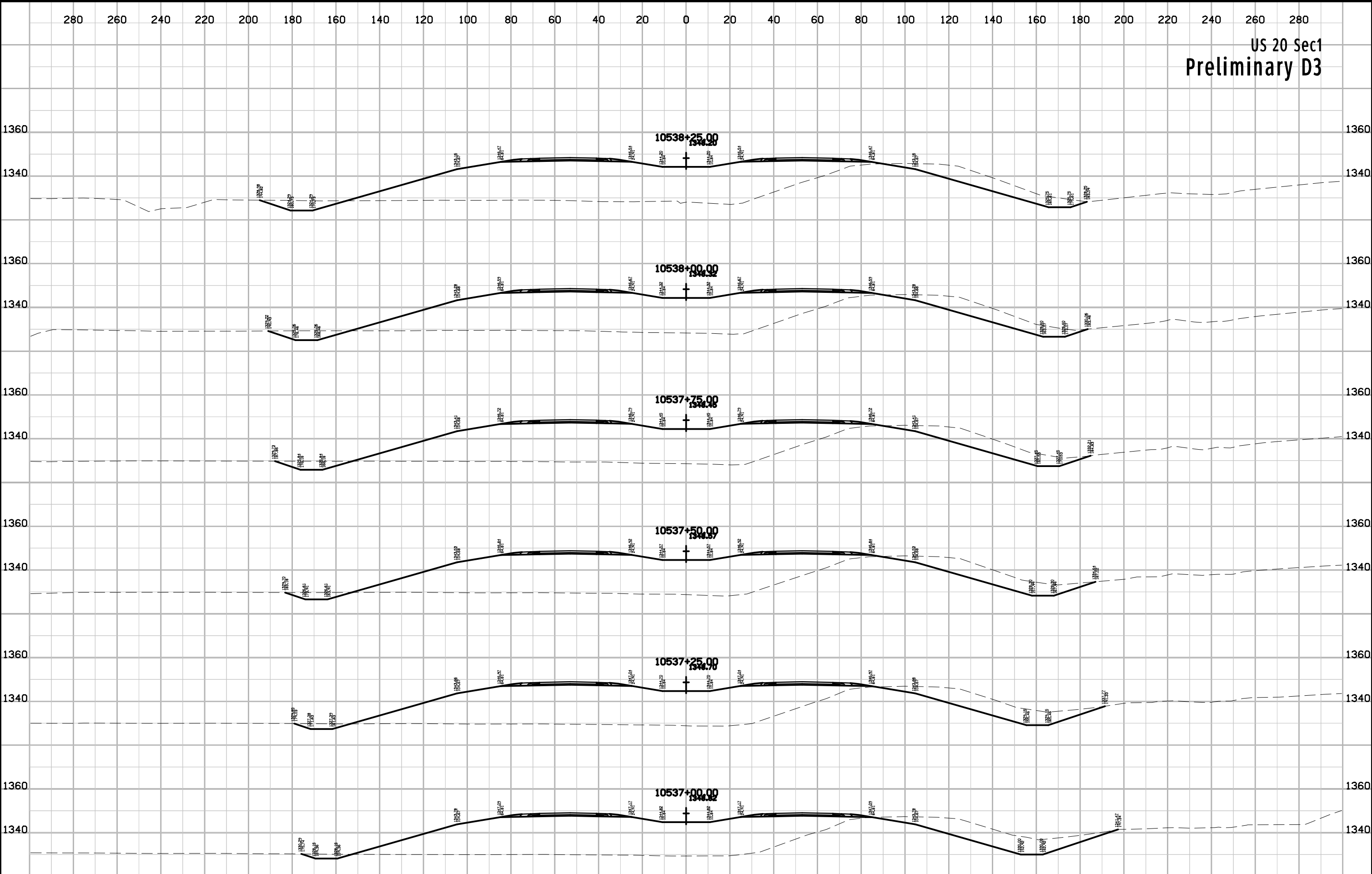
US 20 Sec1
Preliminary D3



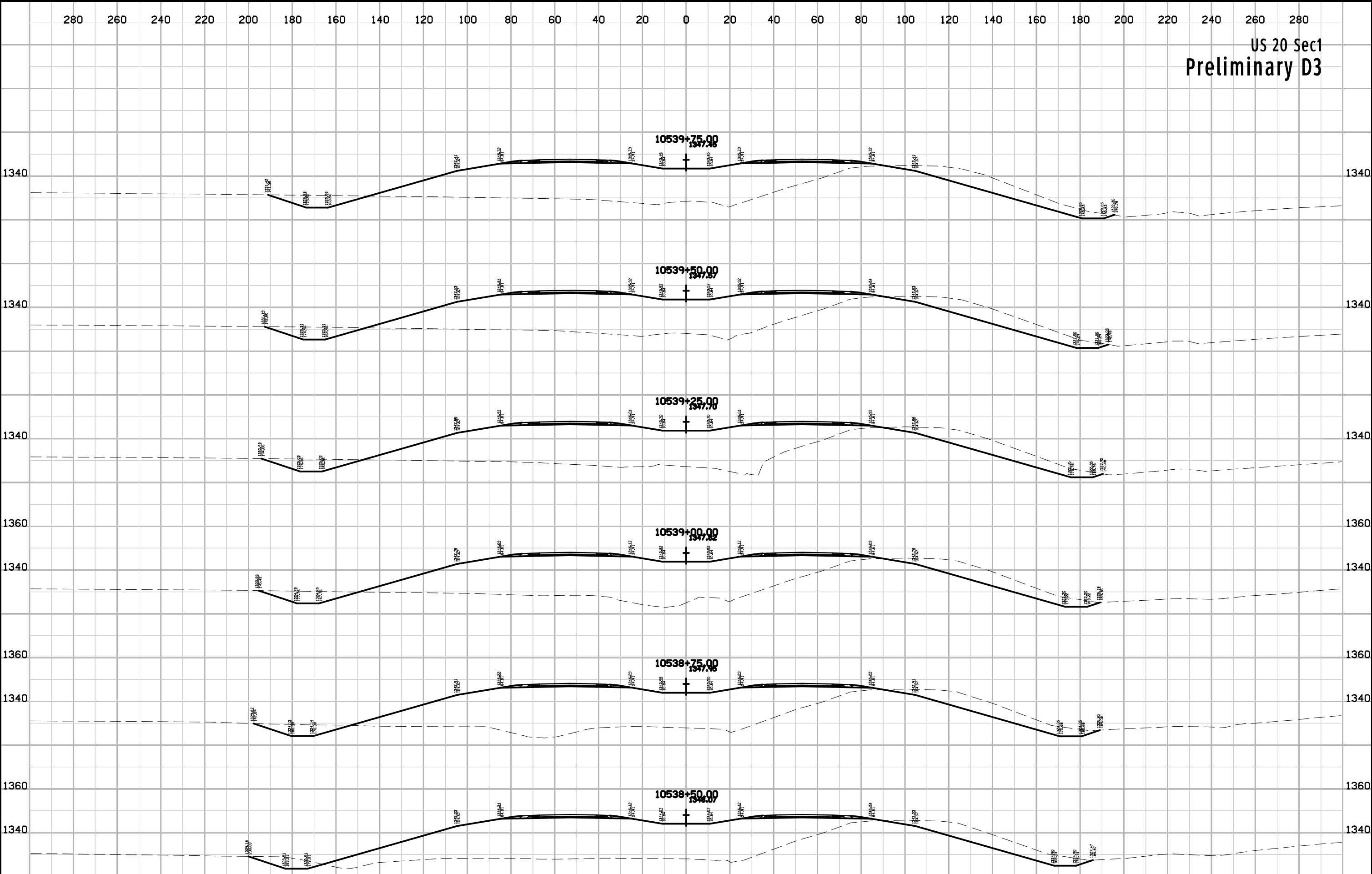
US 20 Sec1
Preliminary D3



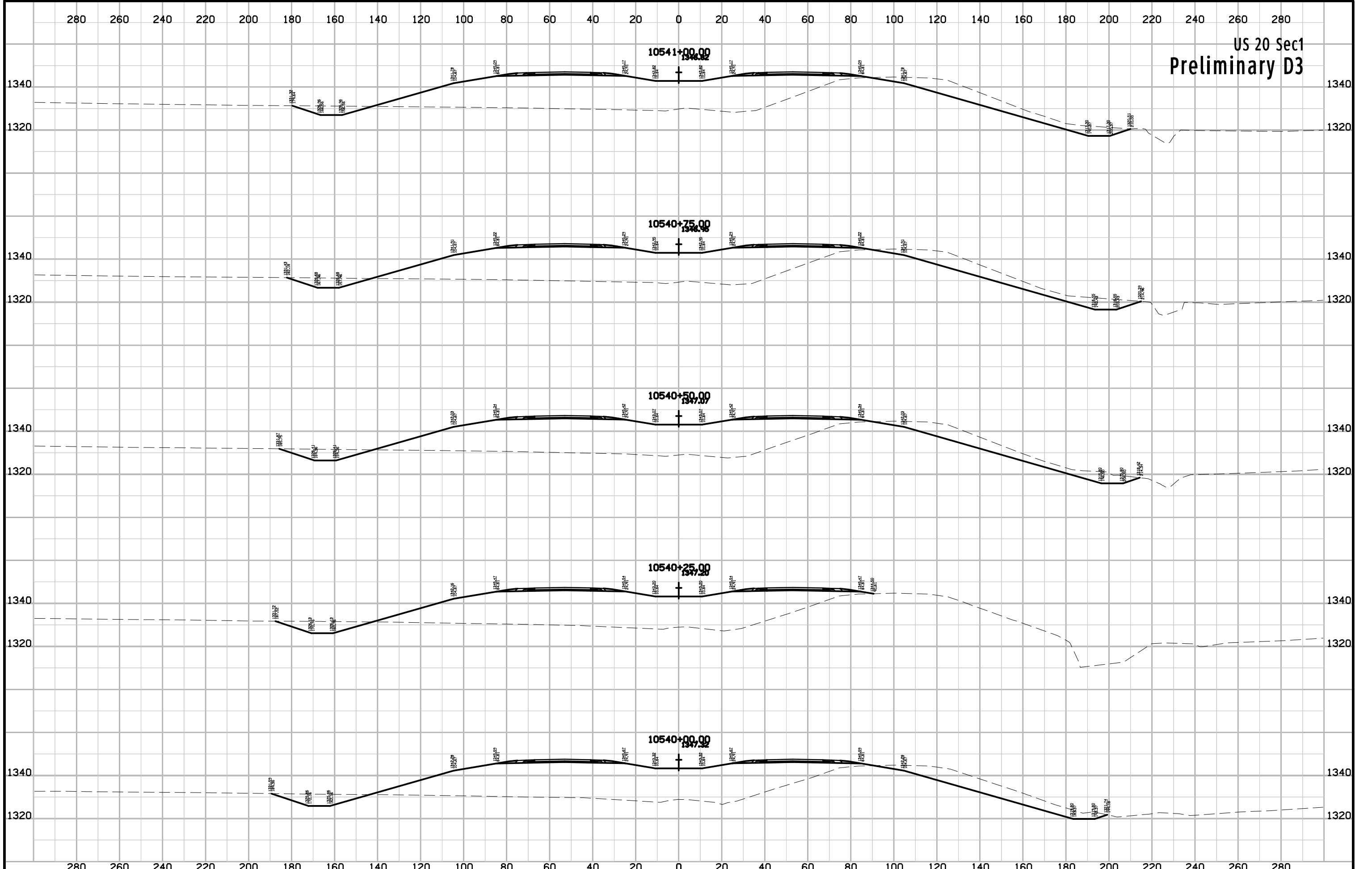
US 20 Sec1
Preliminary D3



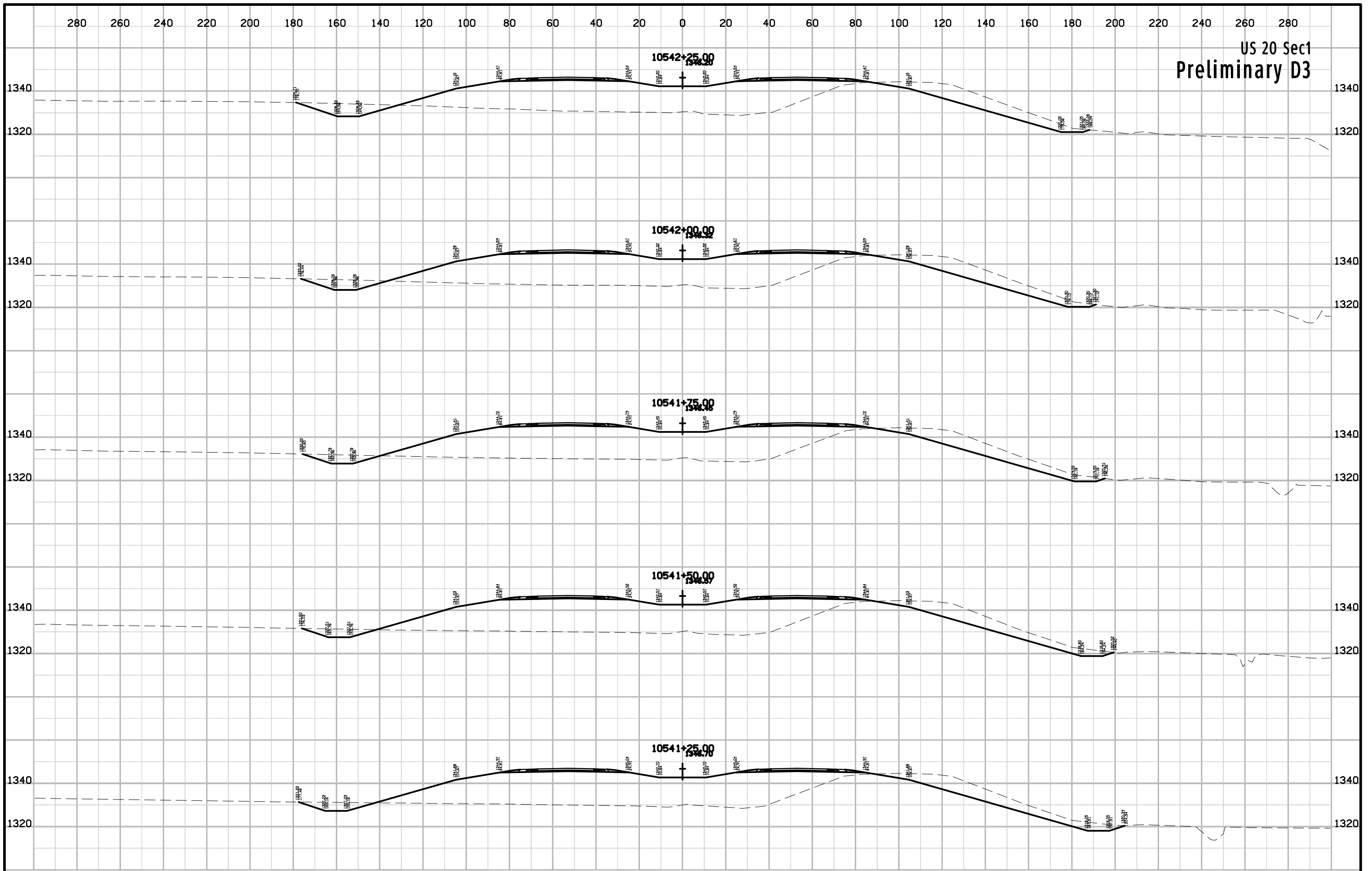
US 20 Sec1
Preliminary D3



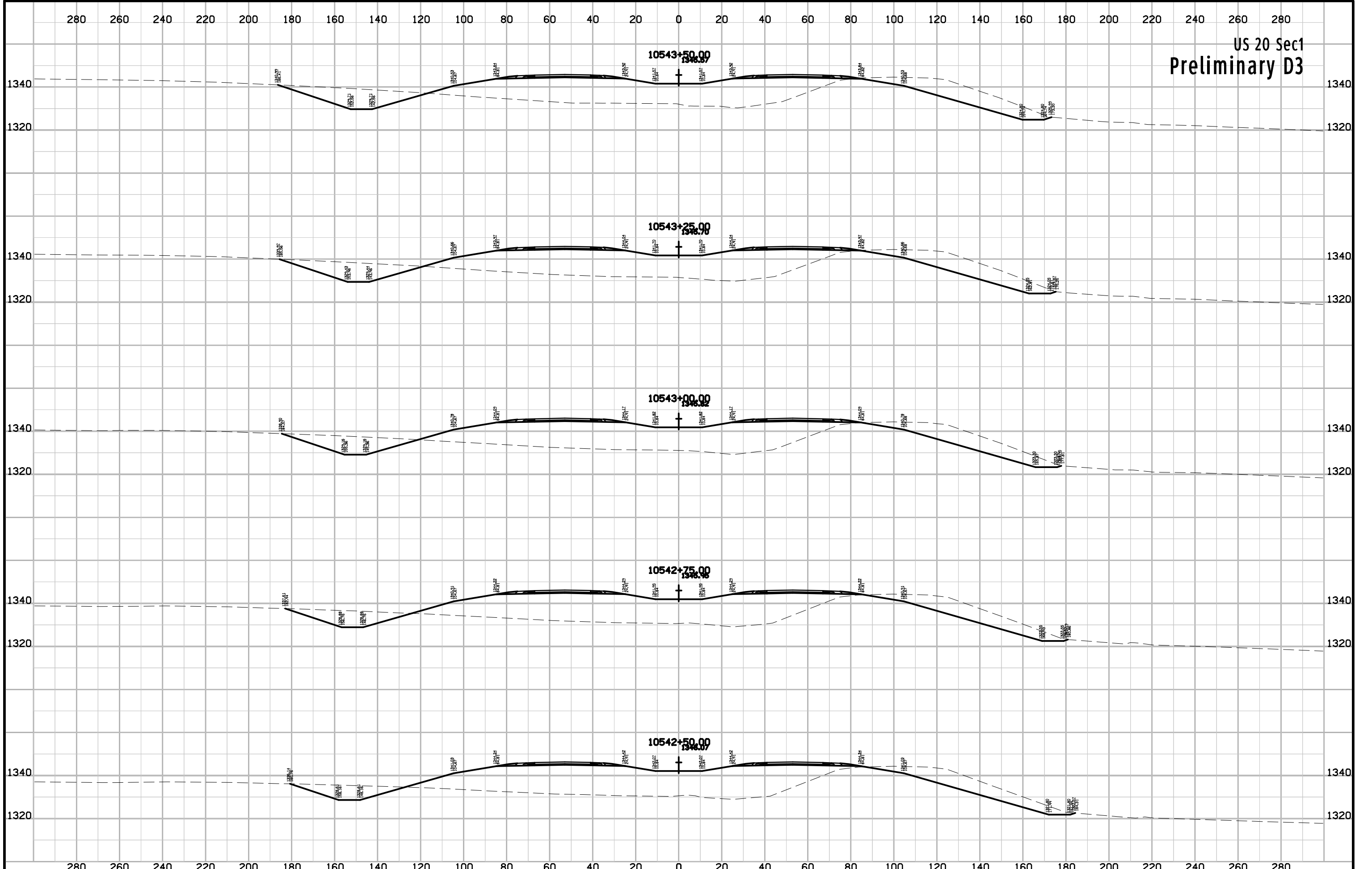
US 20 Sec1
Preliminary D3



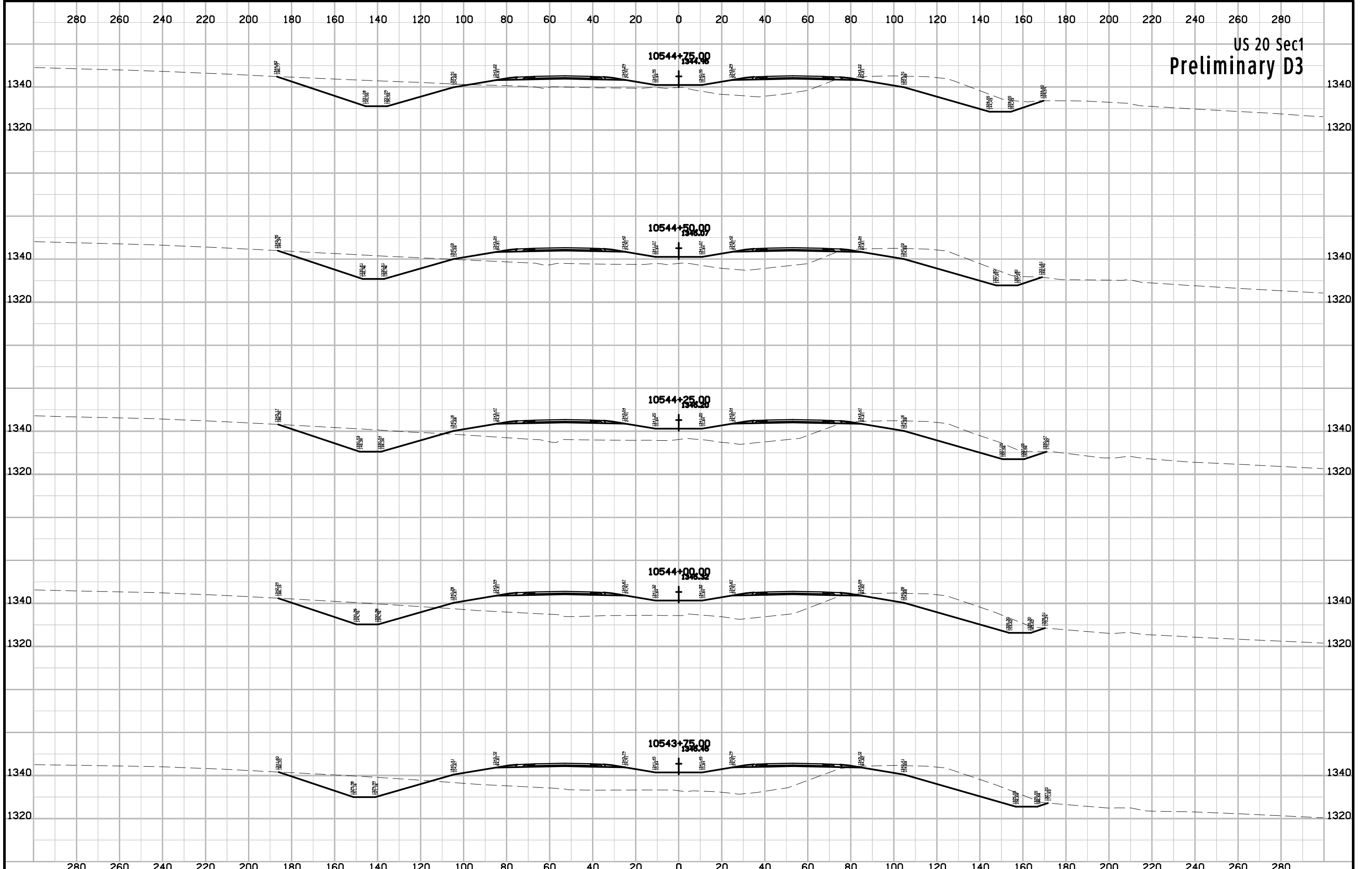
US 20 Sec1
Preliminary D3



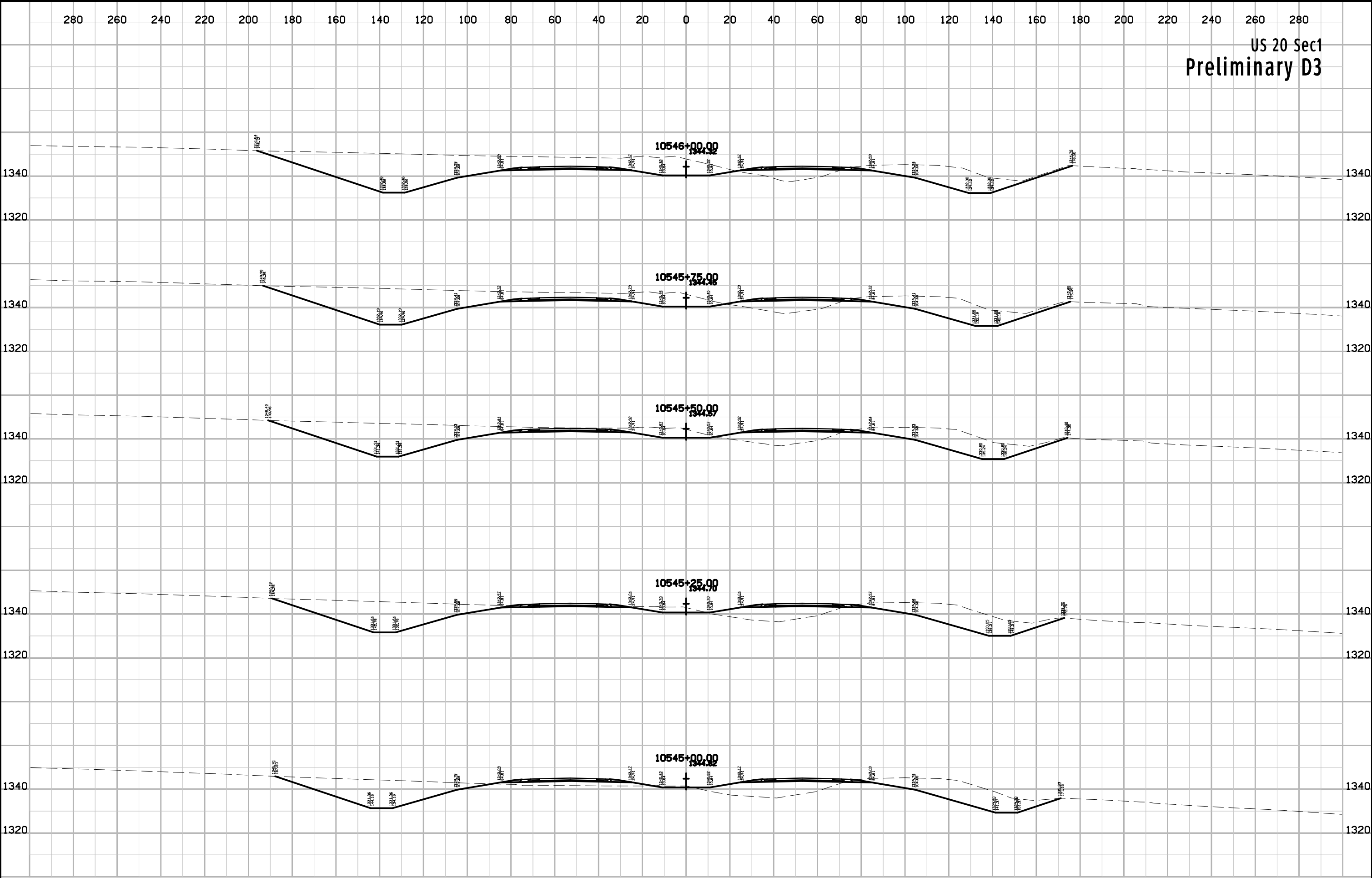
US 20 Sec1
Preliminary D3



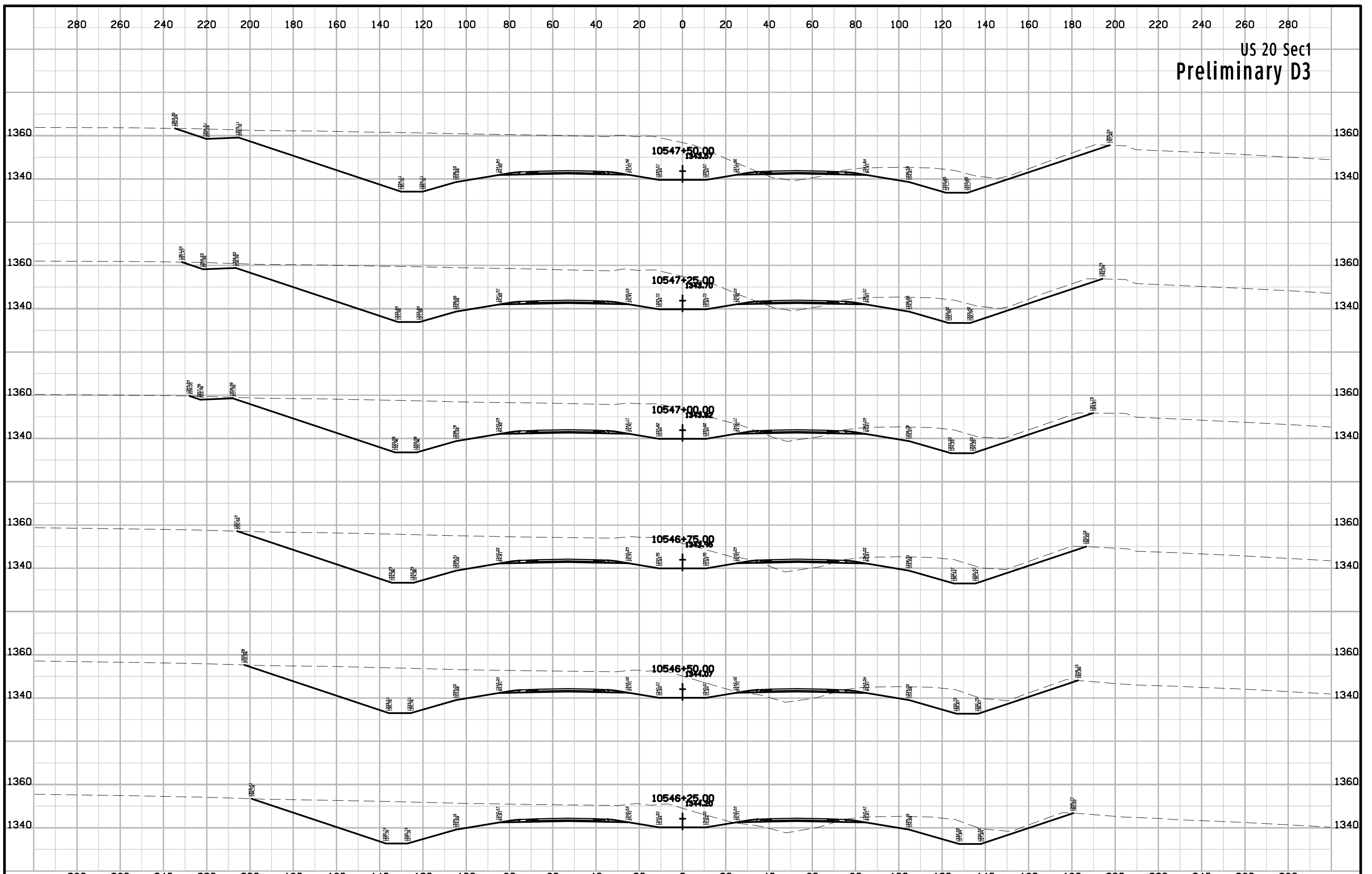
US 20 Sec1
Preliminary D3



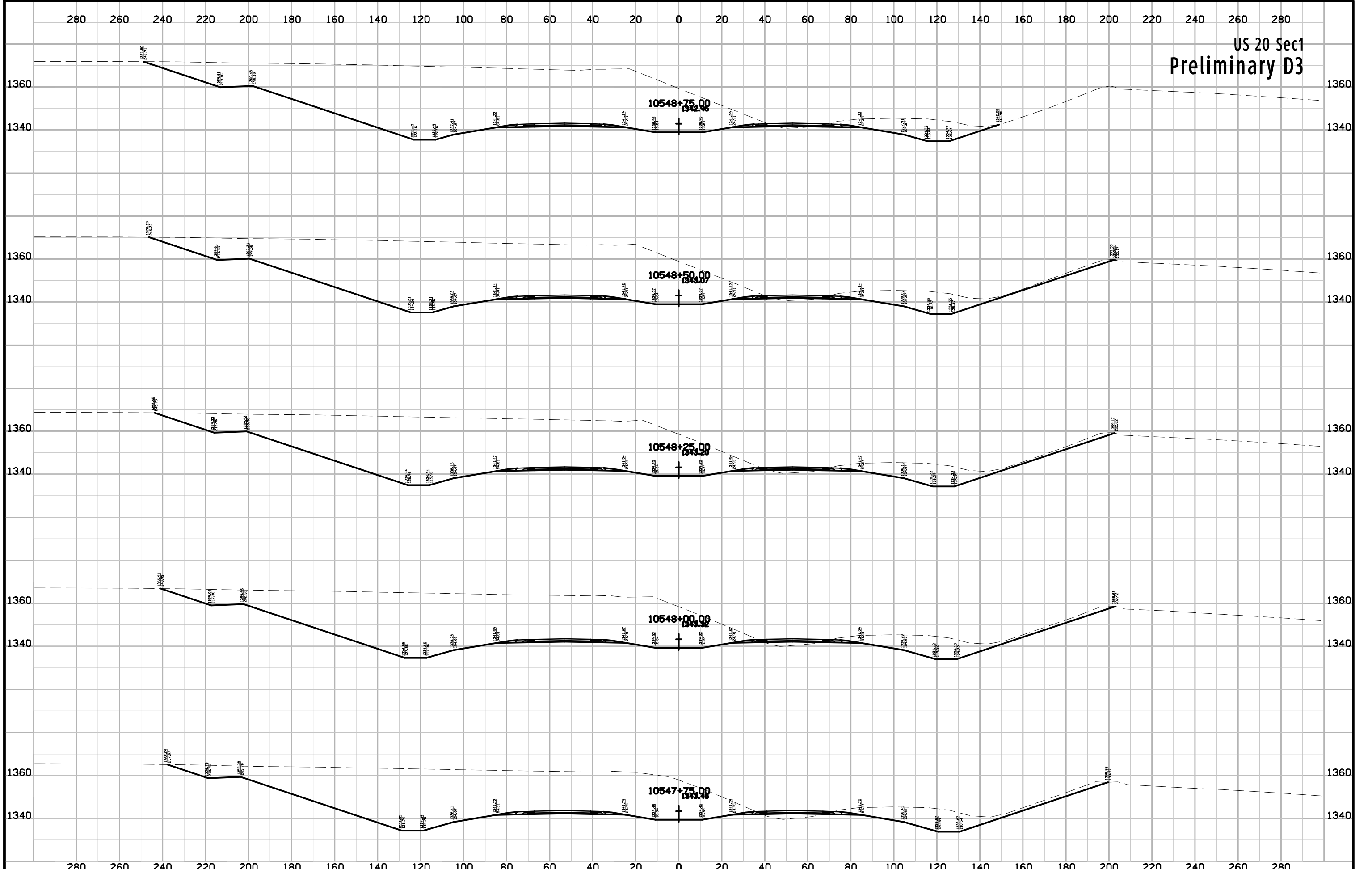
US 20 Sec1
Preliminary D3



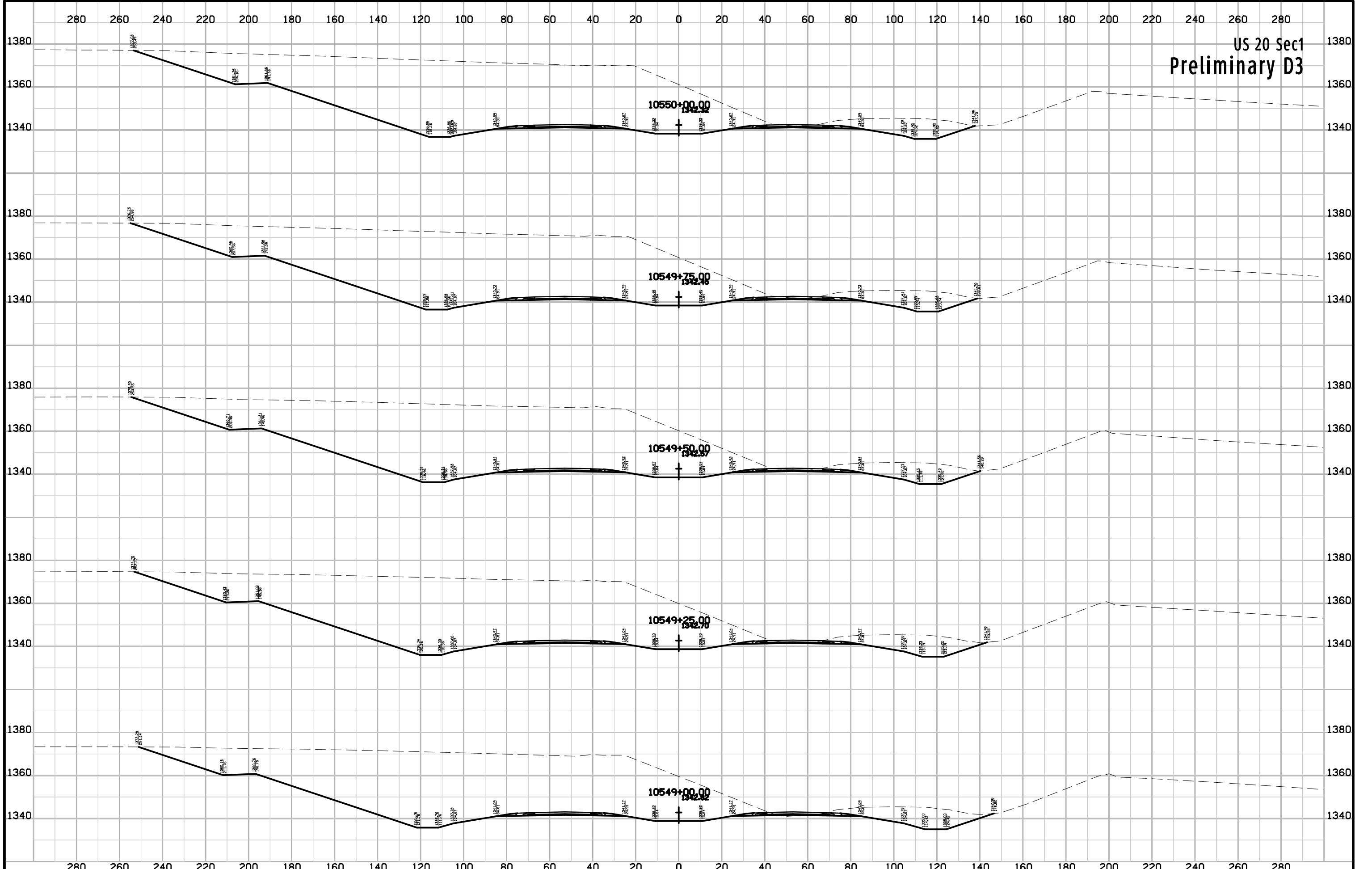
US 20 Sec1
Preliminary D3



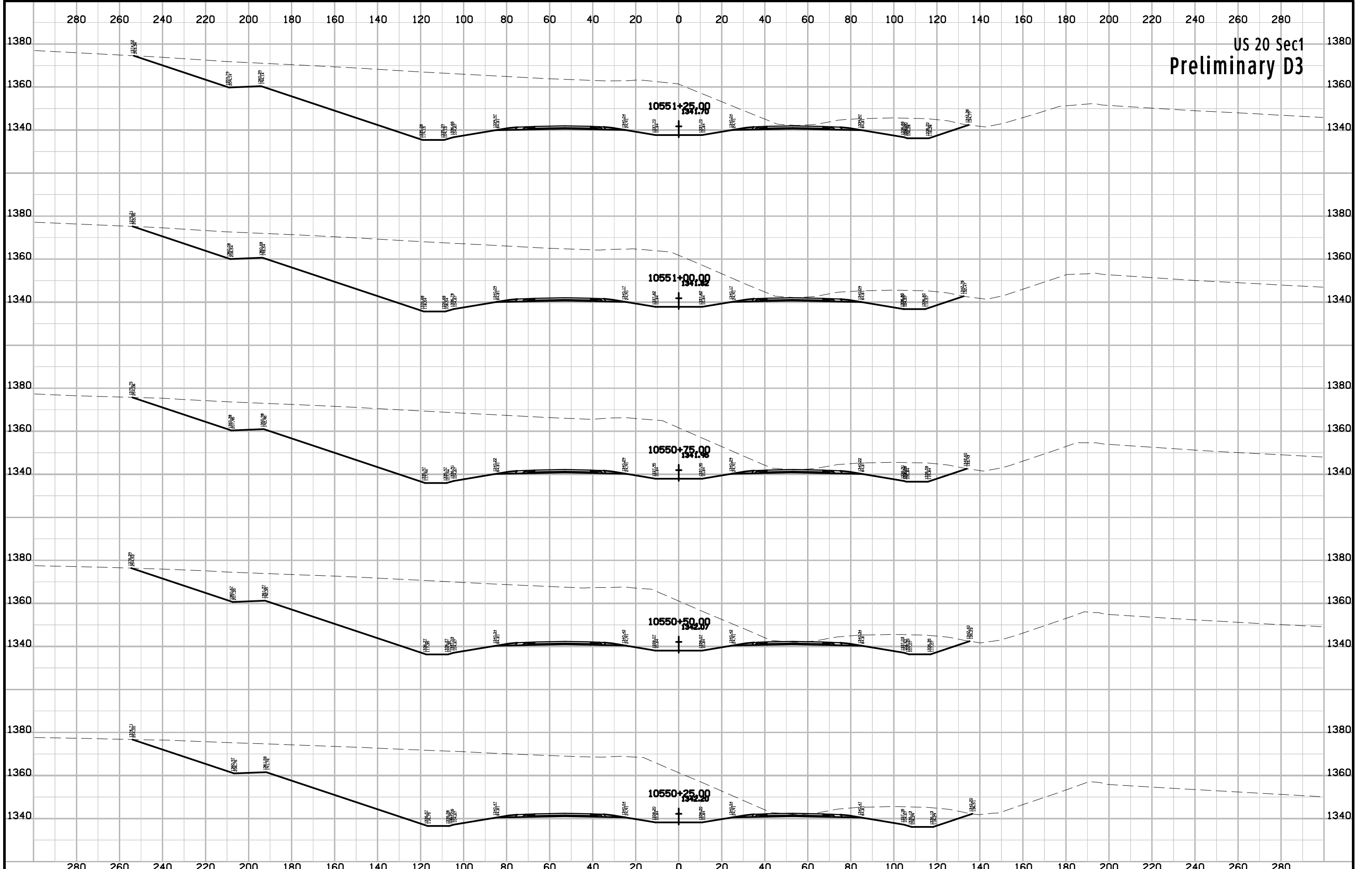
US 20 Sec1
Preliminary D3



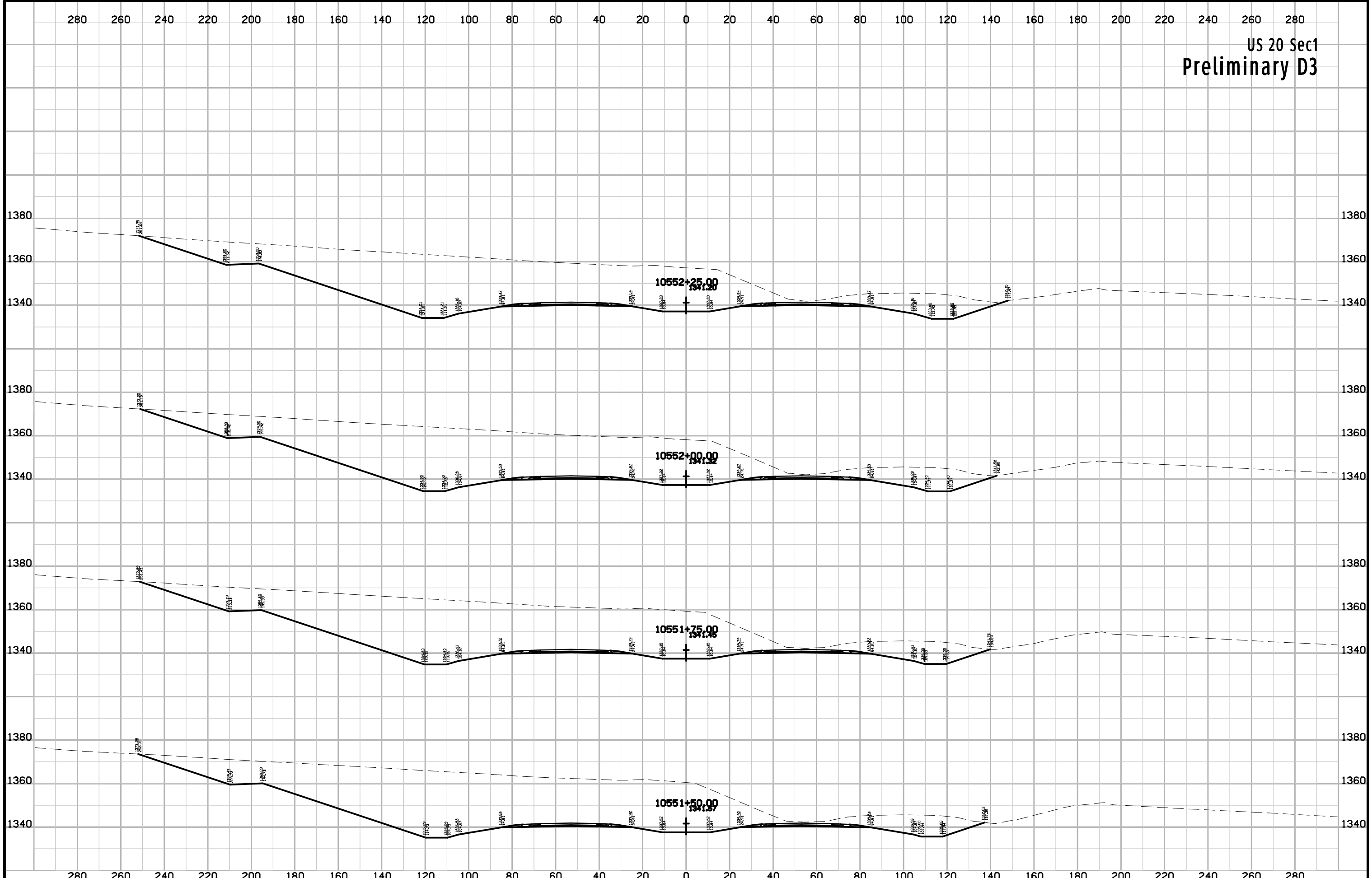
US 20 Sec1
Preliminary D3



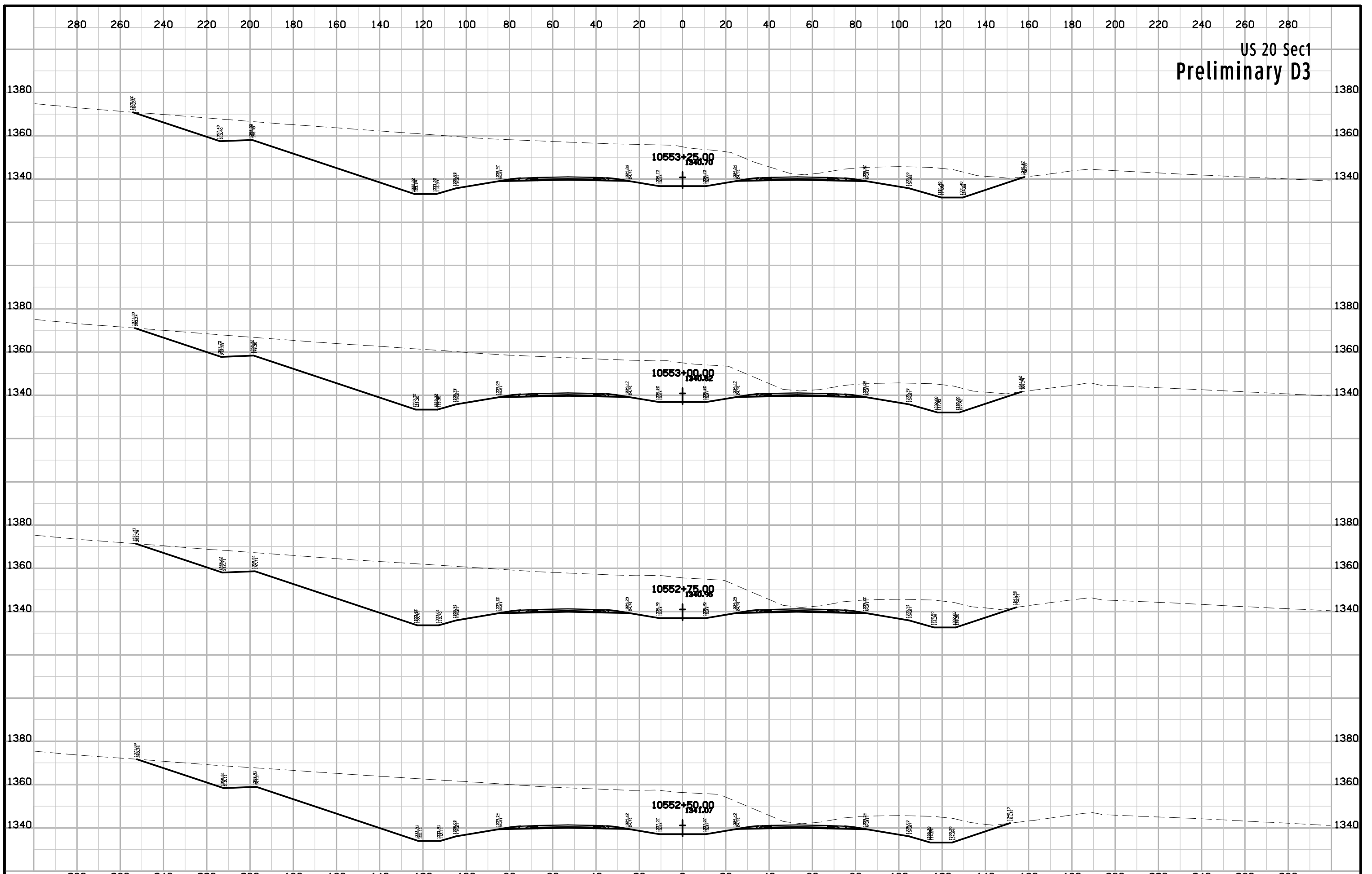
US 20 Sec1
Preliminary D3



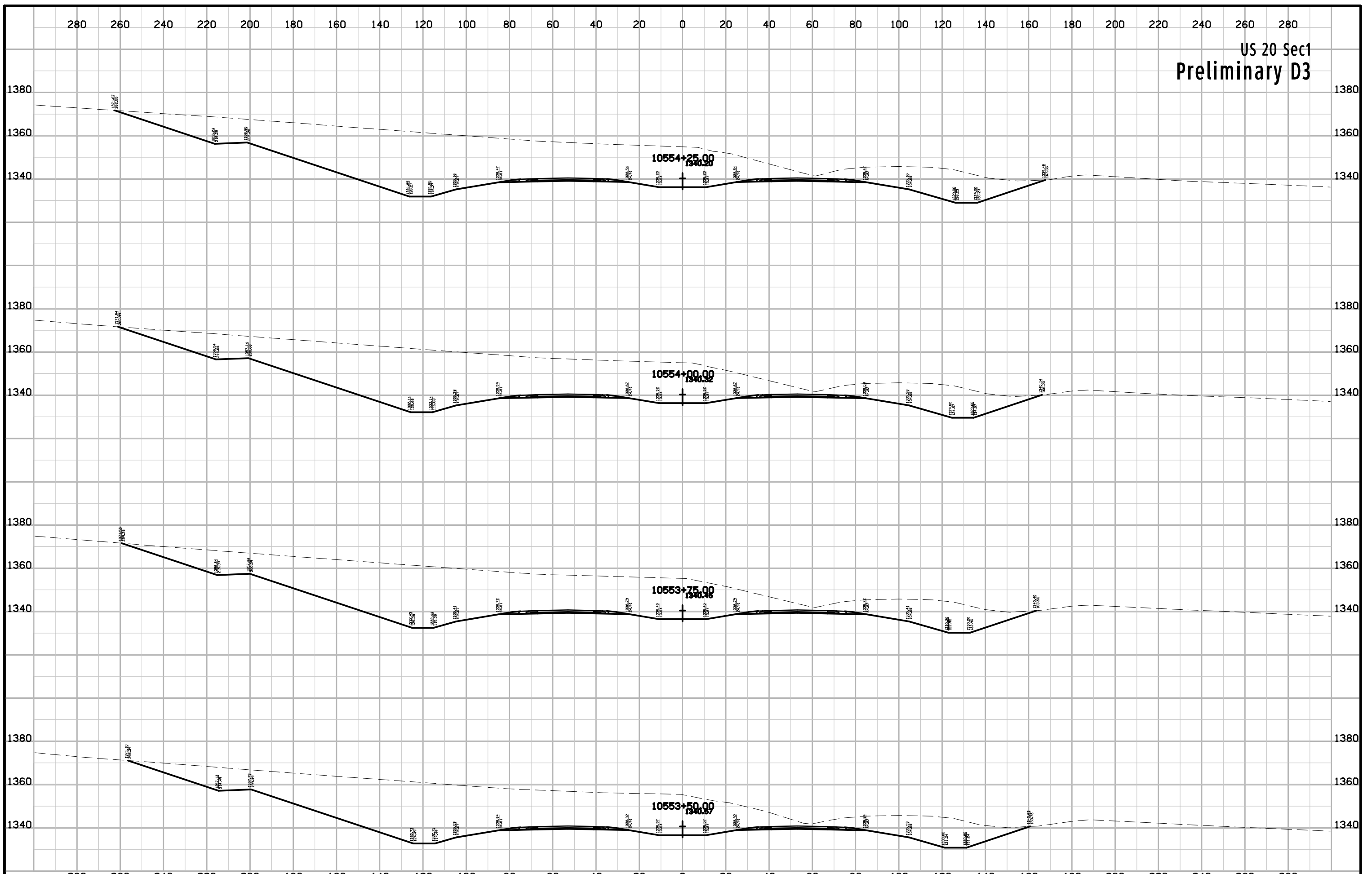
US 20 Sec1
Preliminary D3



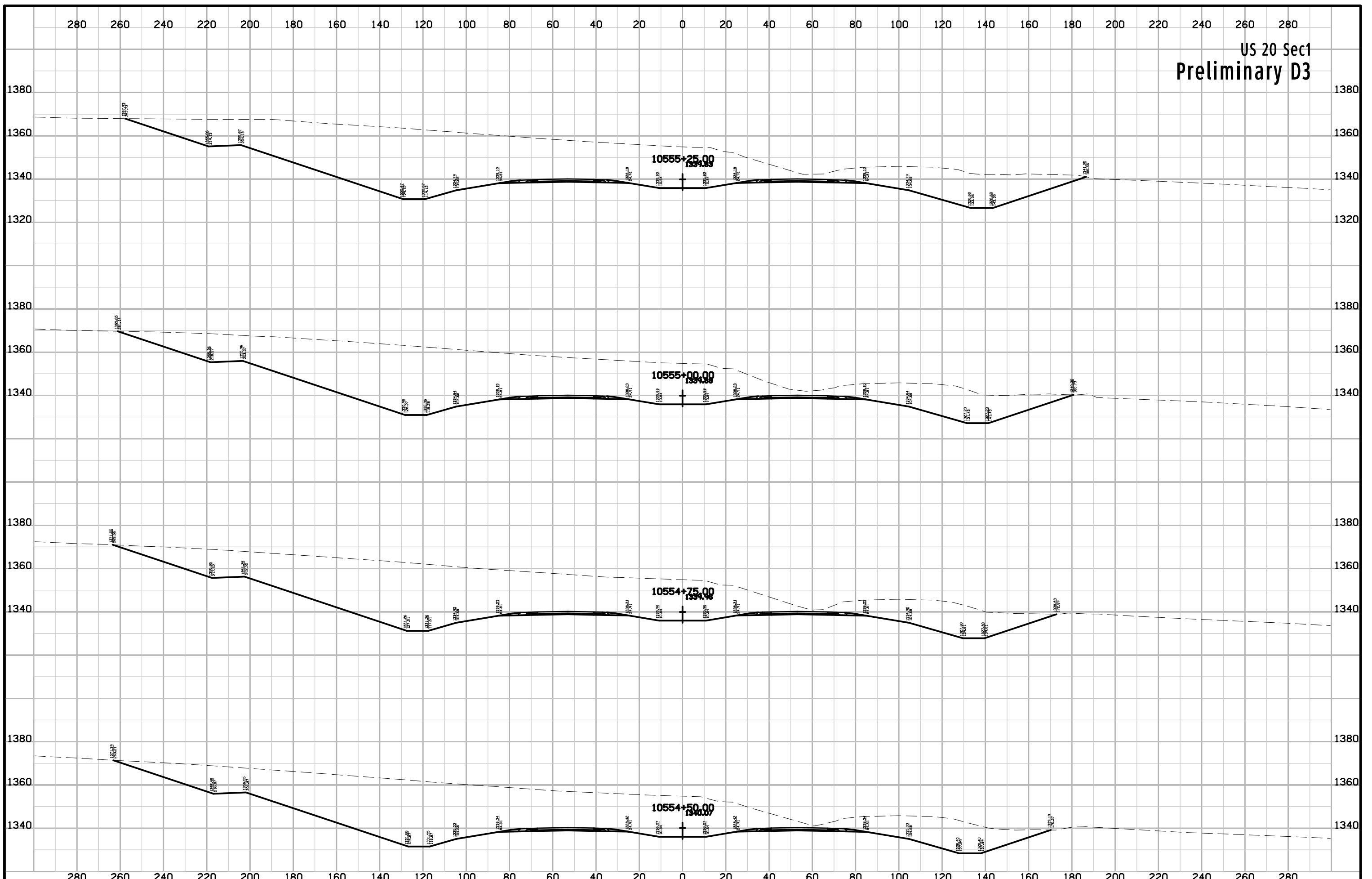
US 20 Sec1
Preliminary D3



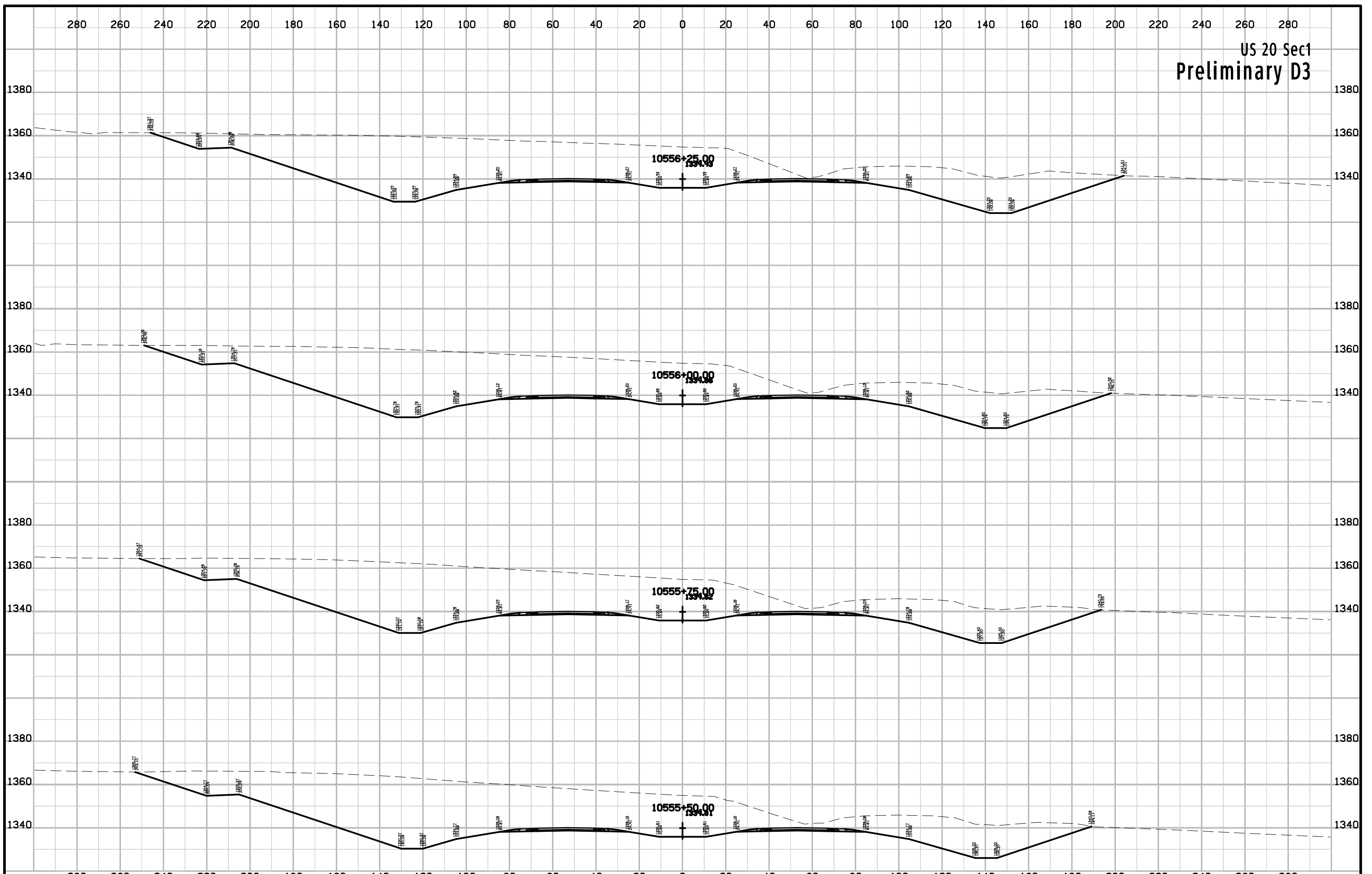
US 20 Sec1
Preliminary D3



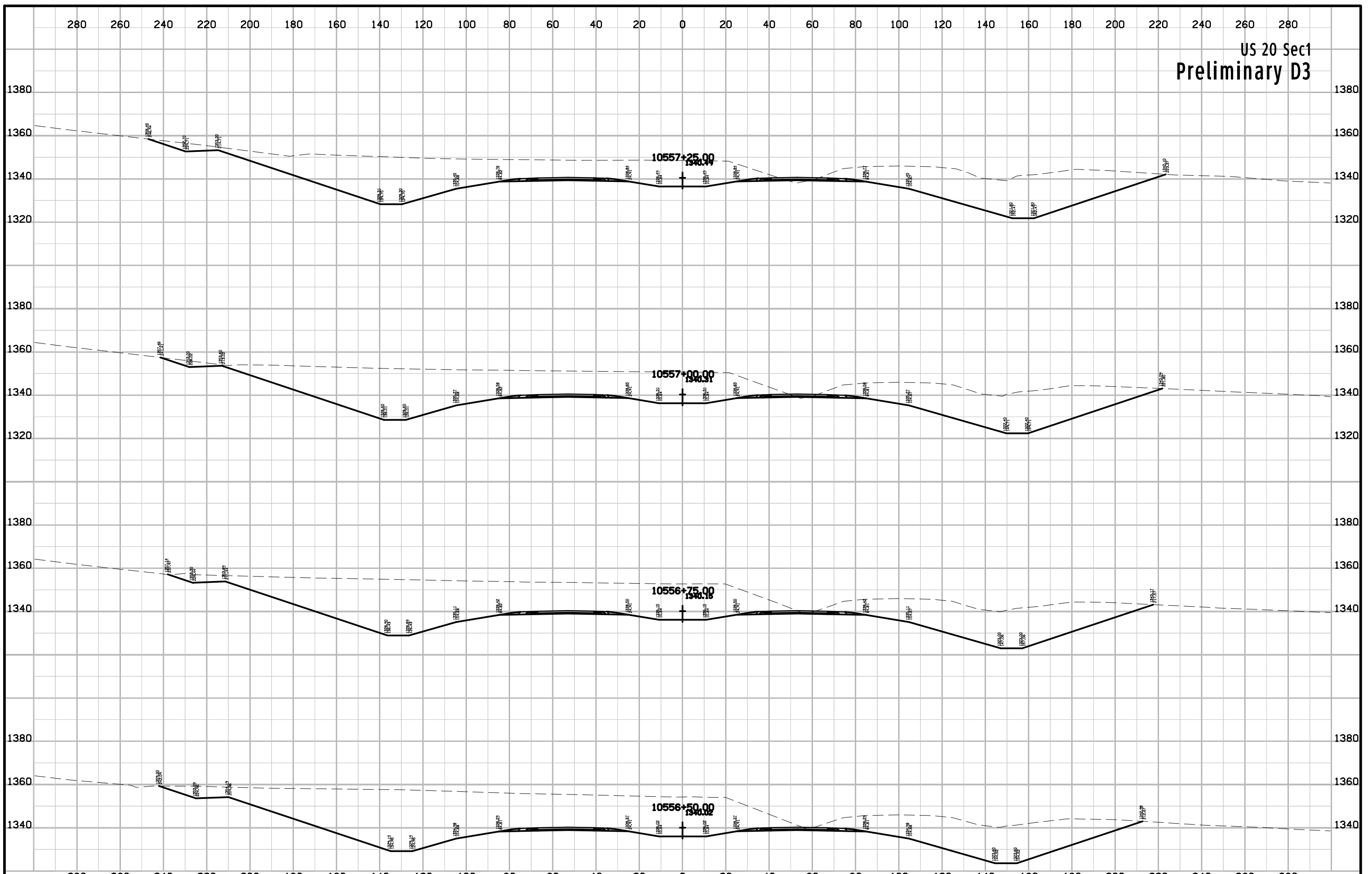
US 20 Sec1
Preliminary D3



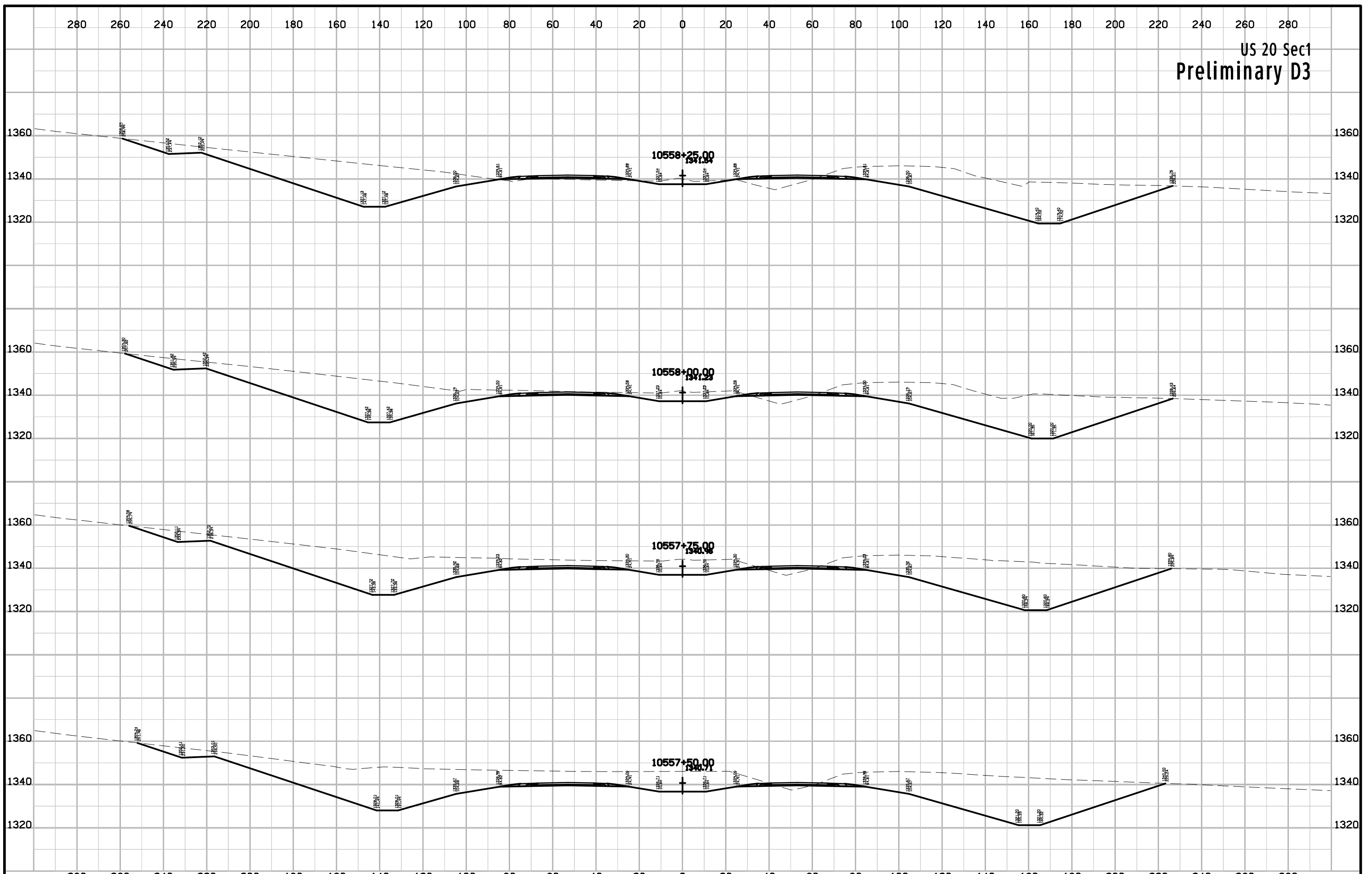
US 20 Sec1
Preliminary D3



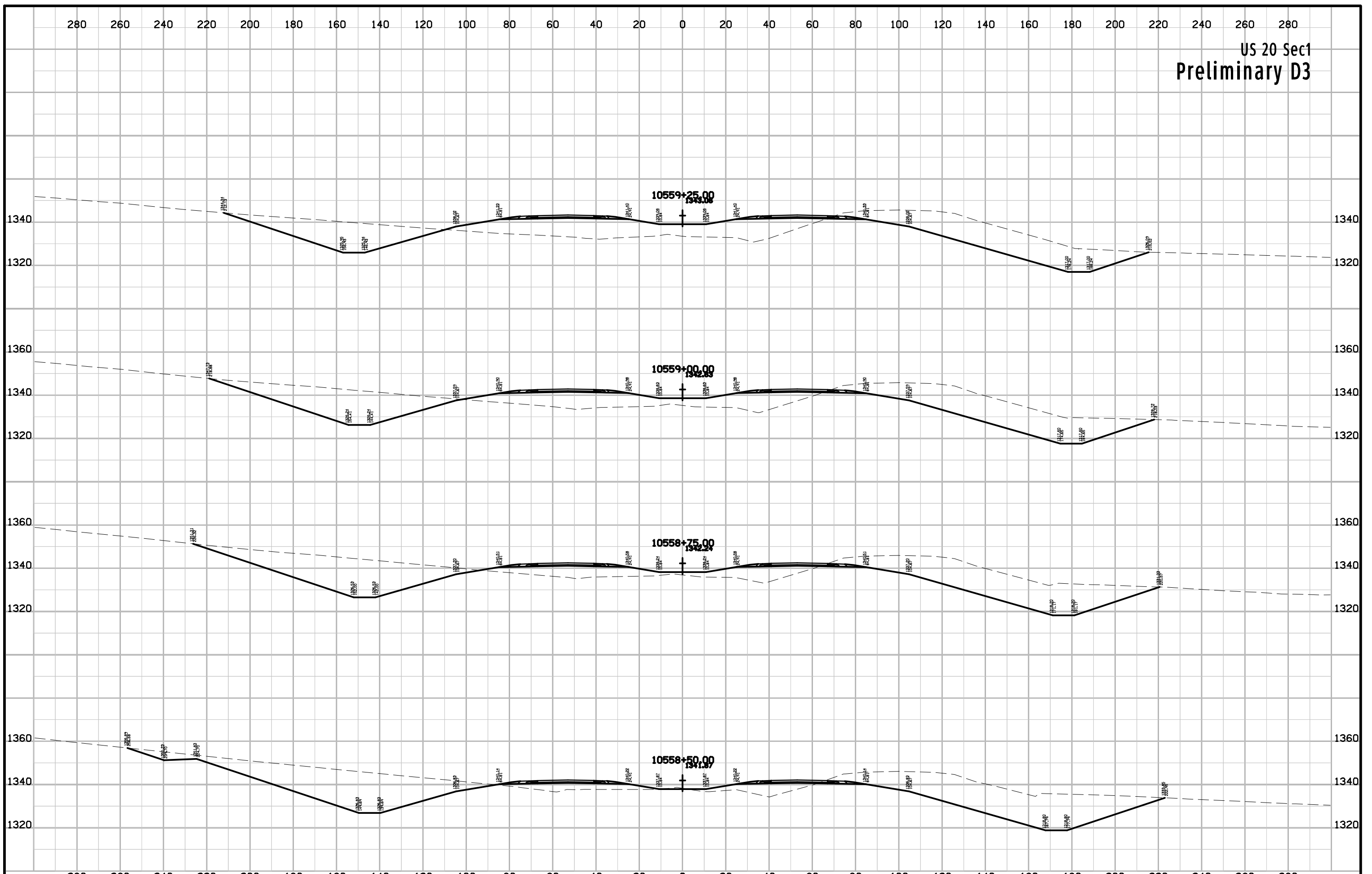
US 20 Sec1
Preliminary D3



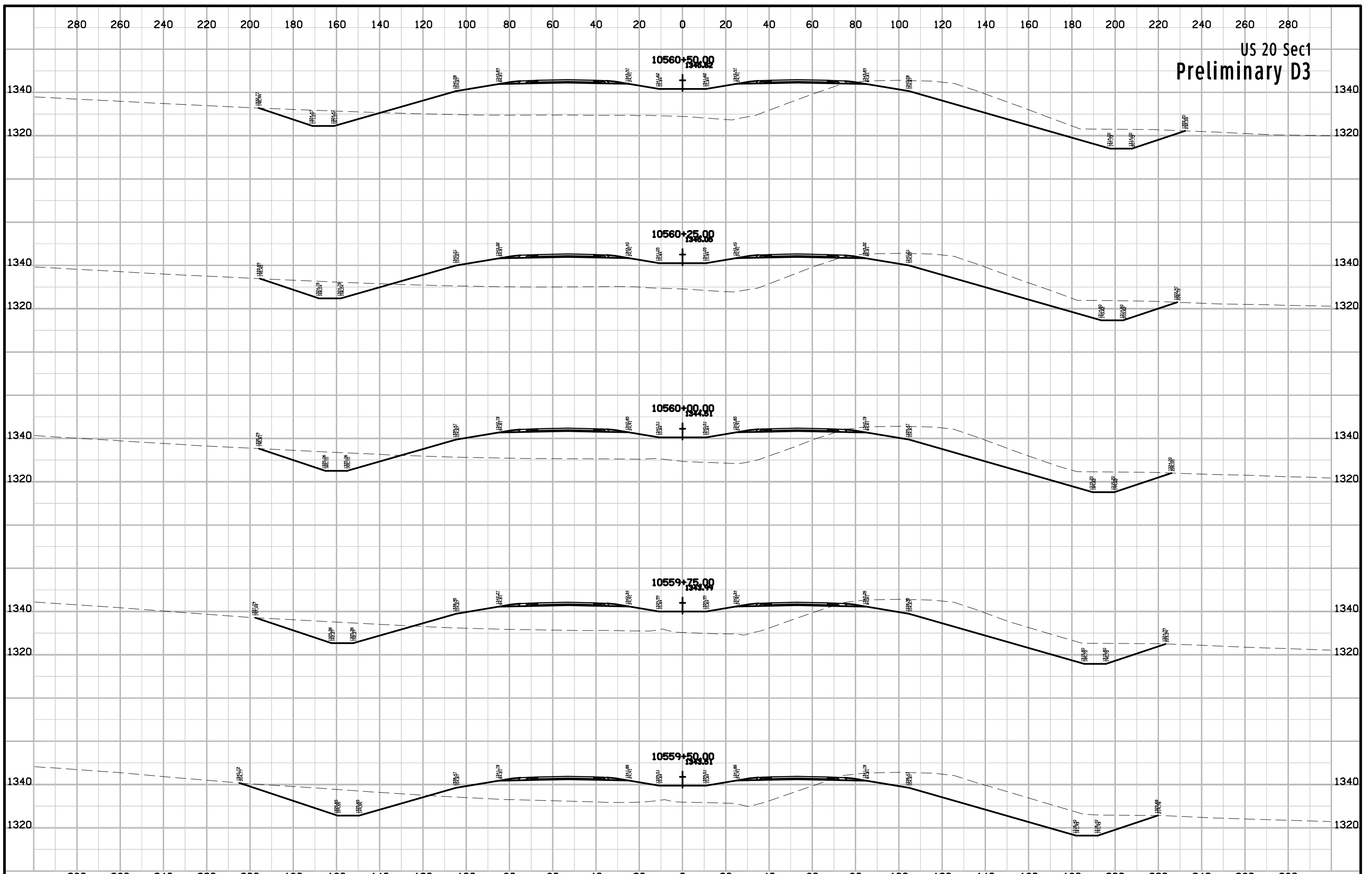
US 20 Sec1
Preliminary D3



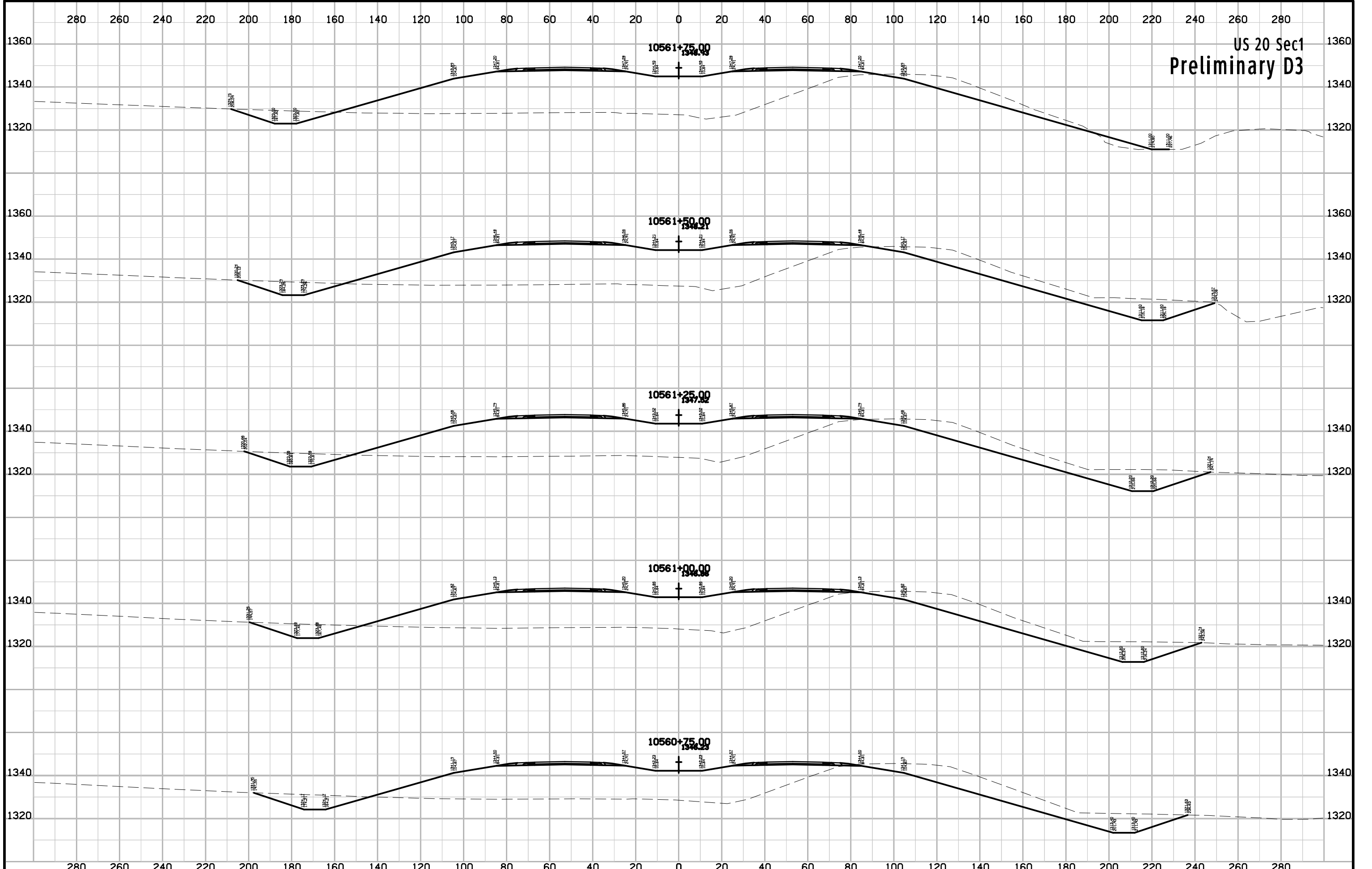
US 20 Sec1
Preliminary D3

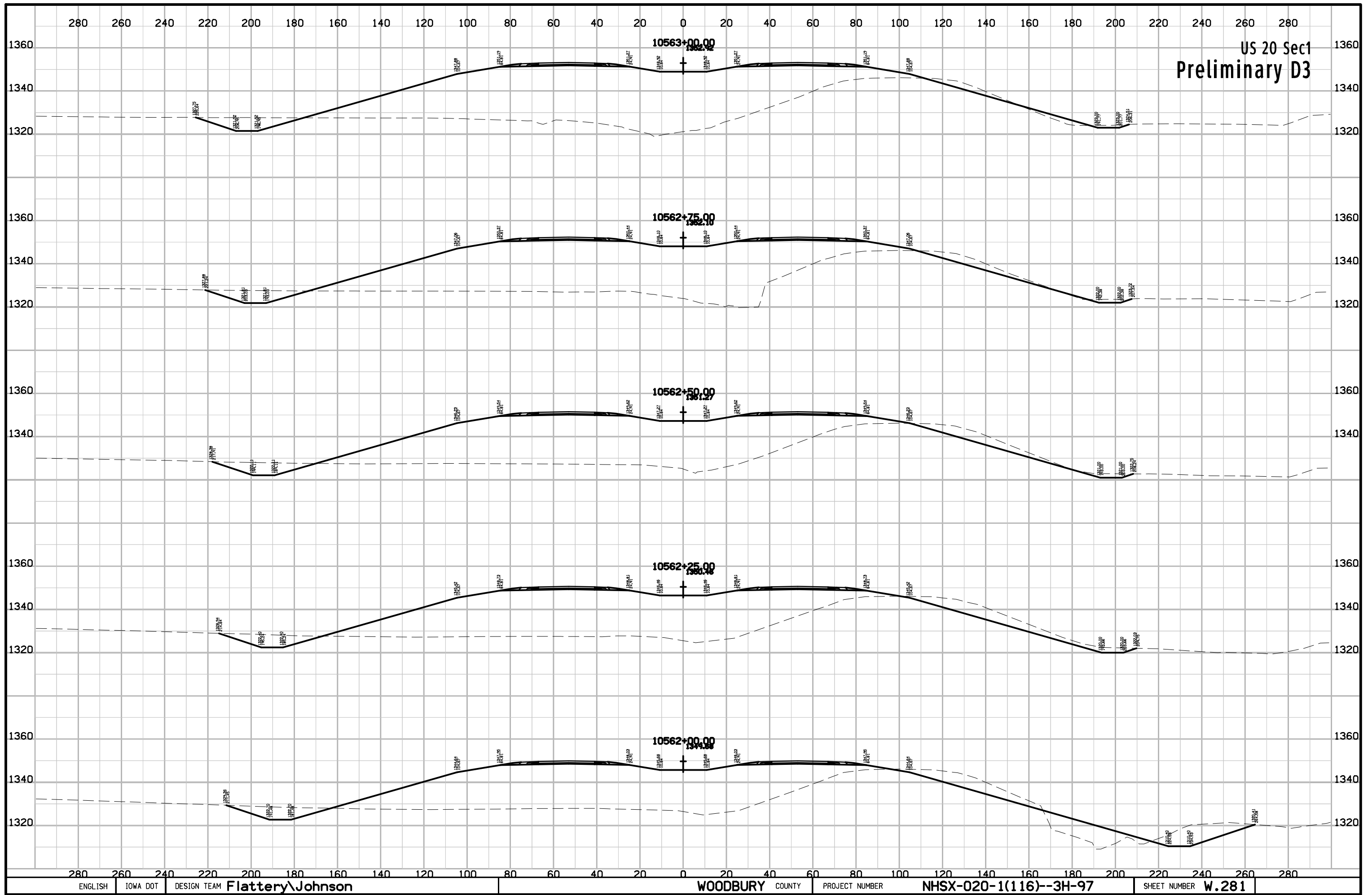


US 20 Sec1
Preliminary D3

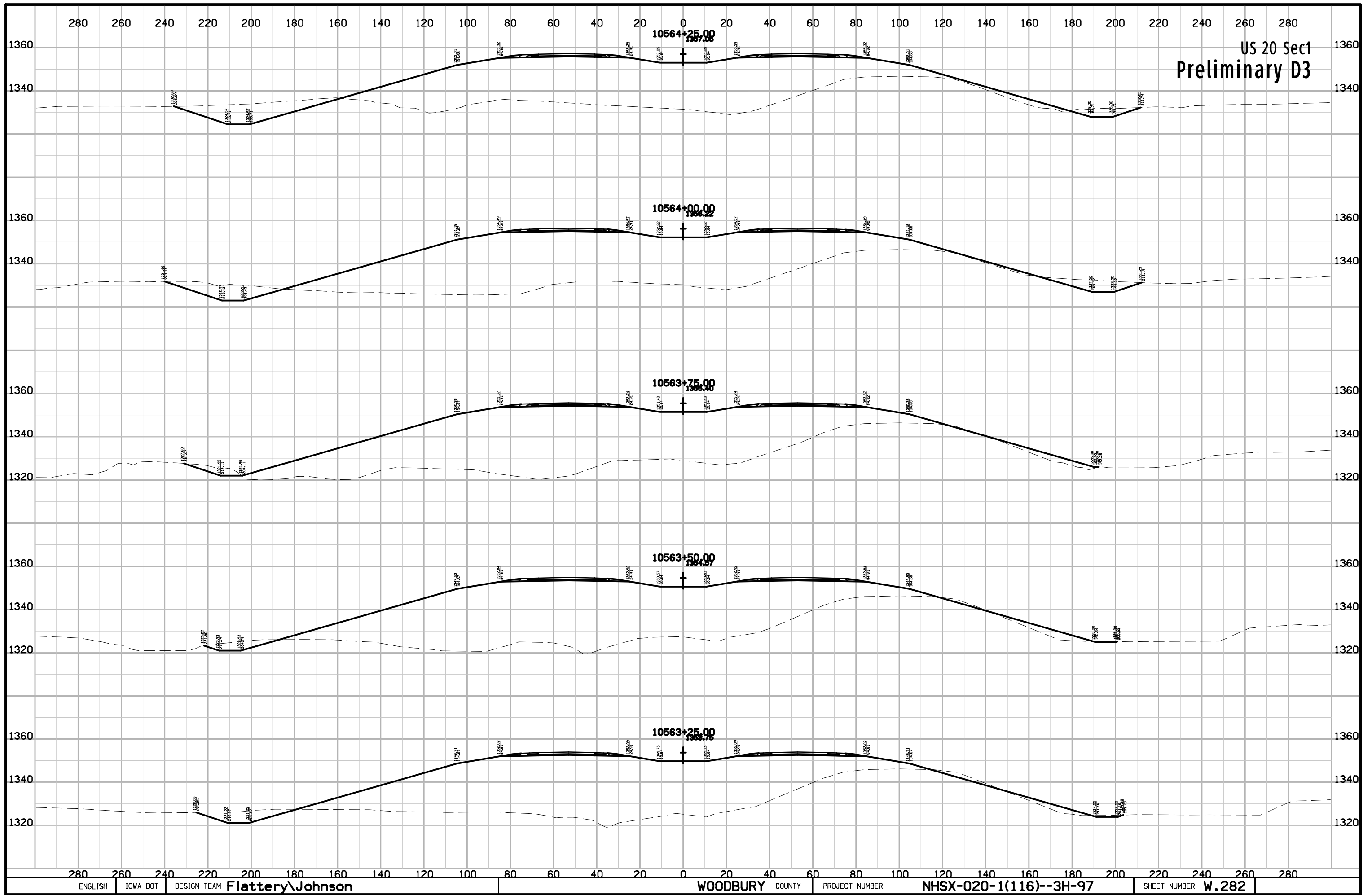


US 20 Sec1
Preliminary D3



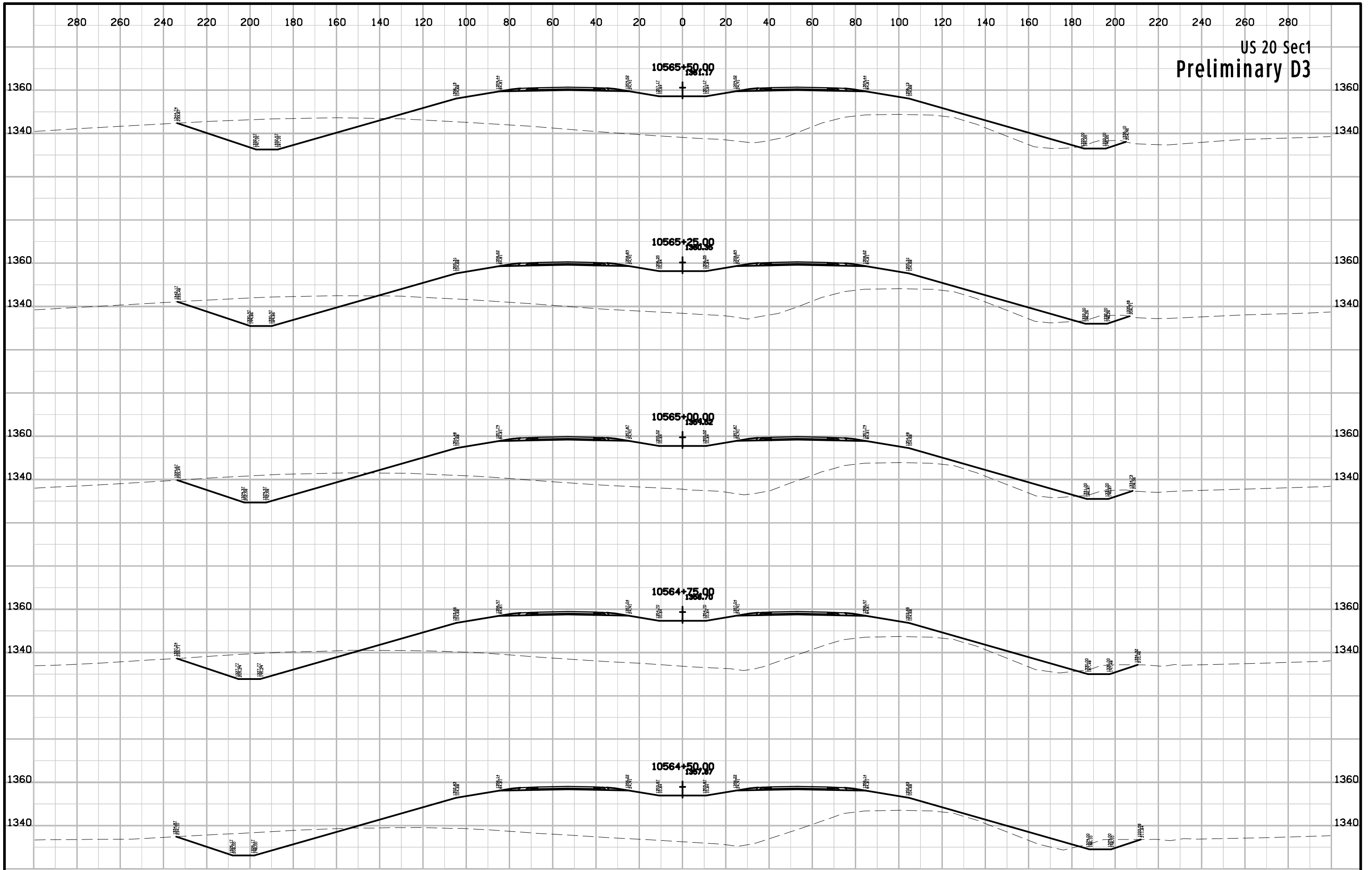


US 20 Sec1
Preliminary D3

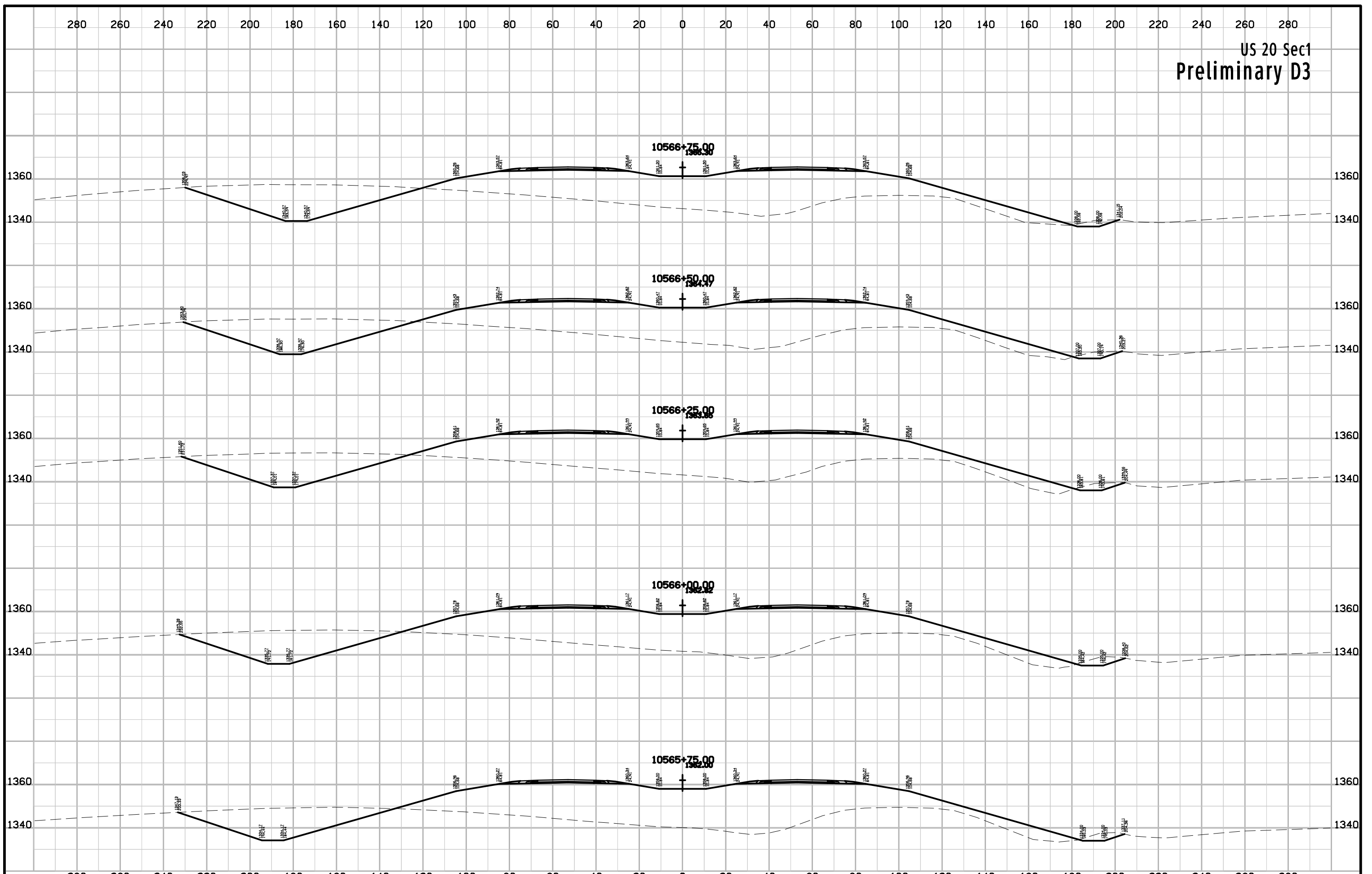


US 20 Sec1
Preliminary D3

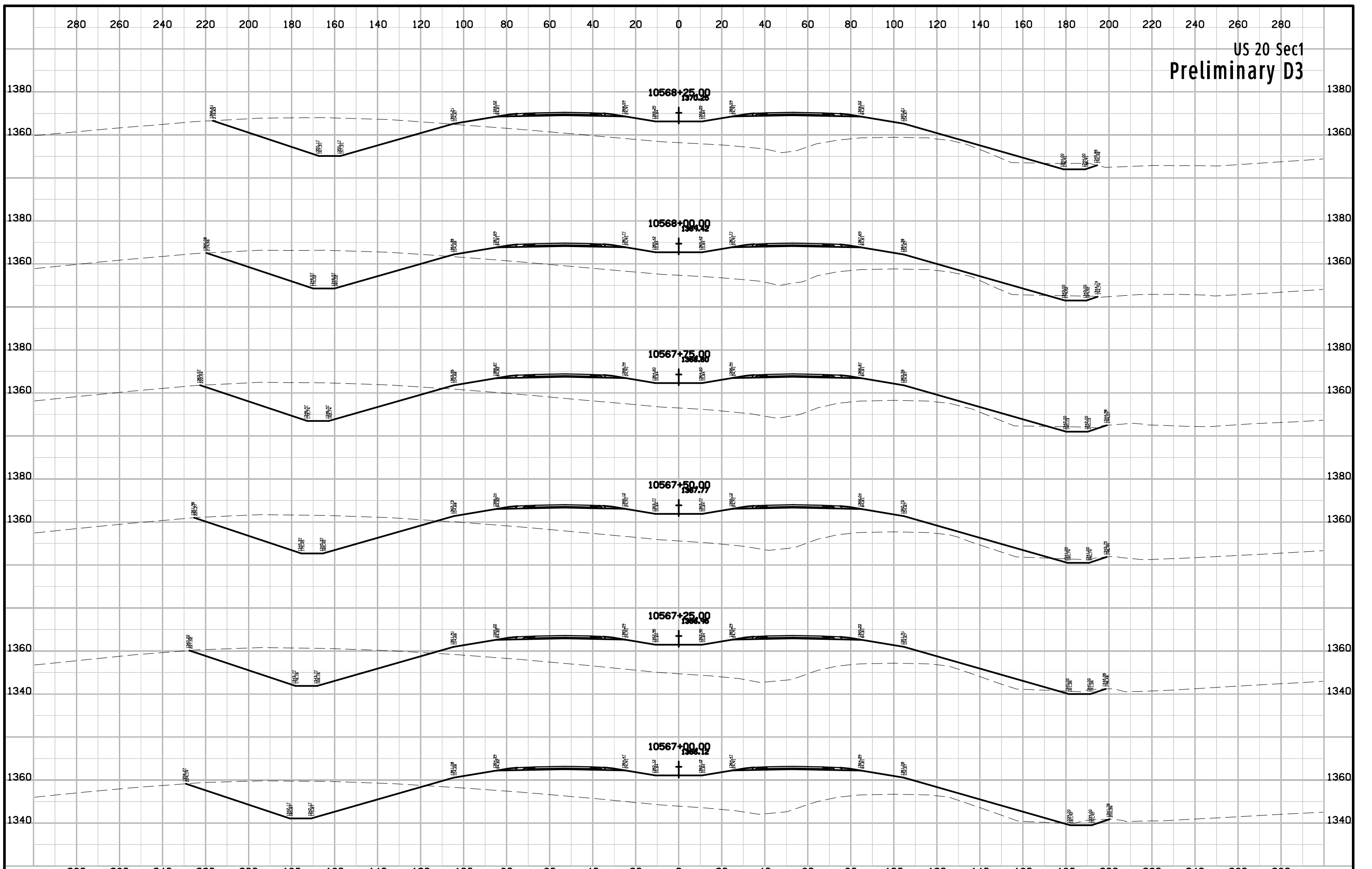
US 20 Sec1
Preliminary D3



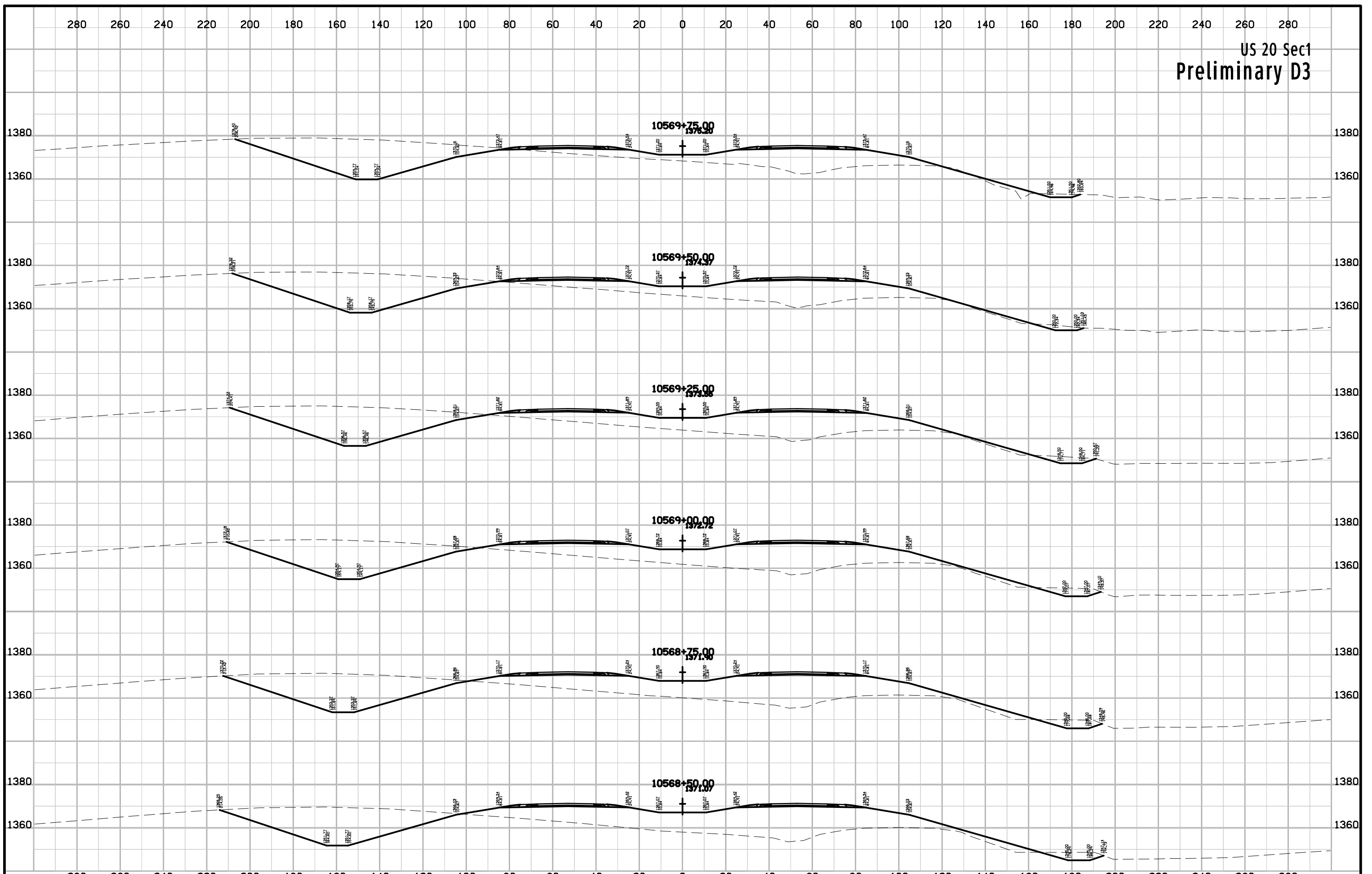
US 20 Sec1
Preliminary D3



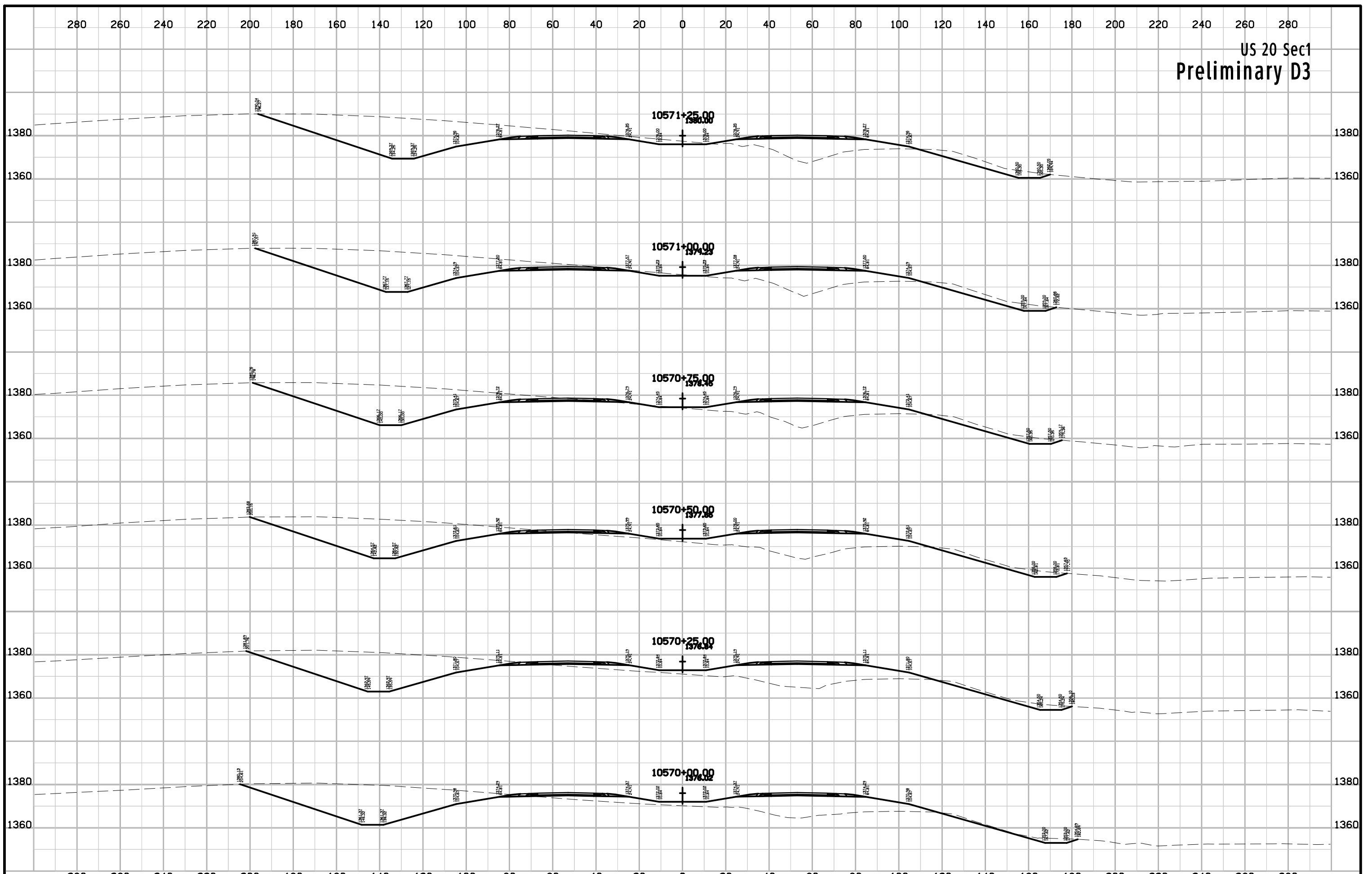
US 20 Sec1
Preliminary D3



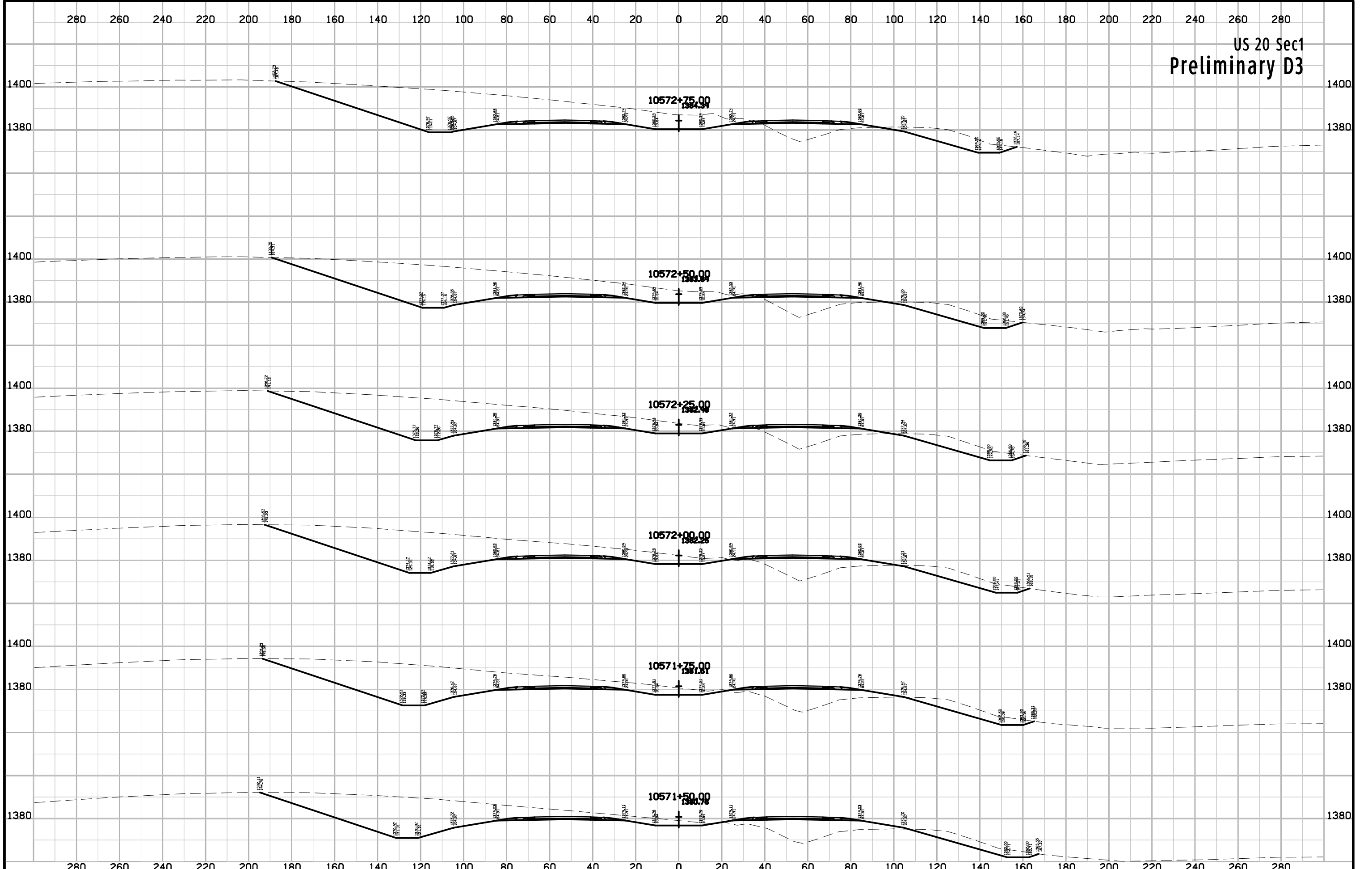
US 20 Sec1
Preliminary D3



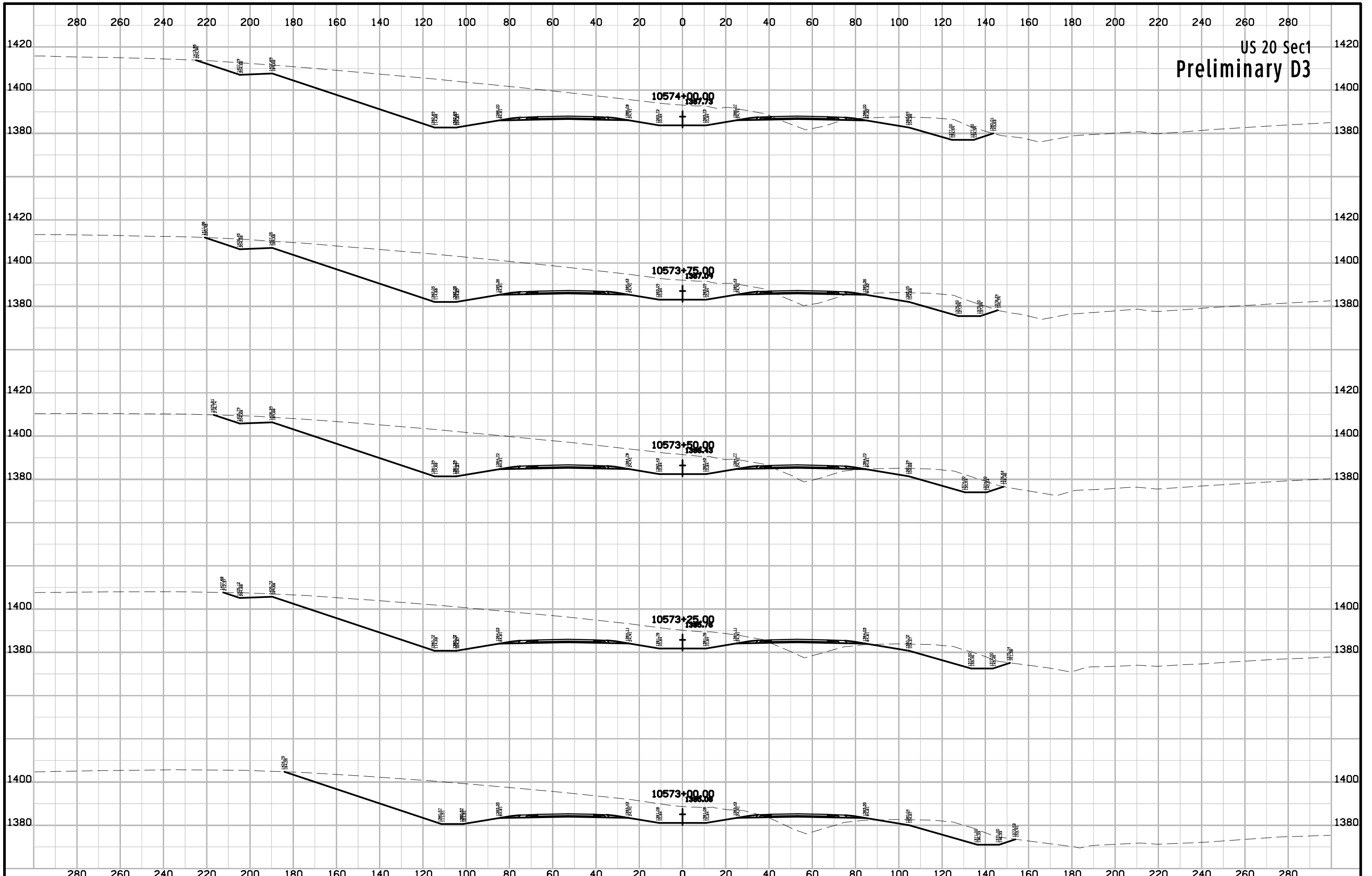
US 20 Sec1
Preliminary D3



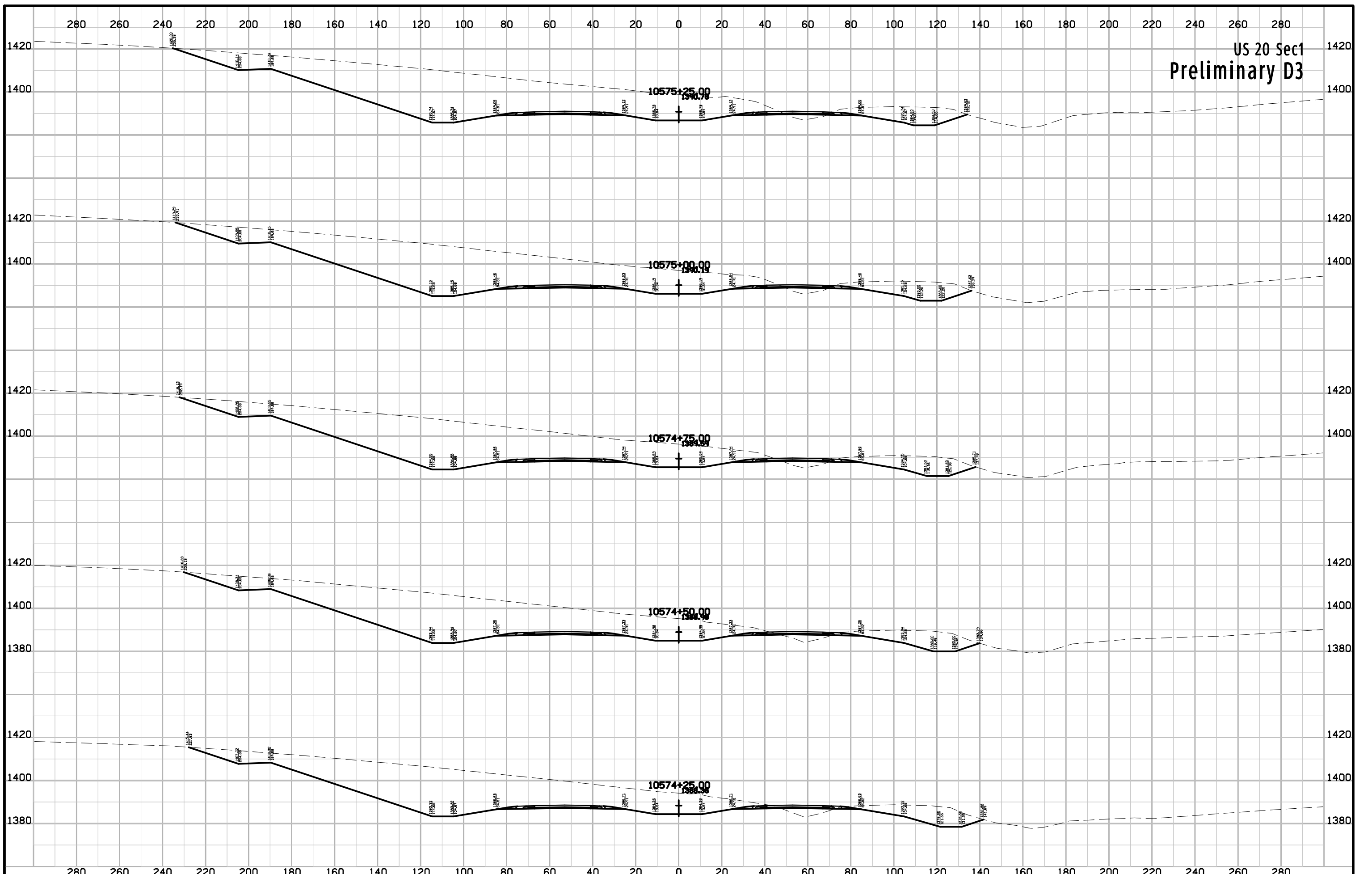
US 20 Sec1
Preliminary D3



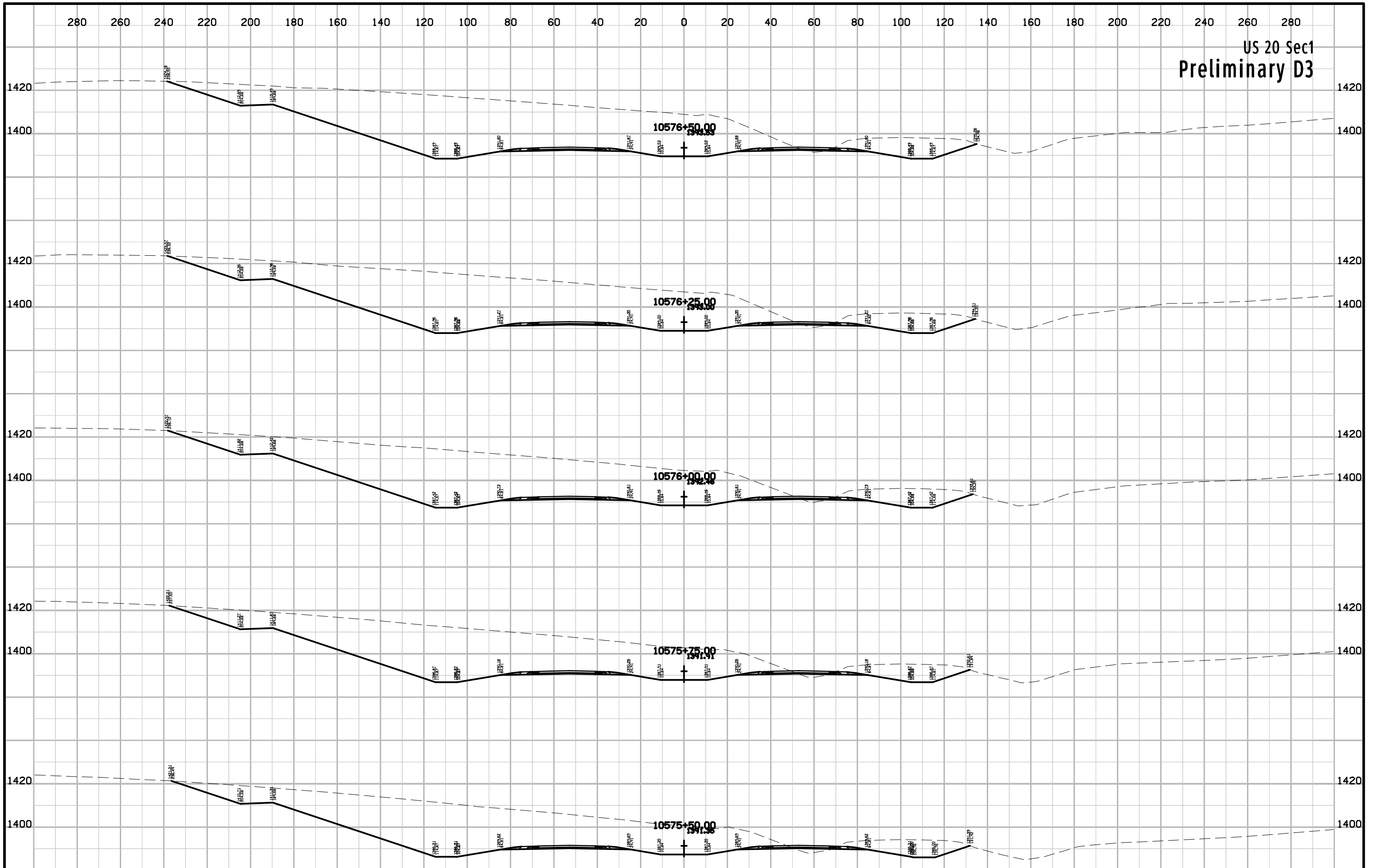
US 20 Sec1
Preliminary D3



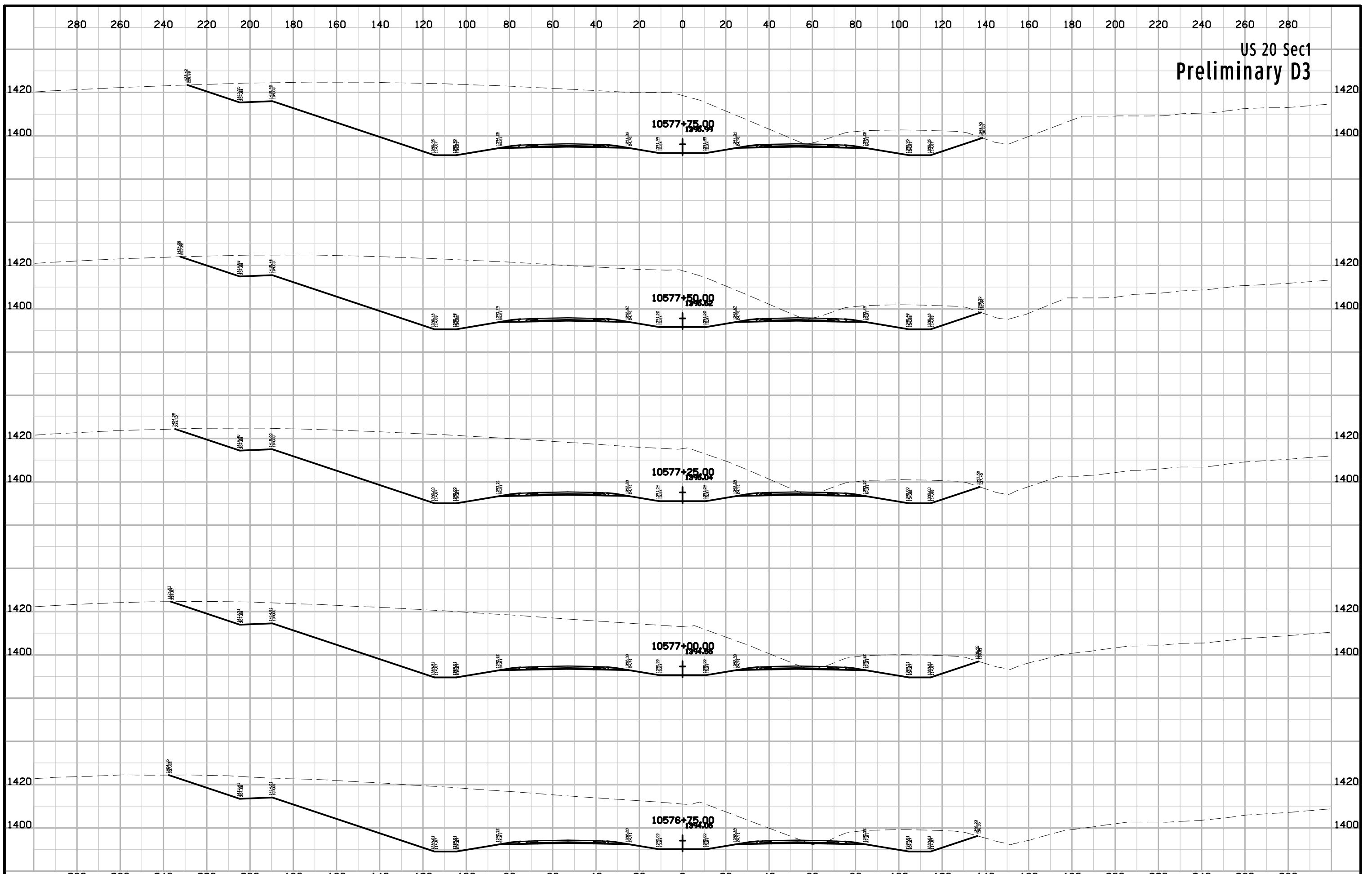
US 20 Sec1
Preliminary D3



US 20 Sec1
Preliminary D3

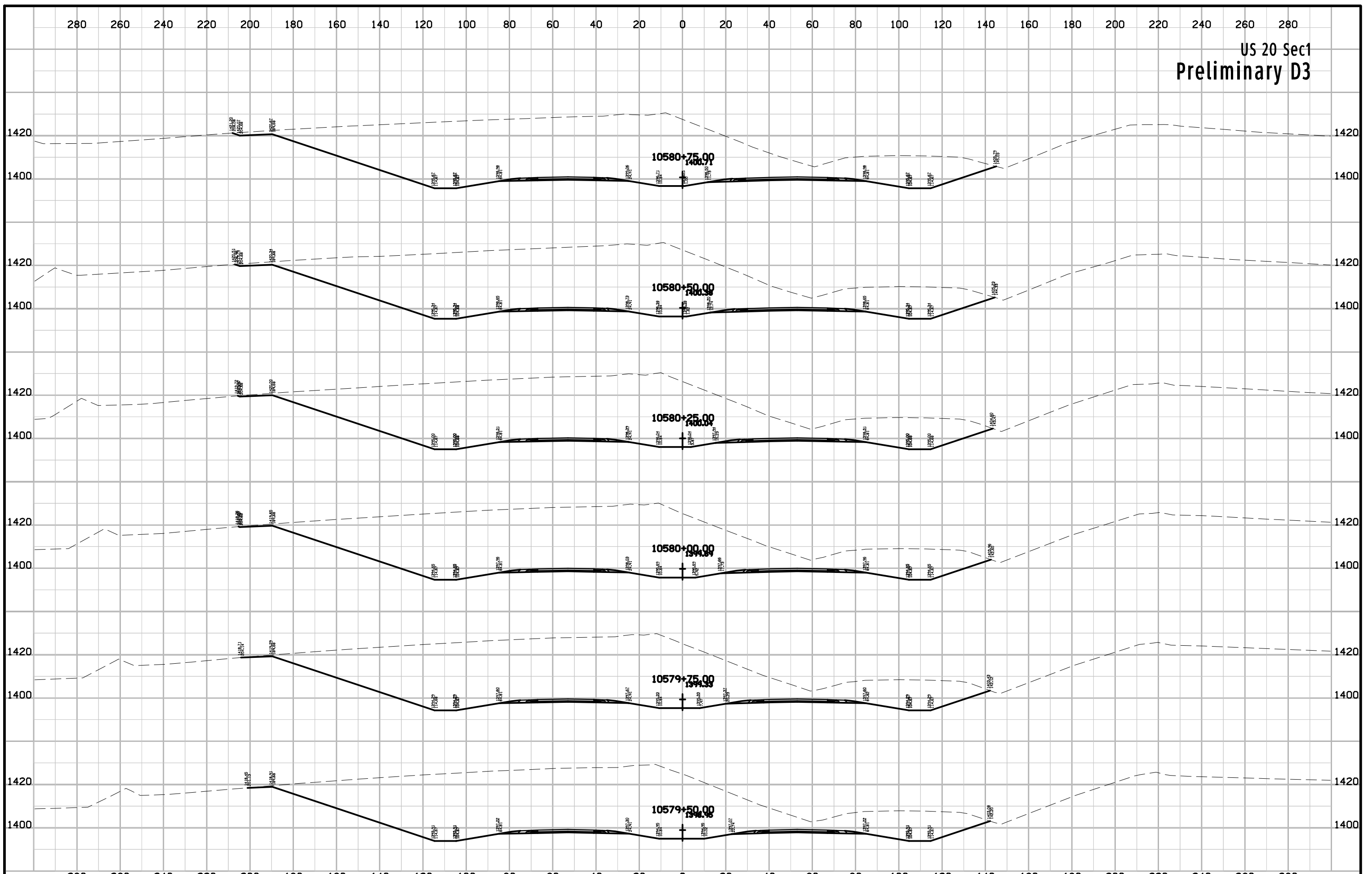


US 20 Sec1
Preliminary D3

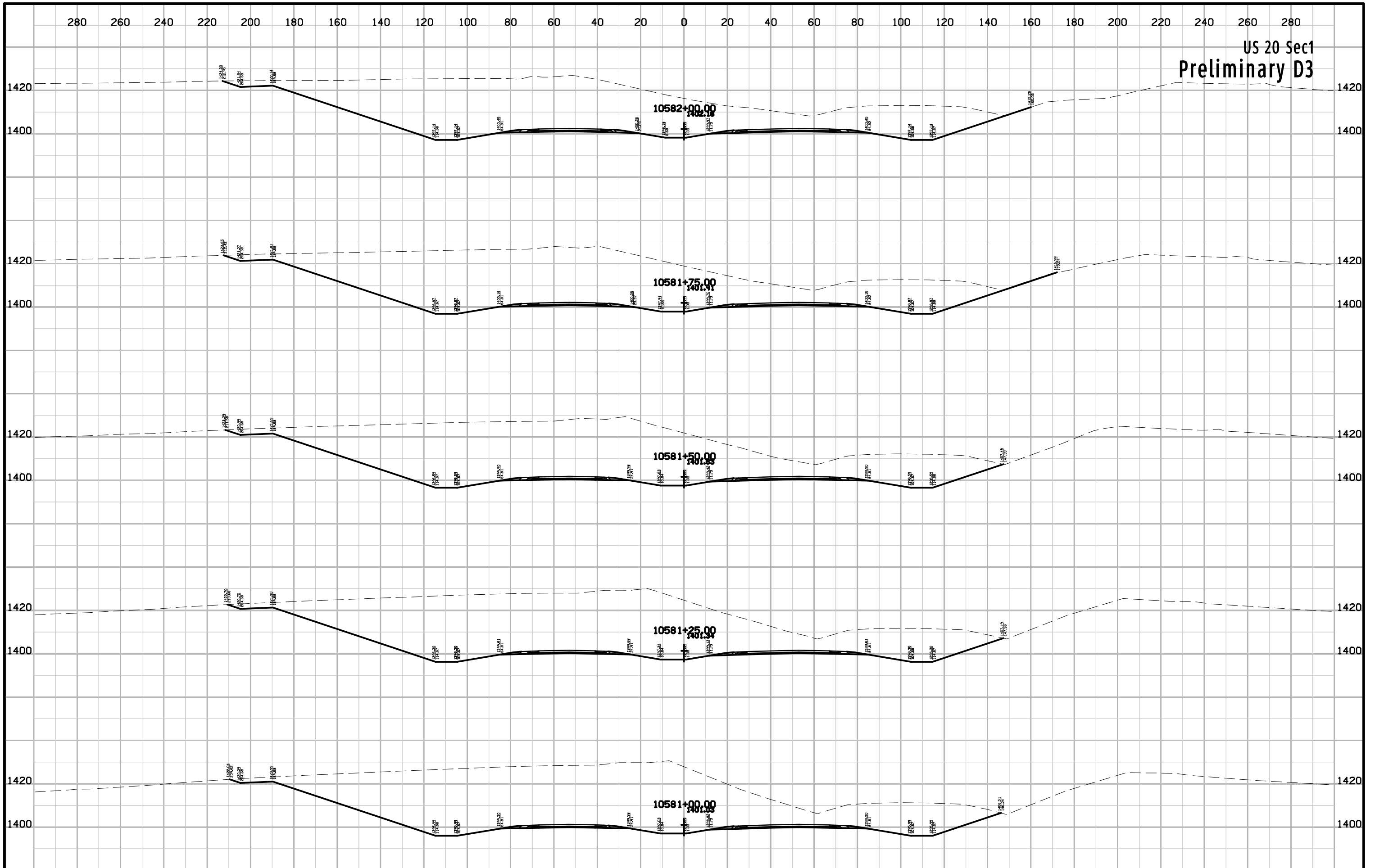


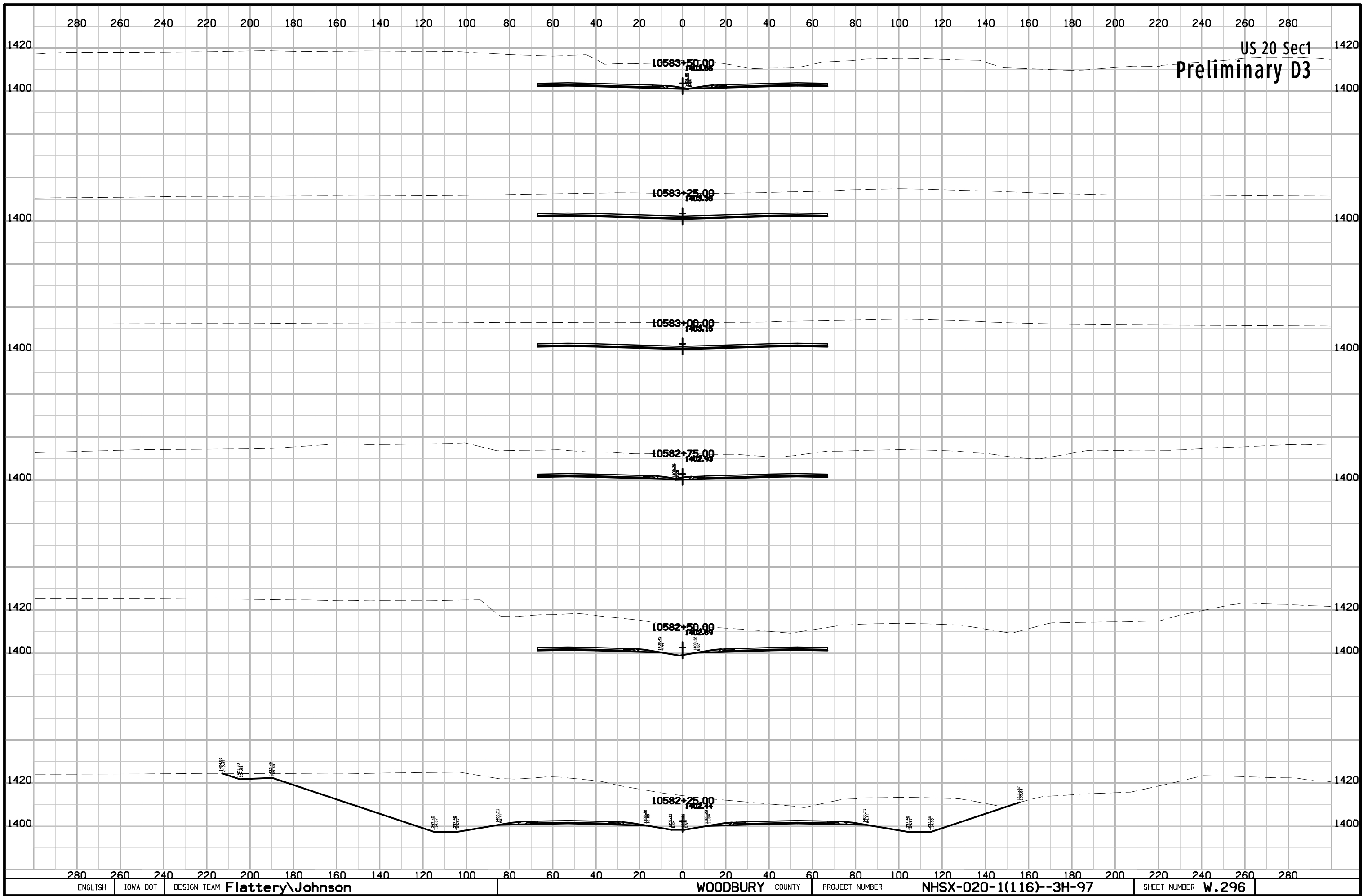


US 20 Sec1
Preliminary D3



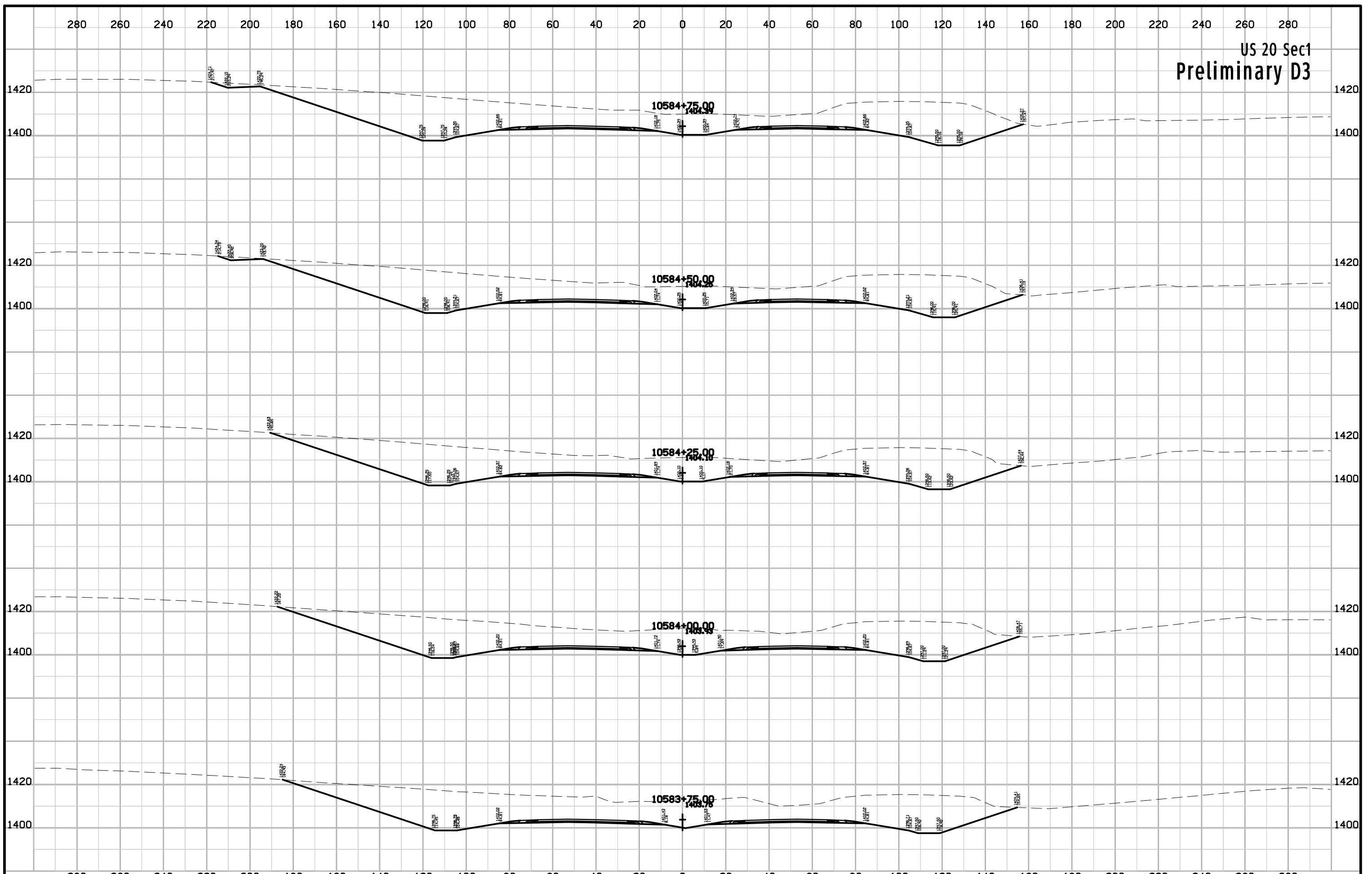
US 20 Sec1
Preliminary D3



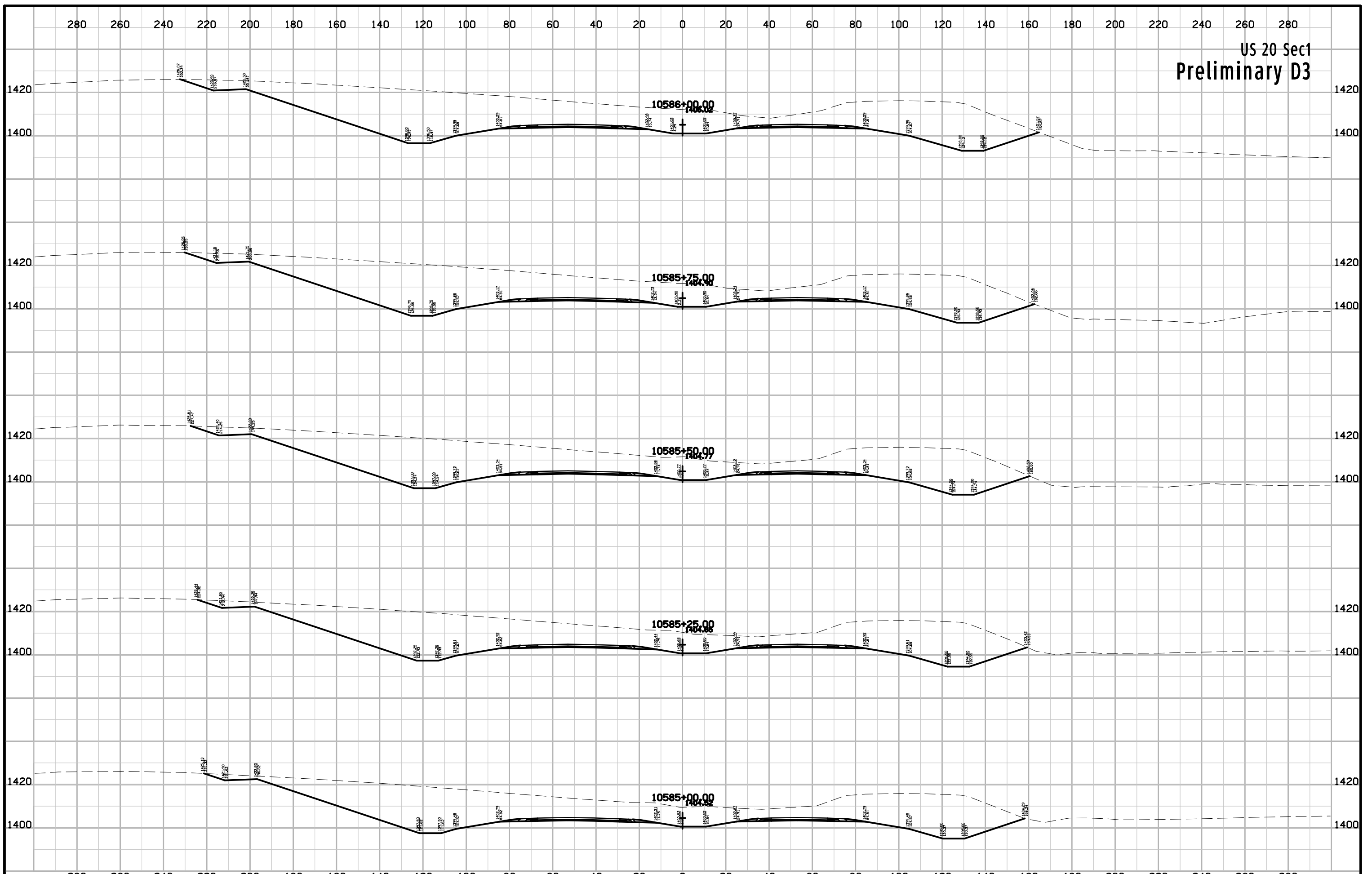


US 20 Sec1
Preliminary D3

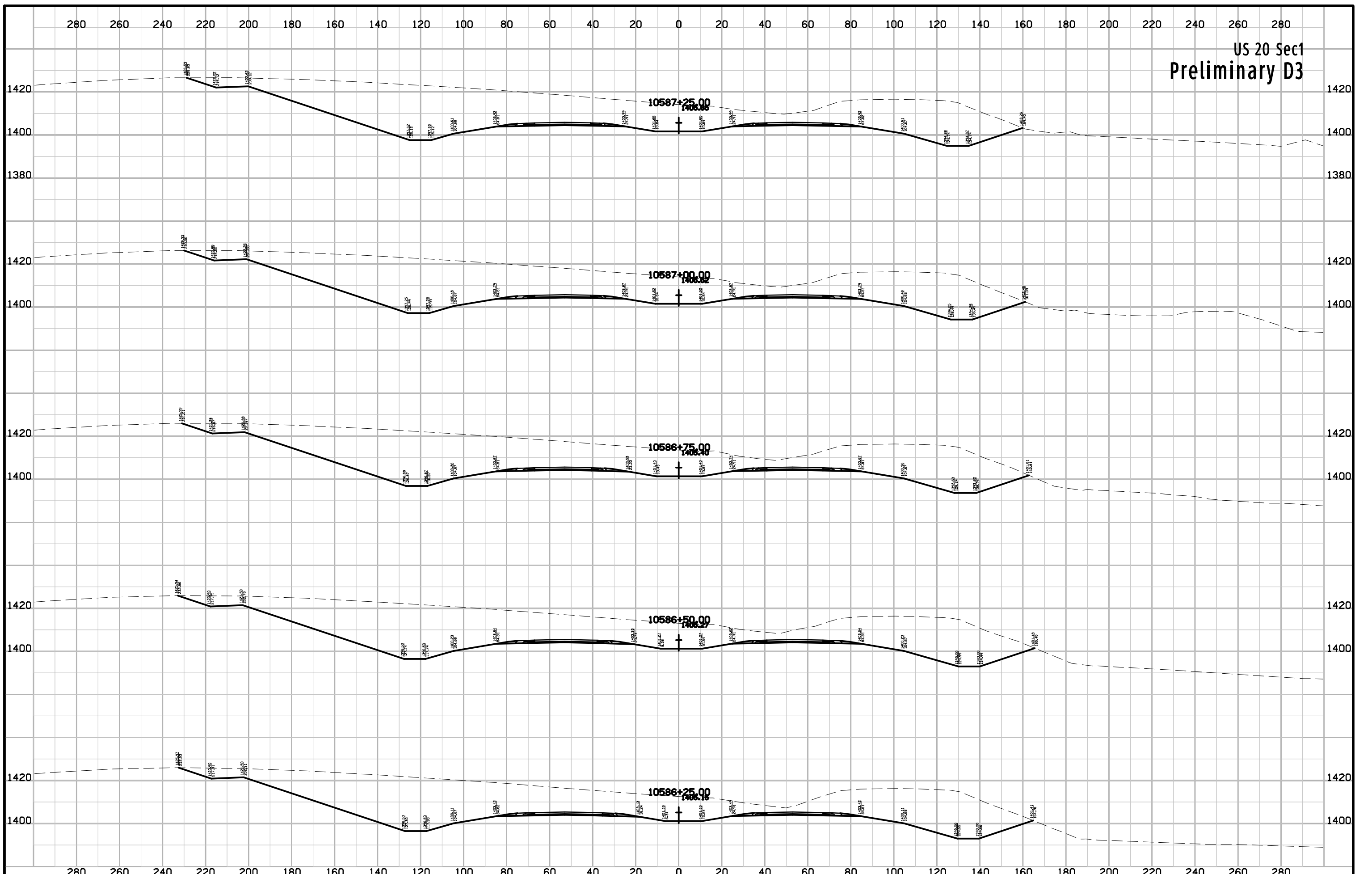
US 20 Sec1
Preliminary D3



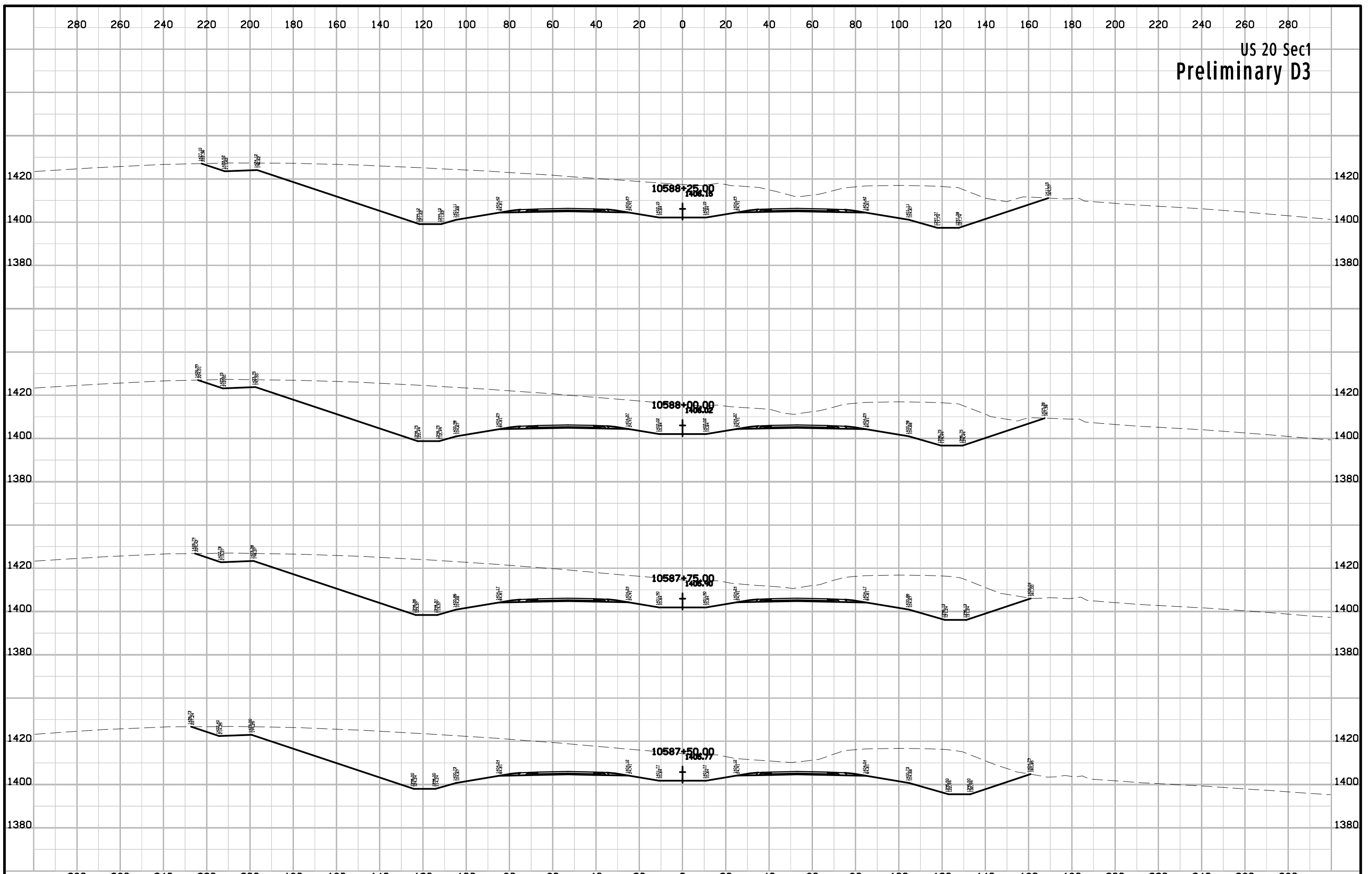
US 20 Sec1
Preliminary D3



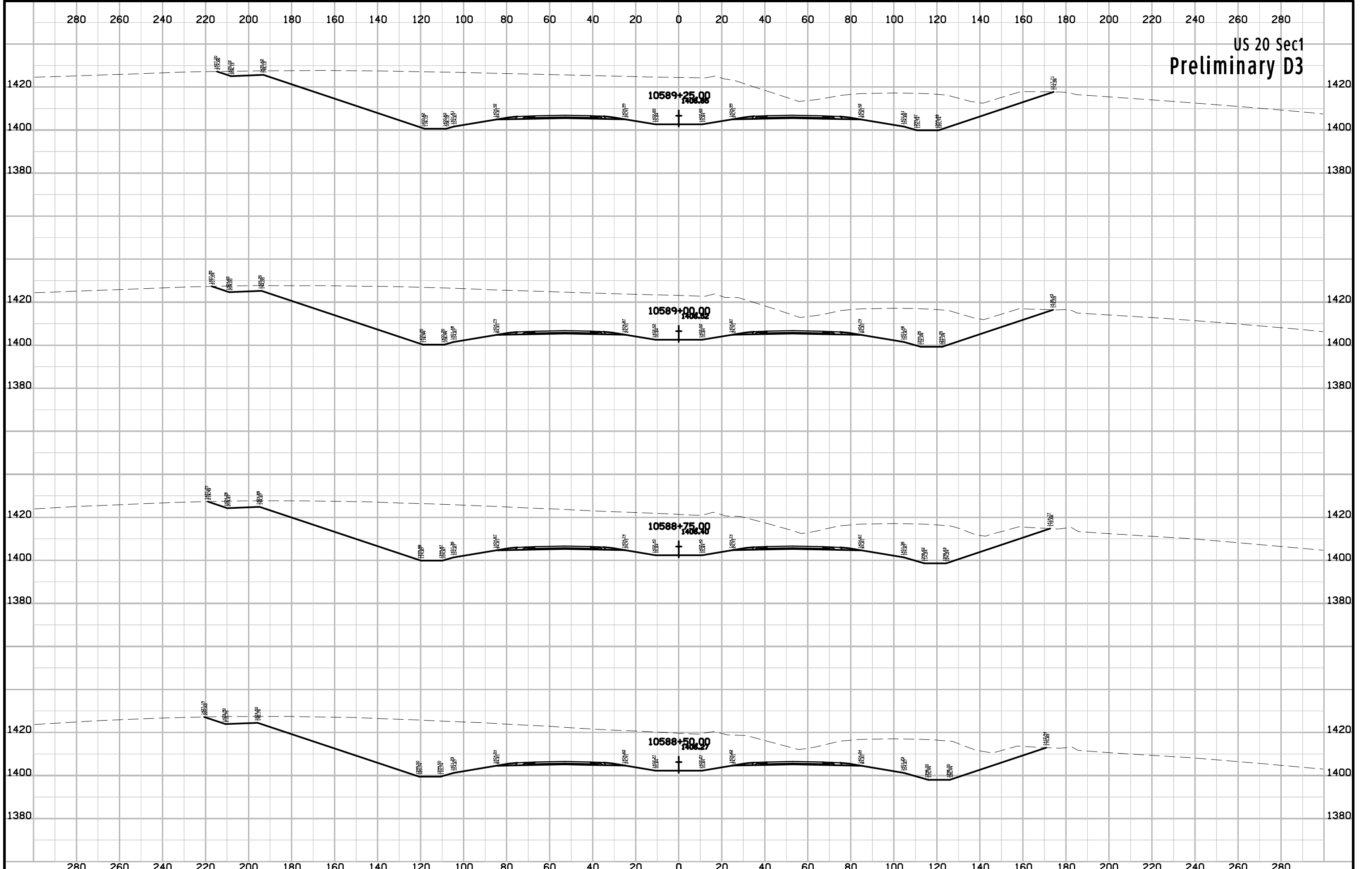
US 20 Sec1
Preliminary D3



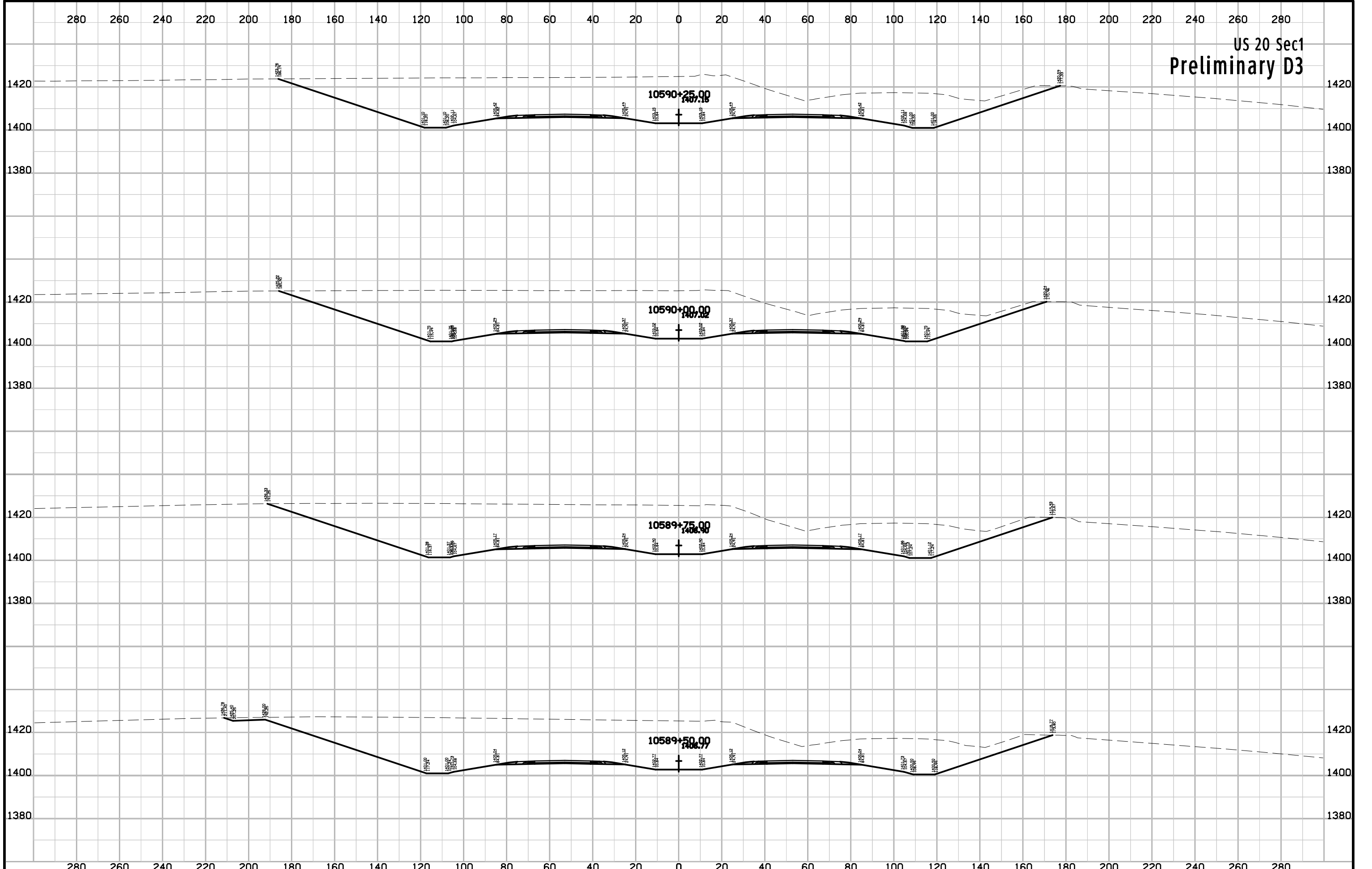
US 20 Sec1
Preliminary D3

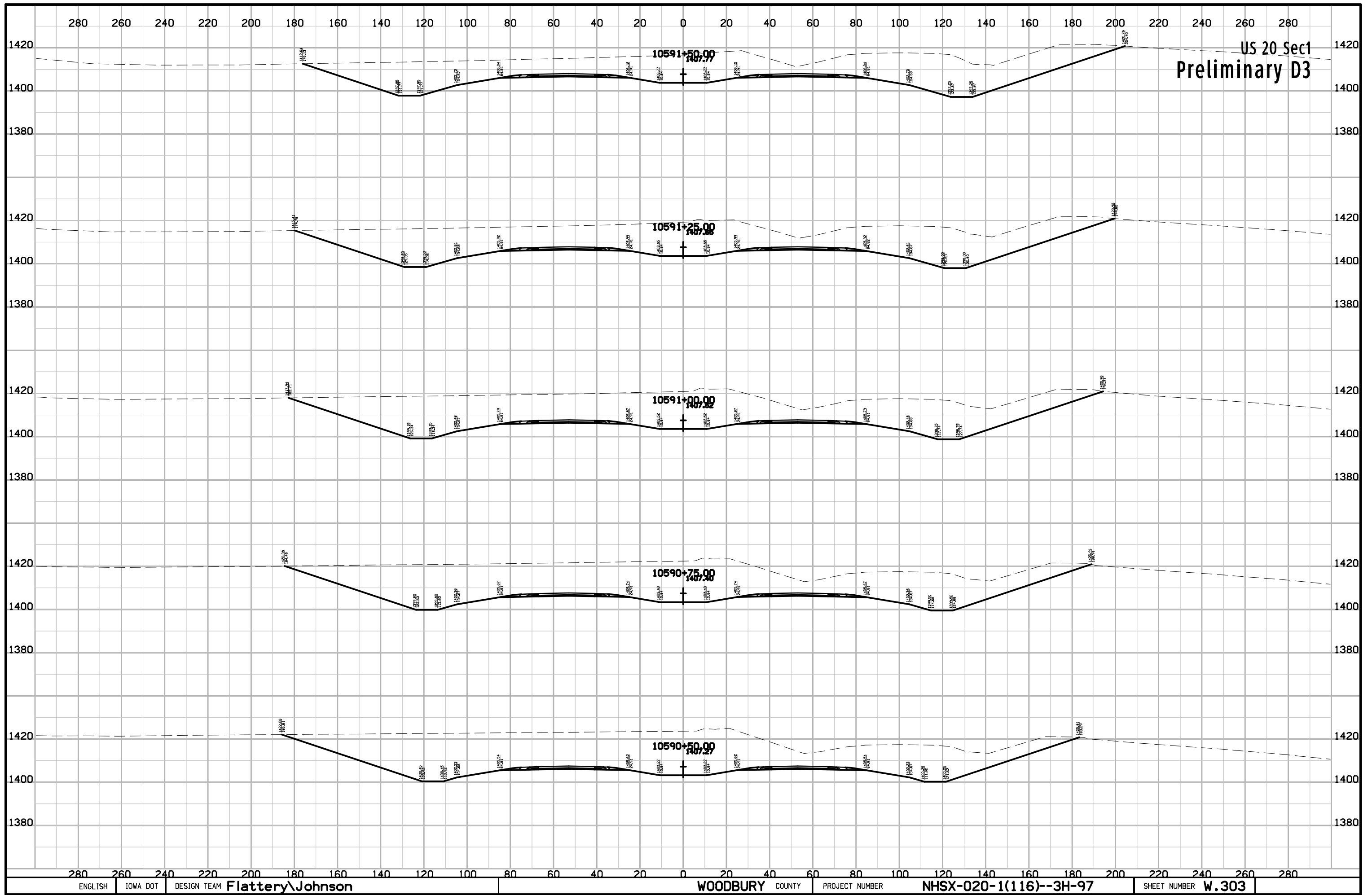


US 20 Sec1
Preliminary D3

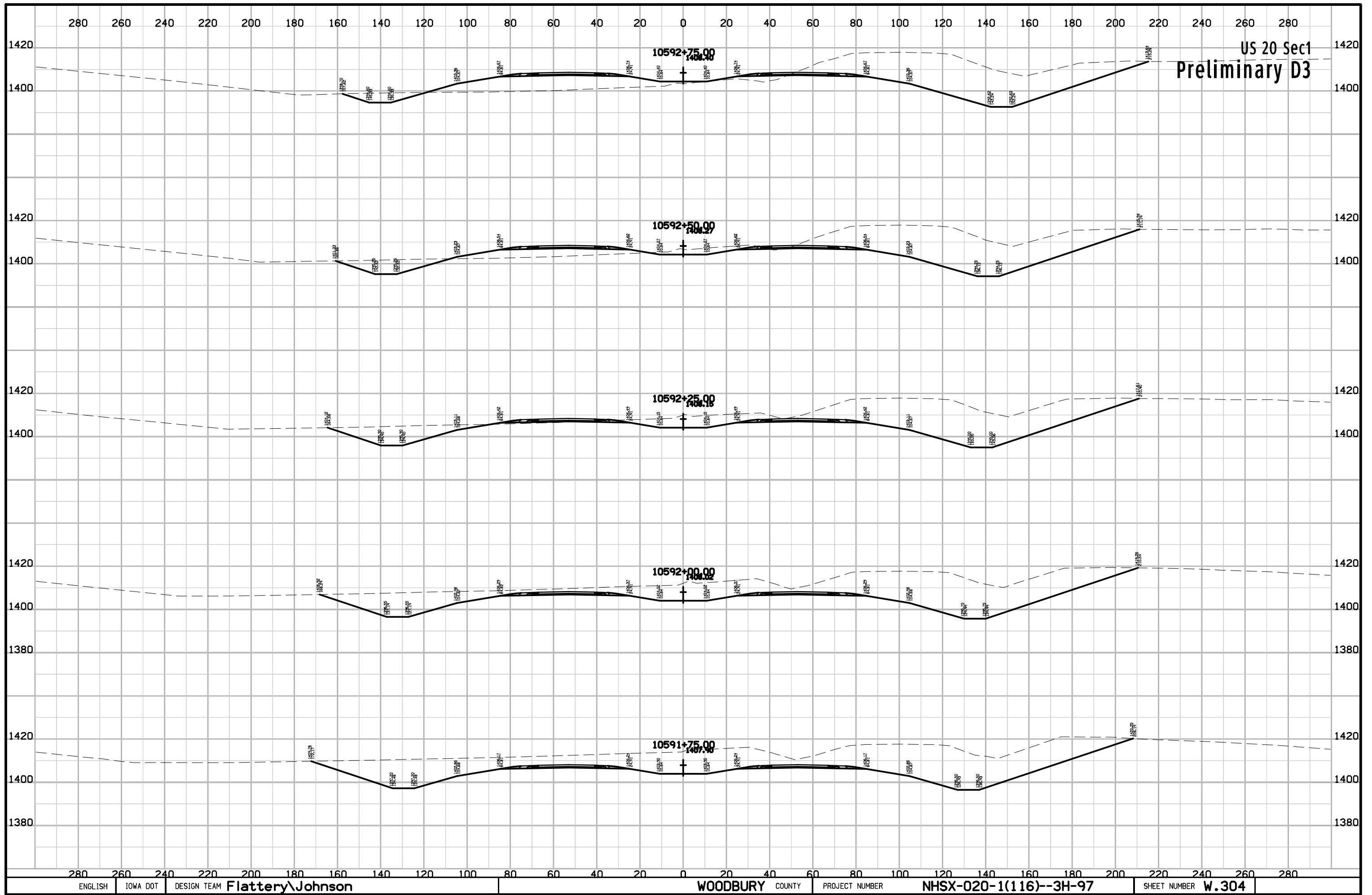


US 20 Sec1
Preliminary D3



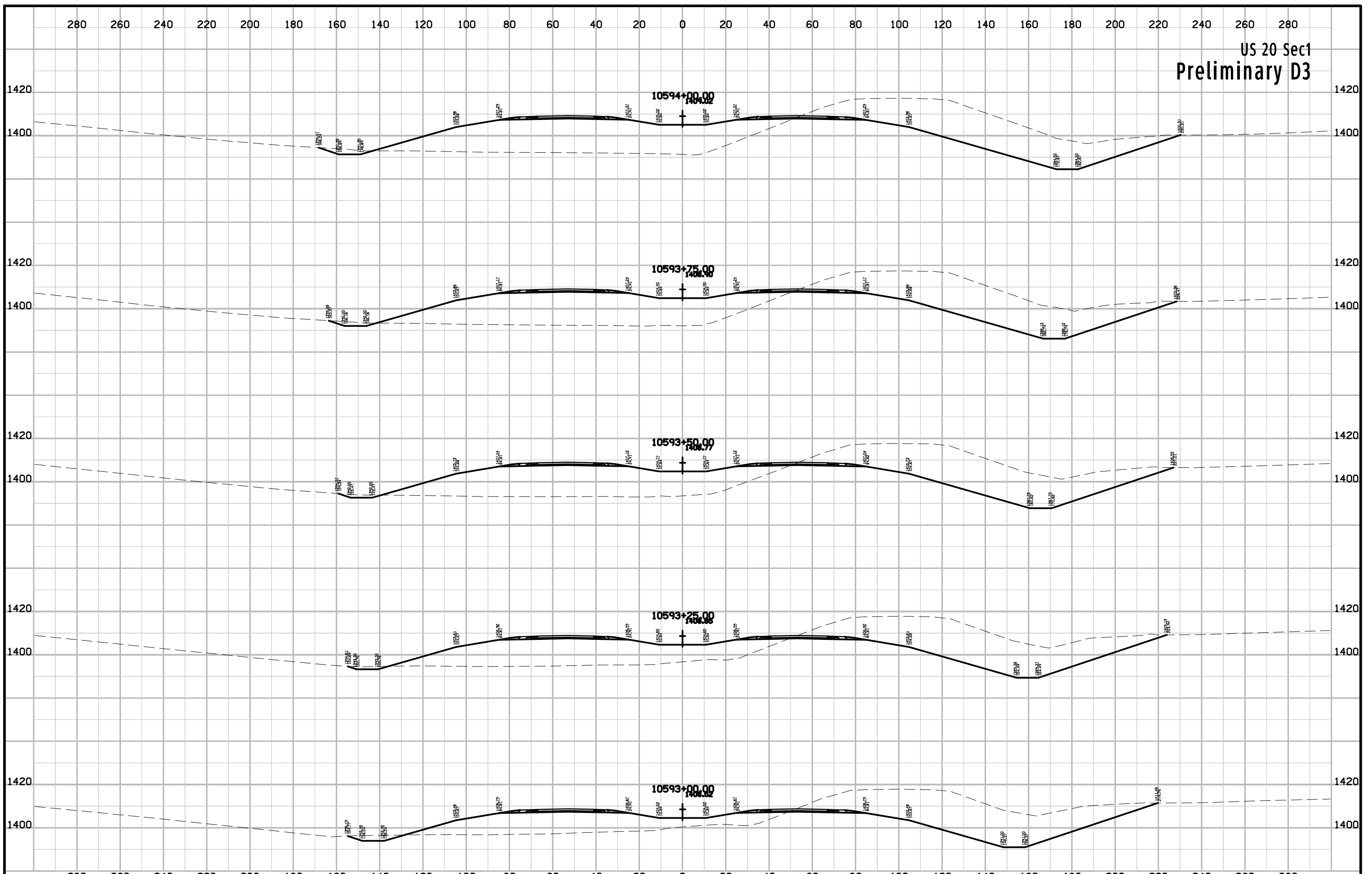


US 20 Sec1
Preliminary D3

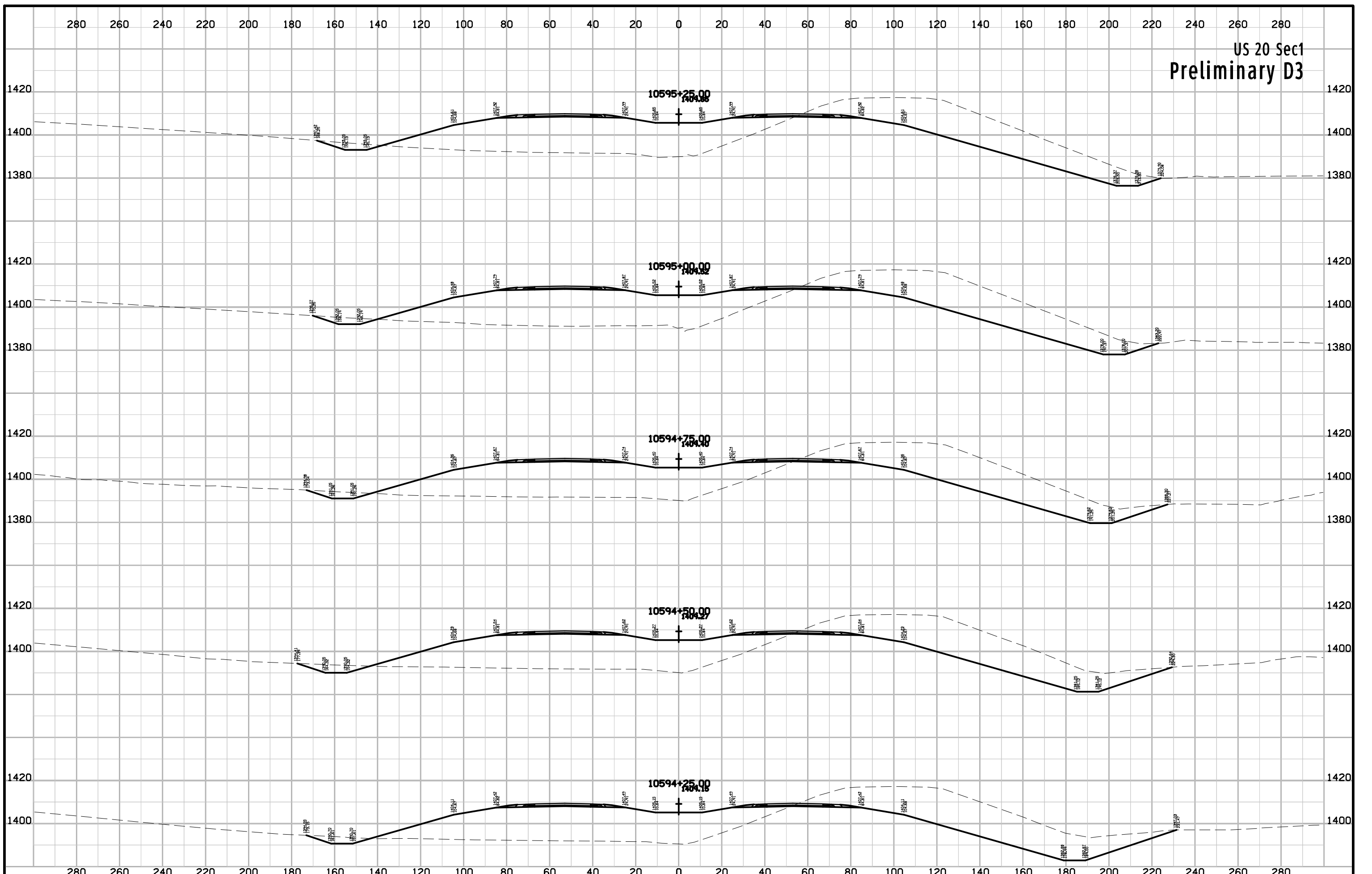


US 20 Sec1
Preliminary D3

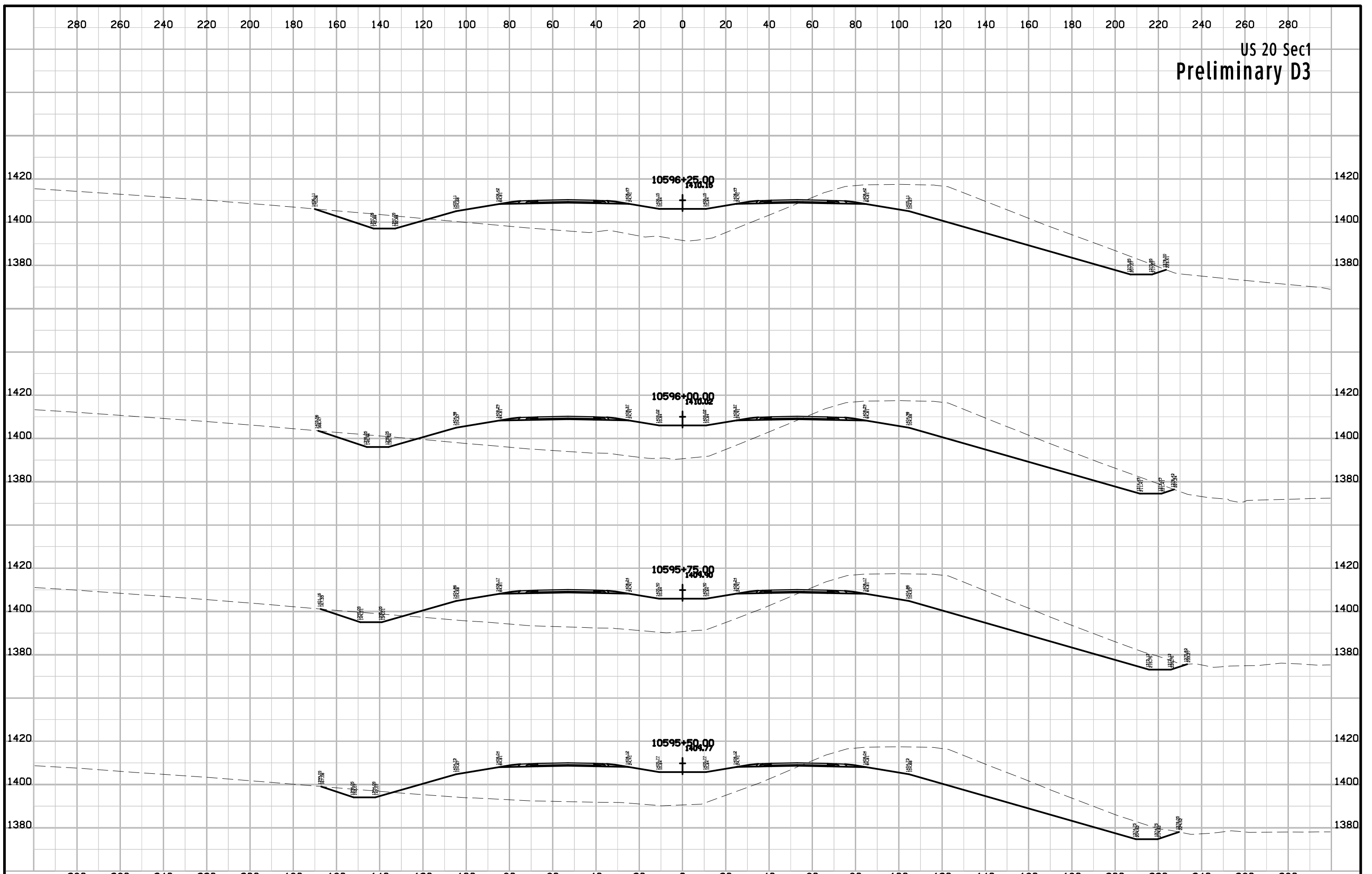
US 20 Sec1
Preliminary D3



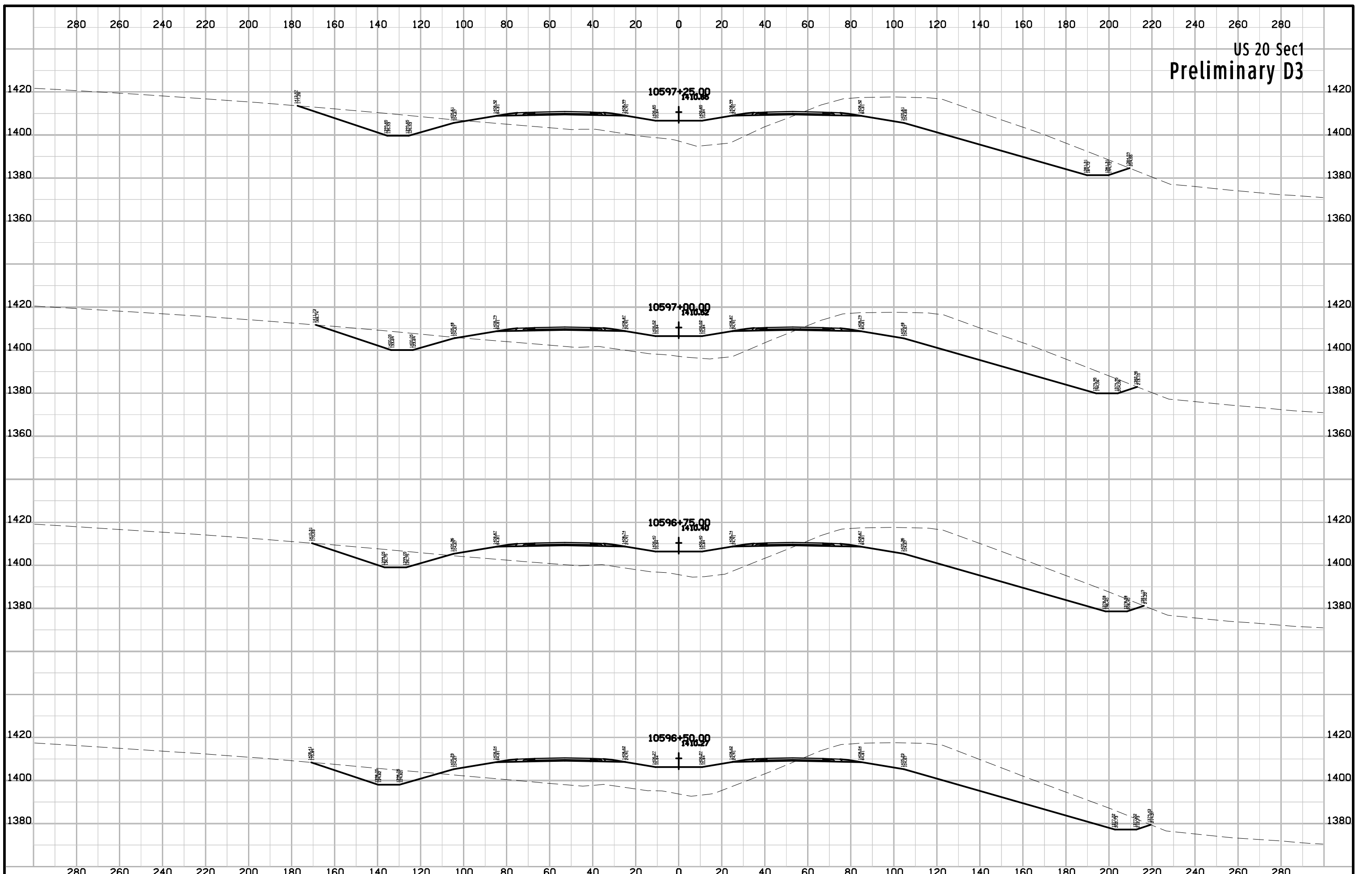
US 20 Sec1
Preliminary D3



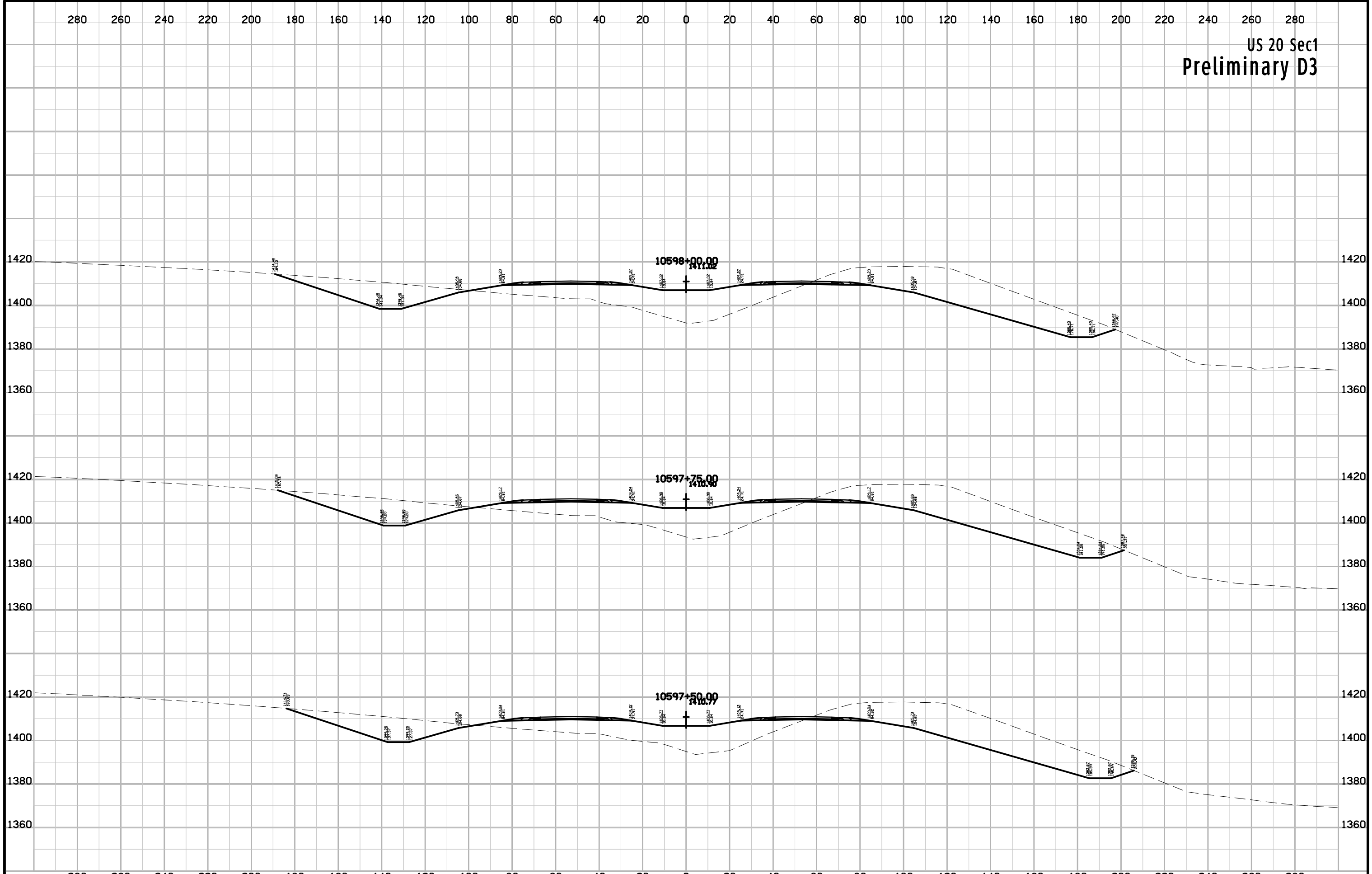
US 20 Sec1
Preliminary D3



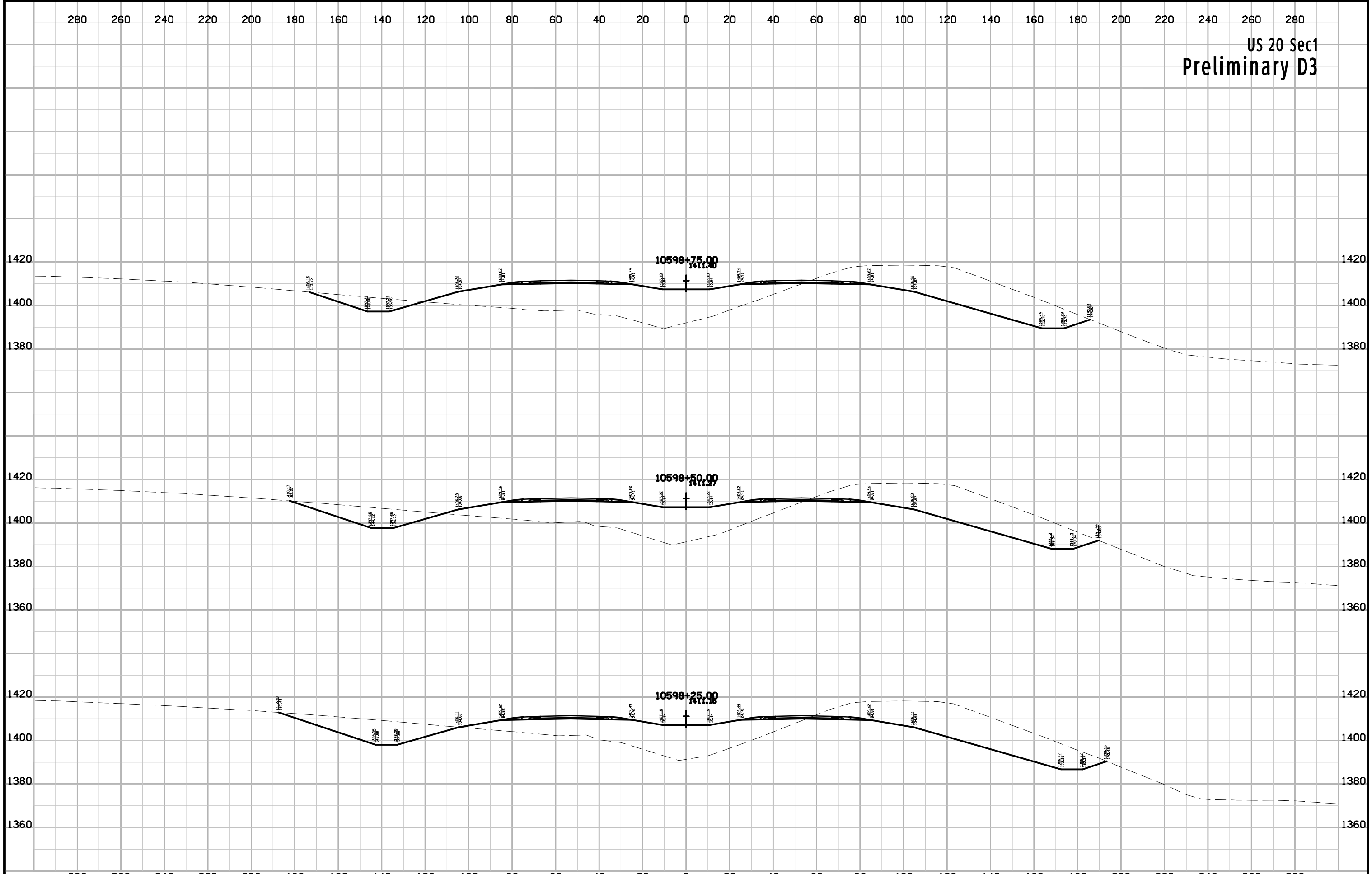
US 20 Sec1
Preliminary D3



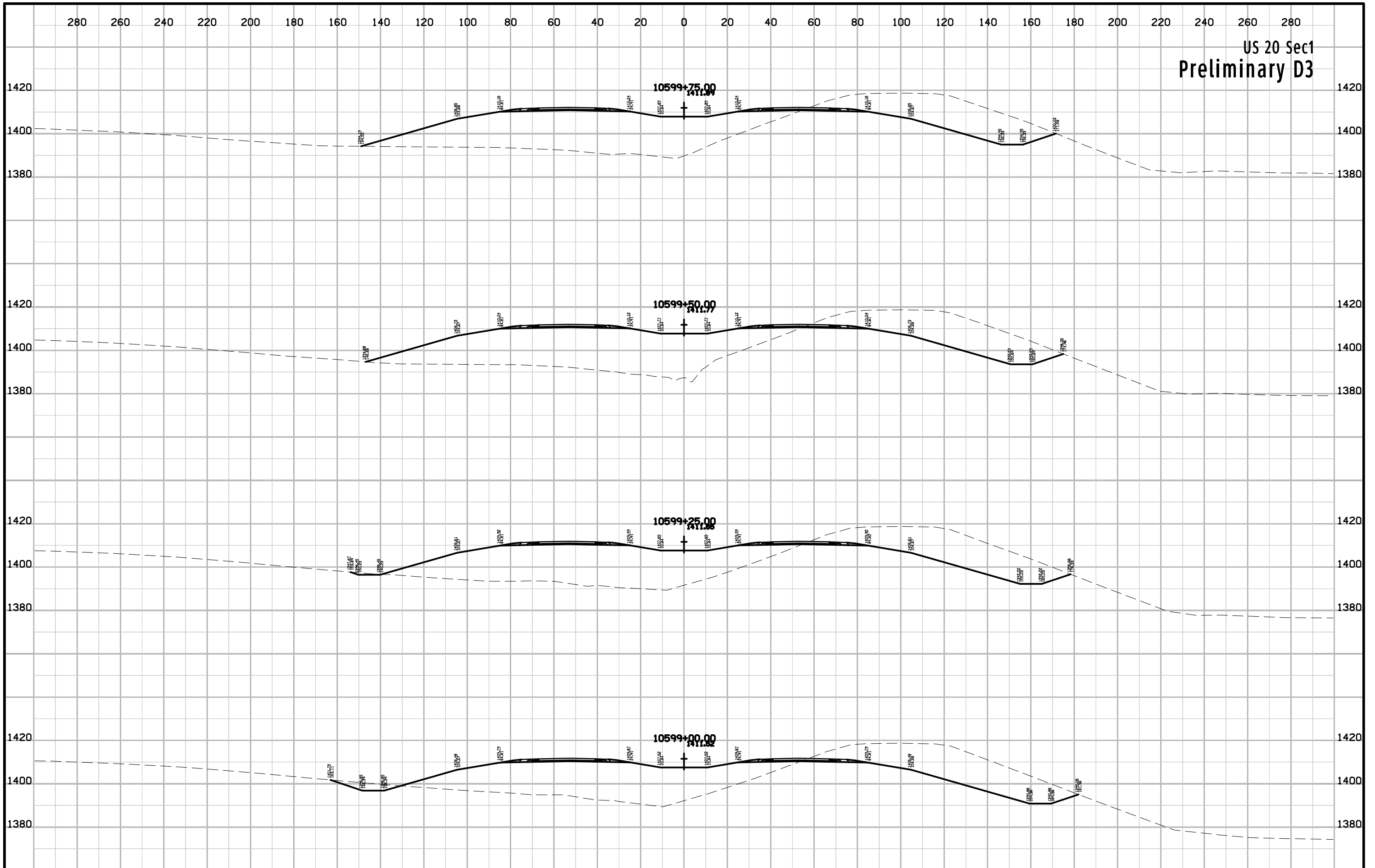
US 20 Sec1
Preliminary D3



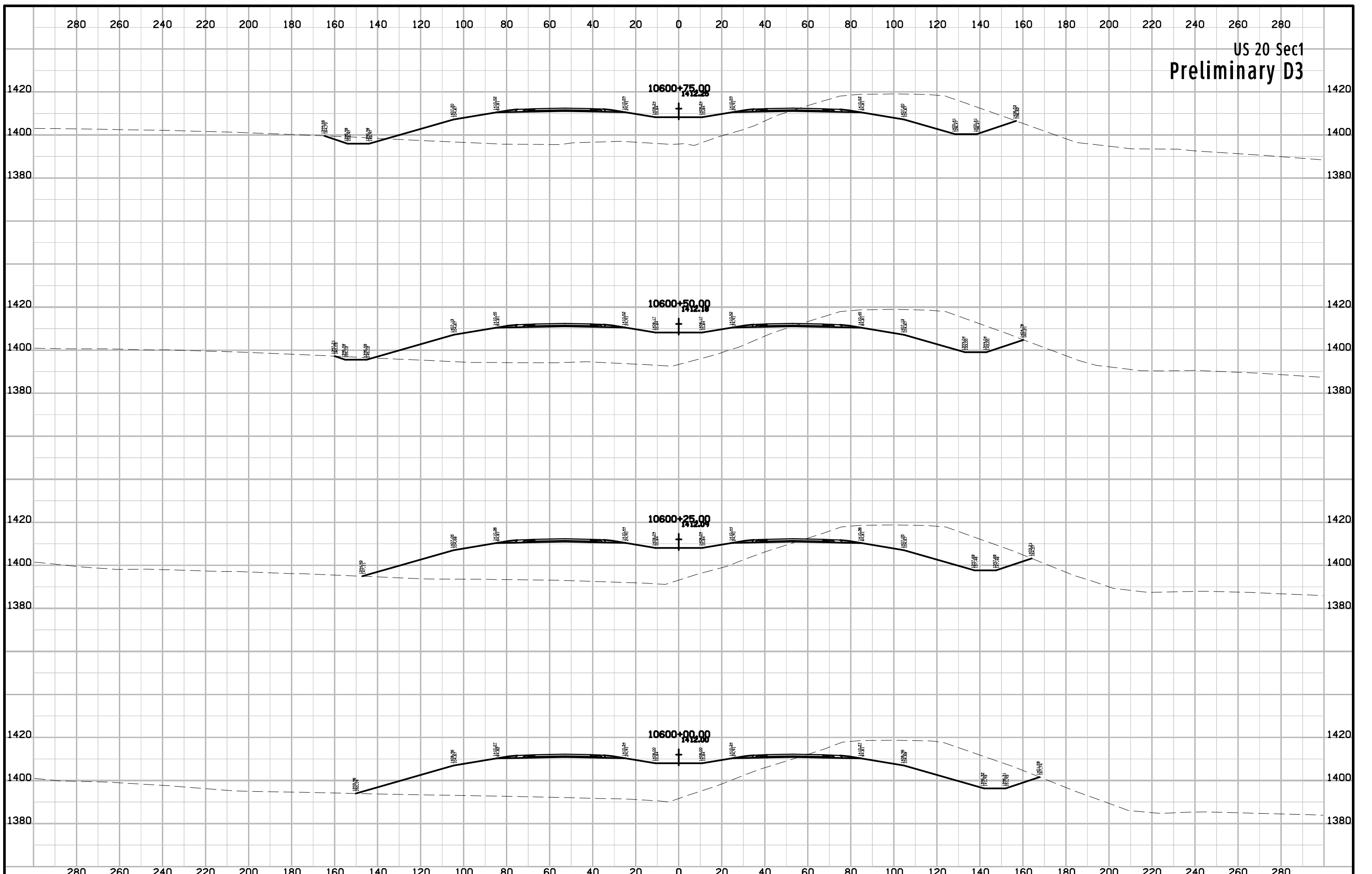
US 20 Sec1
Preliminary D3



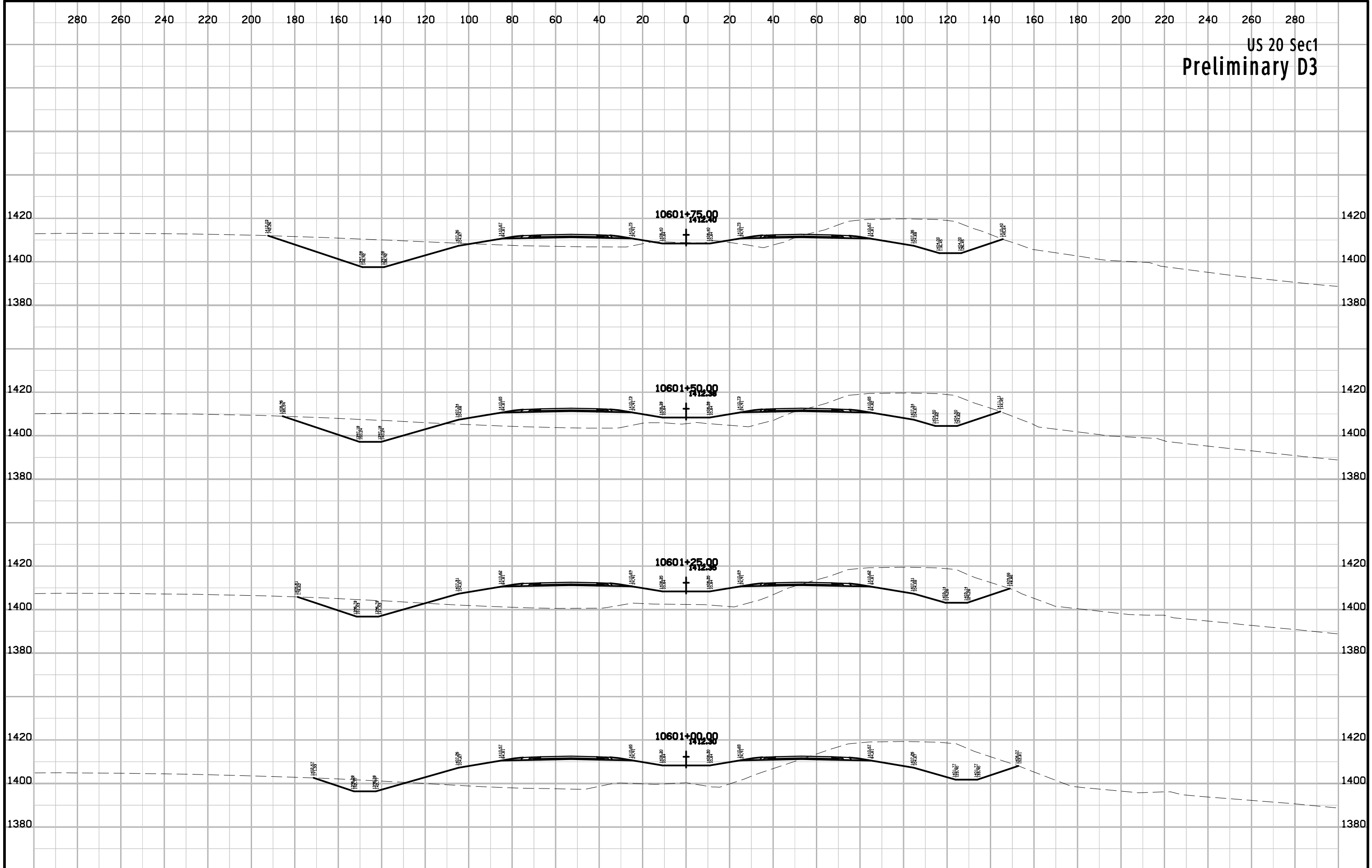
US 20 Sec1
Preliminary D3



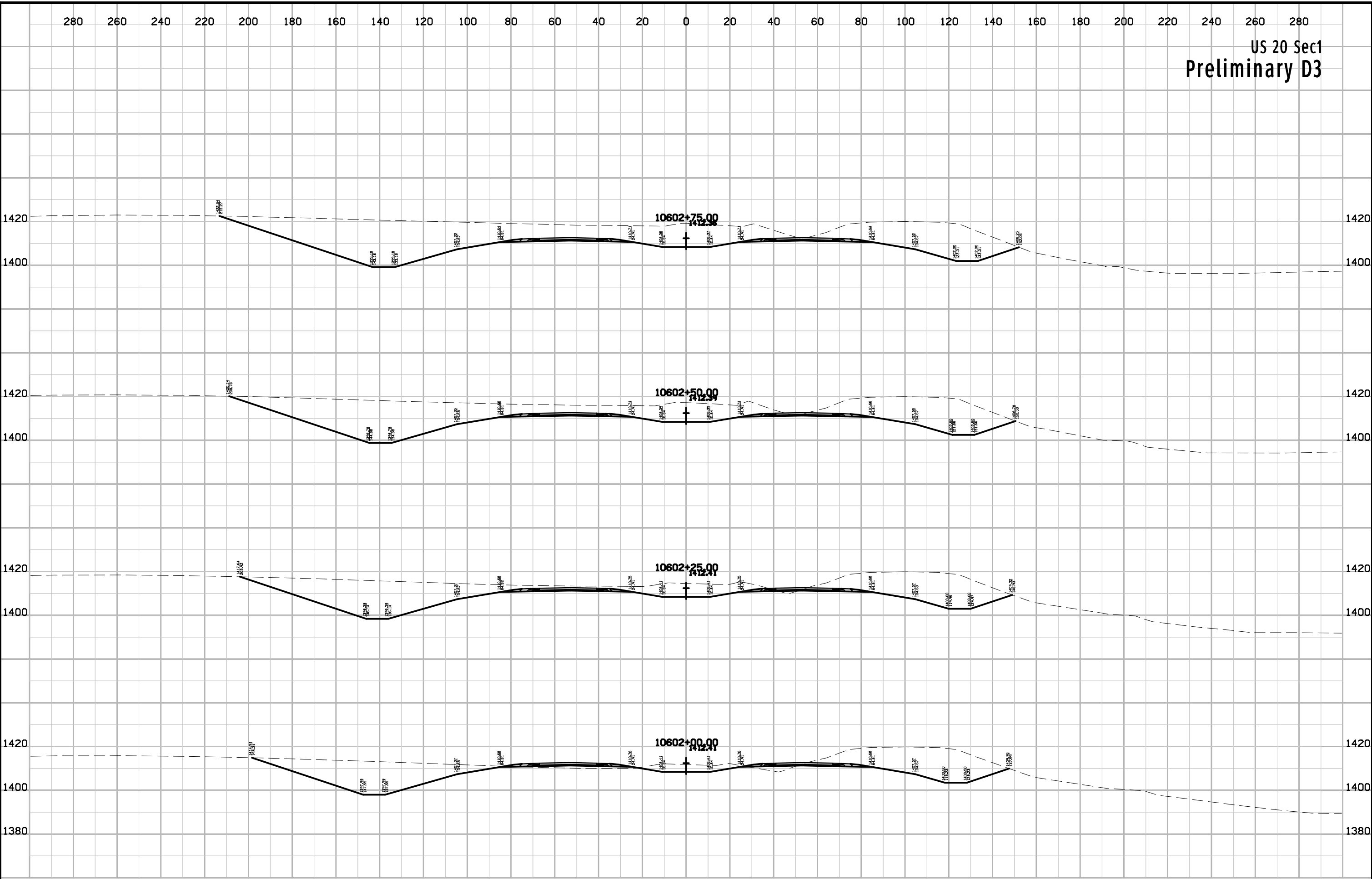
US 20 Sec1
Preliminary D3



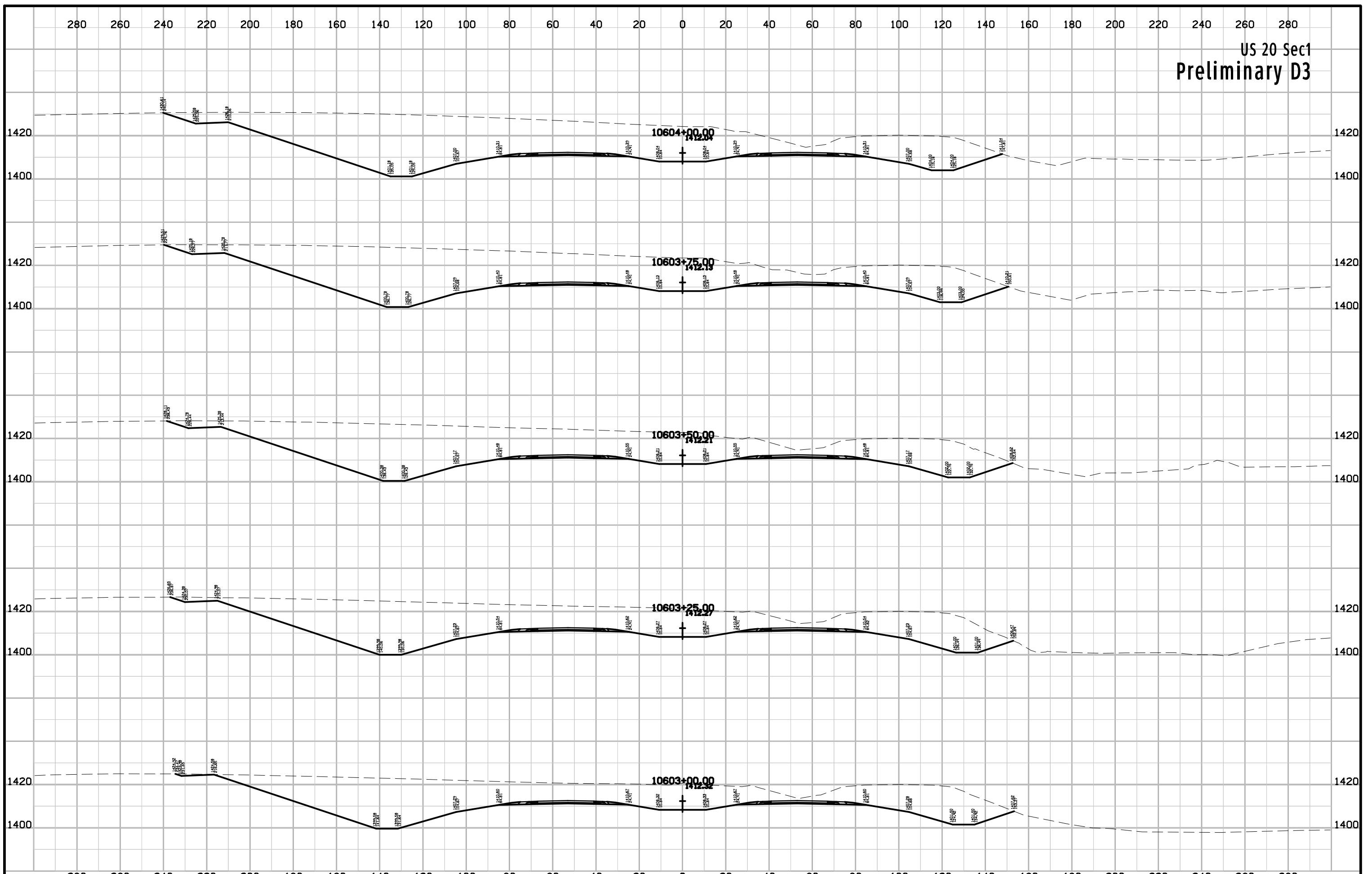
US 20 Sec1
Preliminary D3



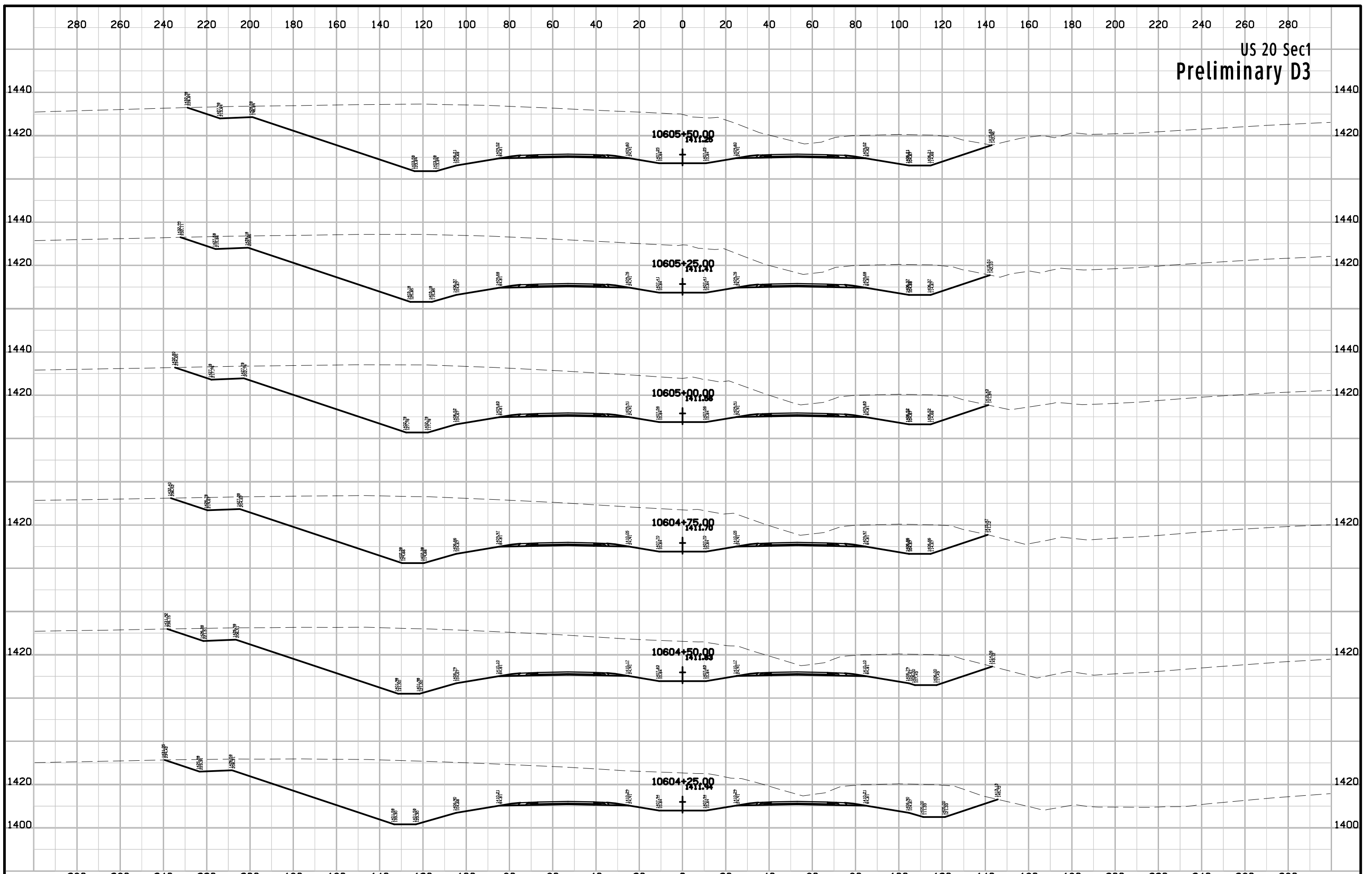
US 20 Sec1
Preliminary D3



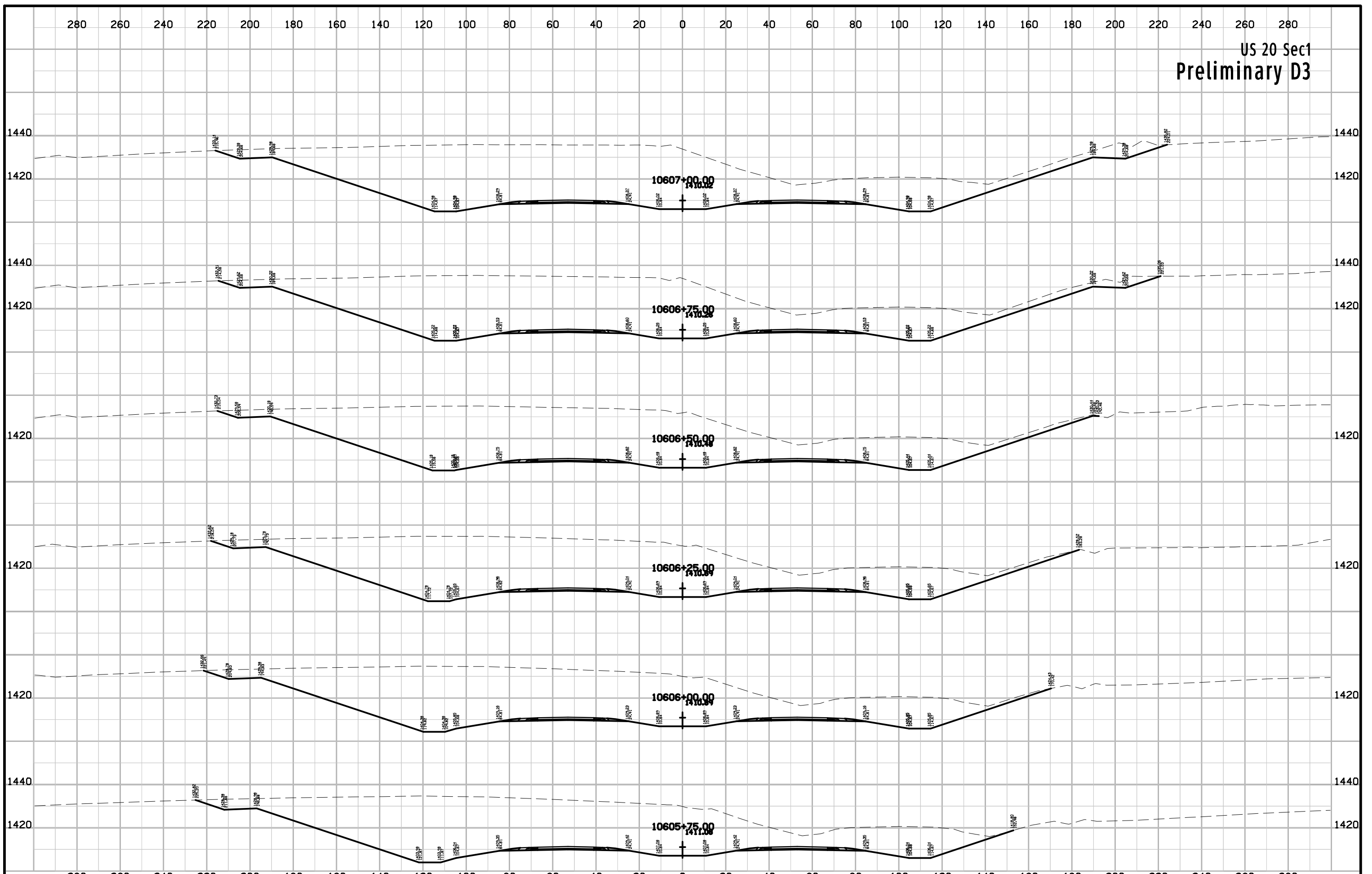
US 20 Sec1
Preliminary D3

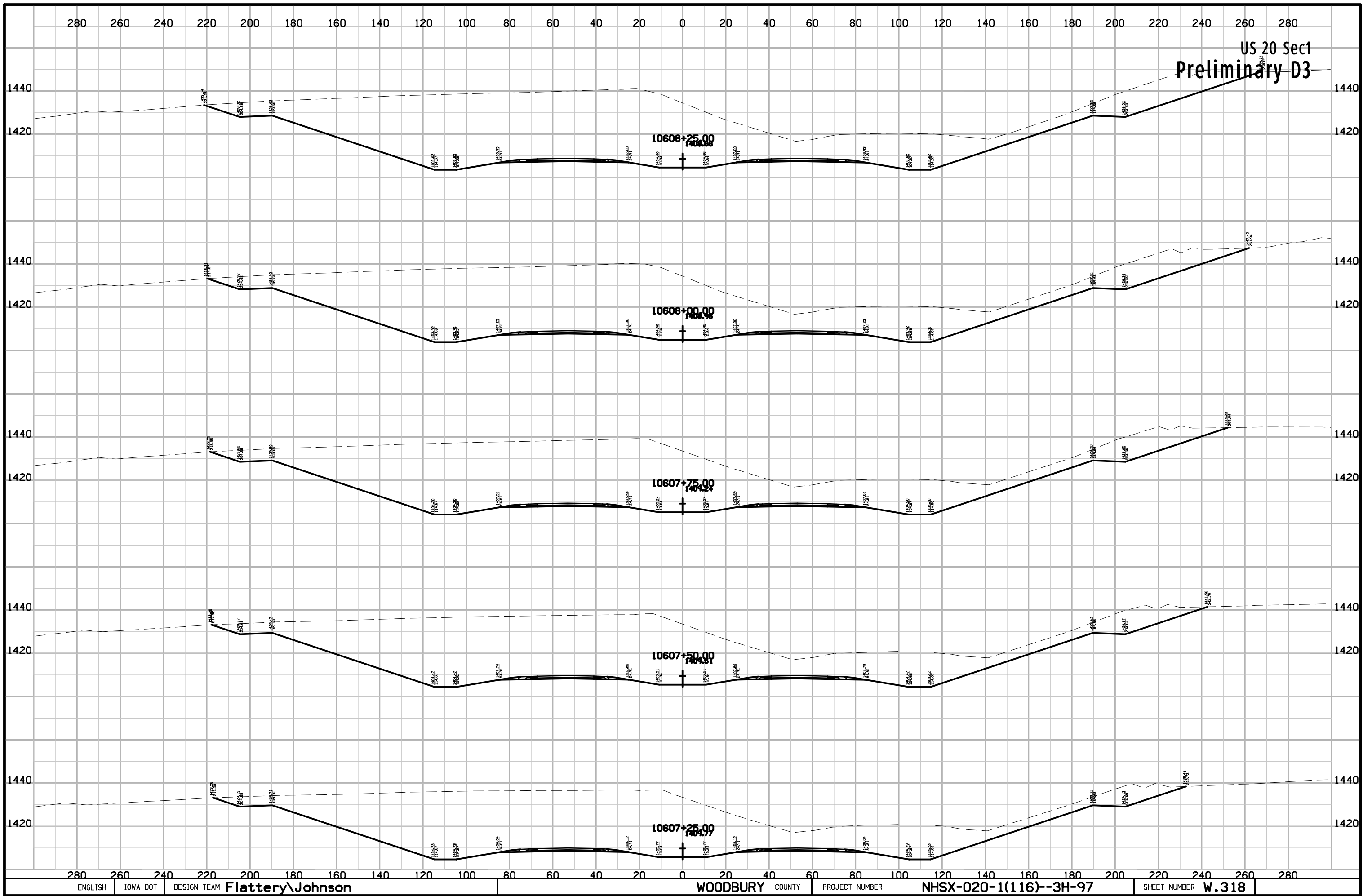


US 20 Sec1
Preliminary D3

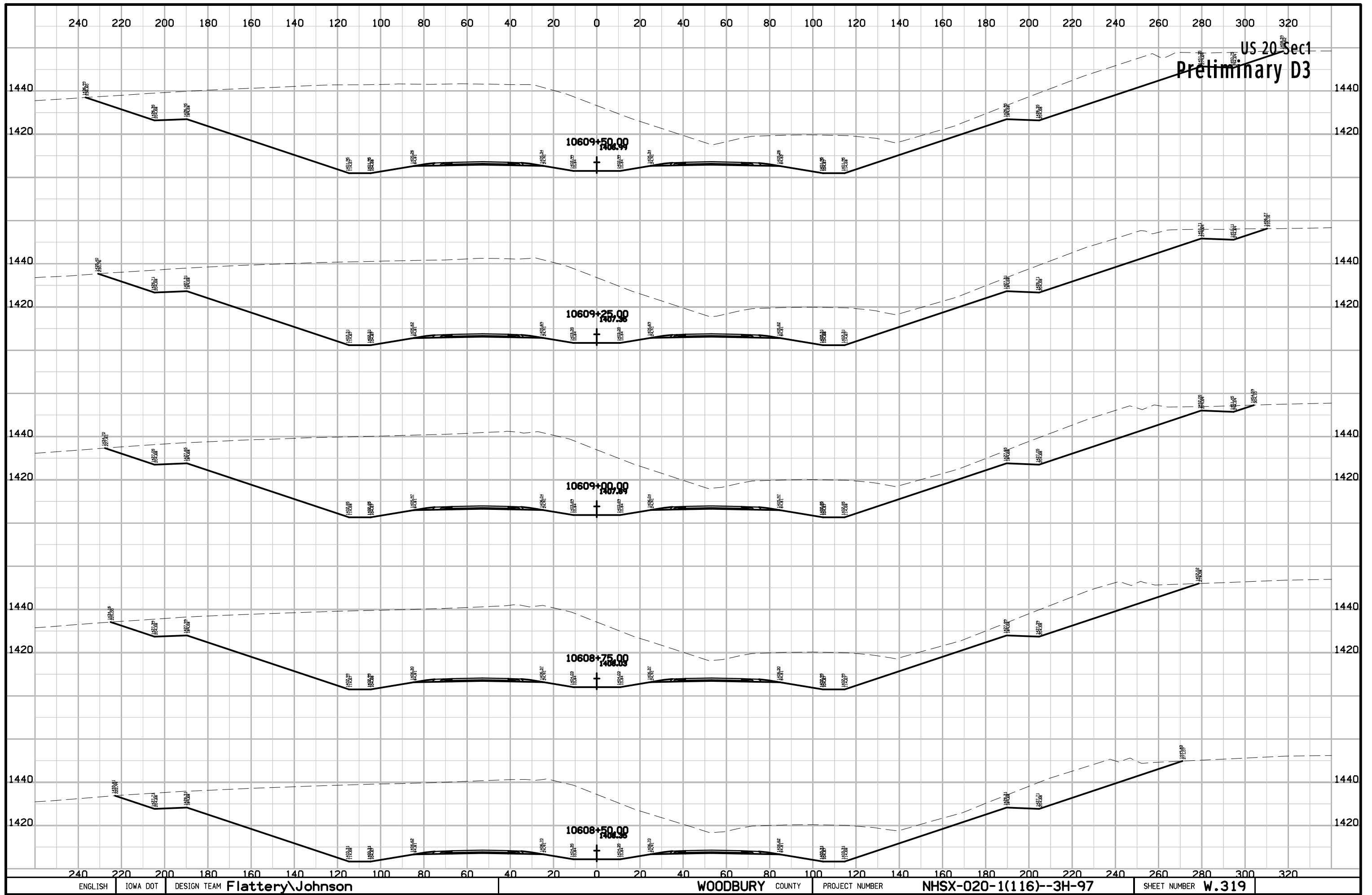


US 20 Sec1
Preliminary D3

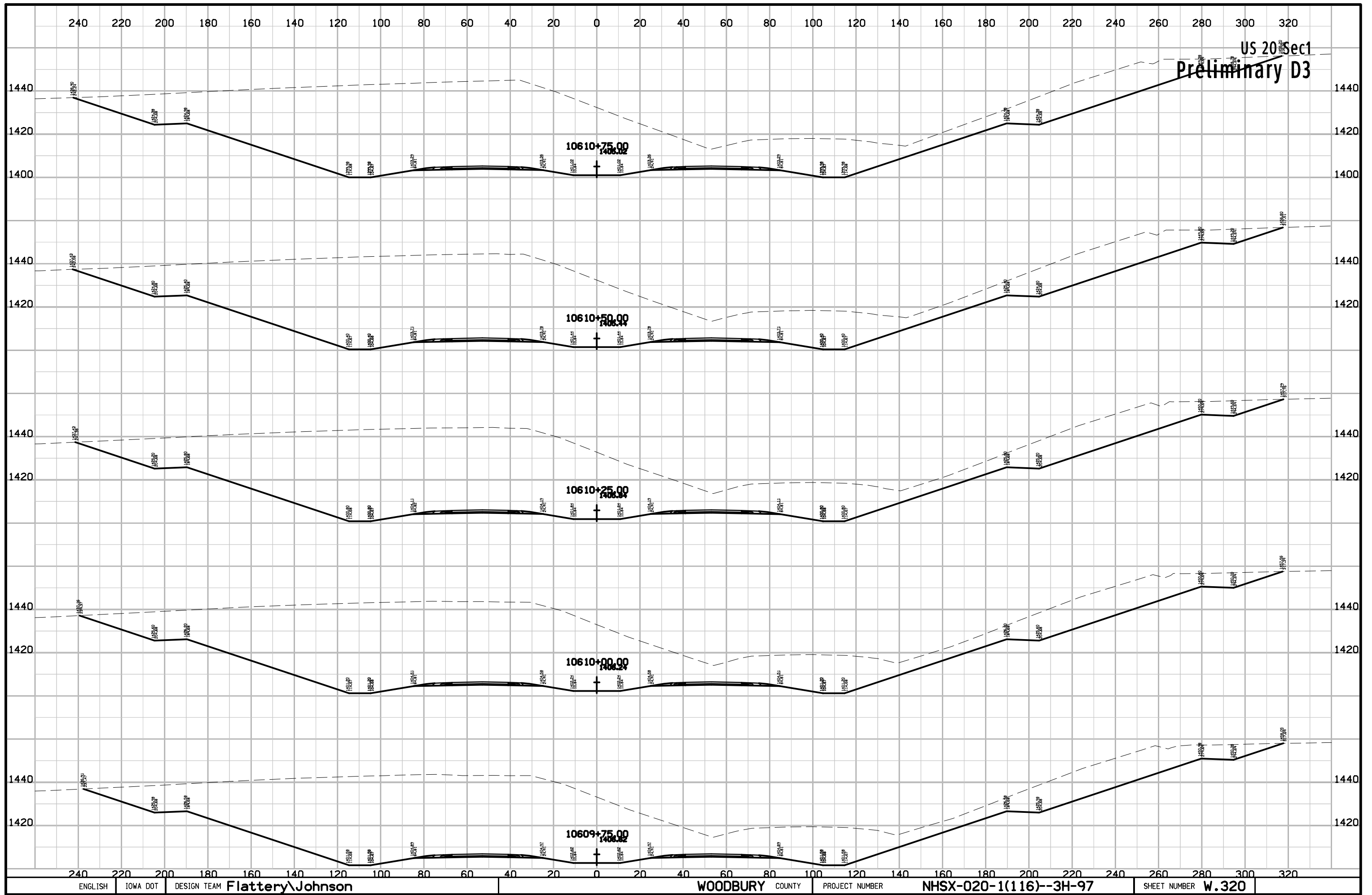




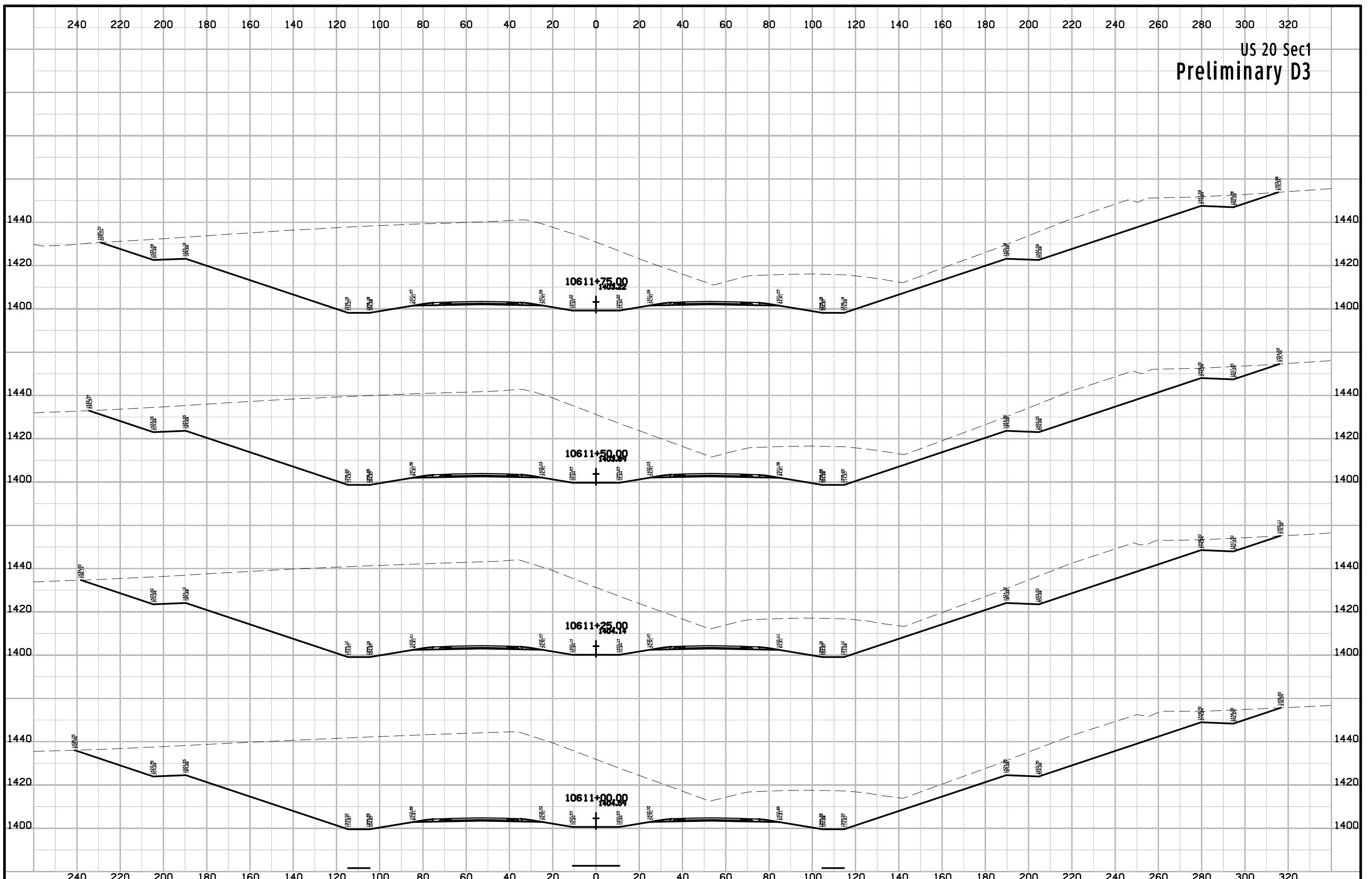
US 20 Sec1
Preliminary D3



US 20 Sec1
Preliminary D3



US 20 Sec1
Preliminary D3



10611+75.00

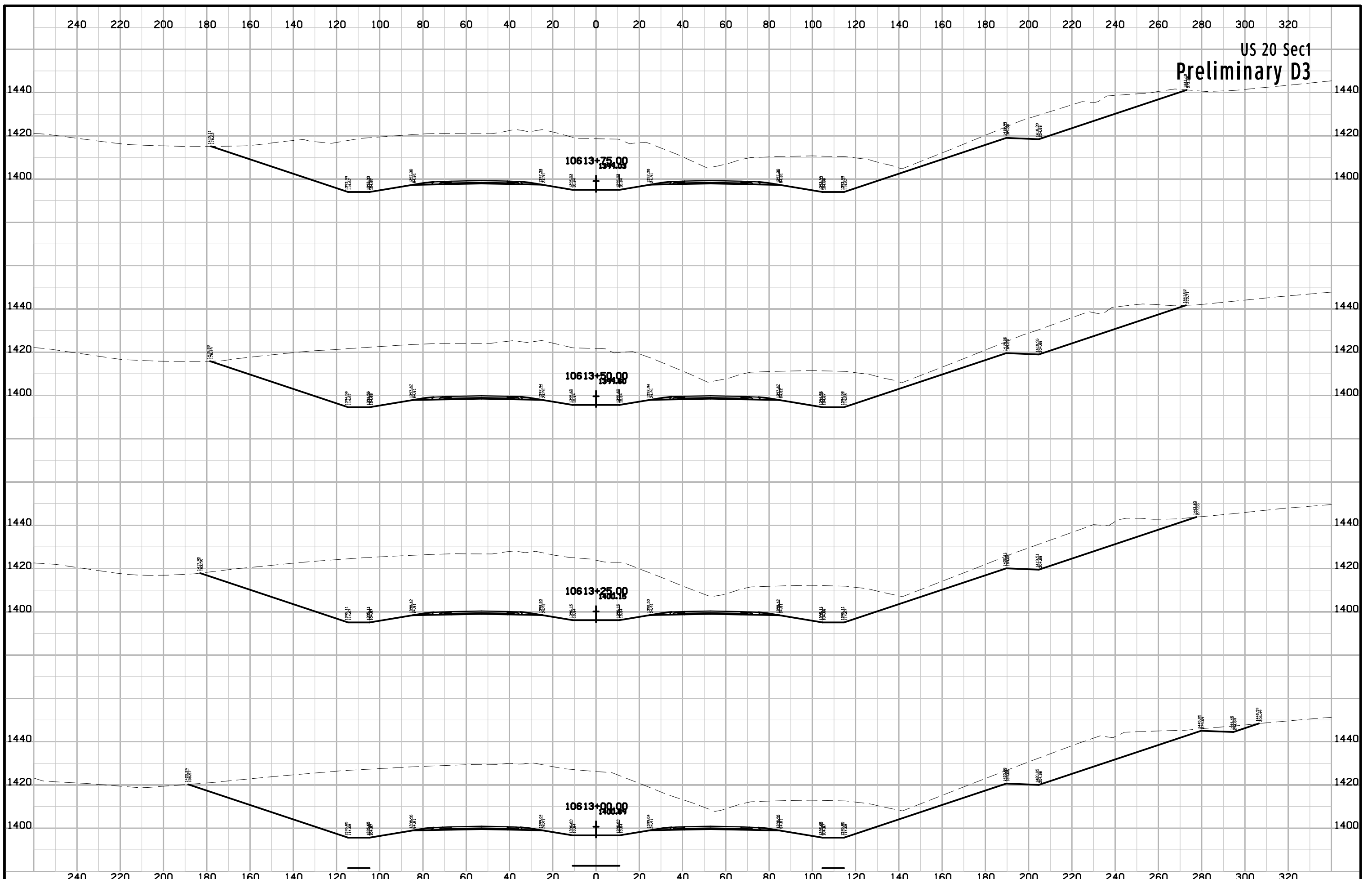
10611+50.00

10611+25.00

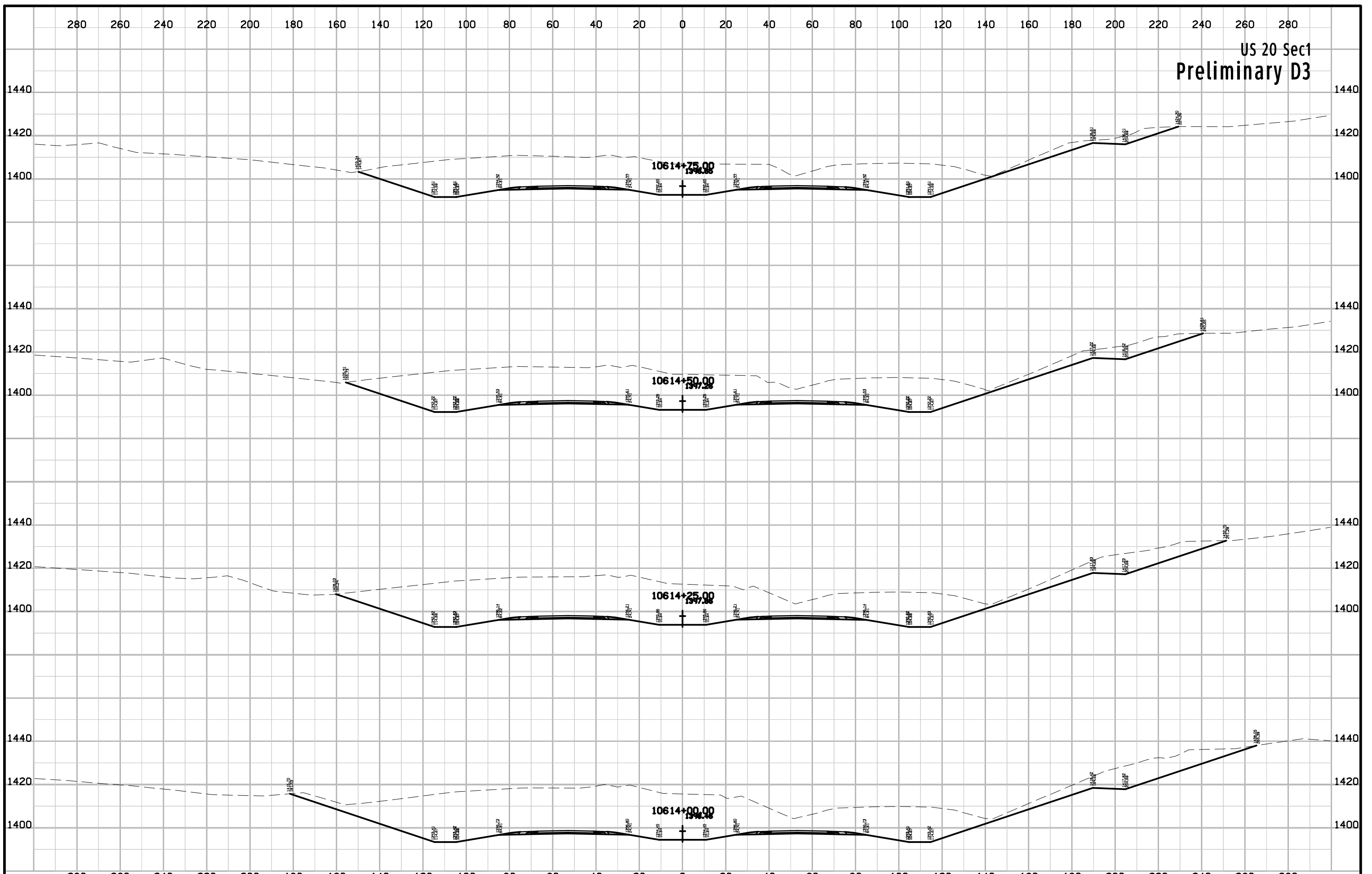
10611+00.00



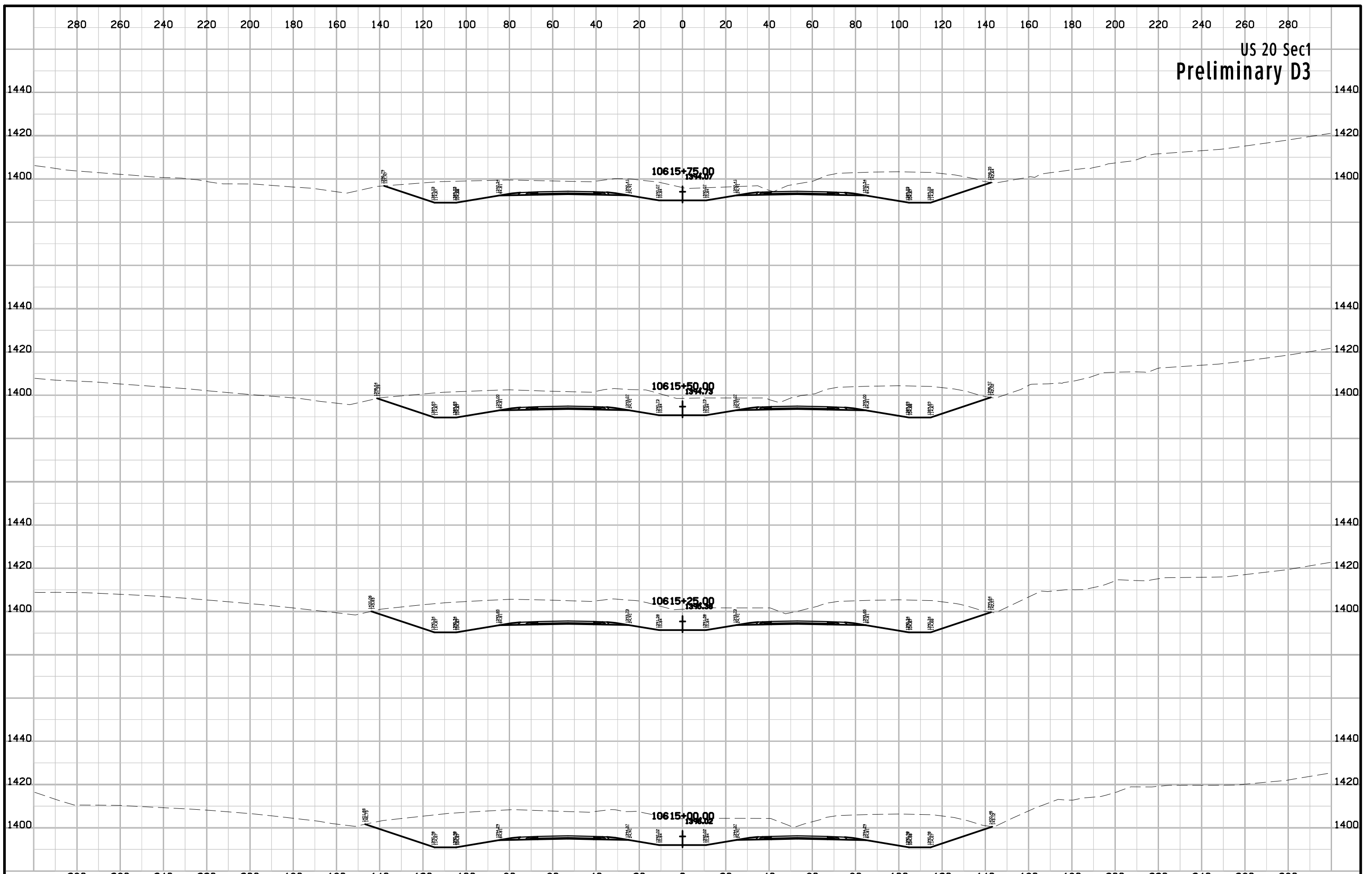
US 20 Sec1
Preliminary D3



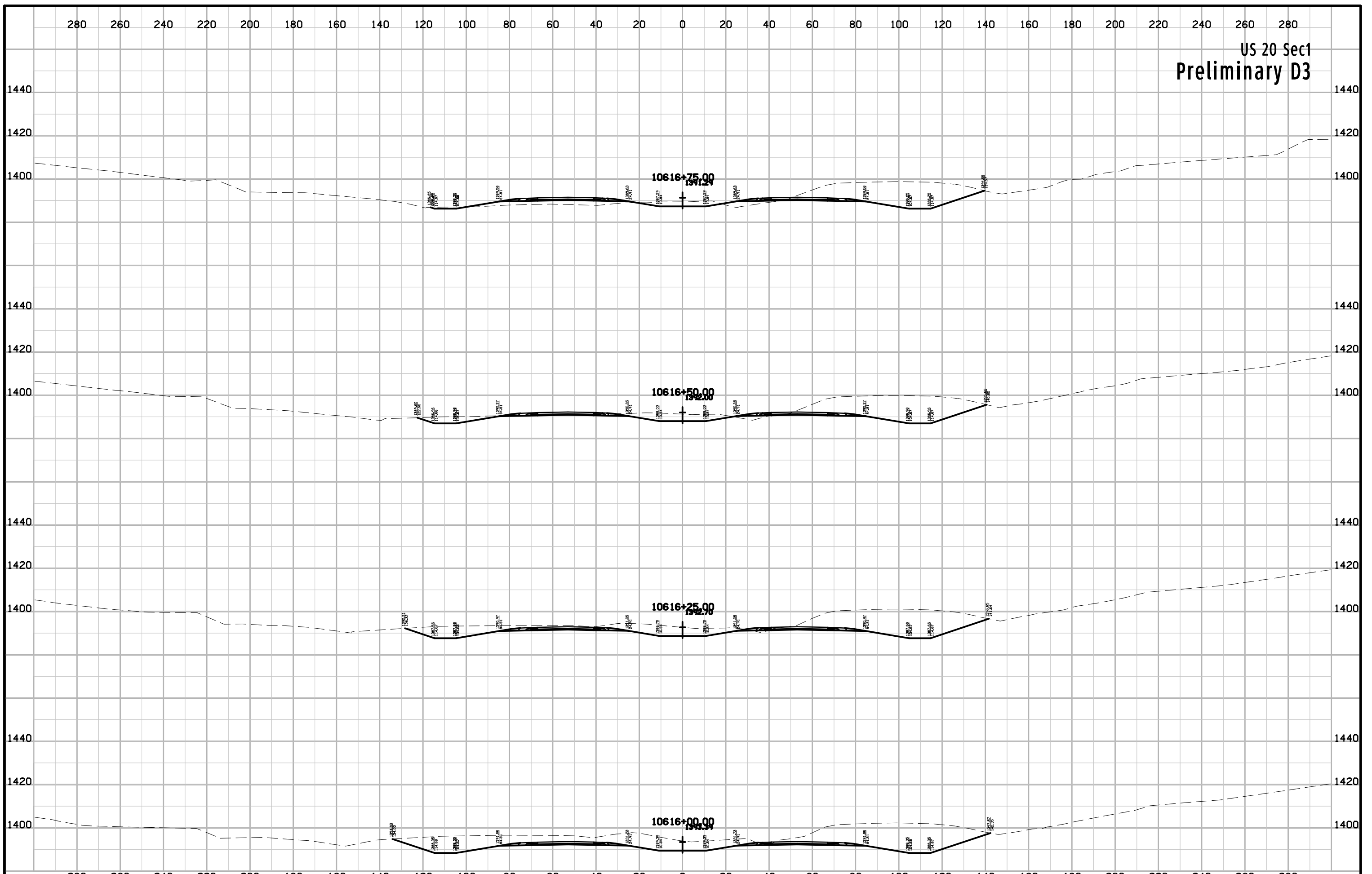
US 20 Sec1
Preliminary D3



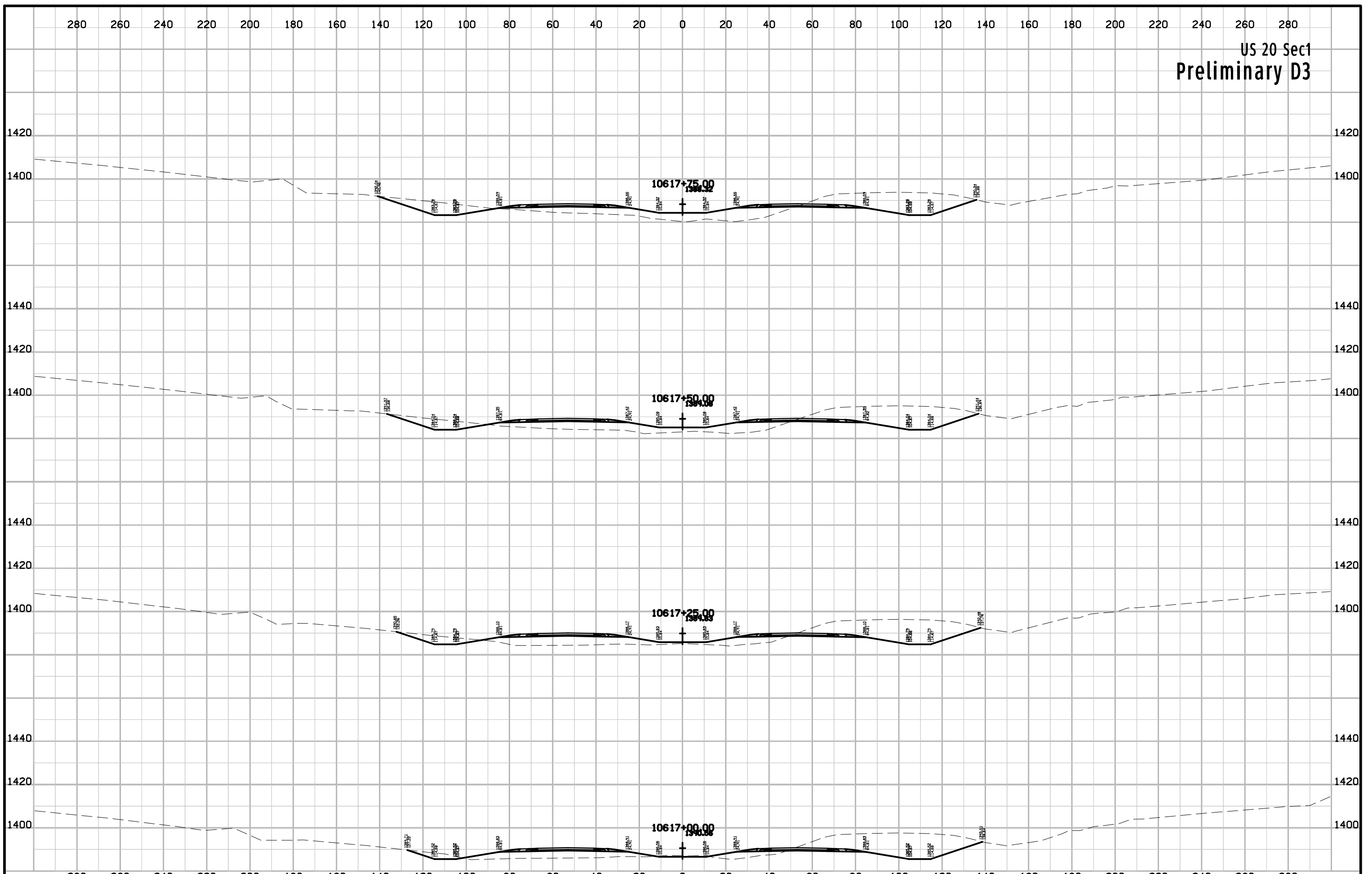
US 20 Sec1
Preliminary D3



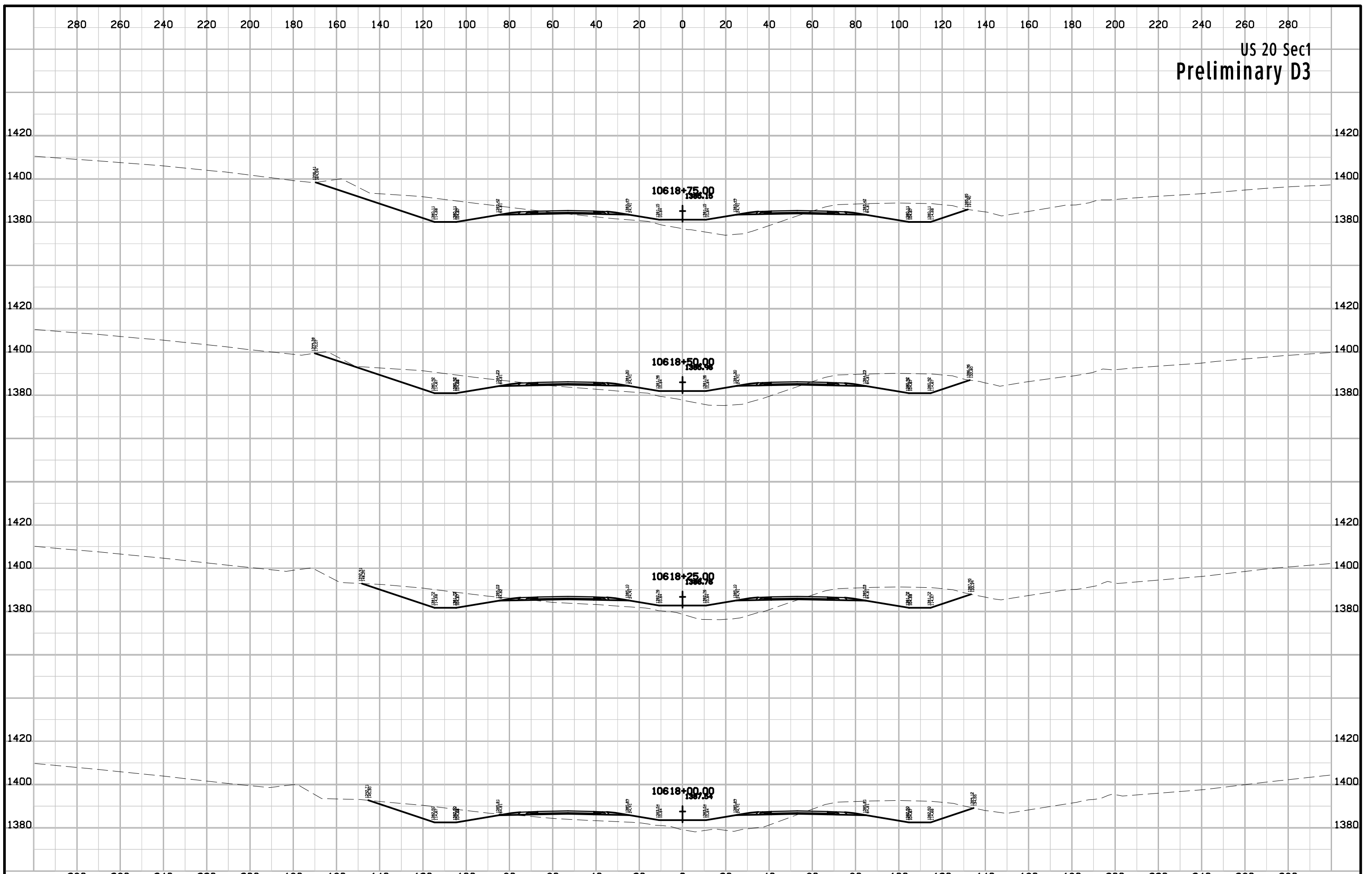
US 20 Sec1
Preliminary D3



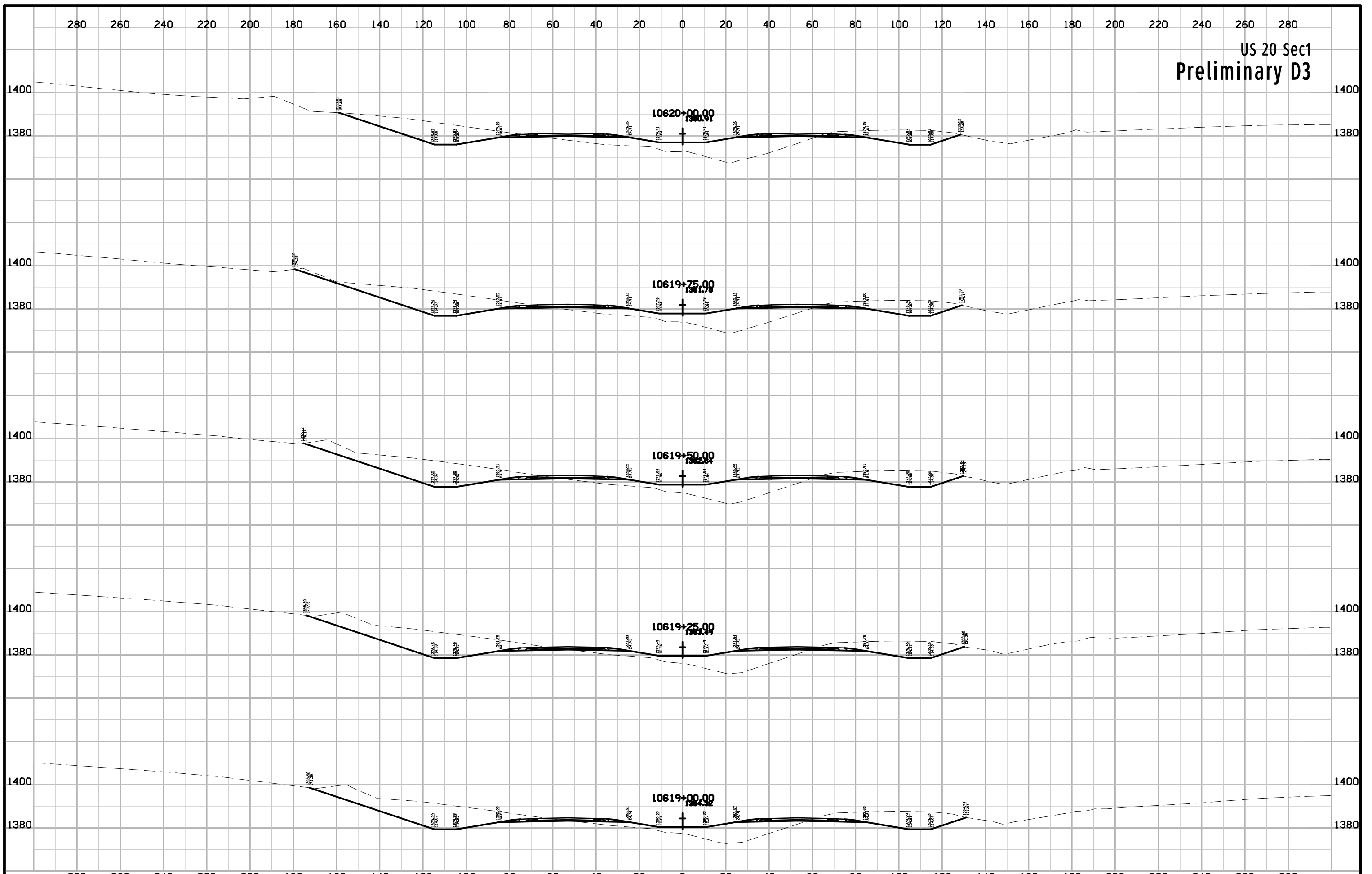
US 20 Sec1
Preliminary D3



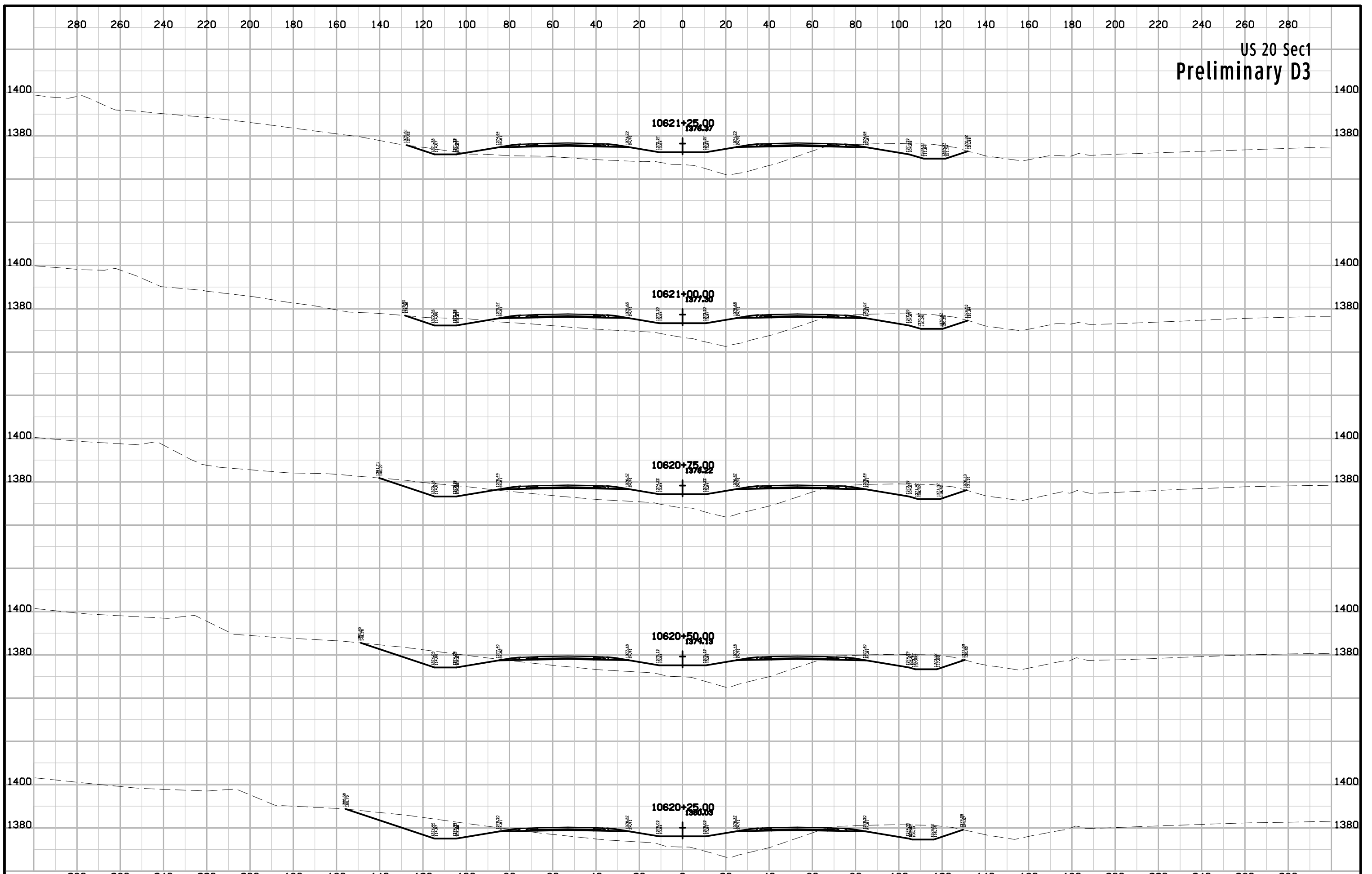
US 20 Sec1
Preliminary D3



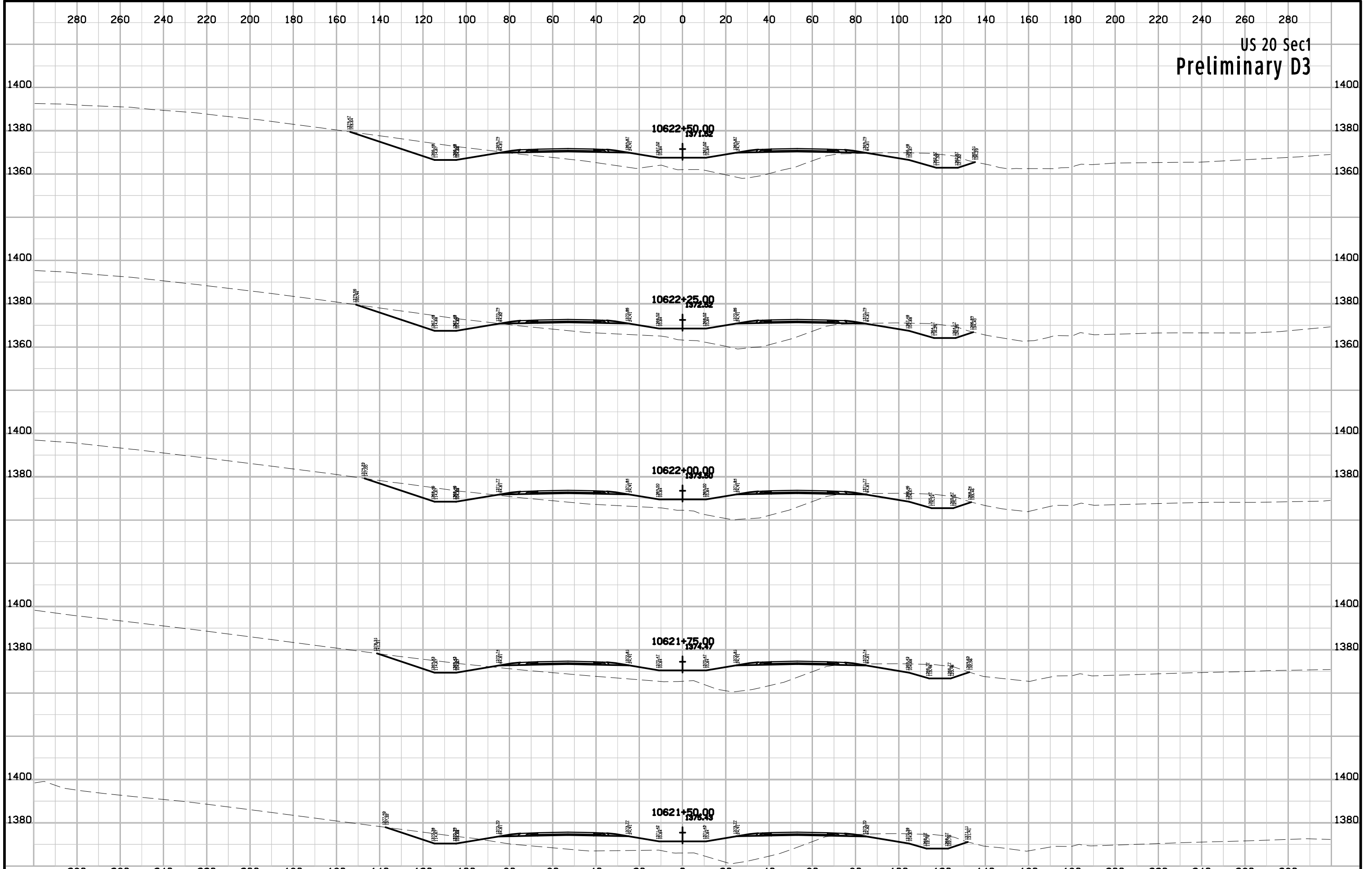
US 20 Sec1
Preliminary D3



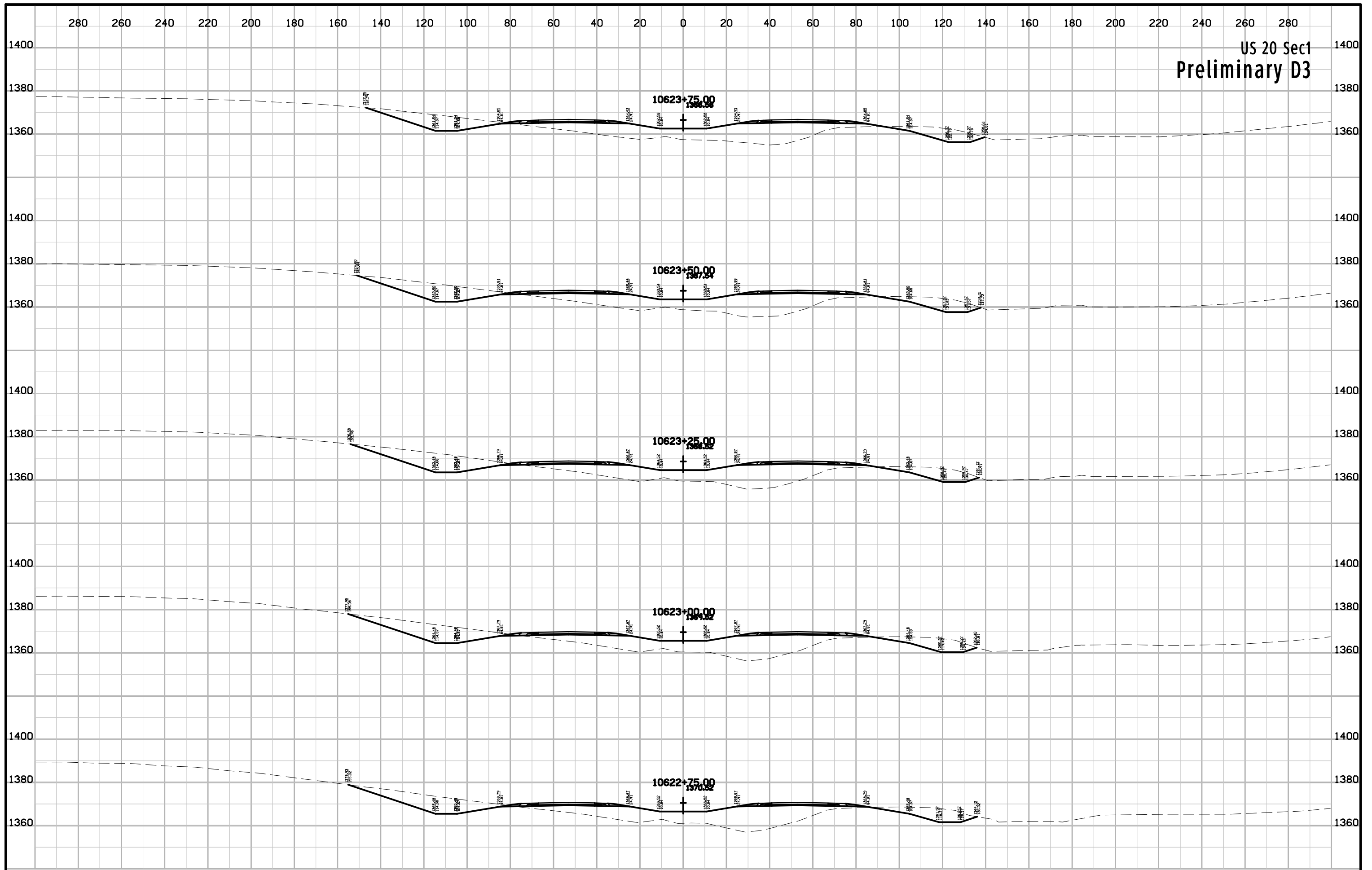
US 20 Sec1
Preliminary D3



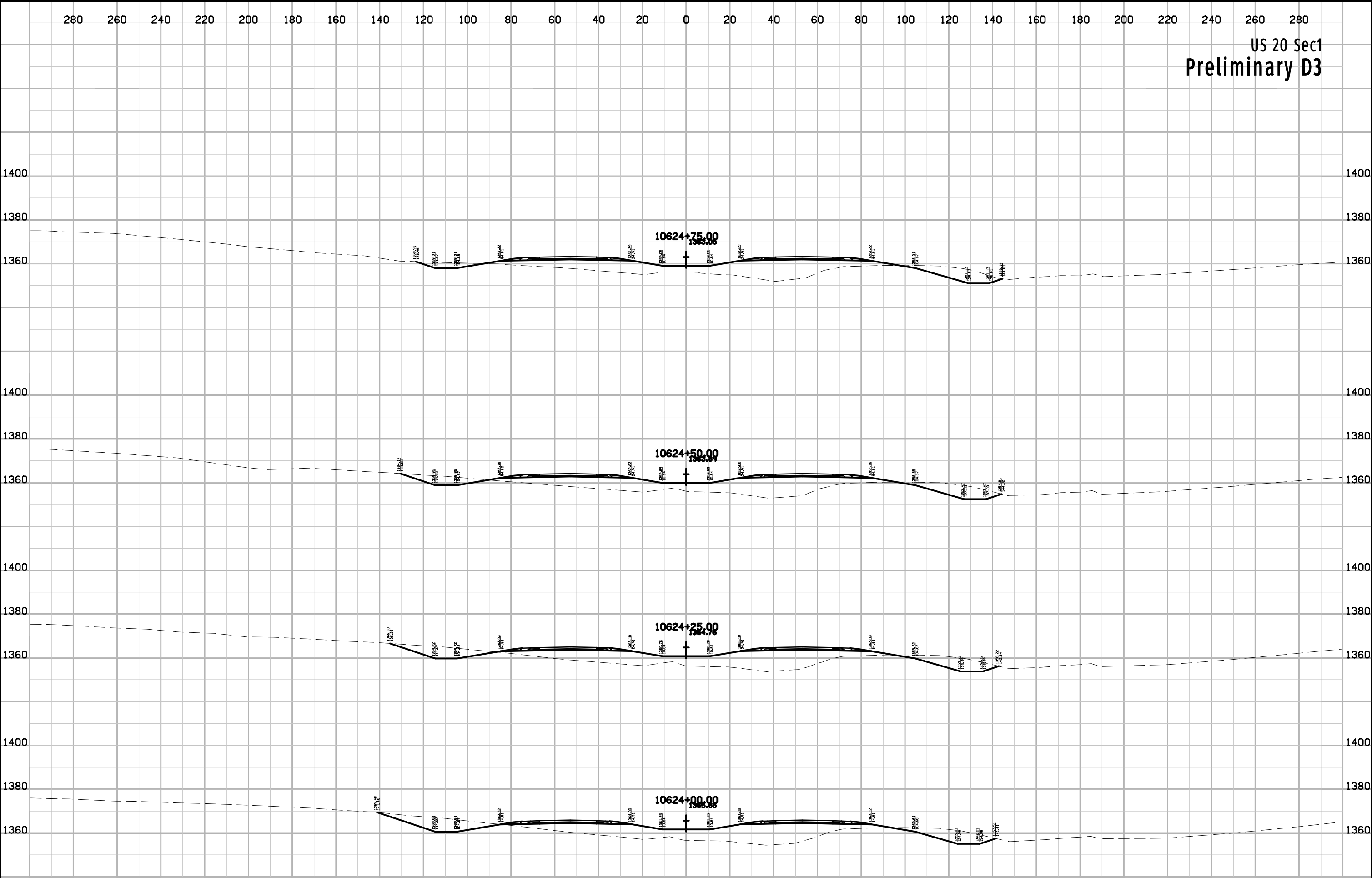
US 20 Sec1
Preliminary D3



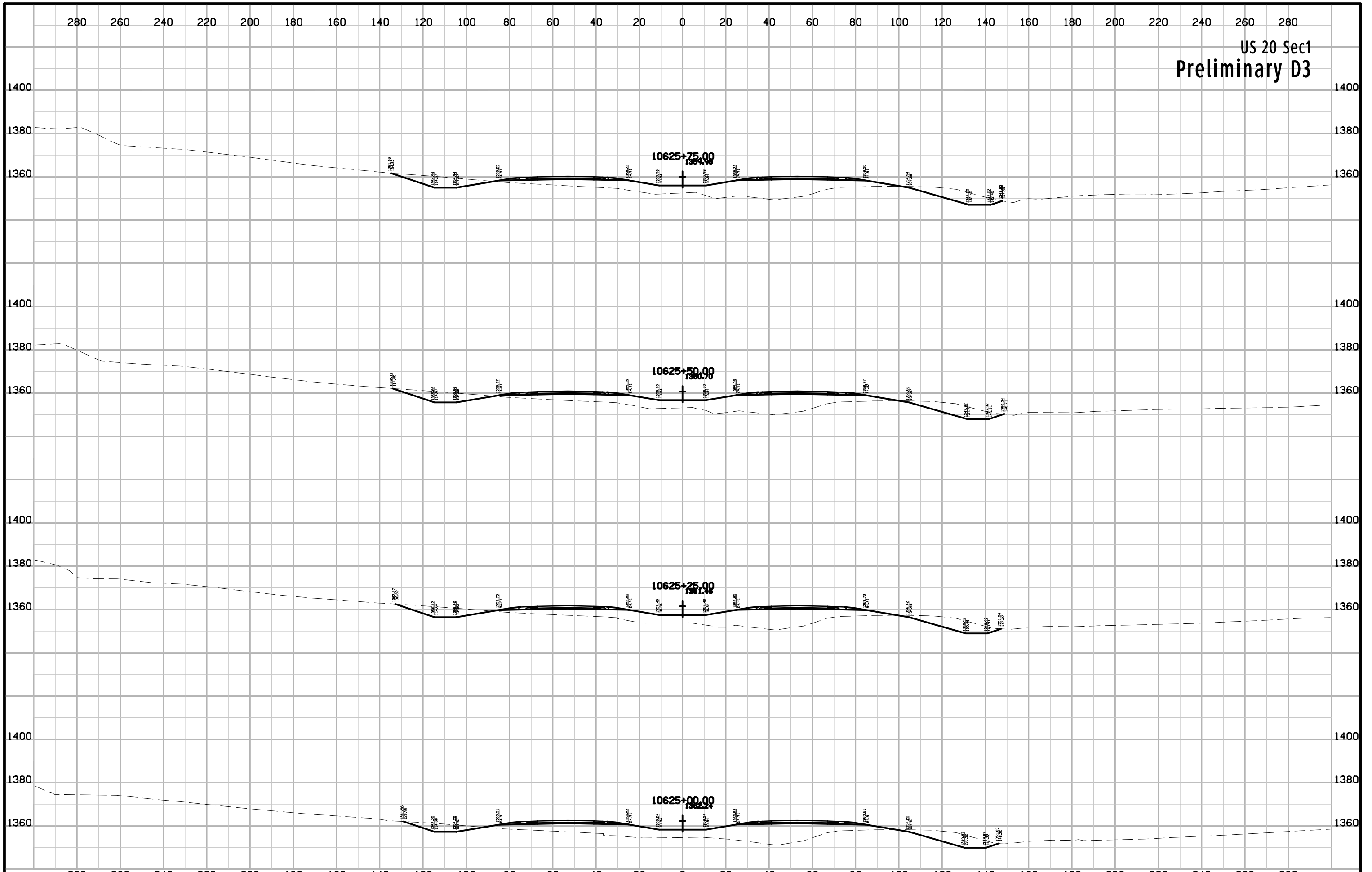
US 20 Sec1
Preliminary D3



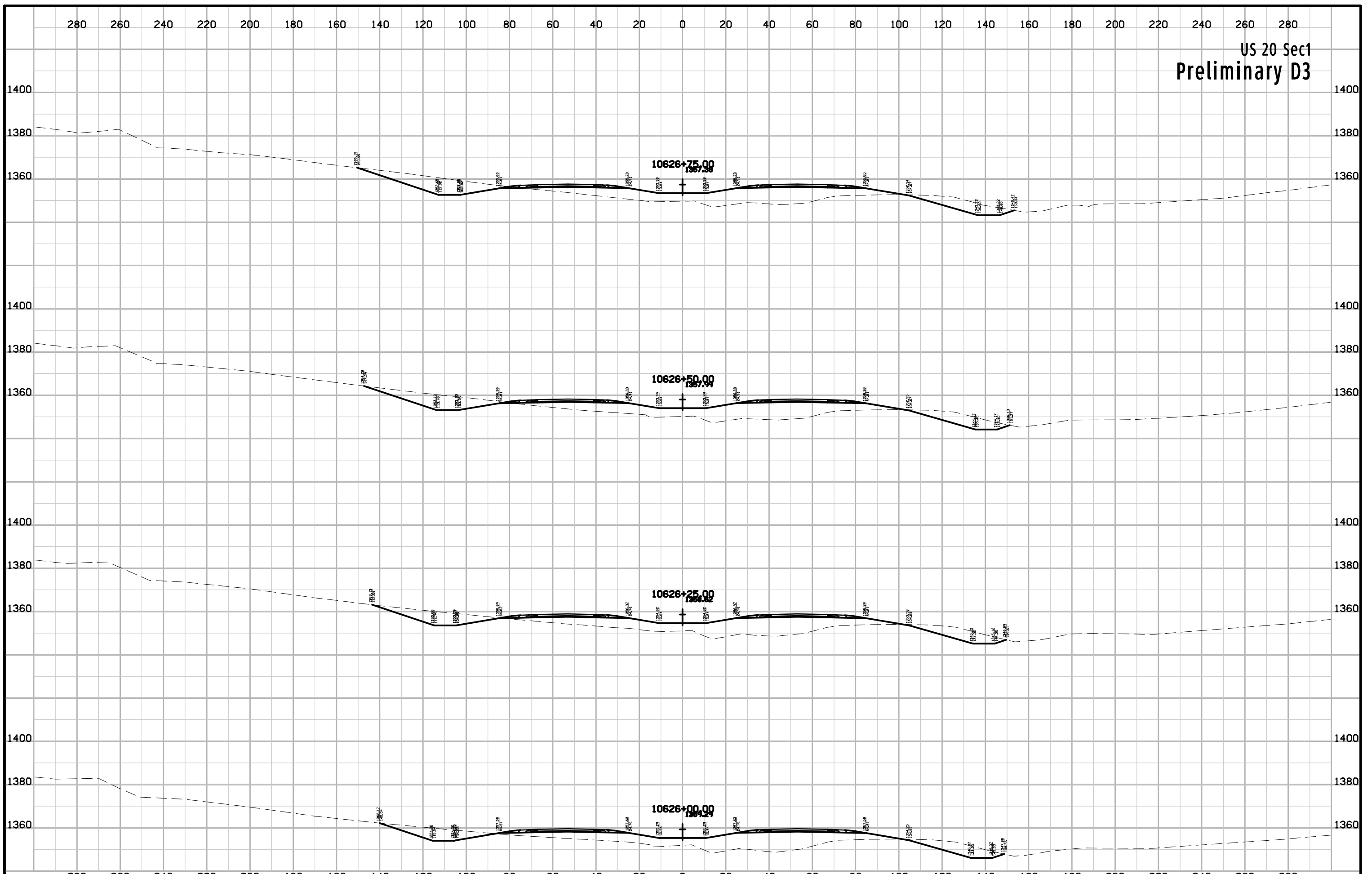
US 20 Sec1
Preliminary D3



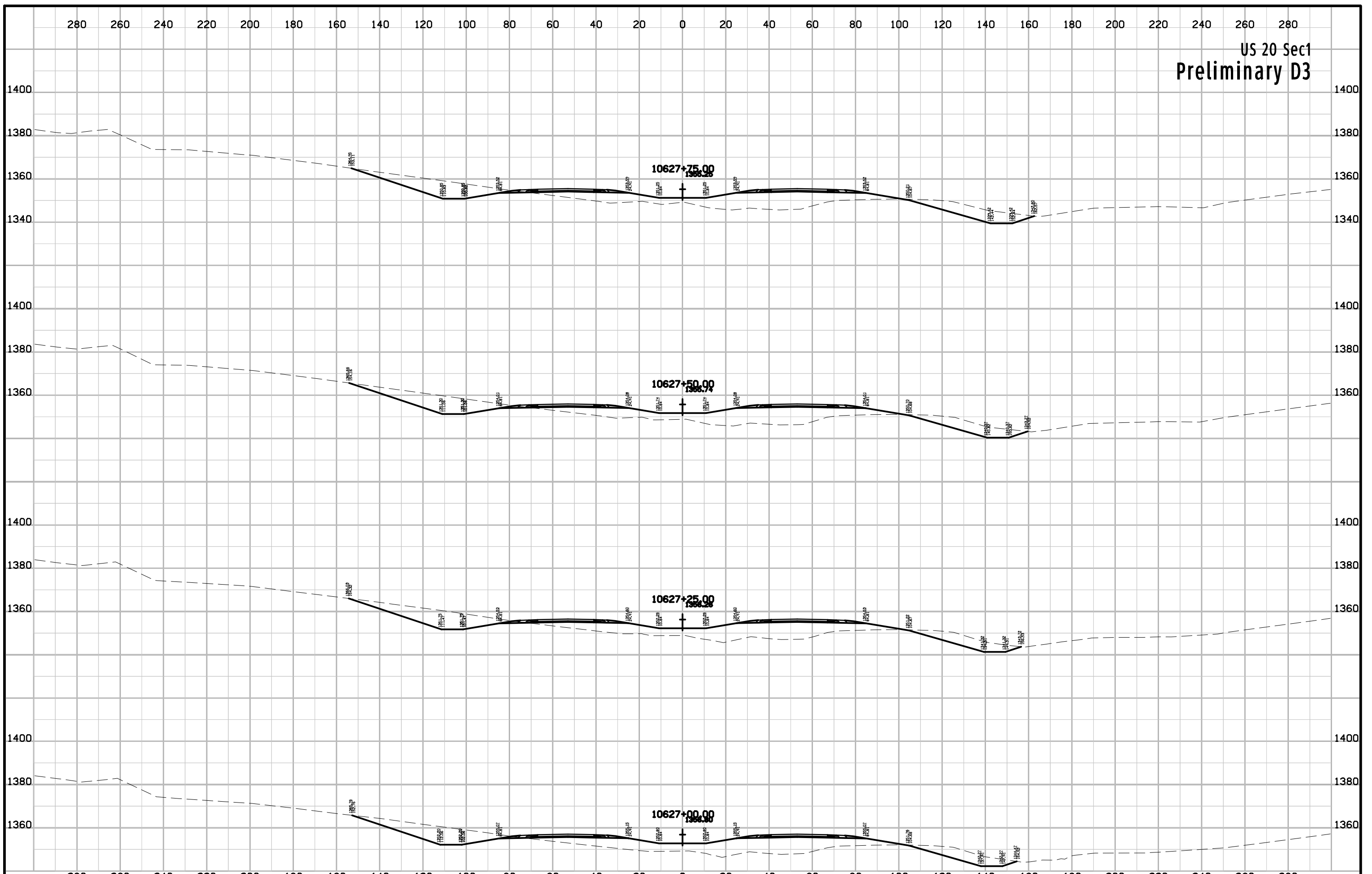
US 20 Sec1
Preliminary D3



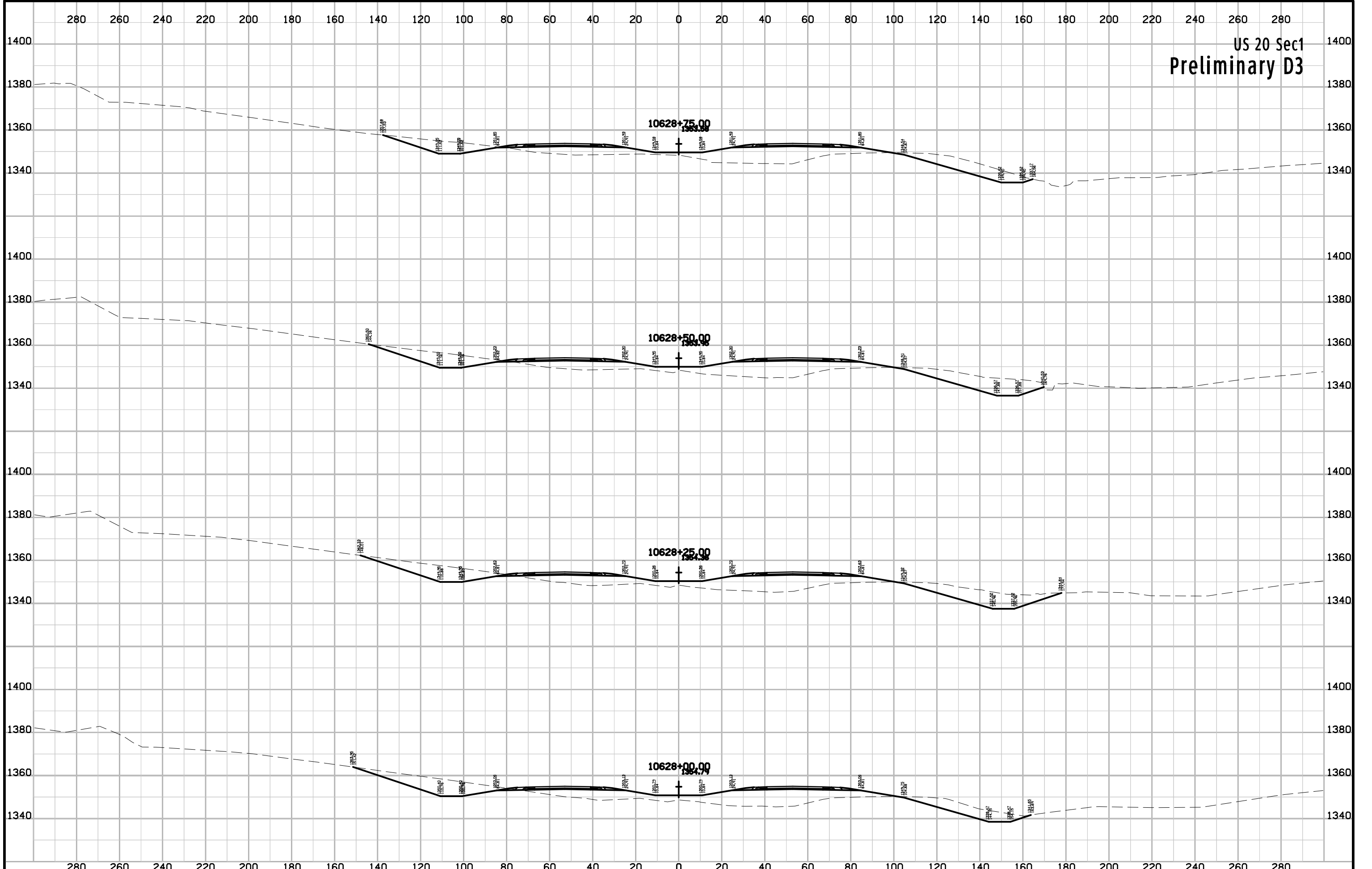
US 20 Sec1
Preliminary D3



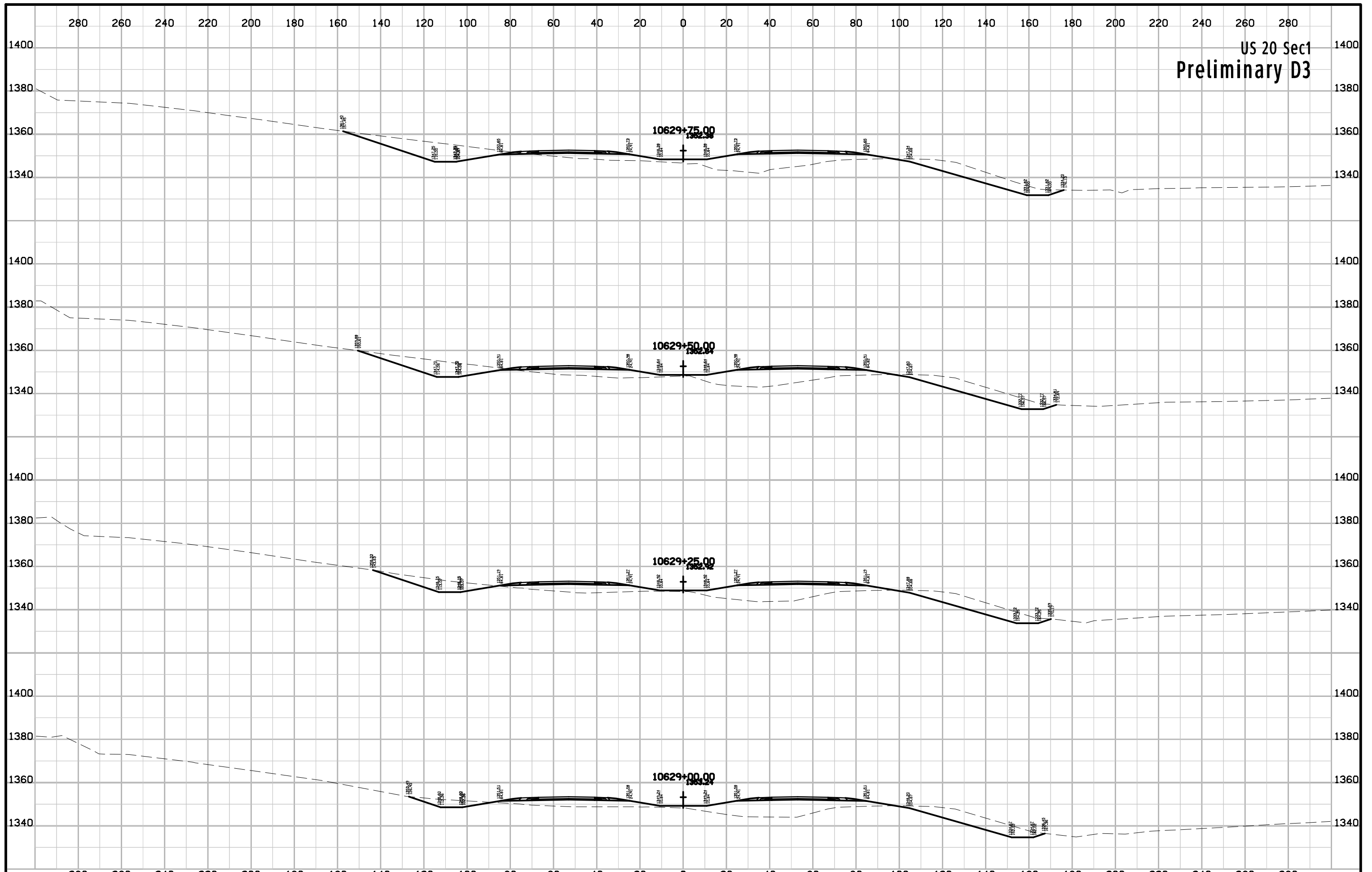
US 20 Sec1
Preliminary D3



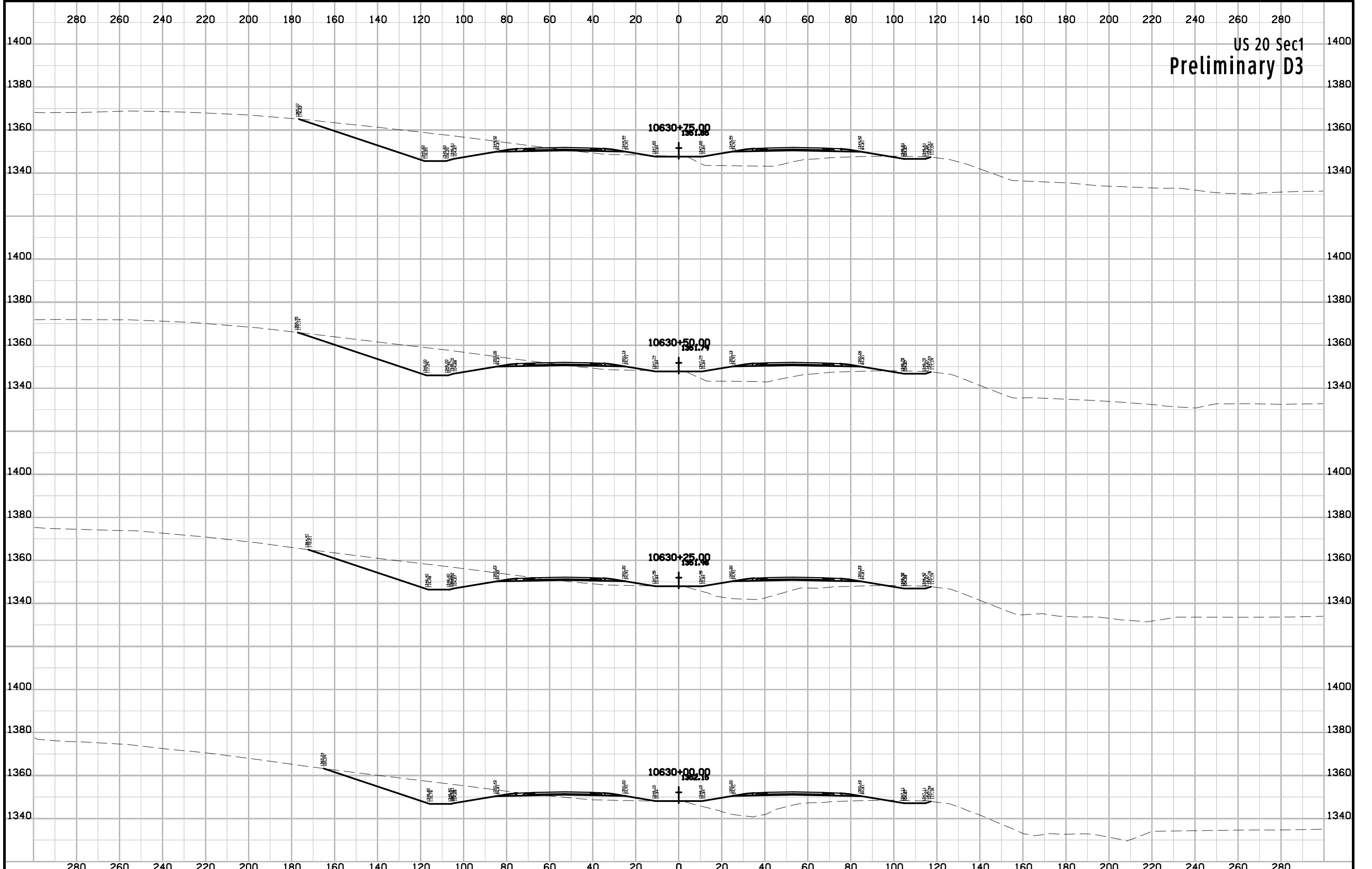
US 20 Sec1
Preliminary D3



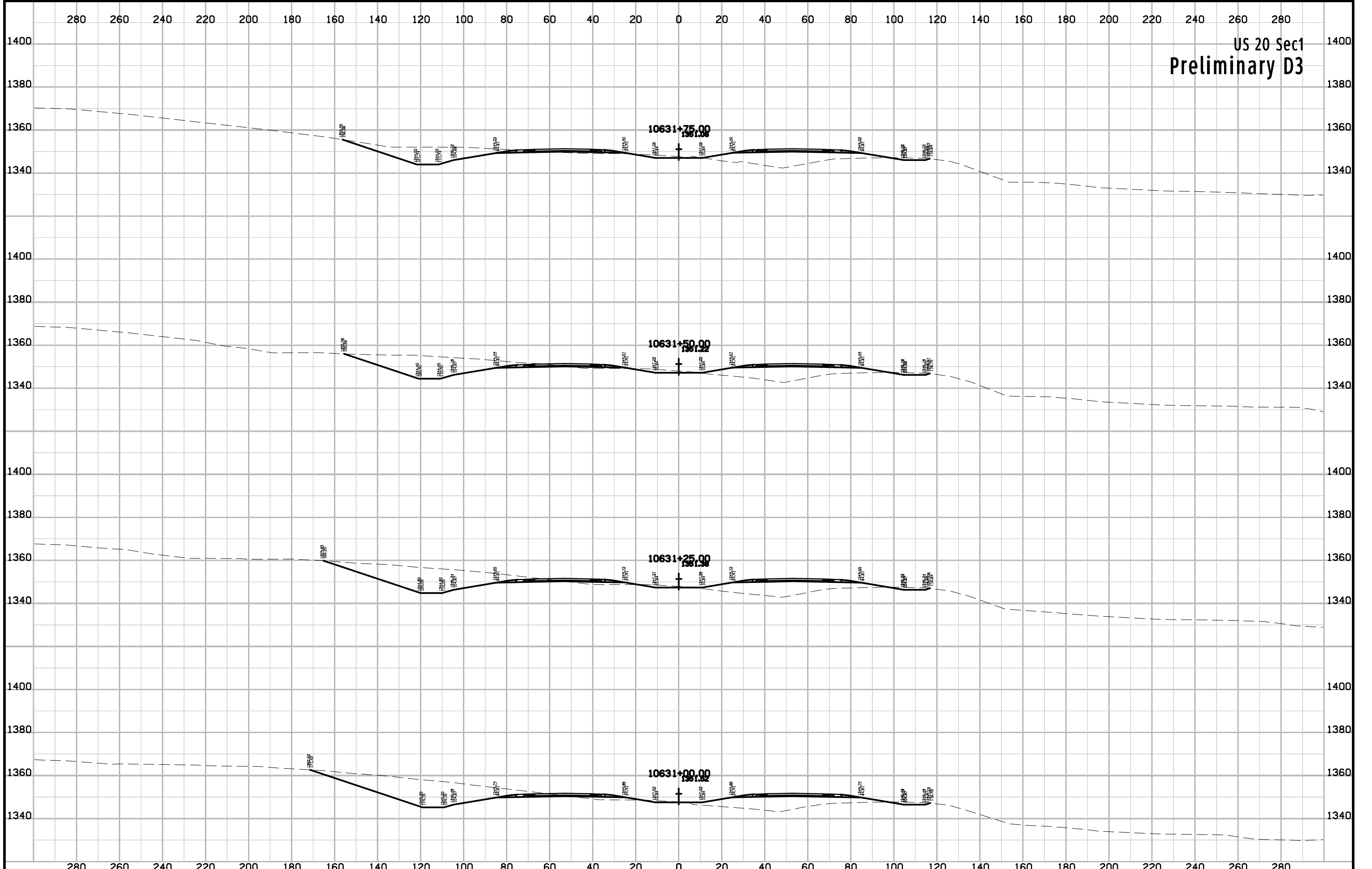
US 20 Sec1
Preliminary D3



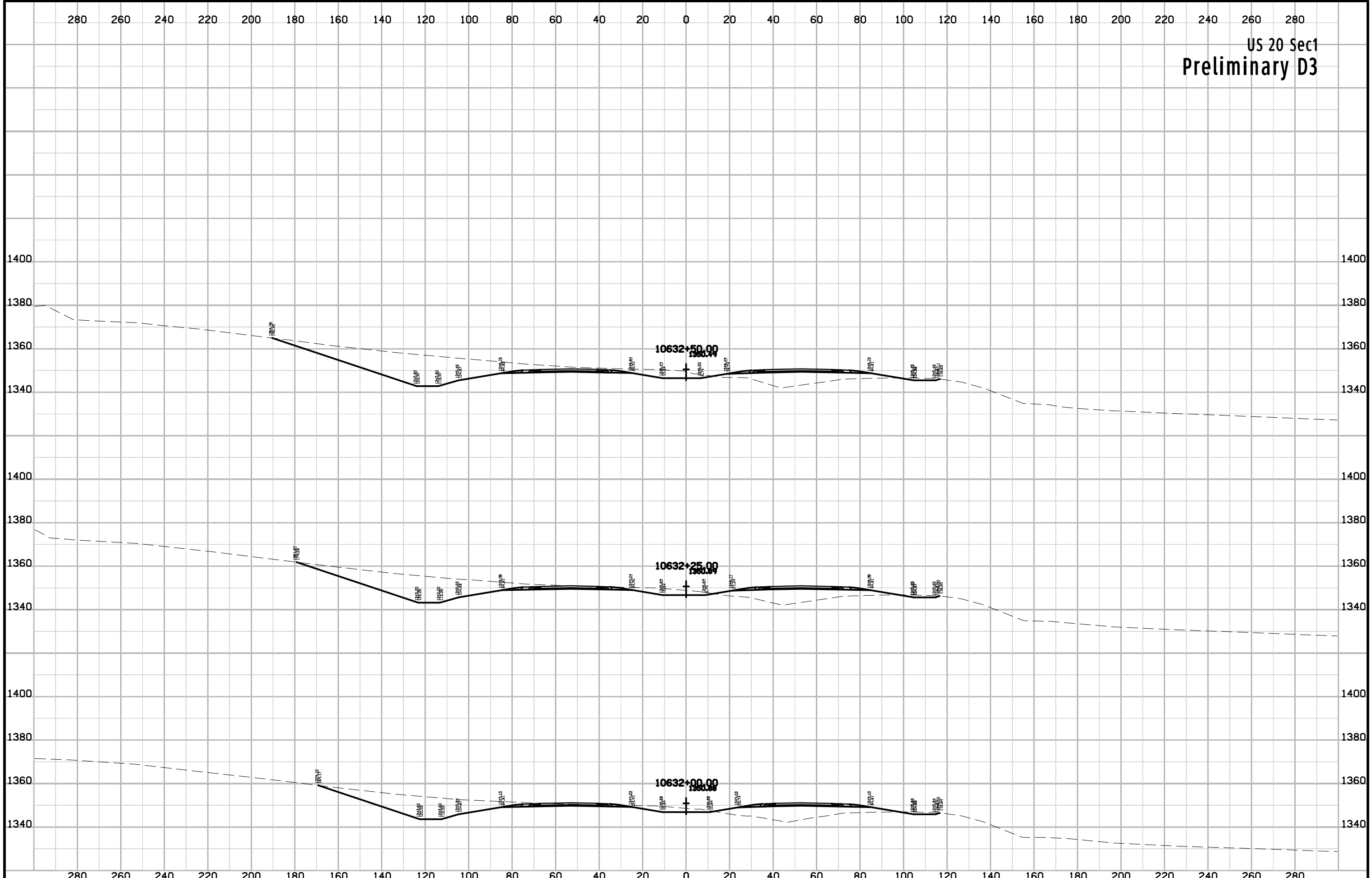
US 20 Sec1
Preliminary D3



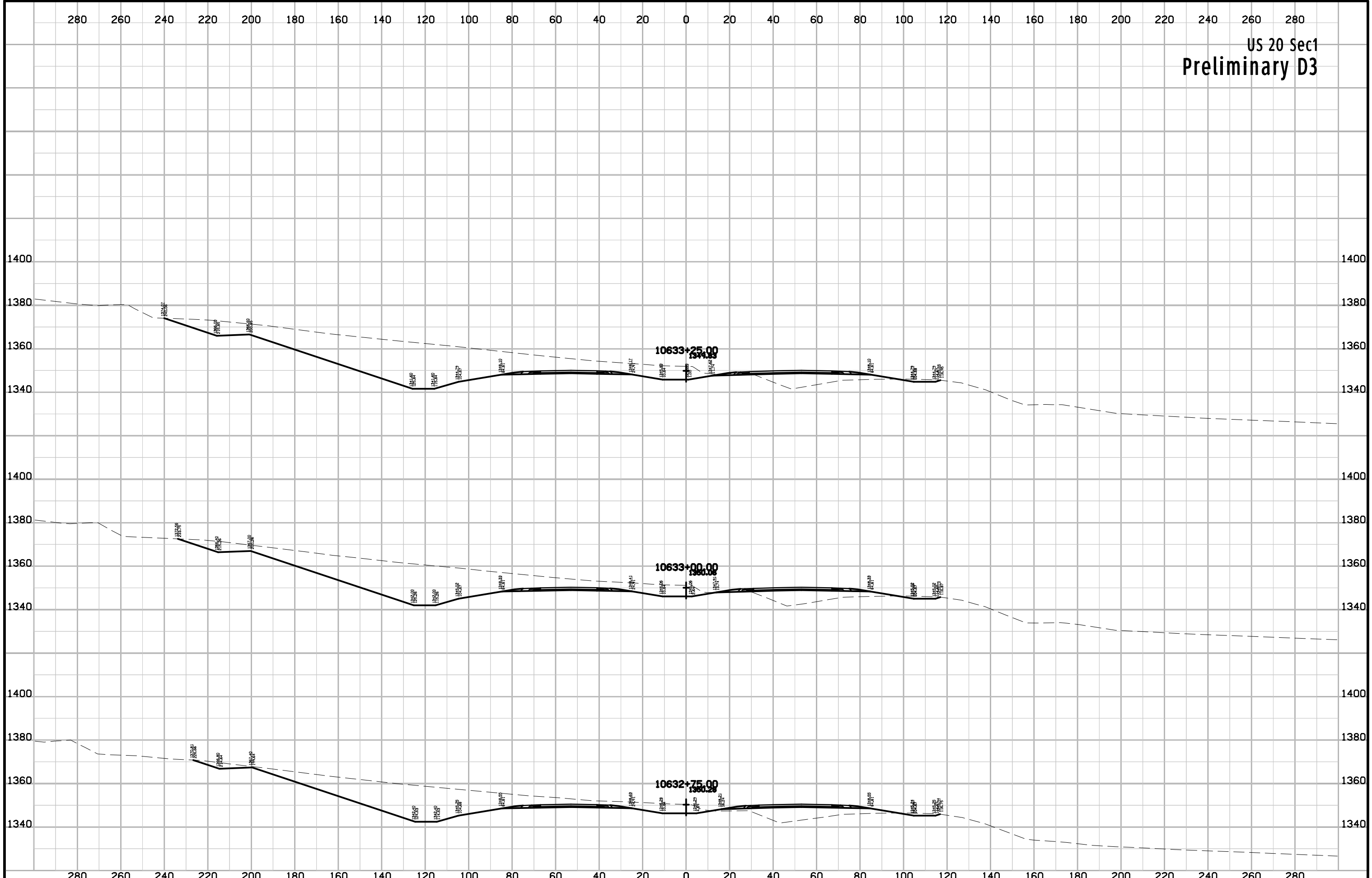
US 20 Sec1
Preliminary D3



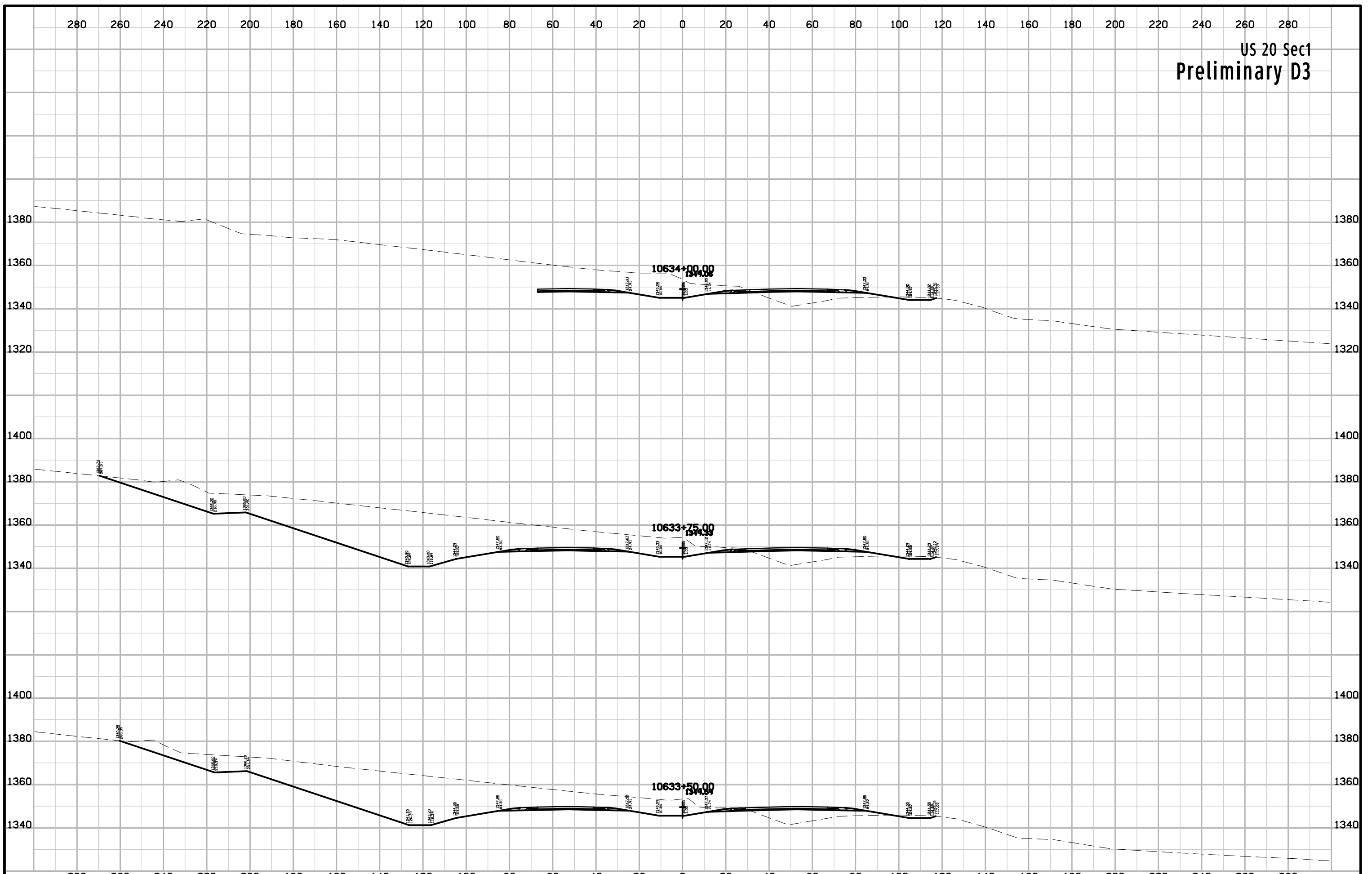
US 20 Sec1
Preliminary D3



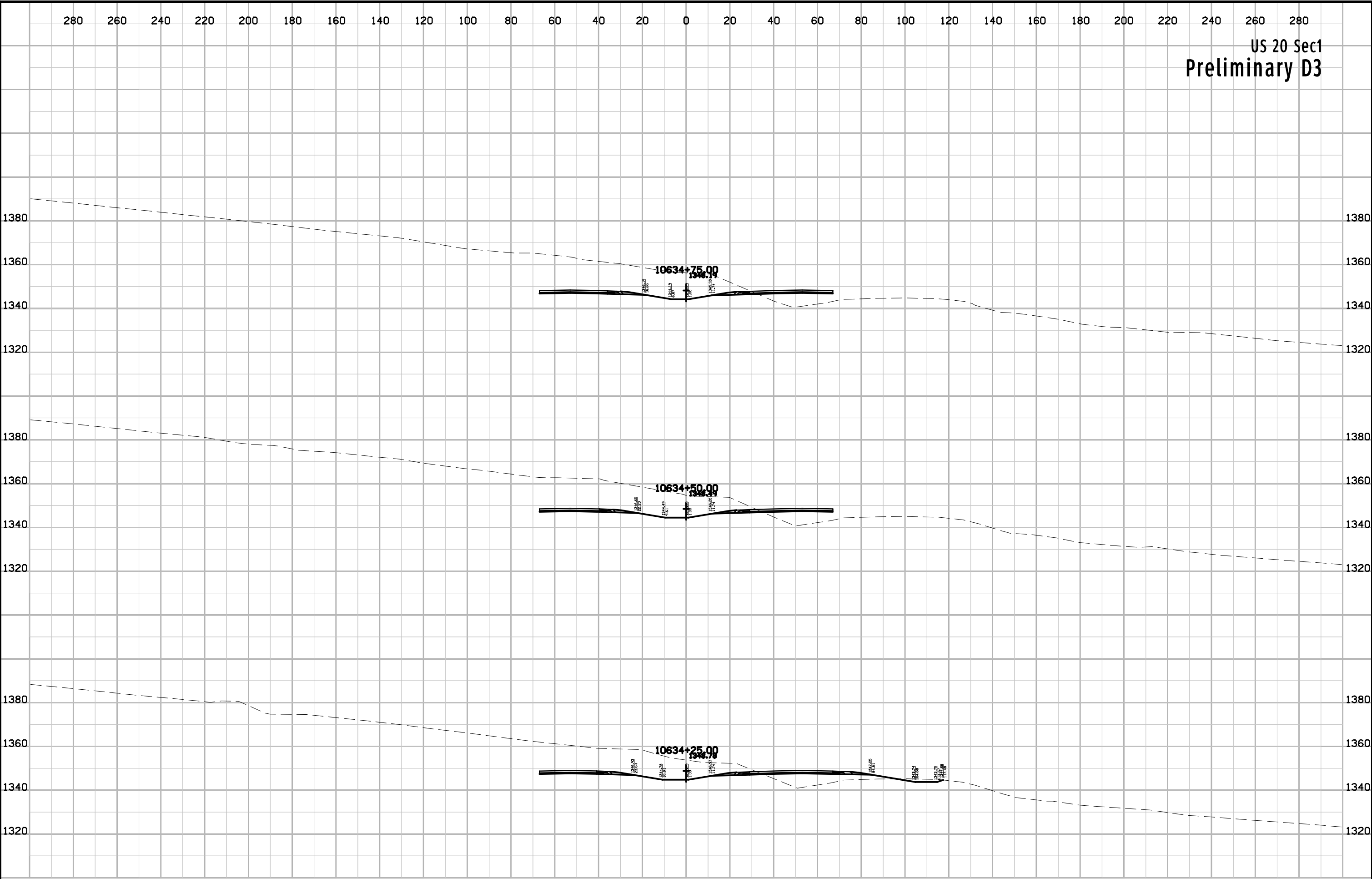
US 20 Sec1
Preliminary D3



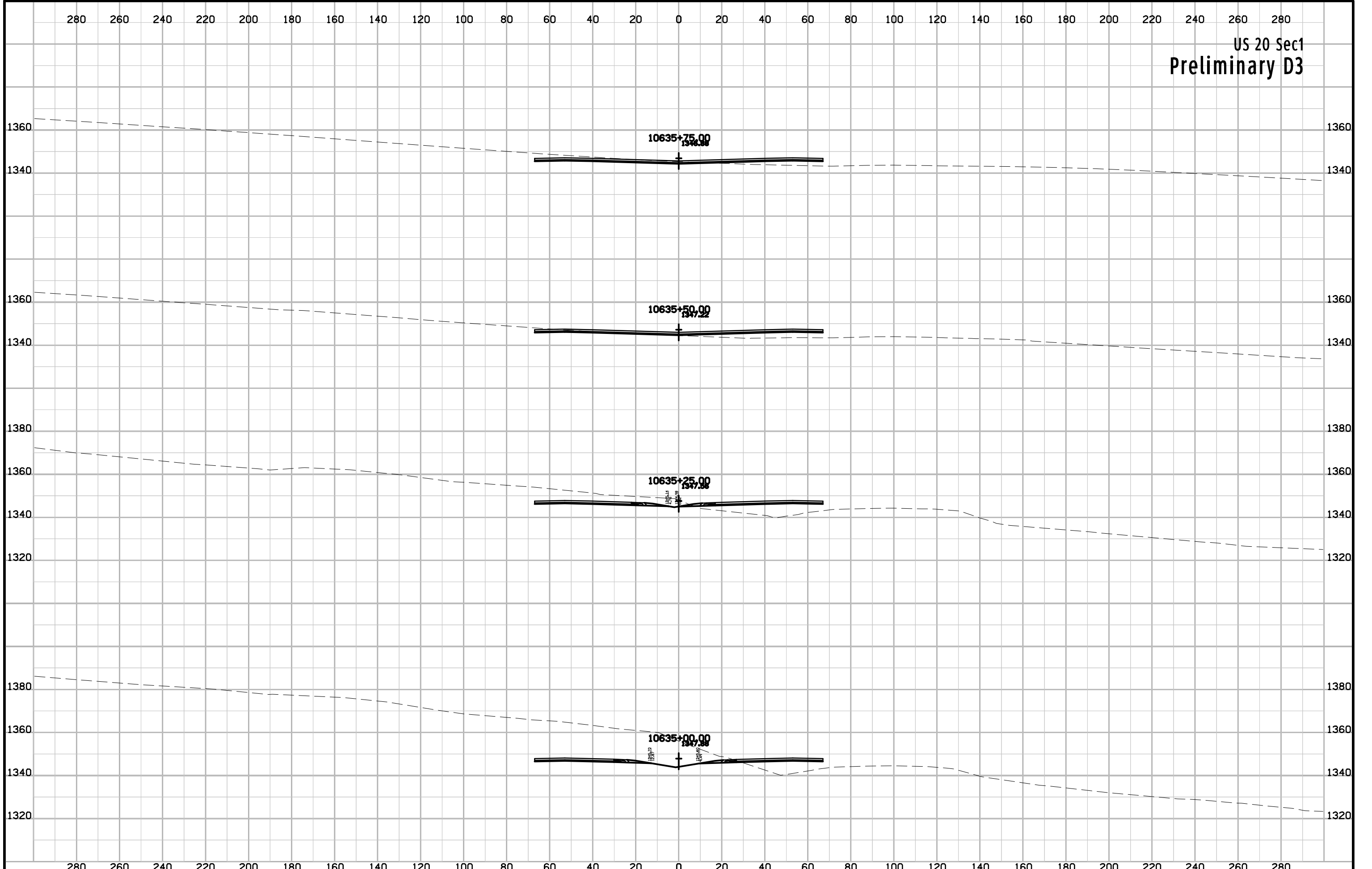
US 20 Sec1
Preliminary D3



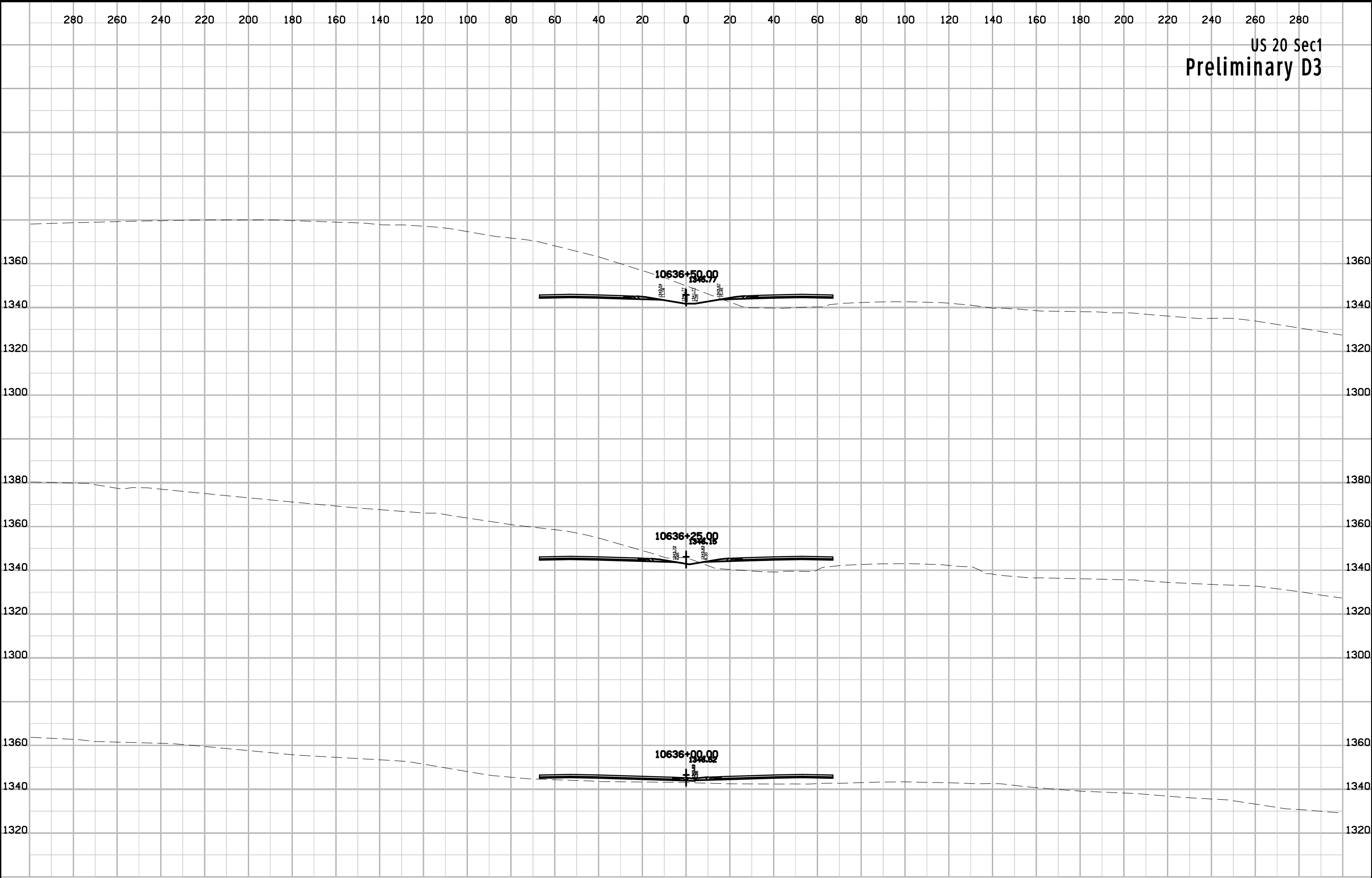
US 20 Sec1
Preliminary D3



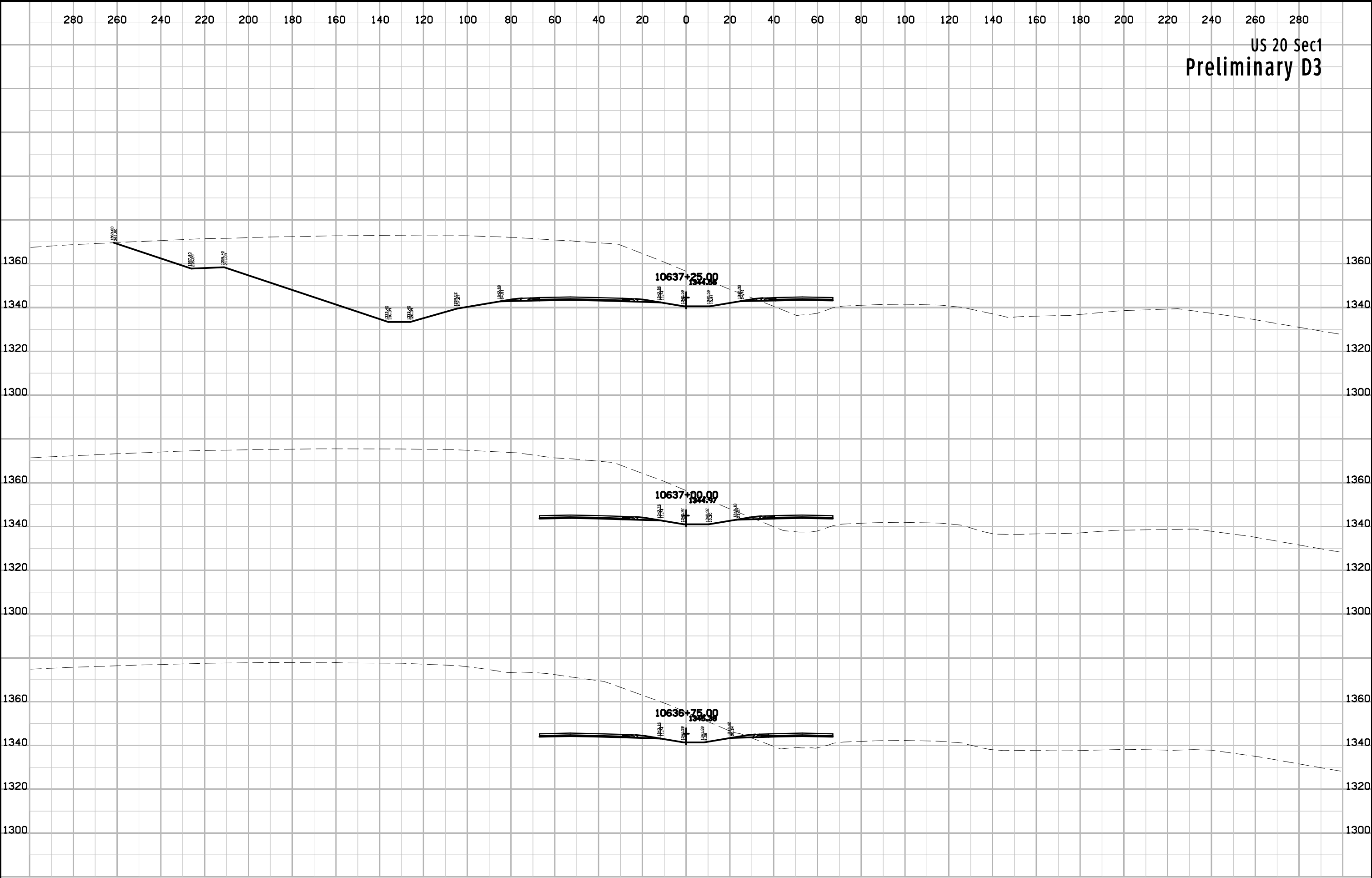
US 20 Sec1
Preliminary D3

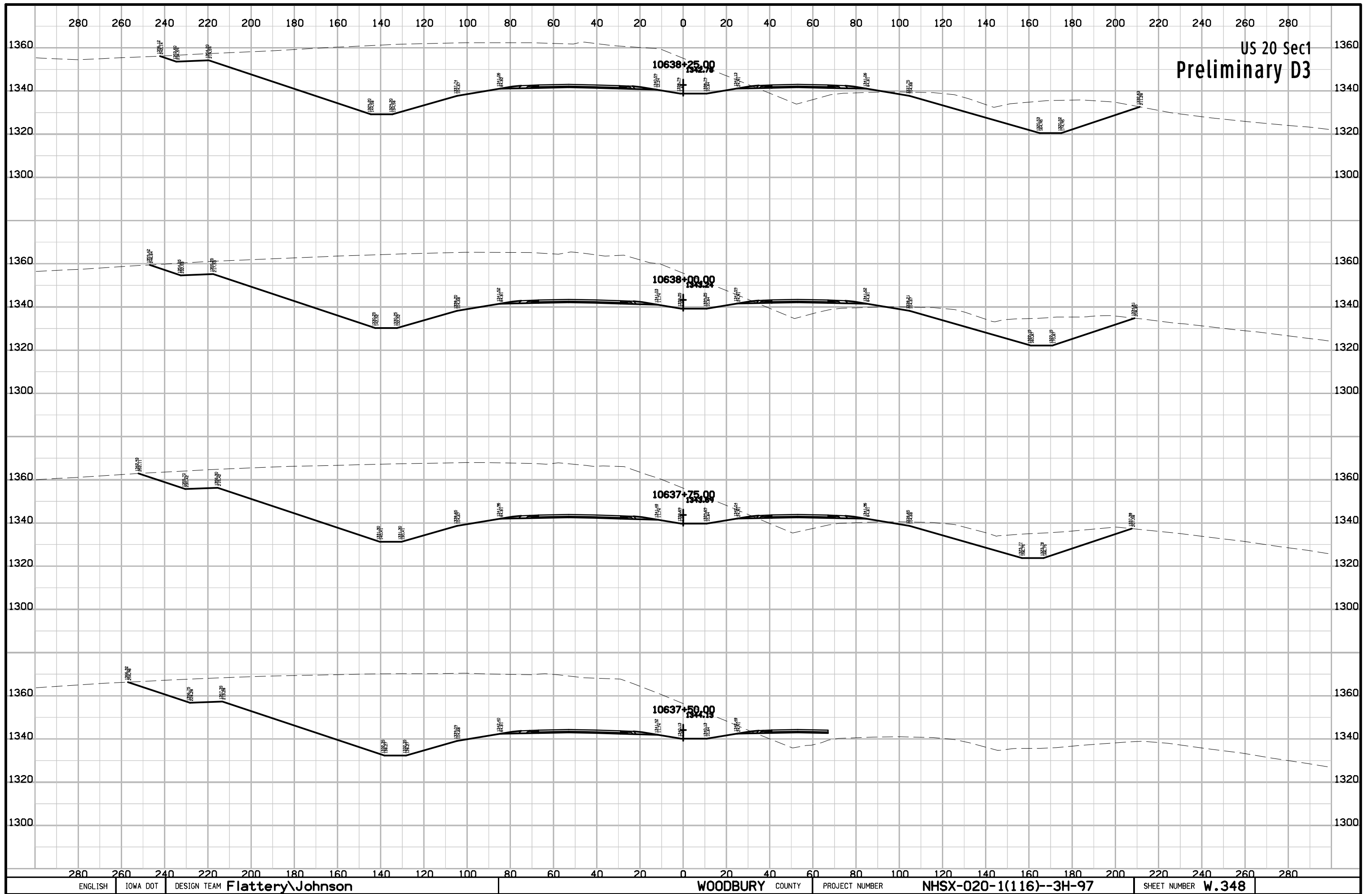


US 20 Sec1
Preliminary D3



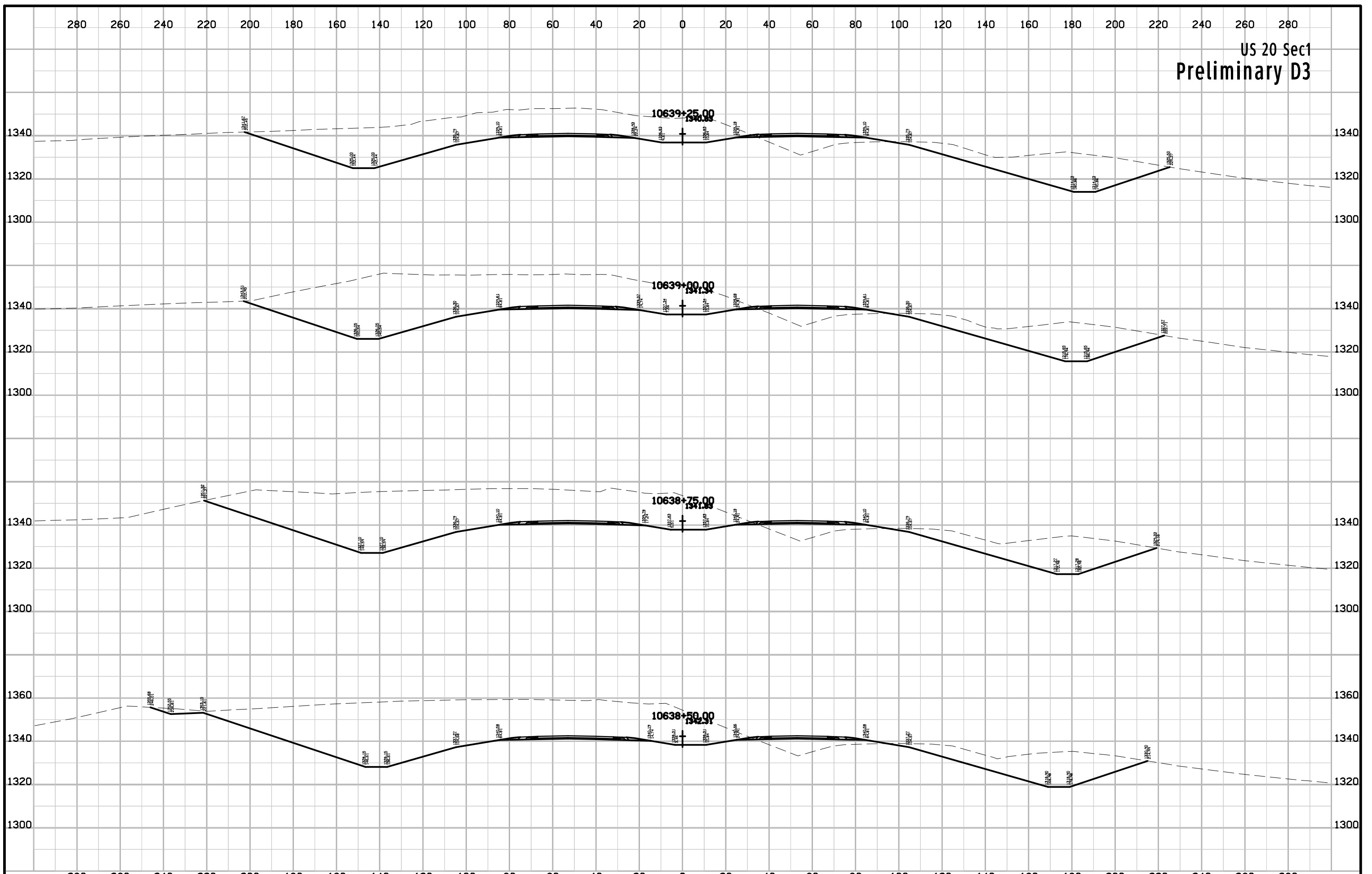
US 20 Sec1
Preliminary D3



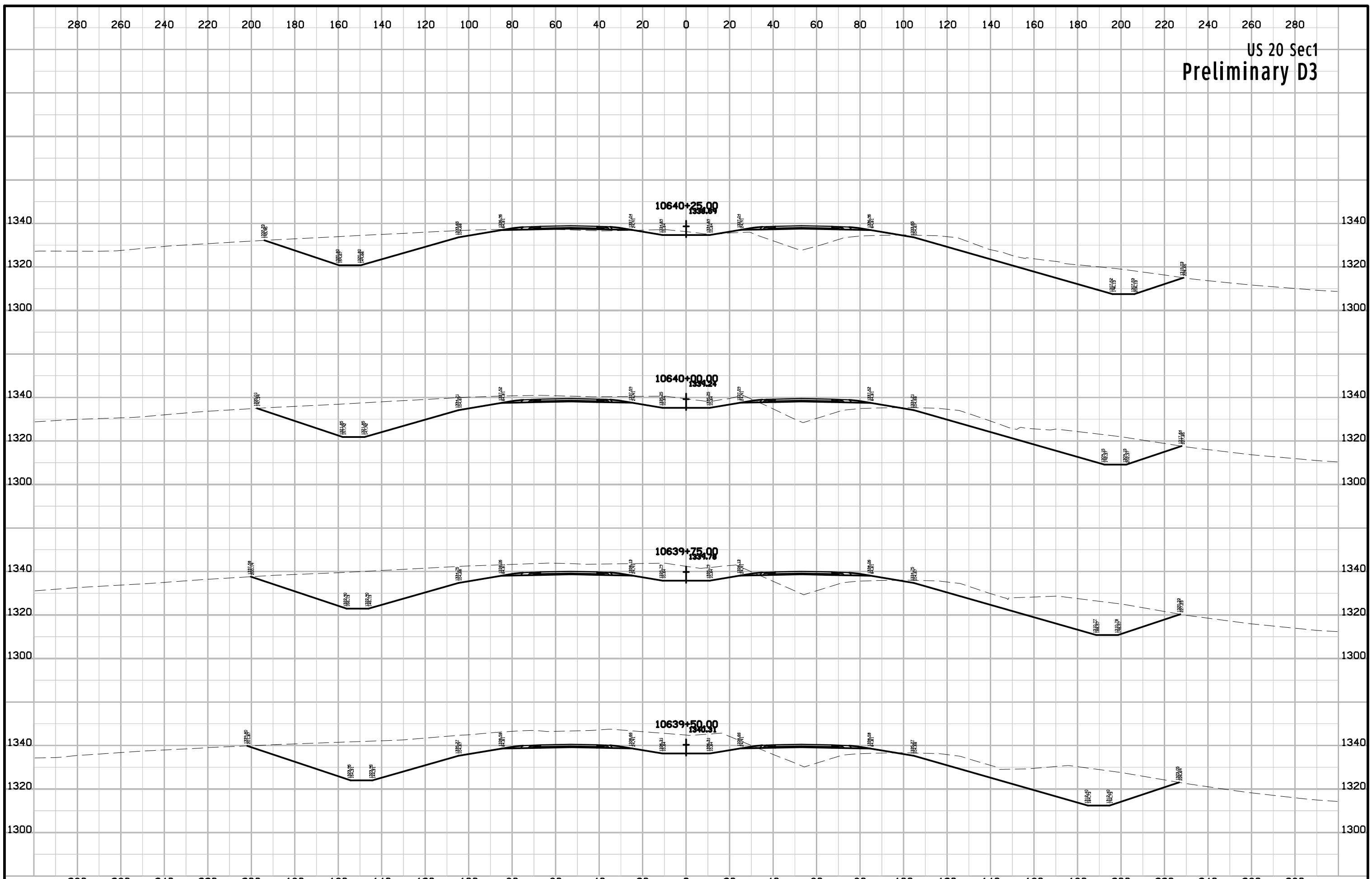


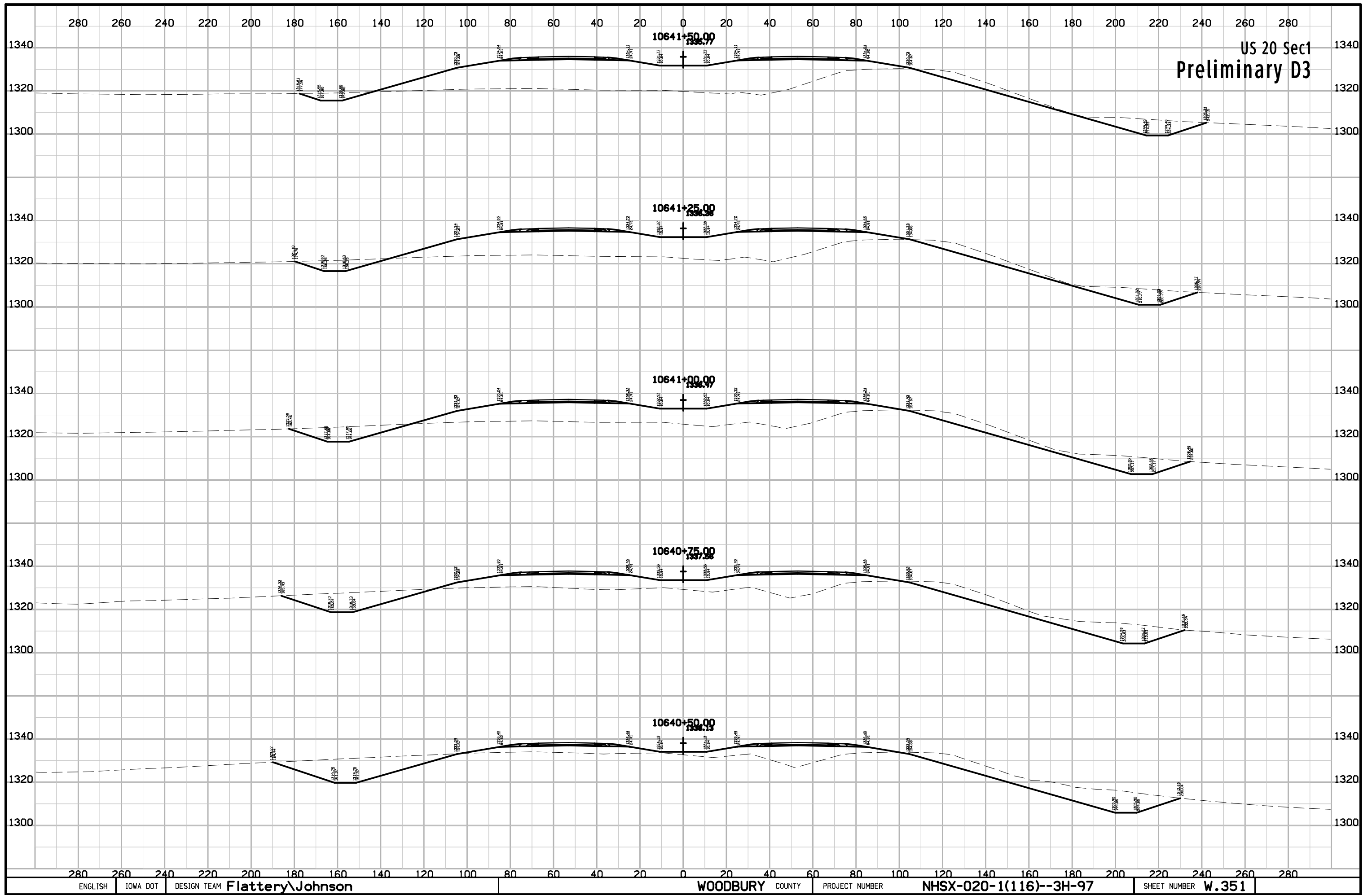
US 20 Sec1
Preliminary D3

US 20 Sec1
Preliminary D3

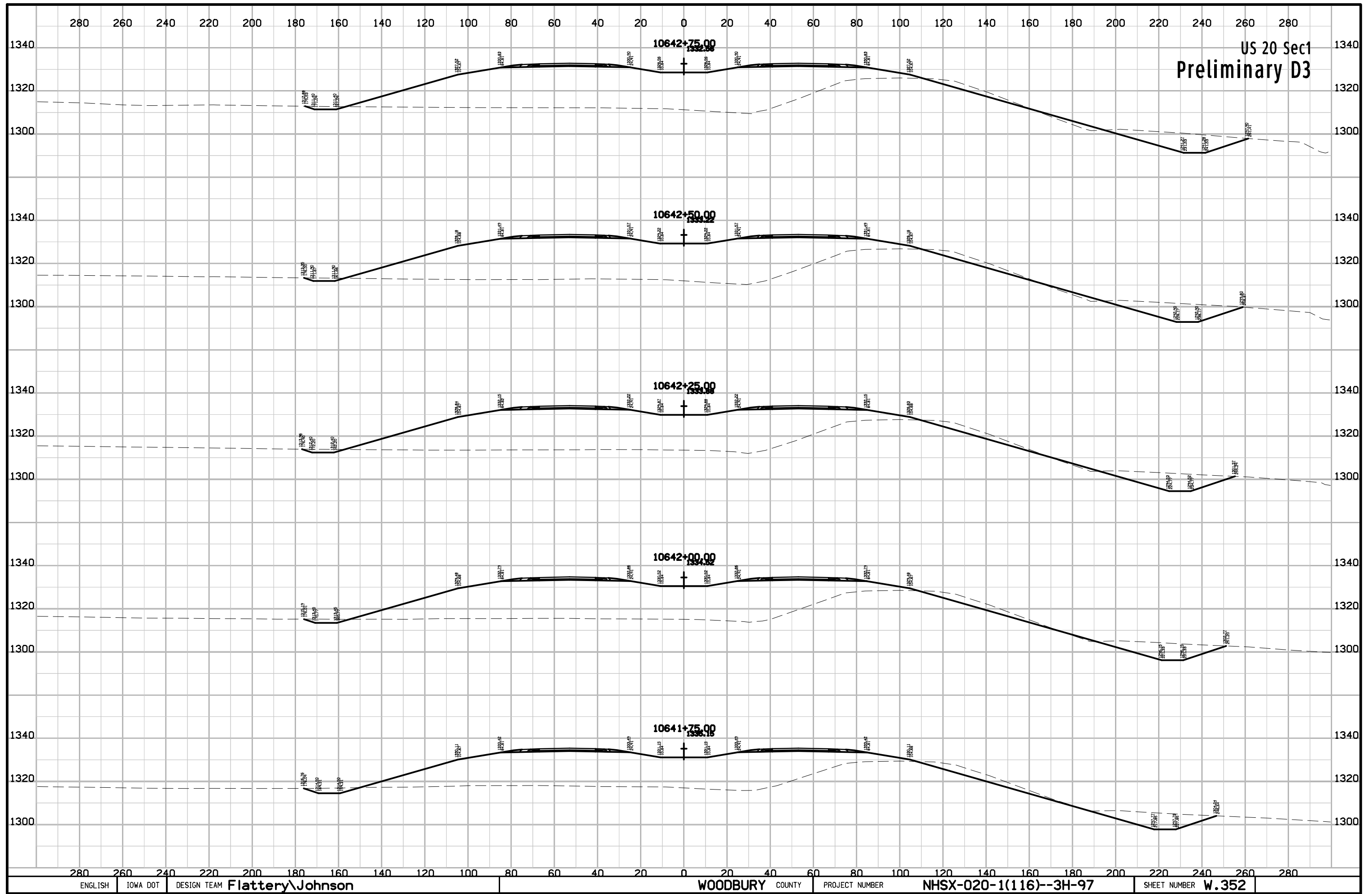


US 20 Sec1
Preliminary D3



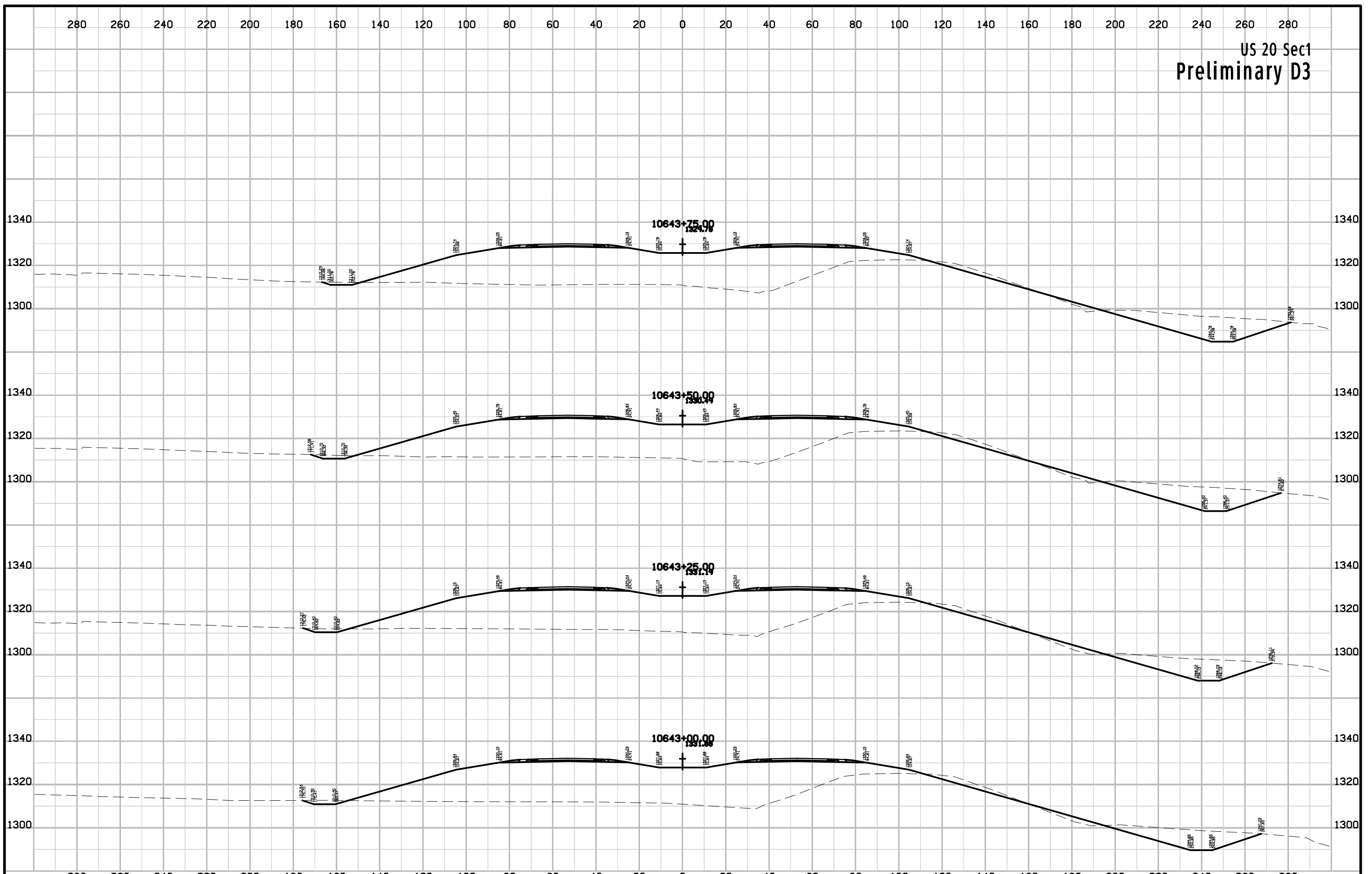


US 20 Sec1
Preliminary D3

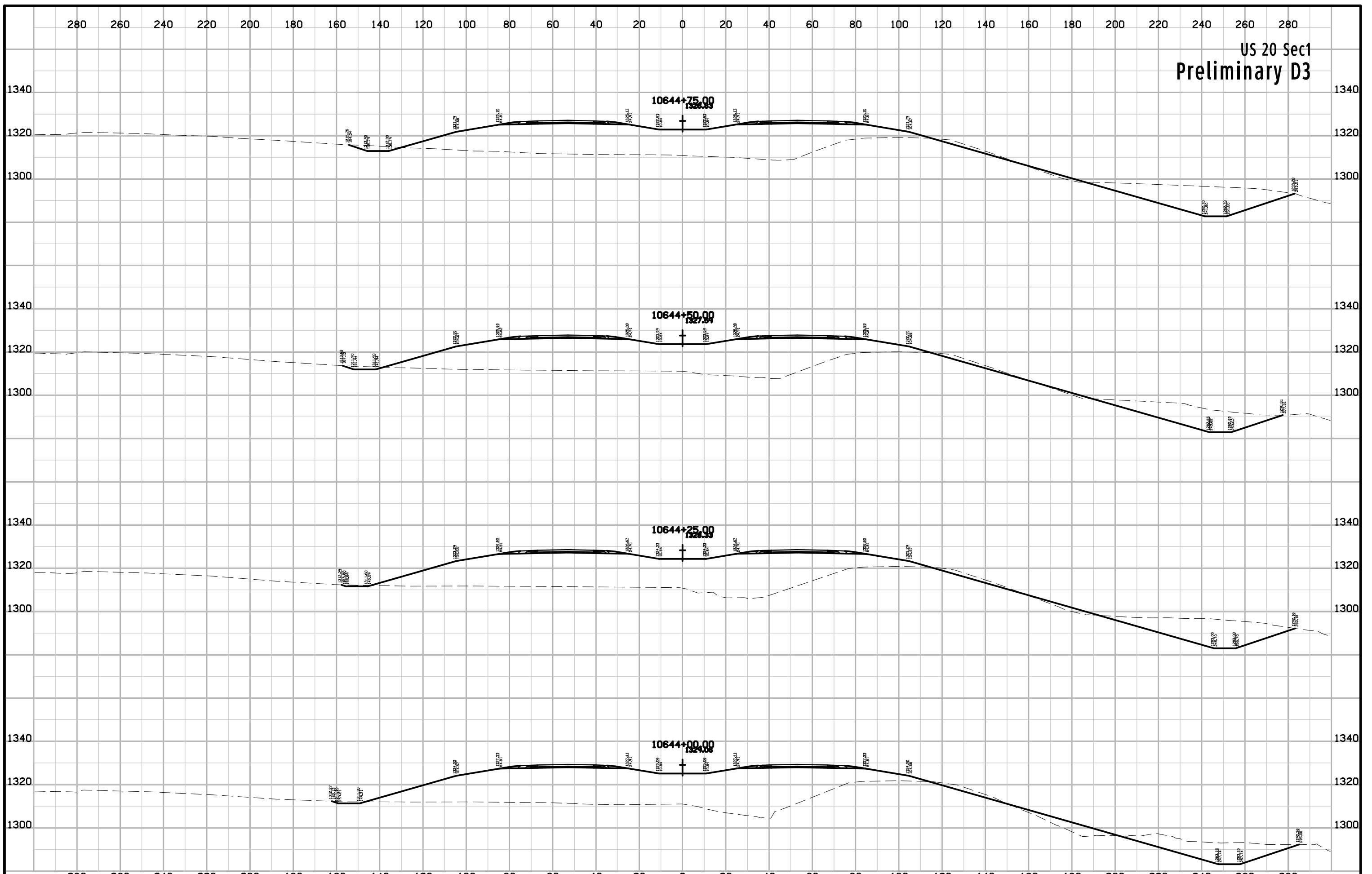


US 20 Sec1
Preliminary D3

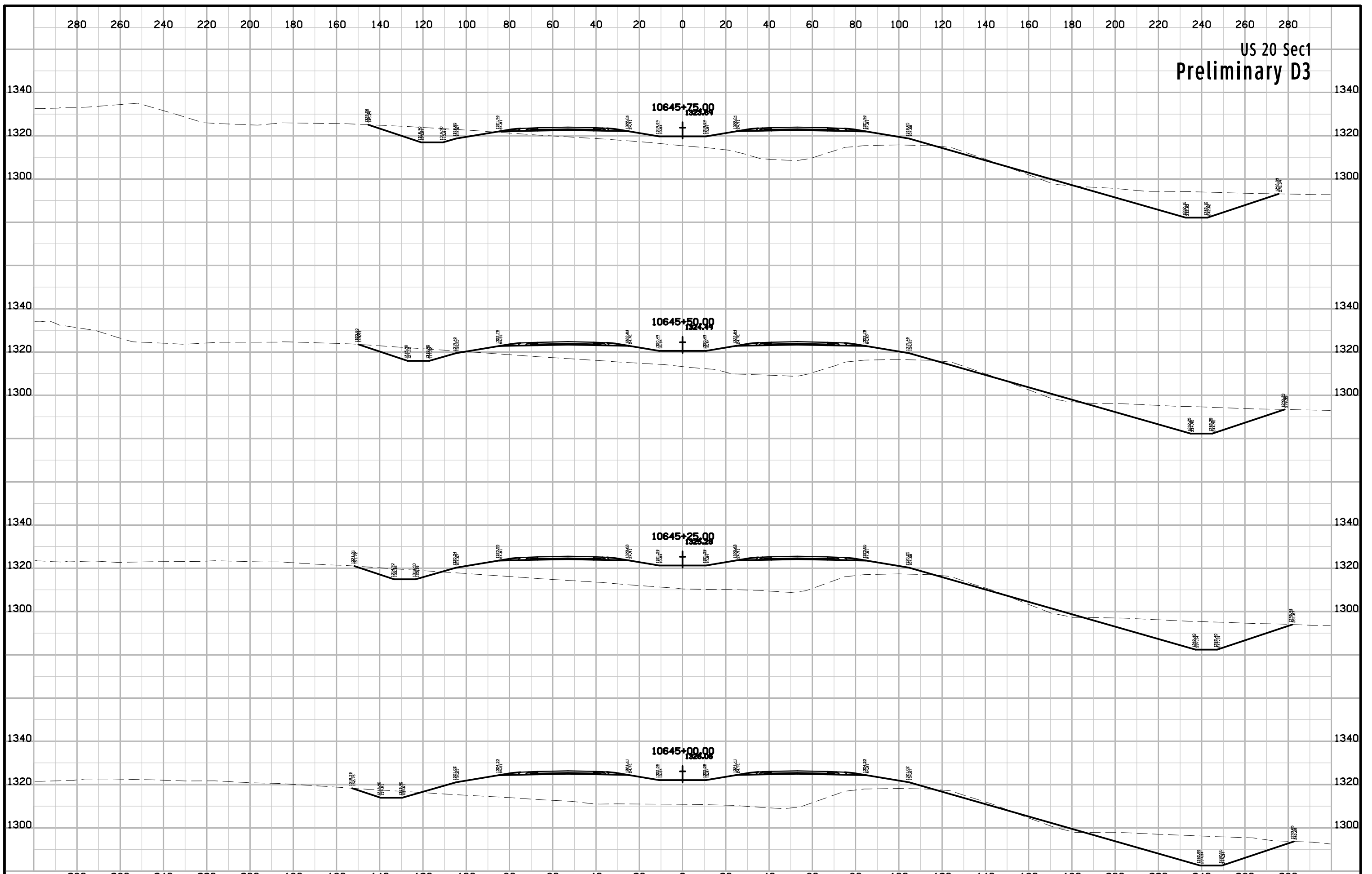
US 20 Sec1
Preliminary D3



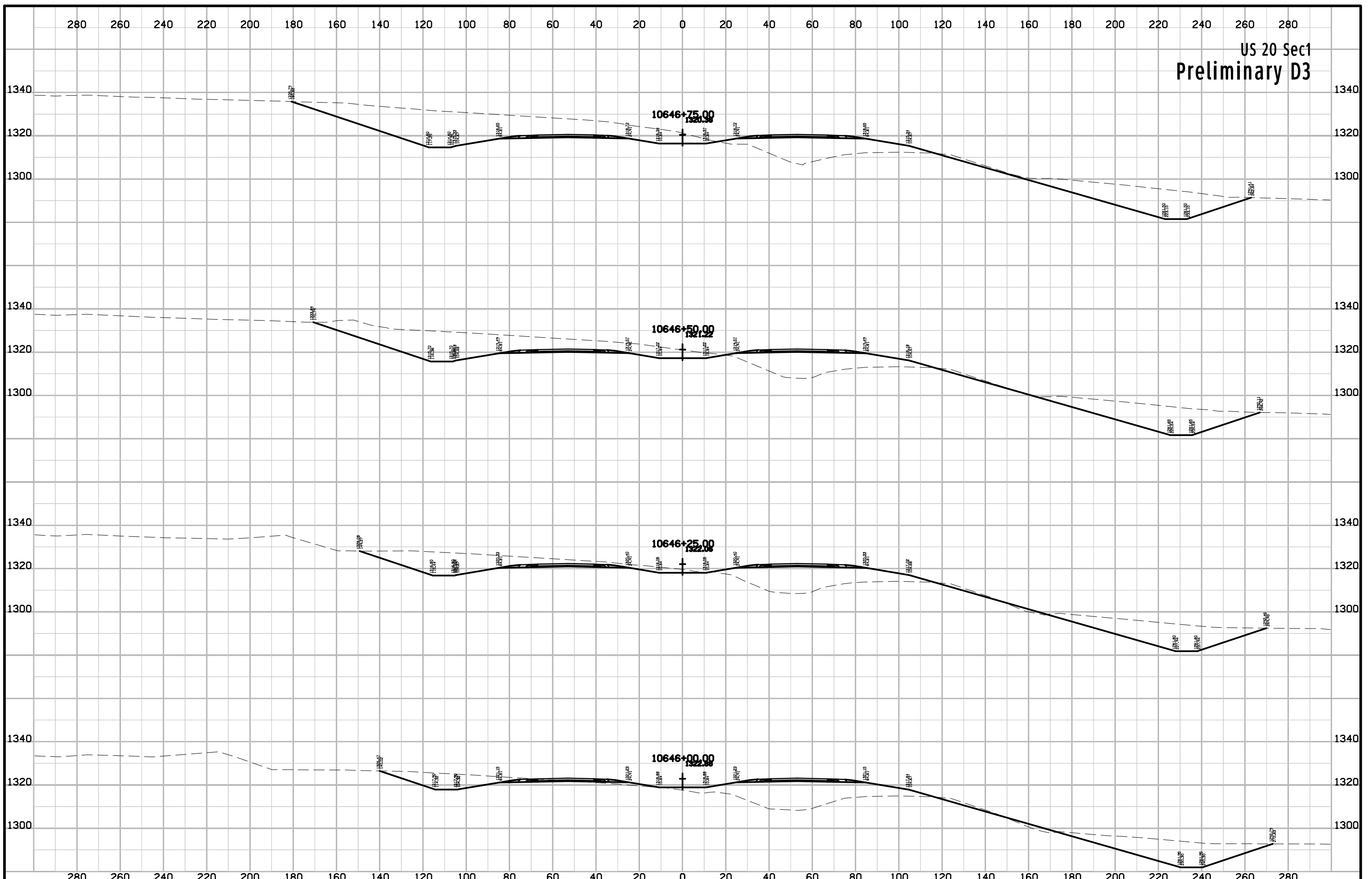
US 20 Sec1
Preliminary D3



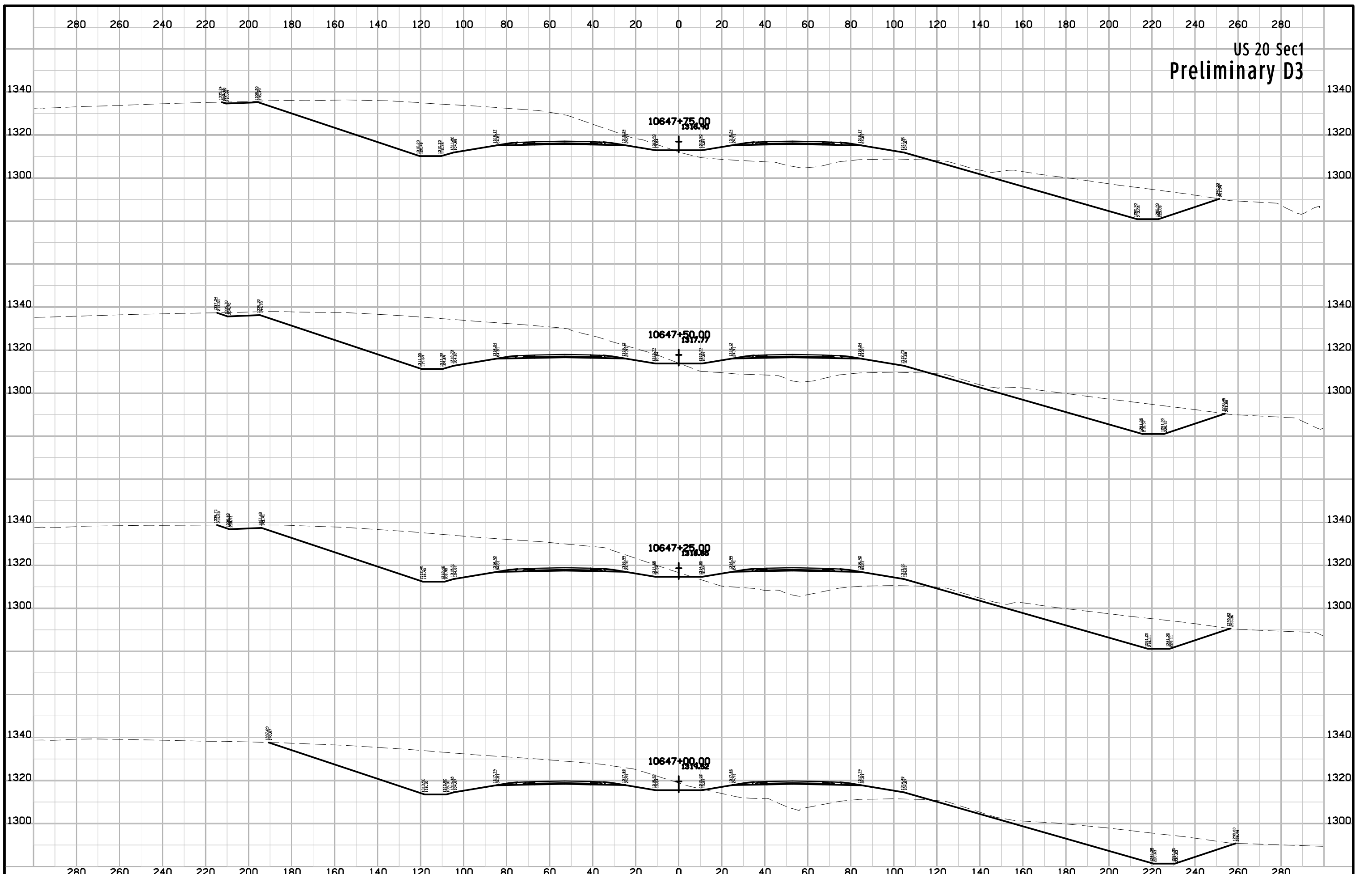
US 20 Sec1
Preliminary D3



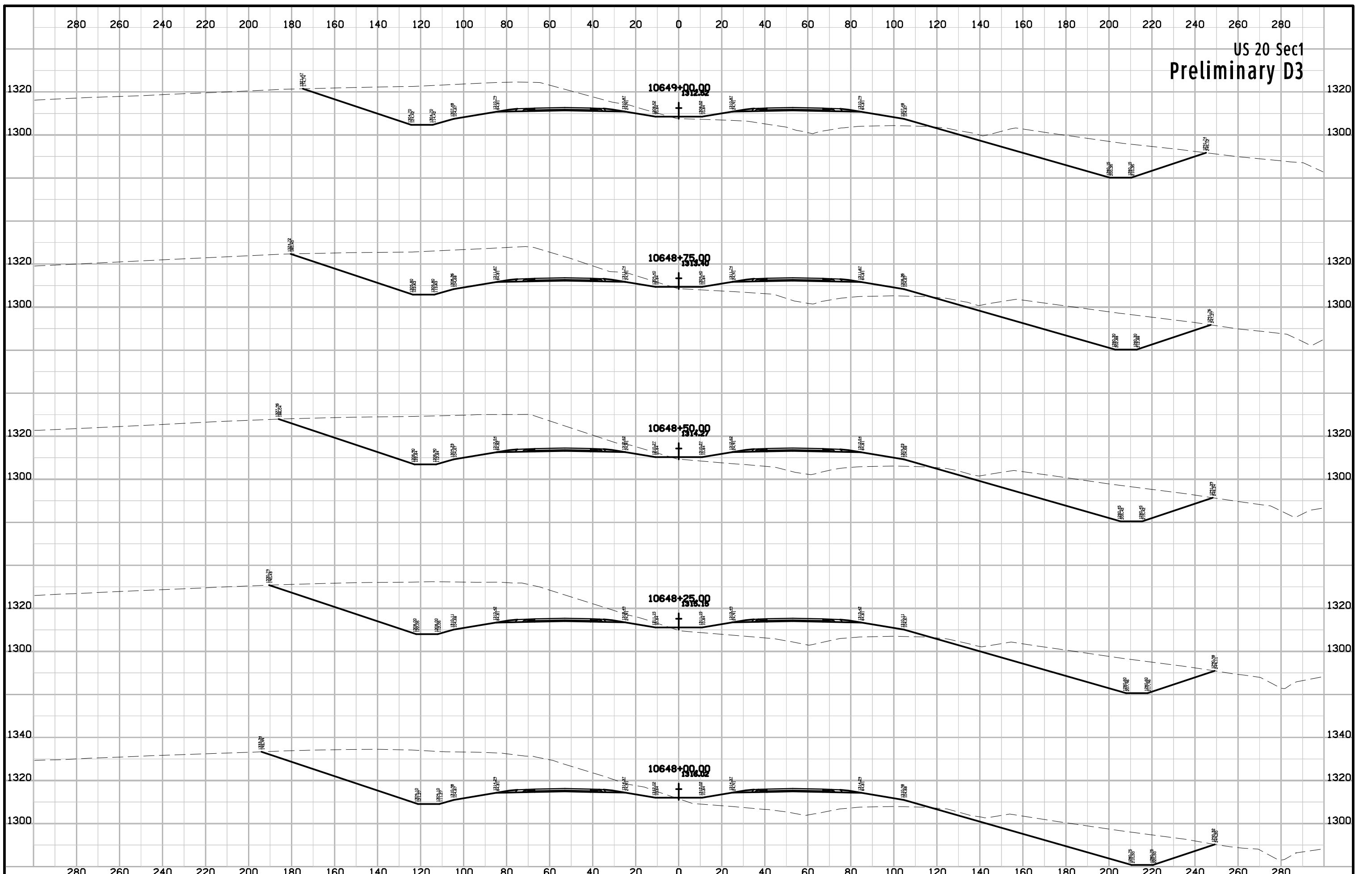
US 20 Sec1
Preliminary D3



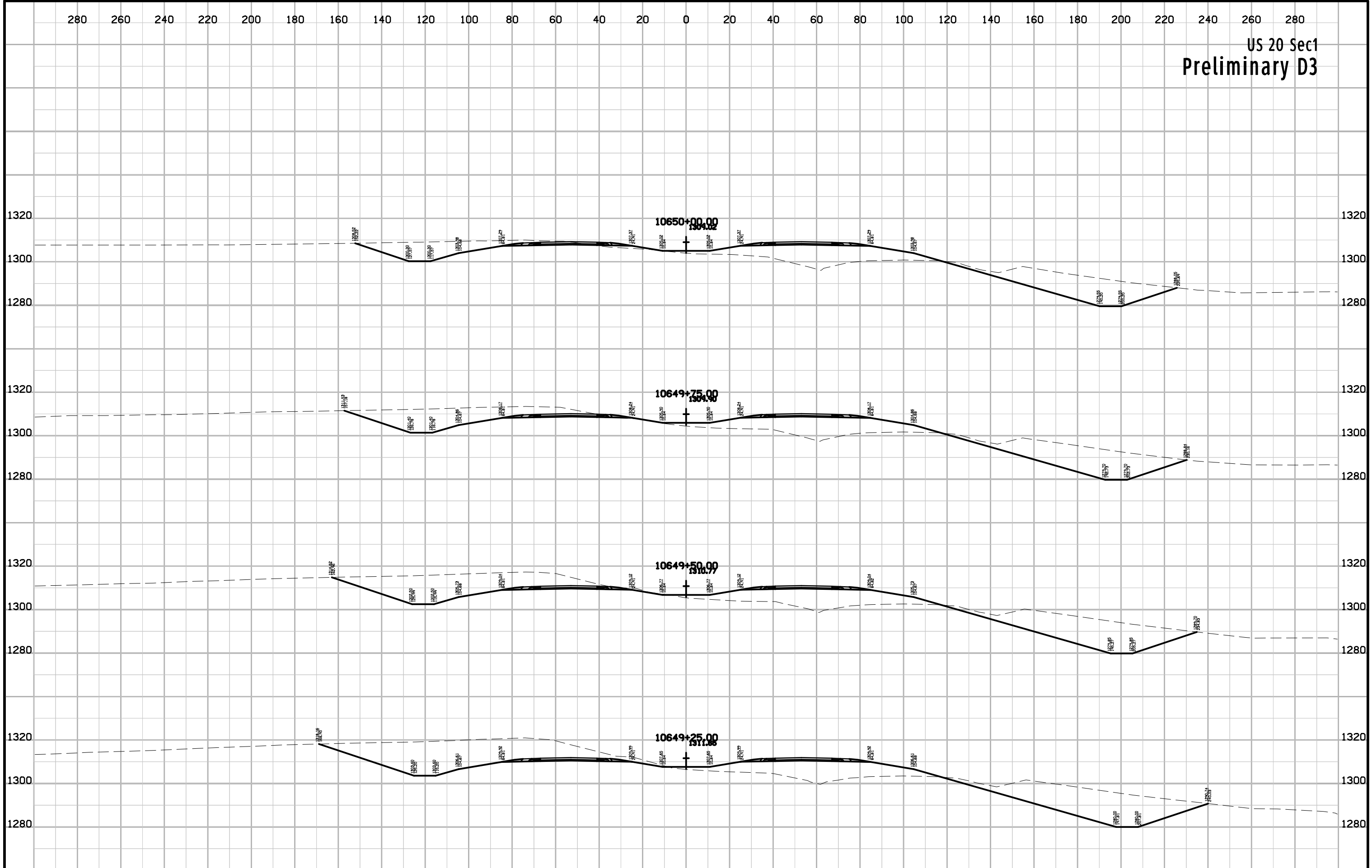
US 20 Sec1
Preliminary D3



US 20 Sec1
Preliminary D3



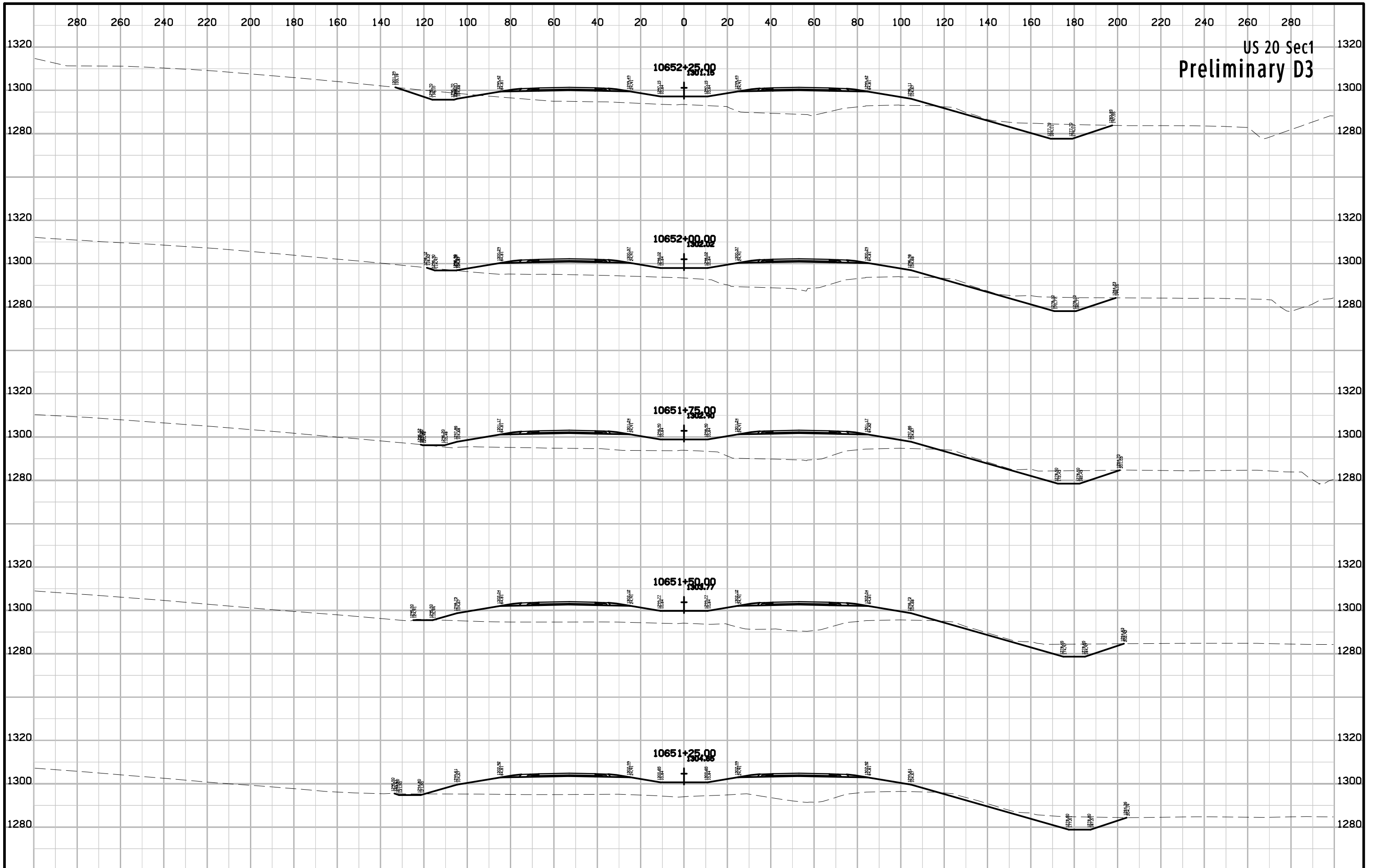
US 20 Sec1
Preliminary D3



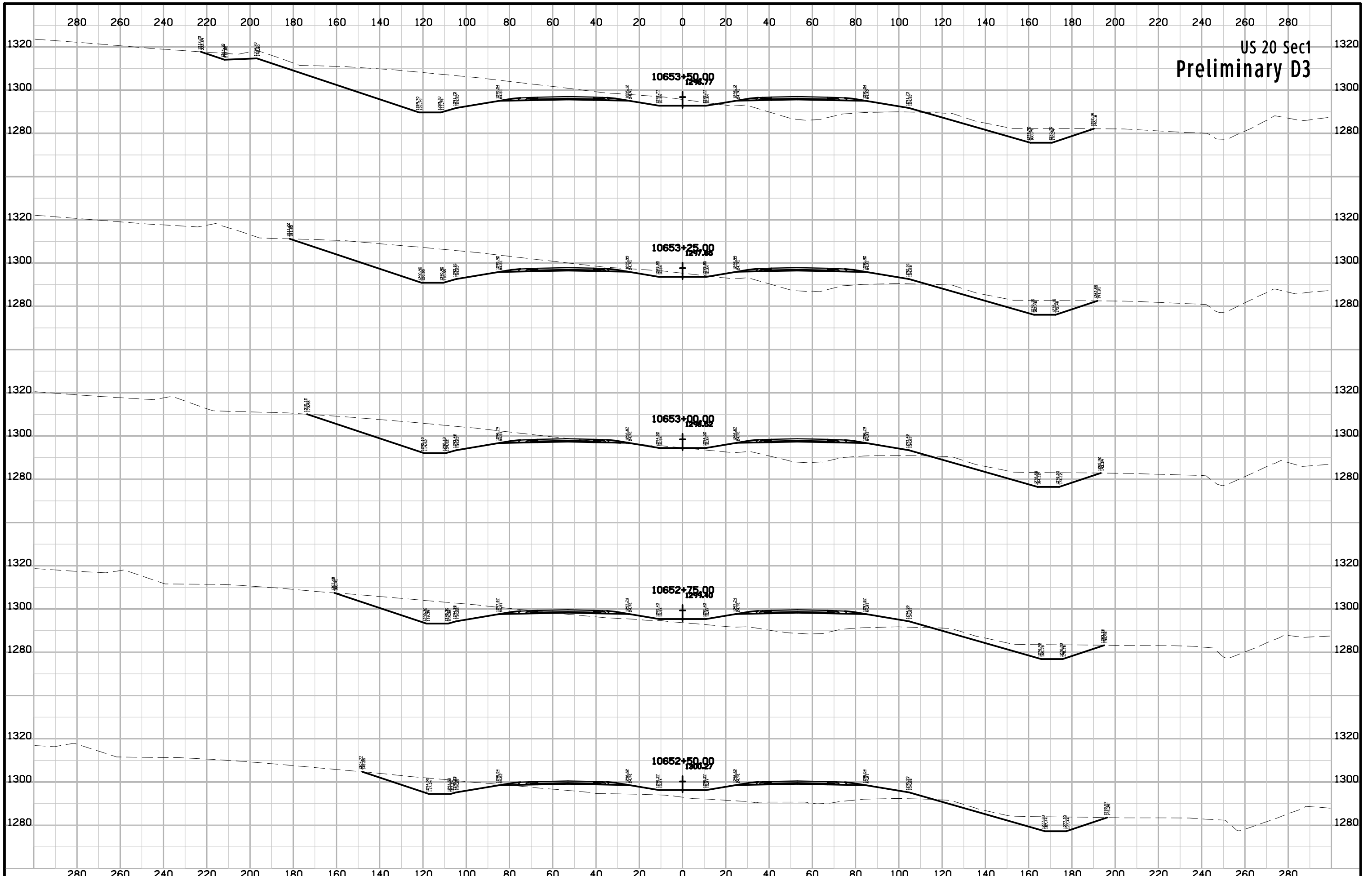
US 20 Sec1
Preliminary D3



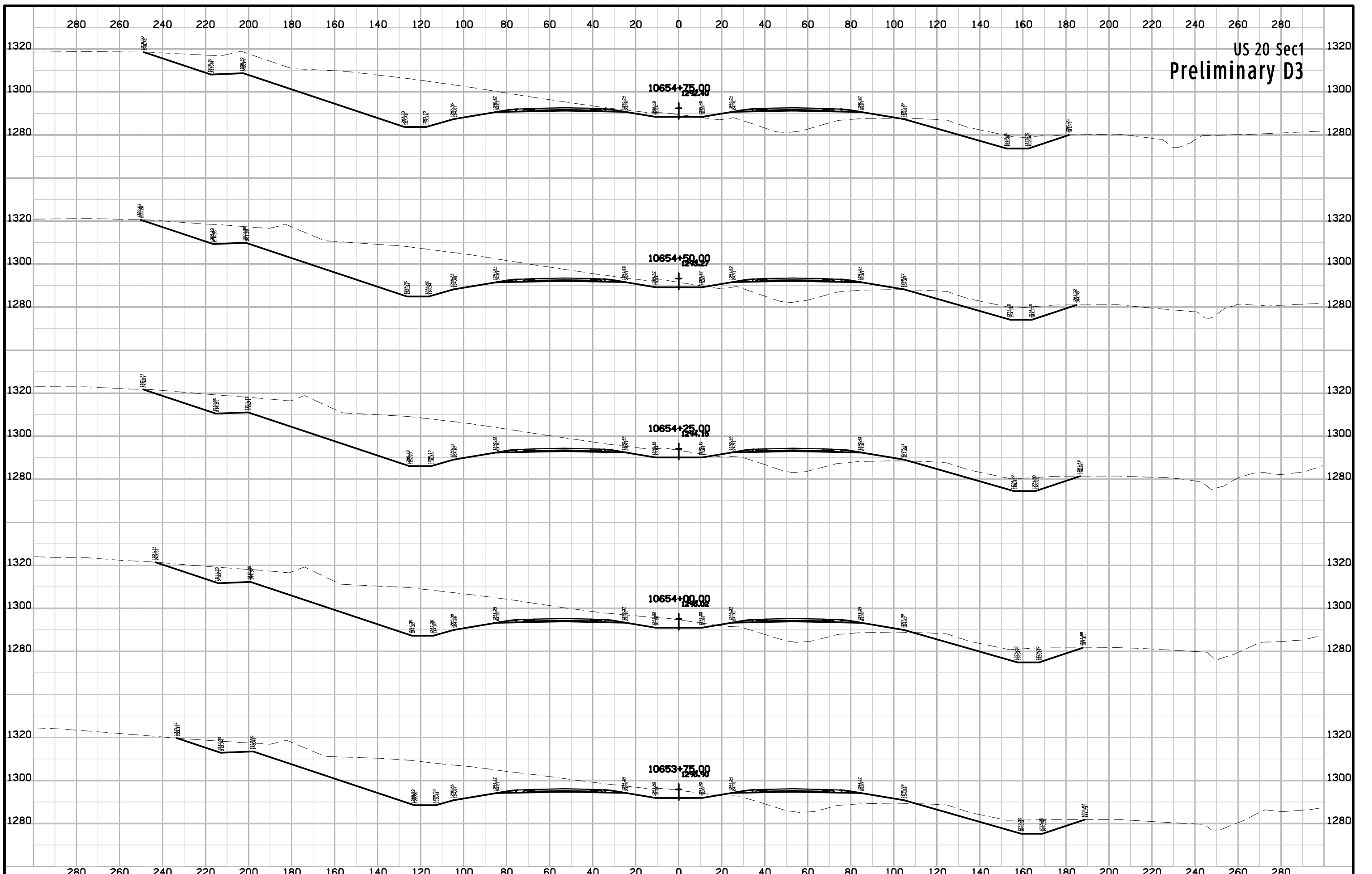
US 20 Sec1
Preliminary D3



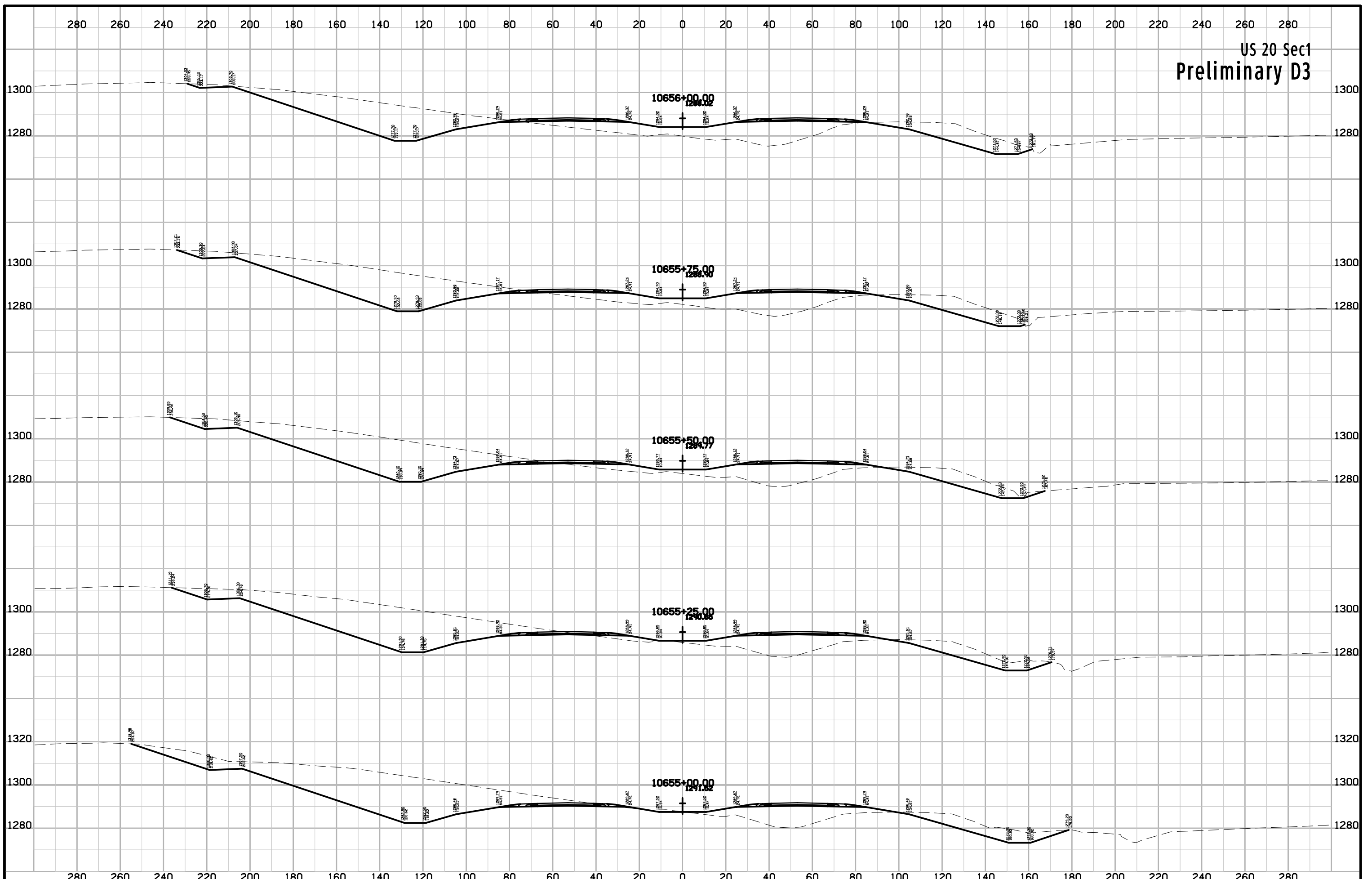
US 20 Sec1
Preliminary D3



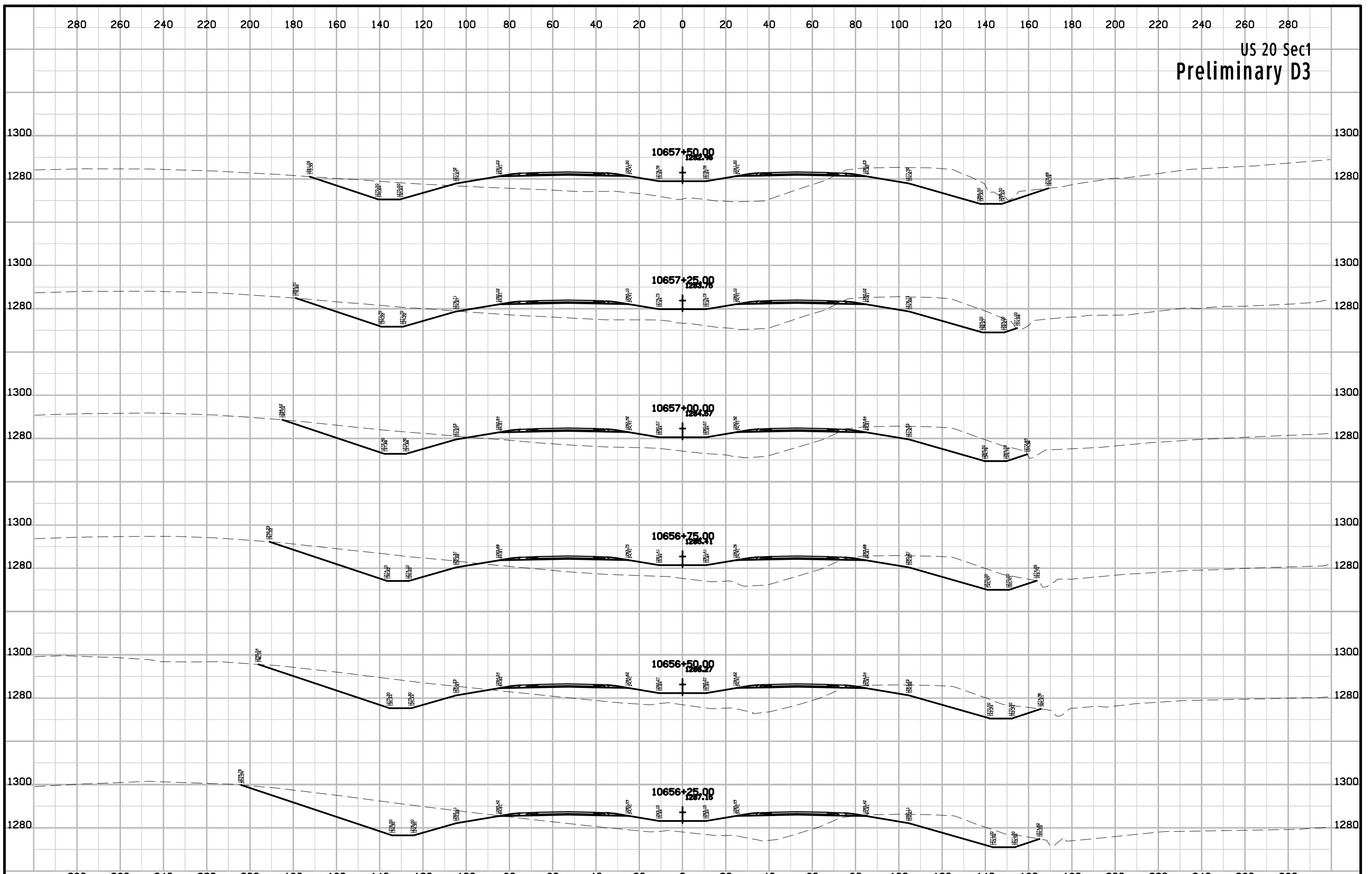
US 20 Sec1
Preliminary D3



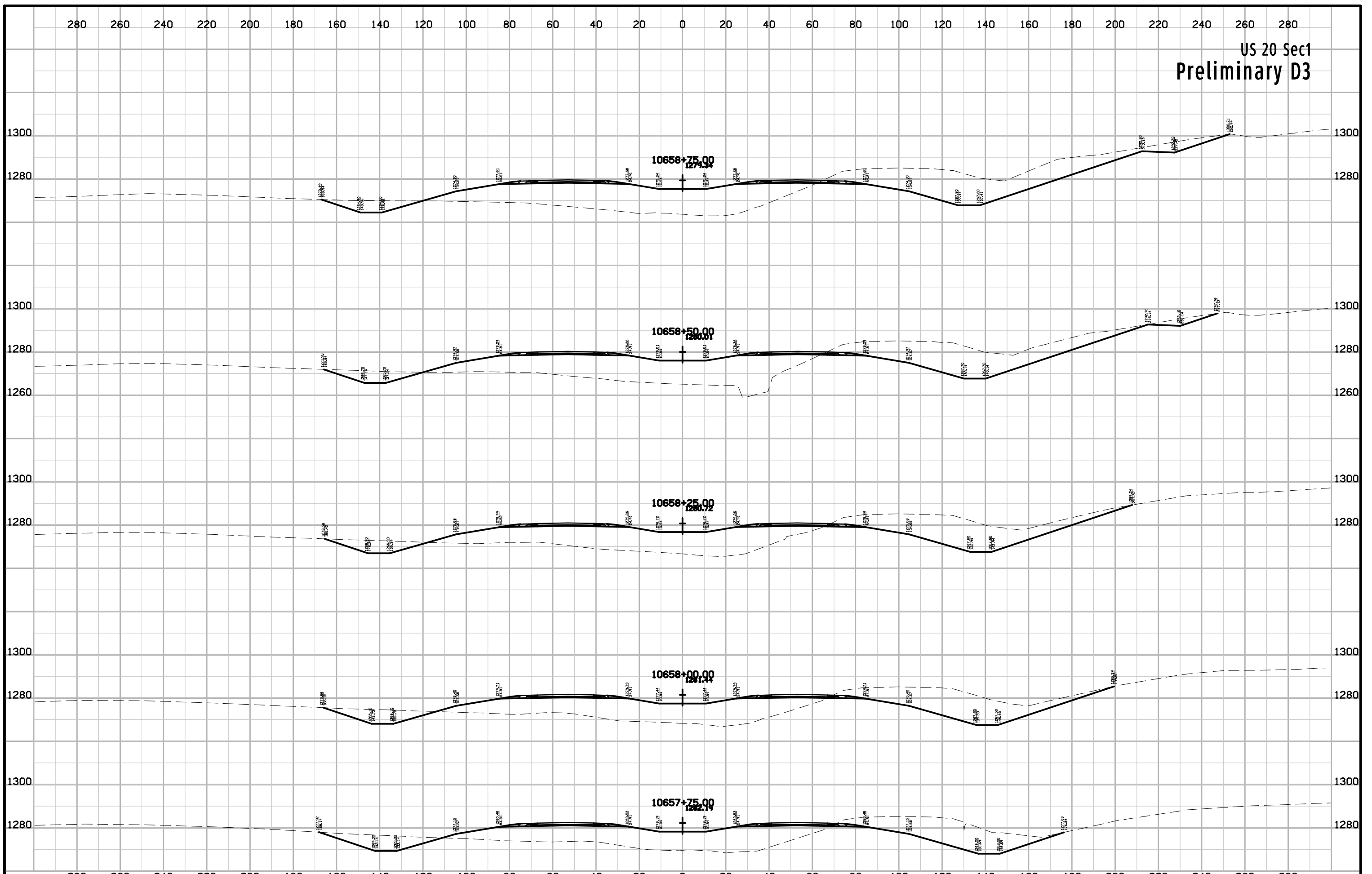
US 20 Sec1
Preliminary D3



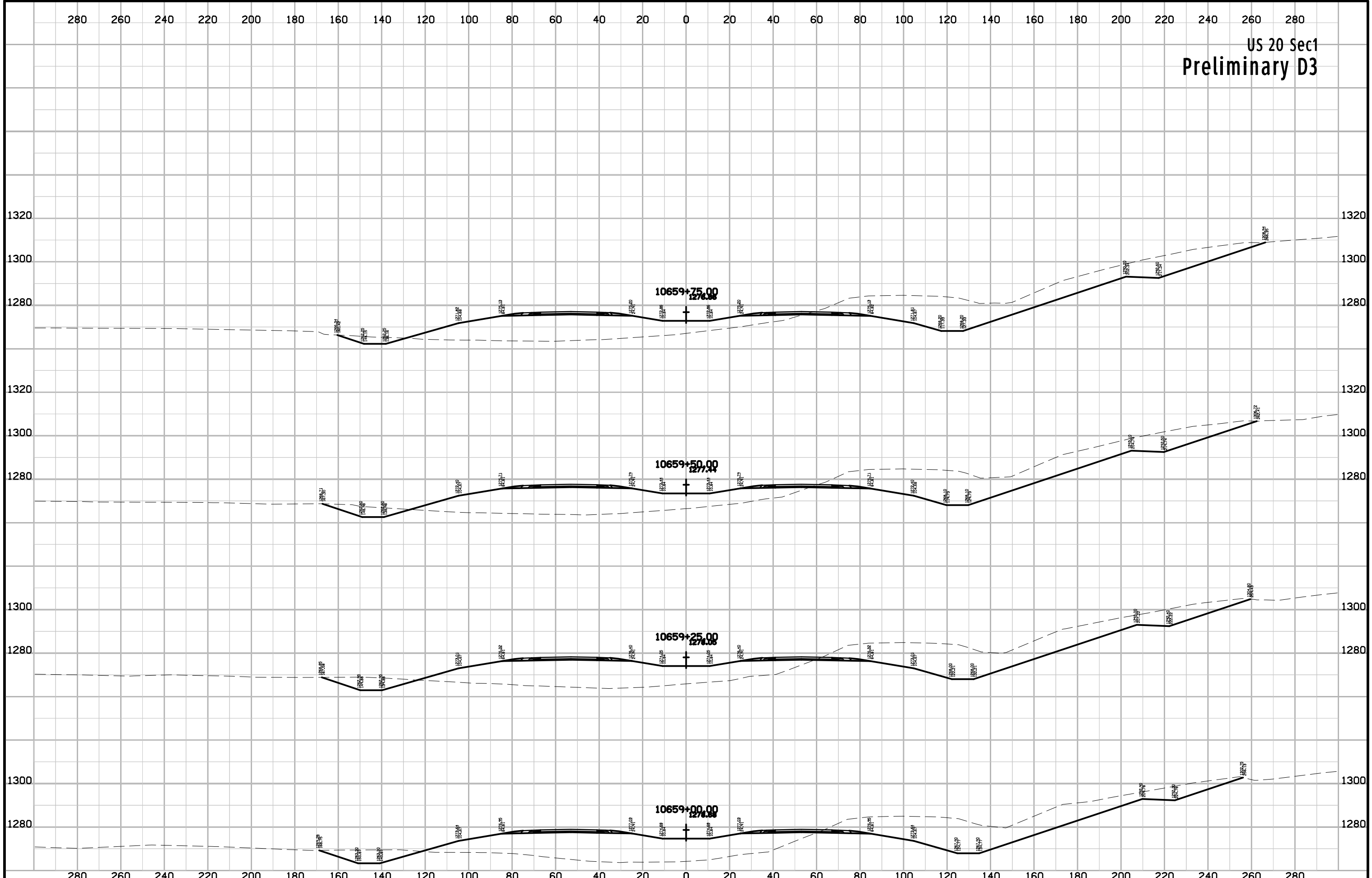
US 20 Sec1
Preliminary D3



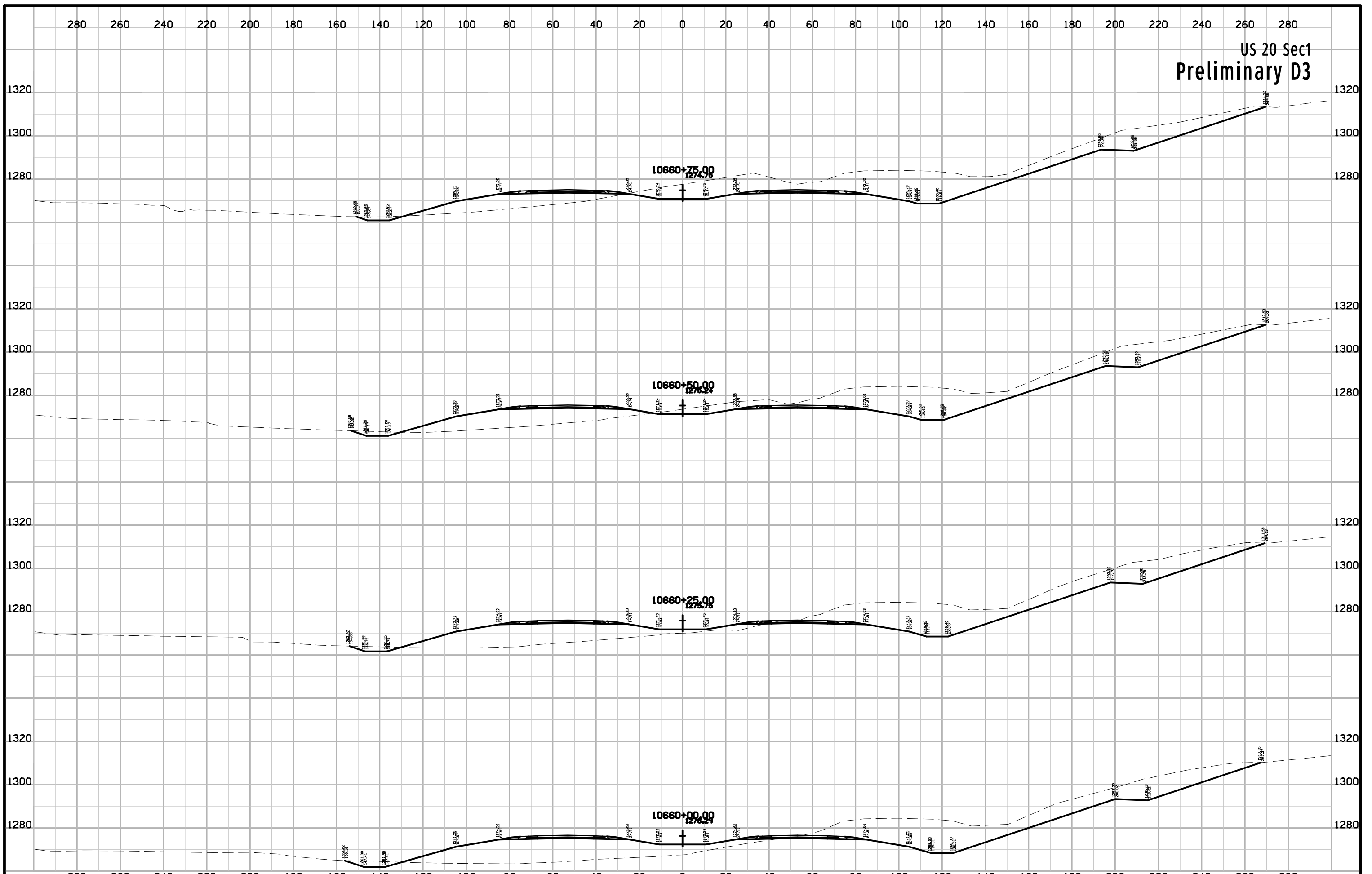
US 20 Sec1
Preliminary D3



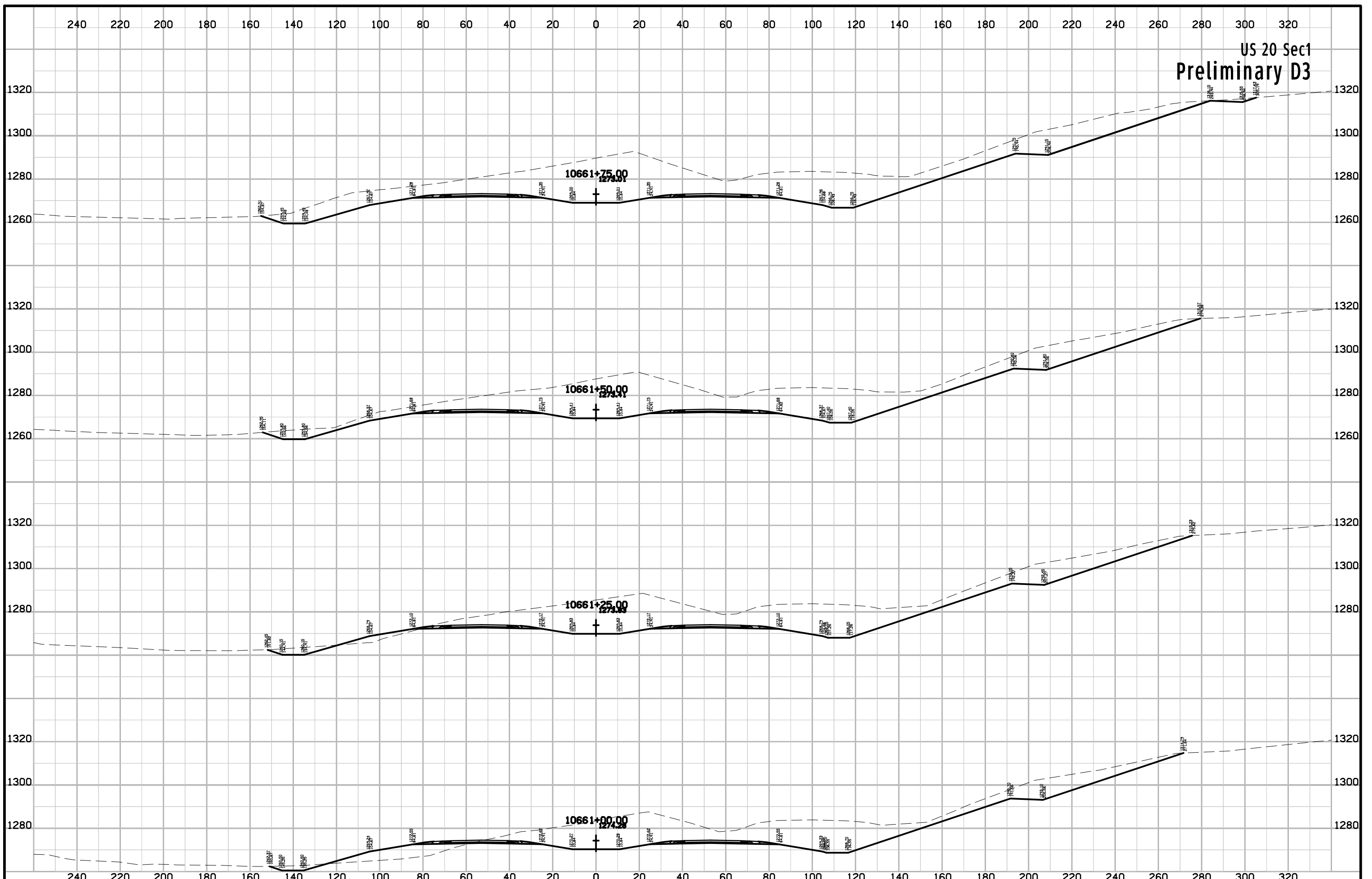
US 20 Sec1
Preliminary D3



US 20 Sec1
Preliminary D3

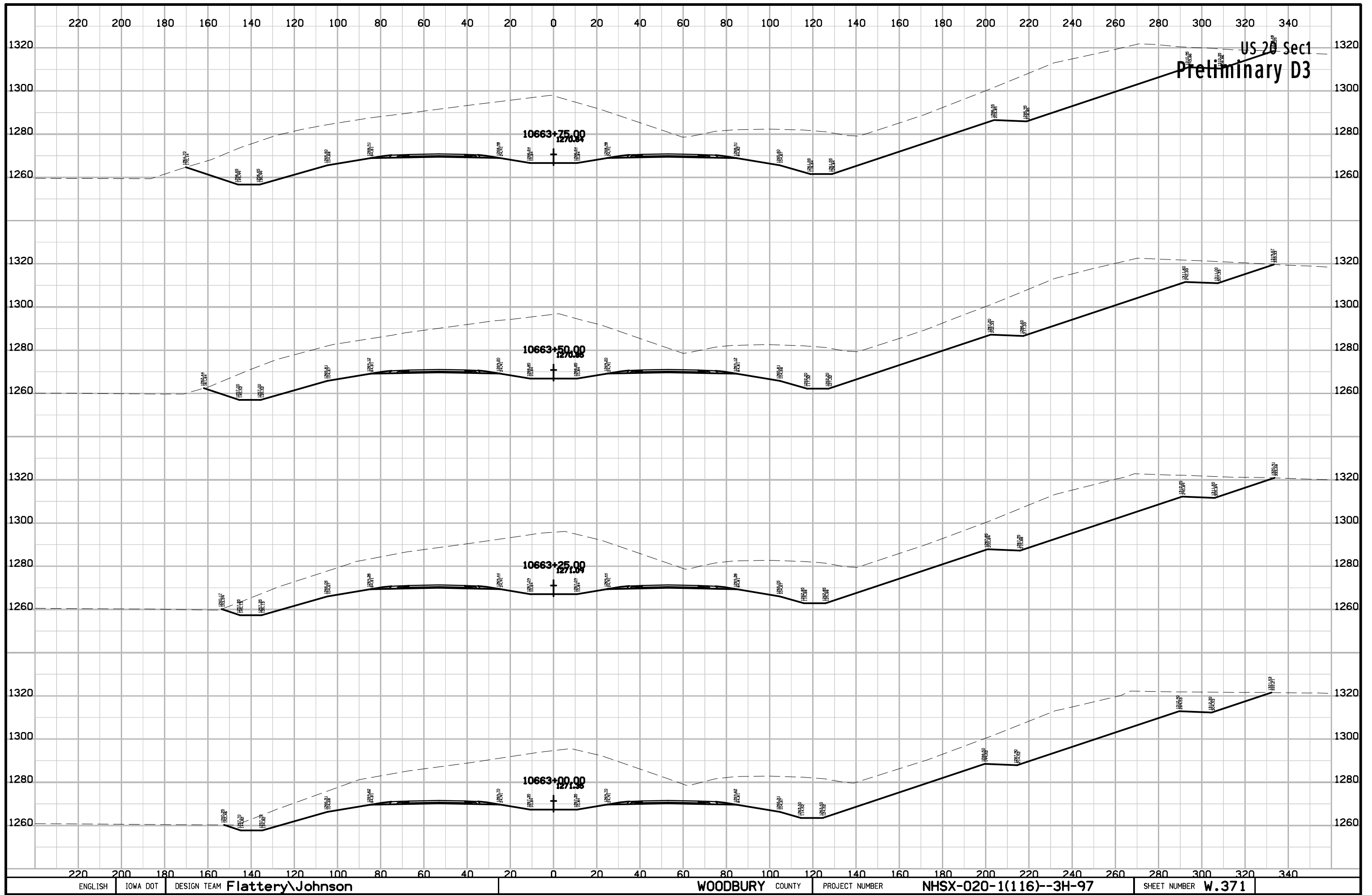


US 20 Sec1
Preliminary D3

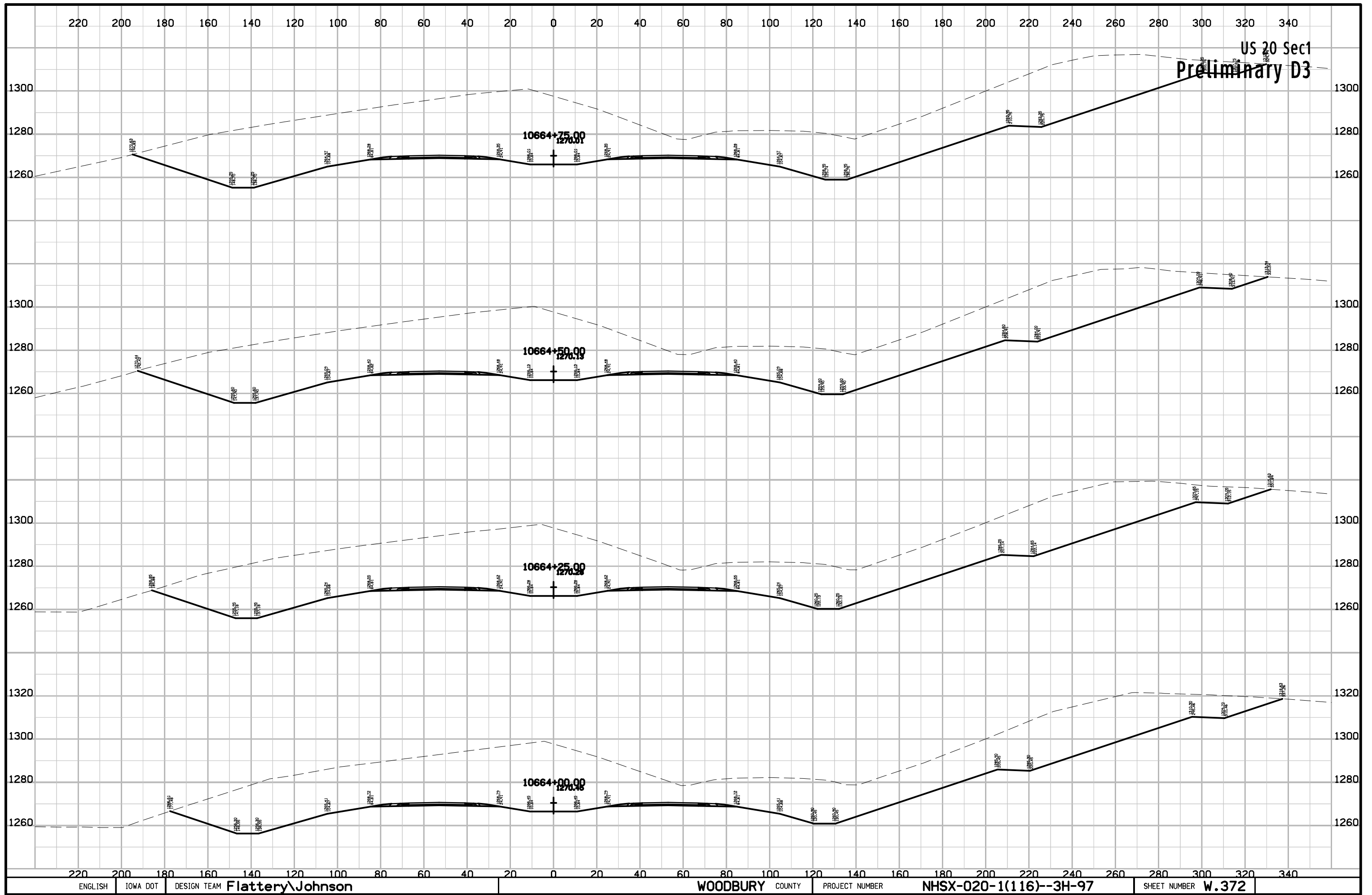




US 20 Sect
Preliminary D3

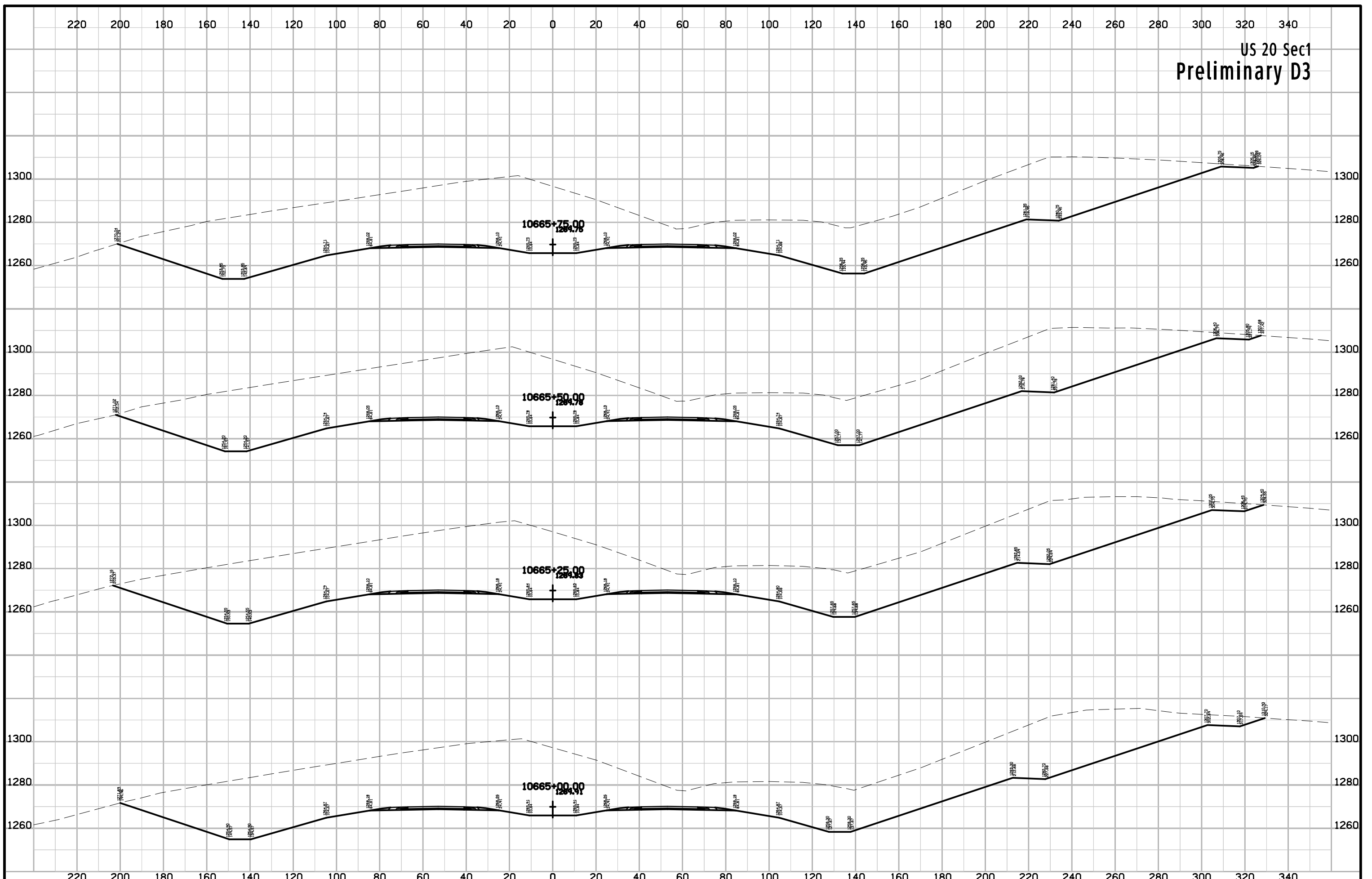


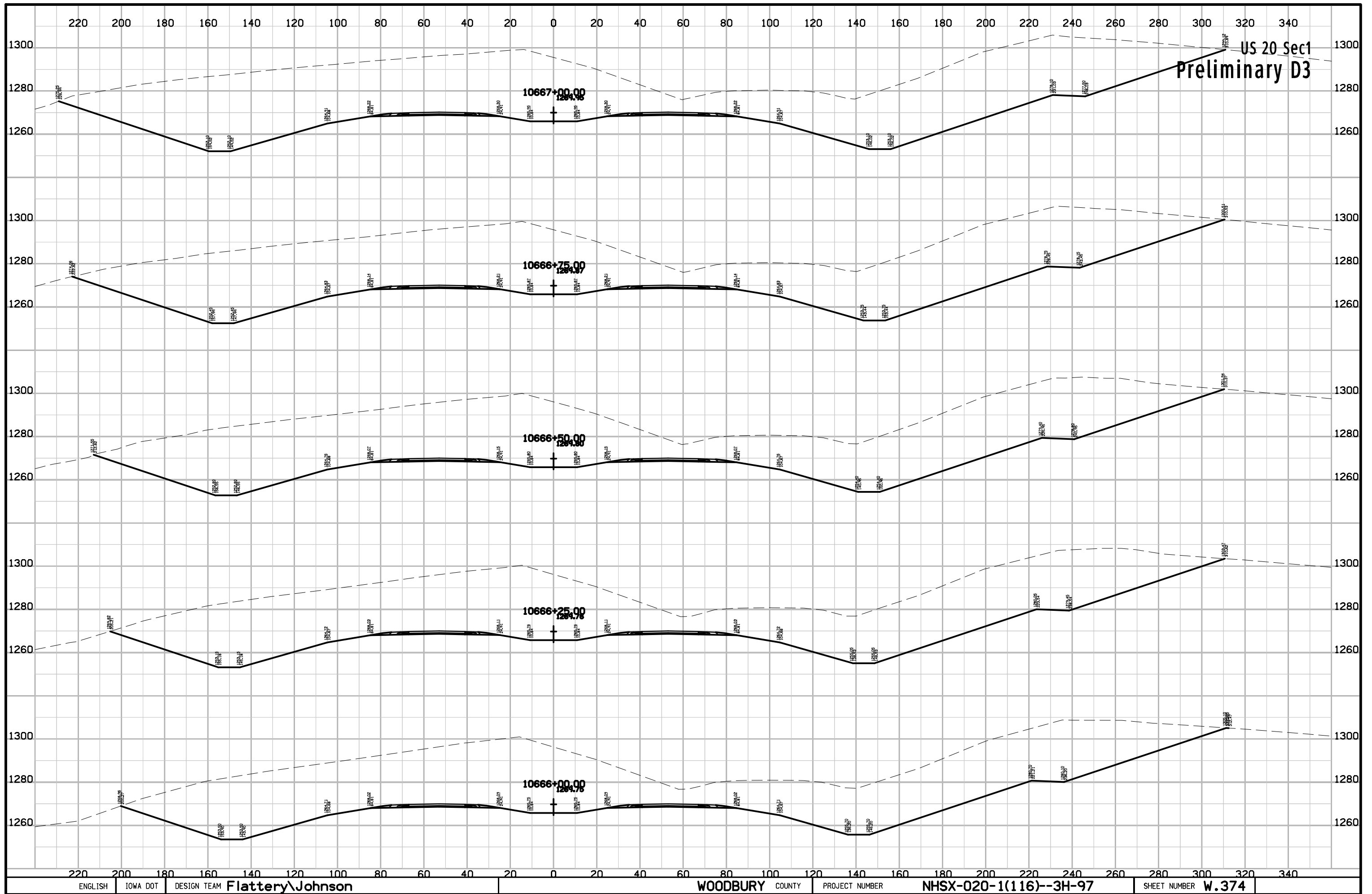
US-20 Sec1
Preliminary D3



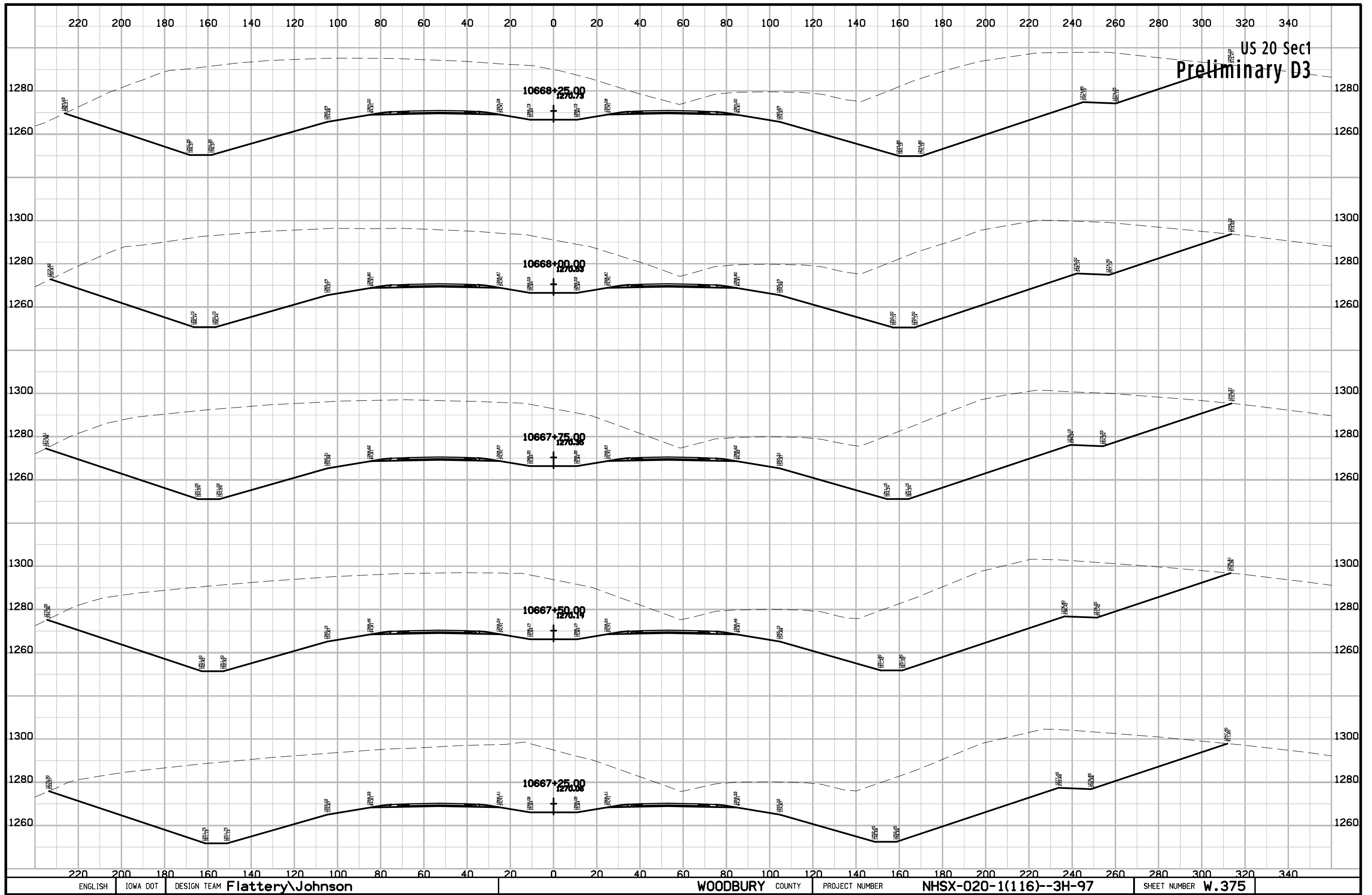
US 20 Sec1
Preliminary D3

US 20 Sec1
Preliminary D3



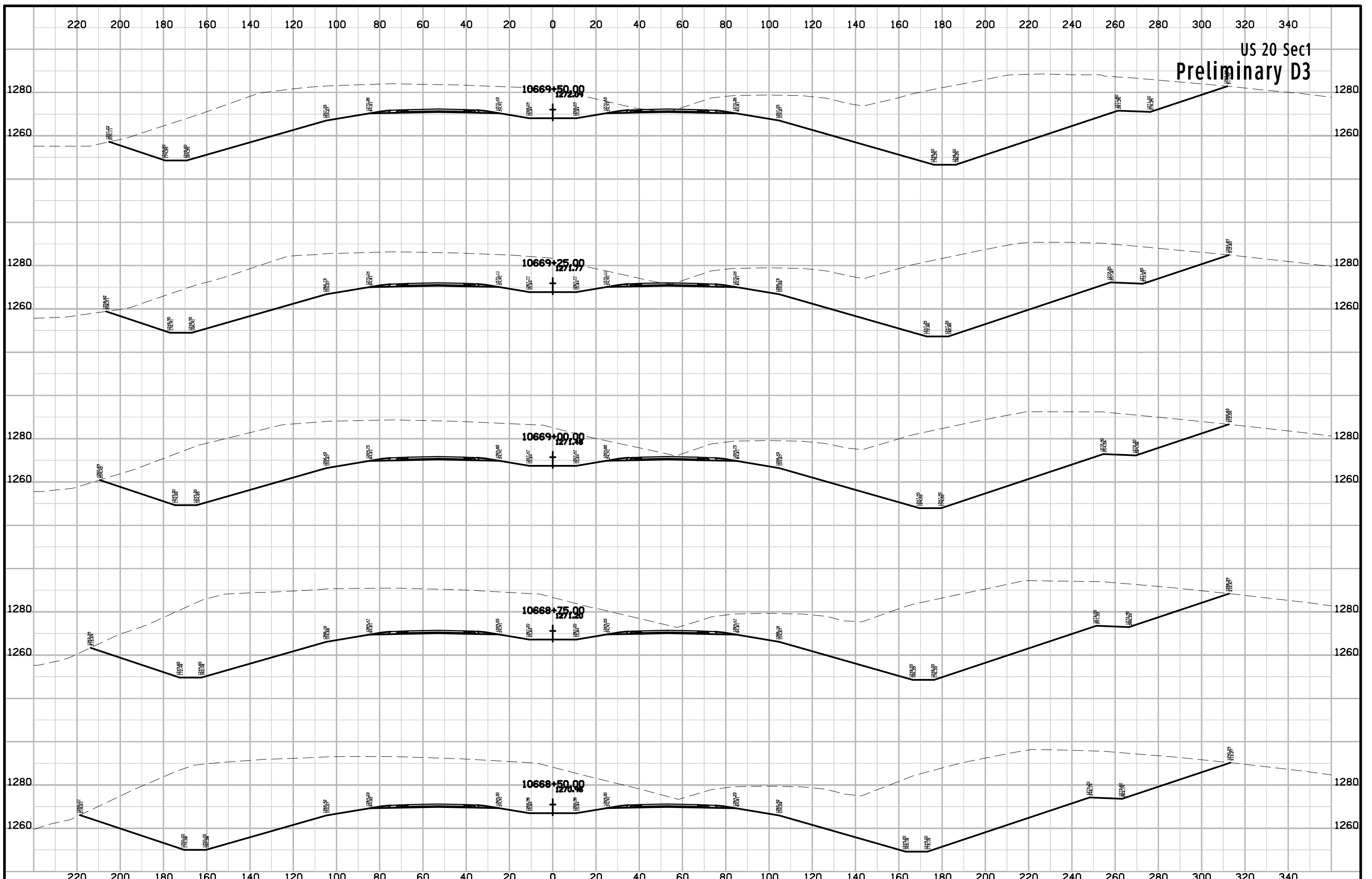


US 20 Sec1
Preliminary D3

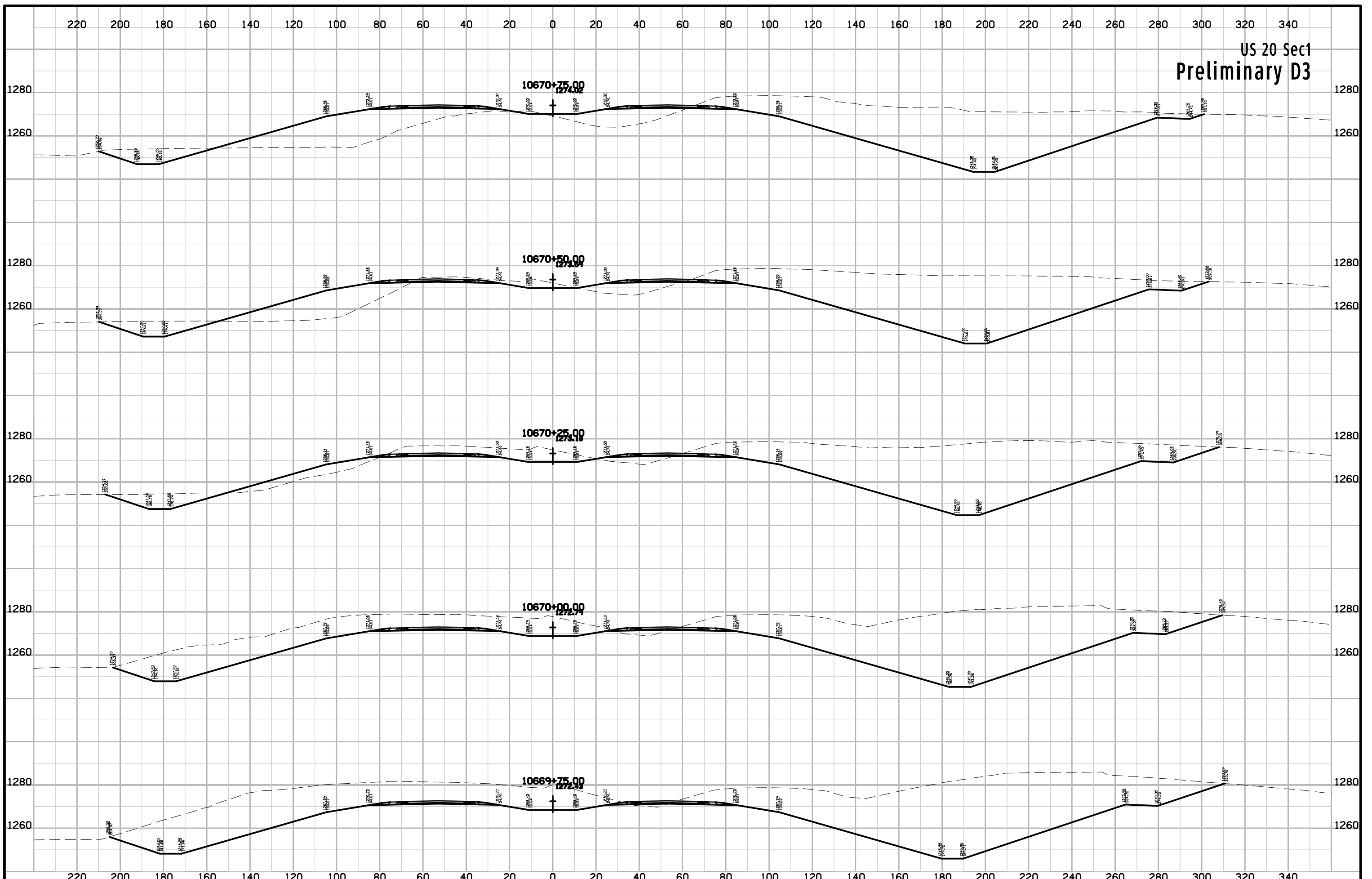


US 20 Sec1
Preliminary D3

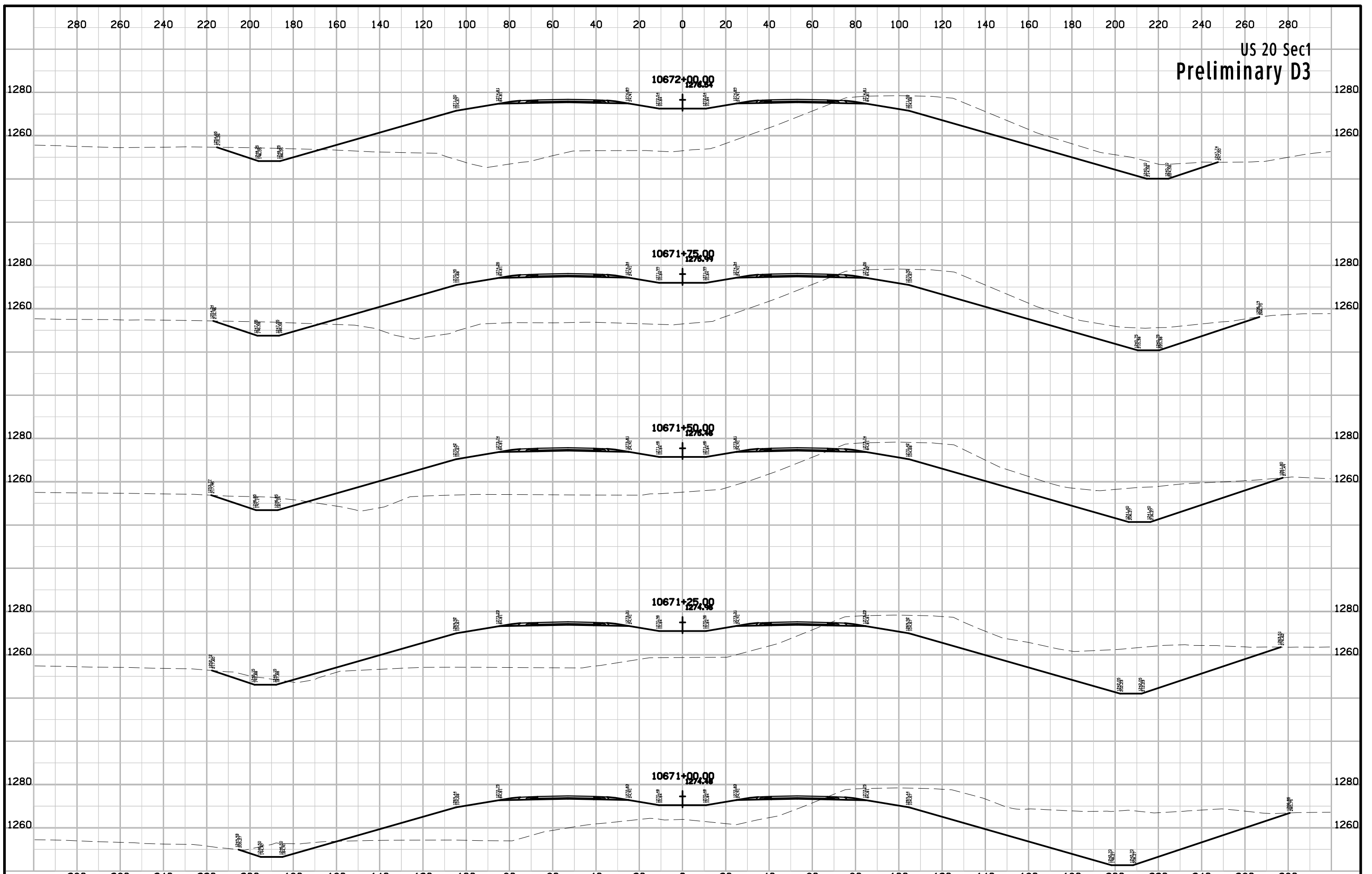
US 20 Sec1
Preliminary D3



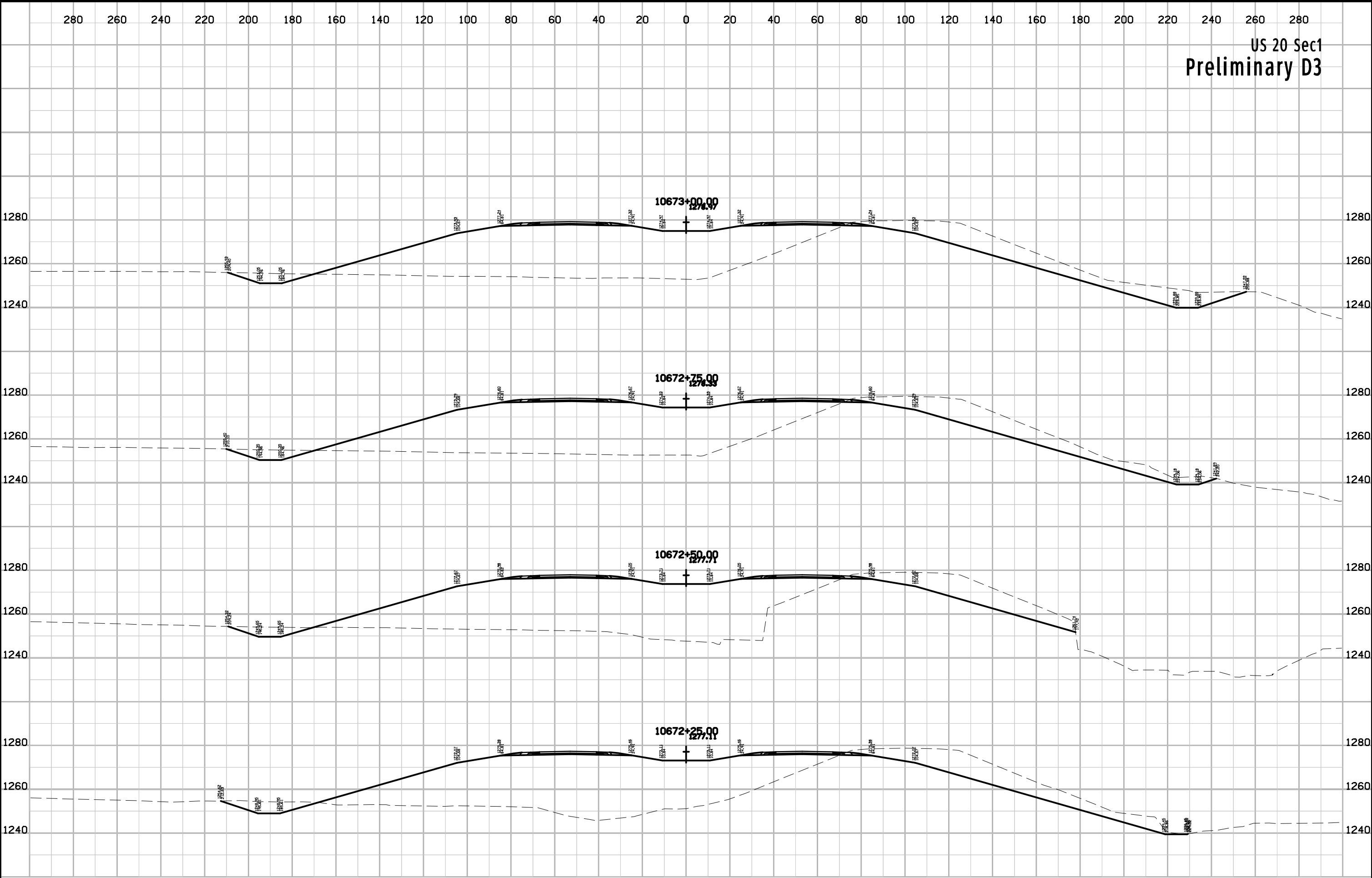
US 20 Sec1
Preliminary D3



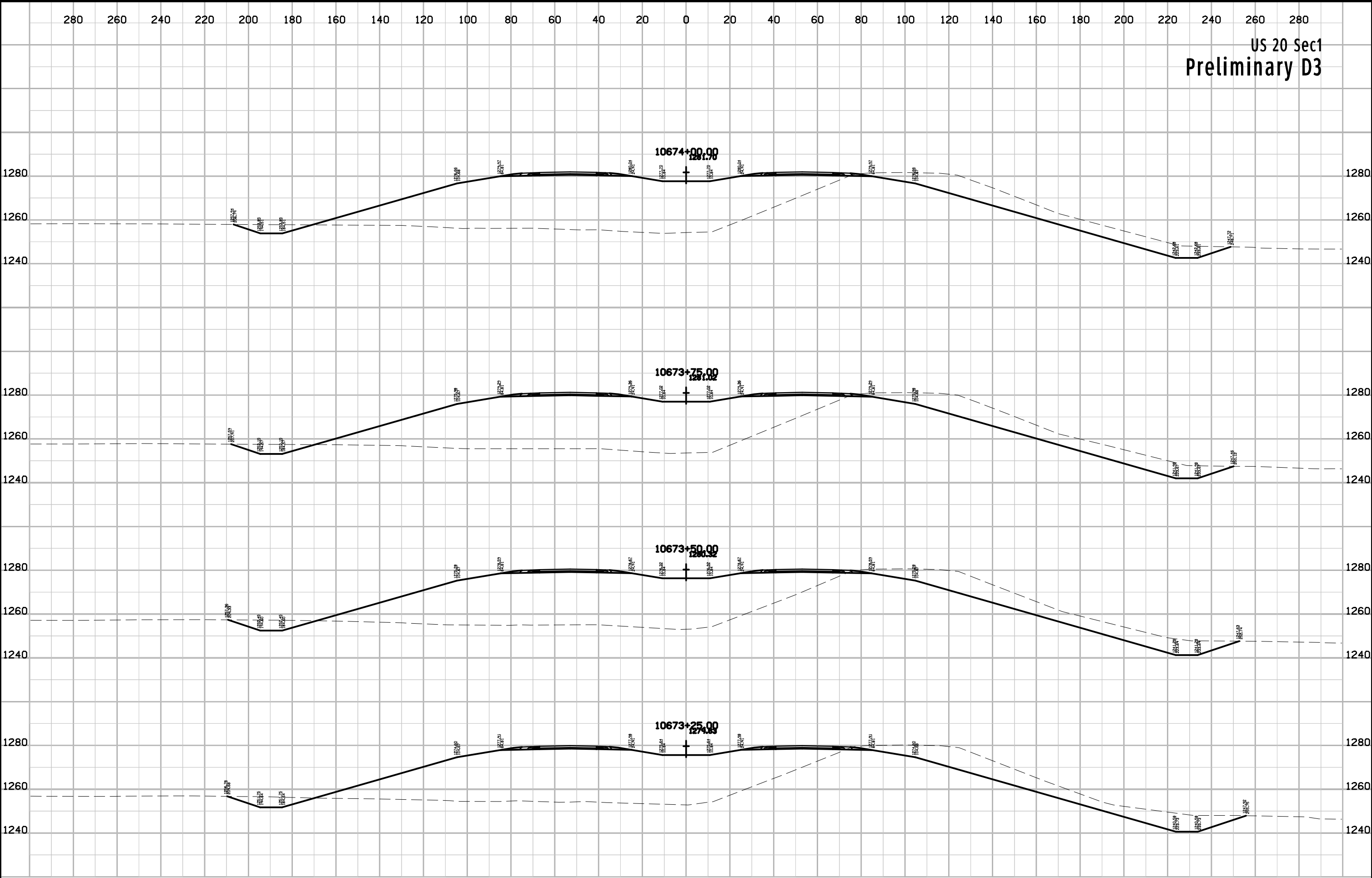
US 20 Sec1
Preliminary D3



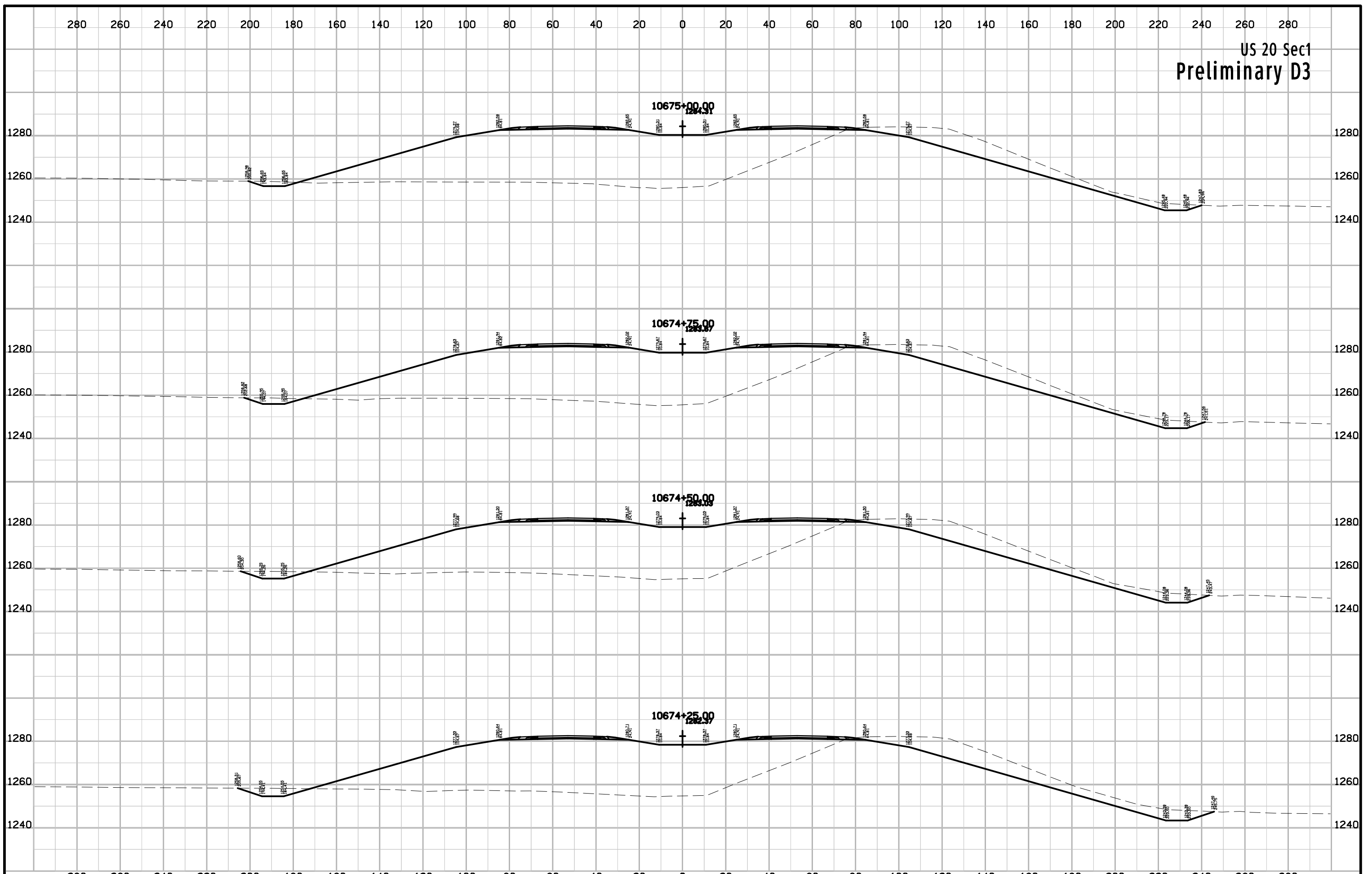
US 20 Sec1
Preliminary D3



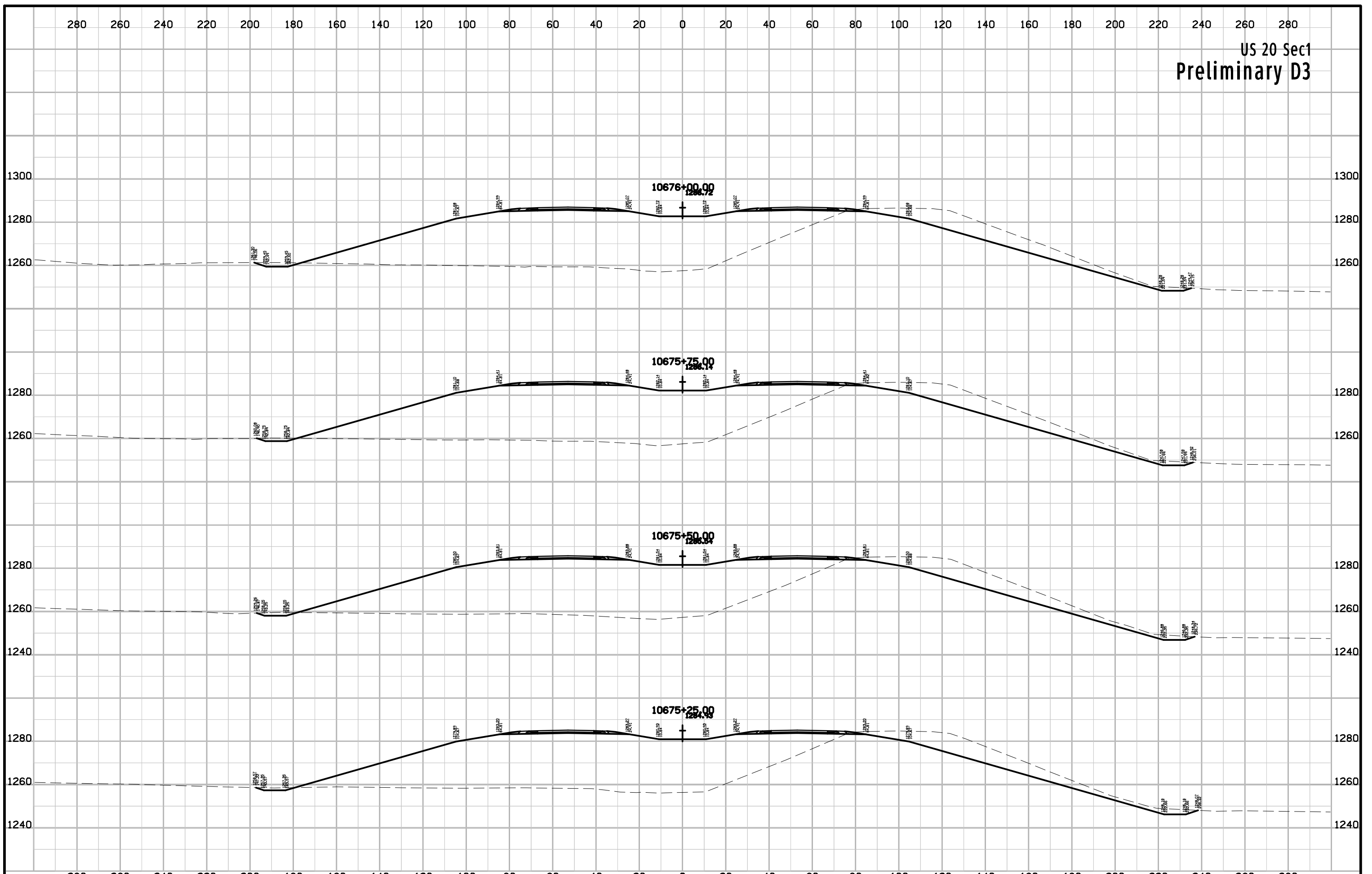
US 20 Sec1
Preliminary D3

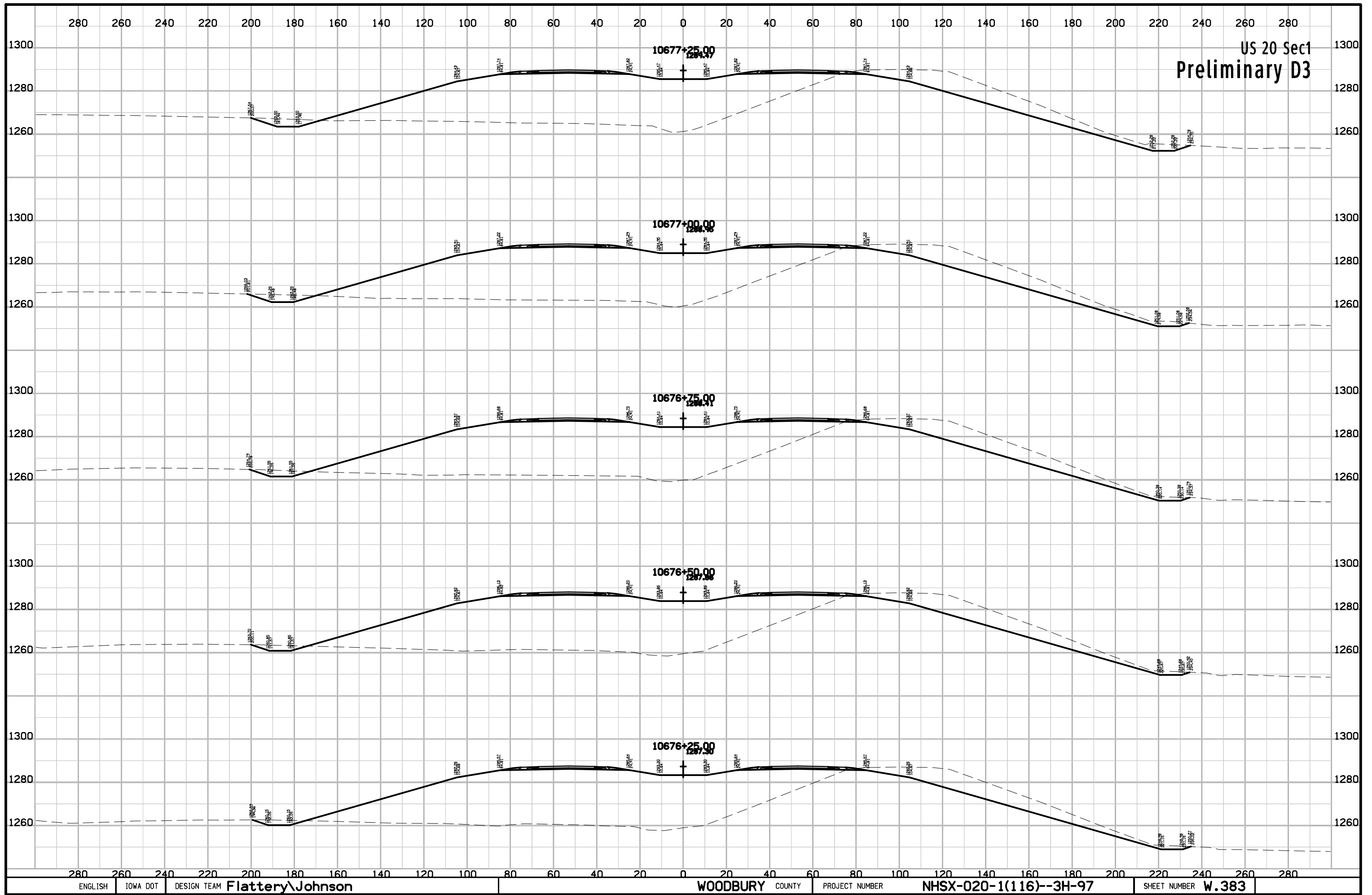


US 20 Sec1
Preliminary D3

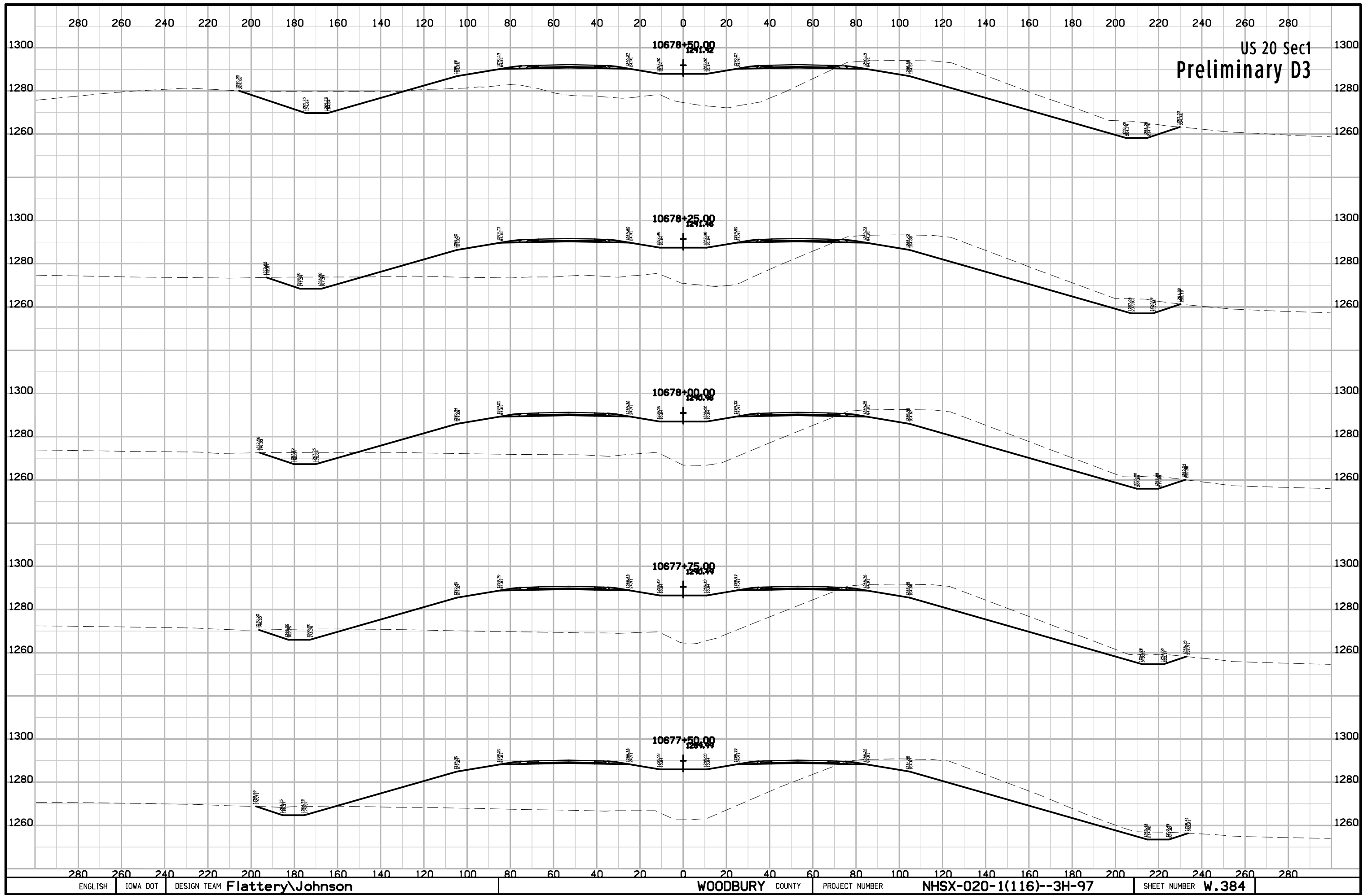


US 20 Sec1
Preliminary D3

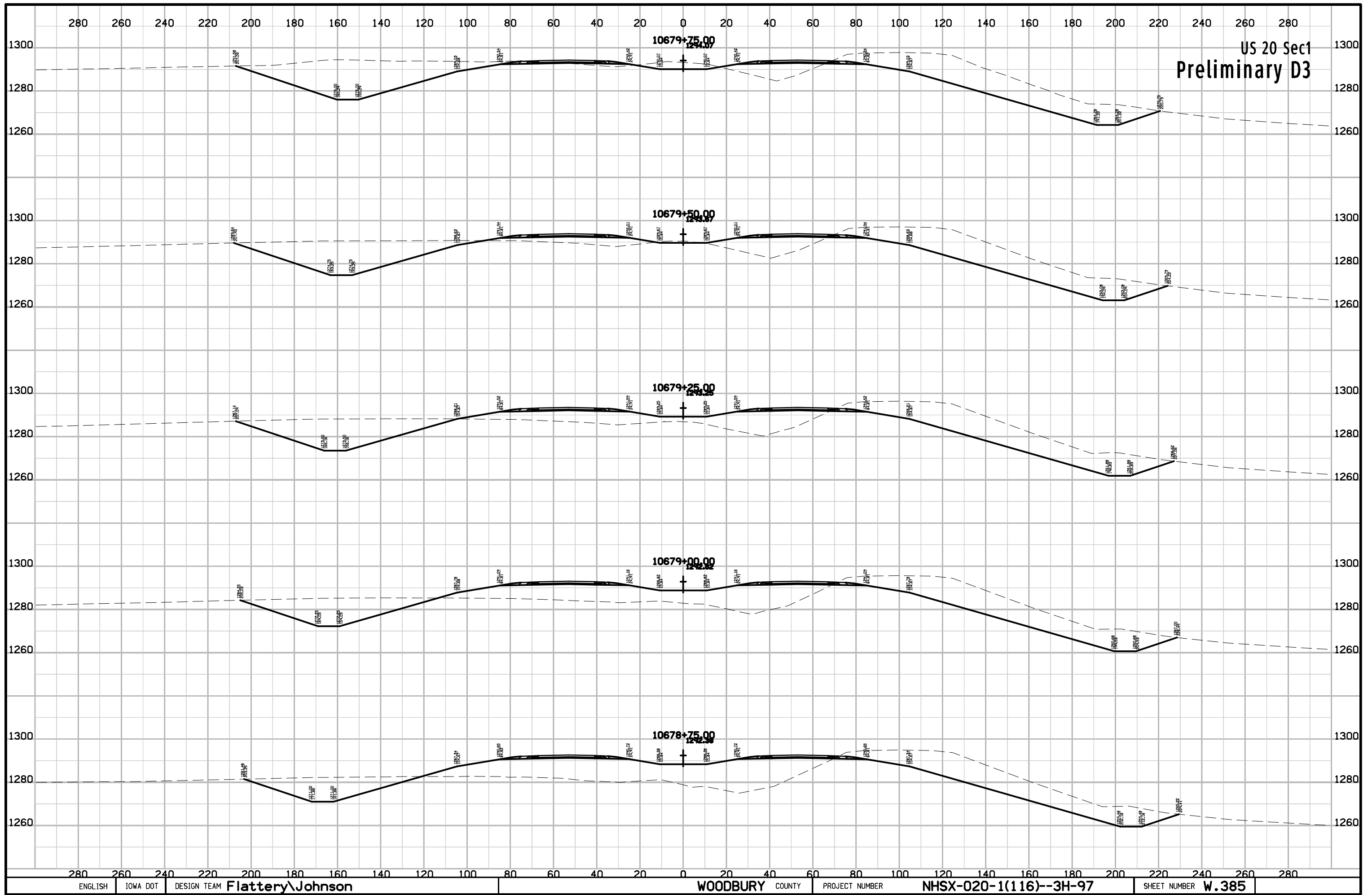




US 20 Sec1
Preliminary D3

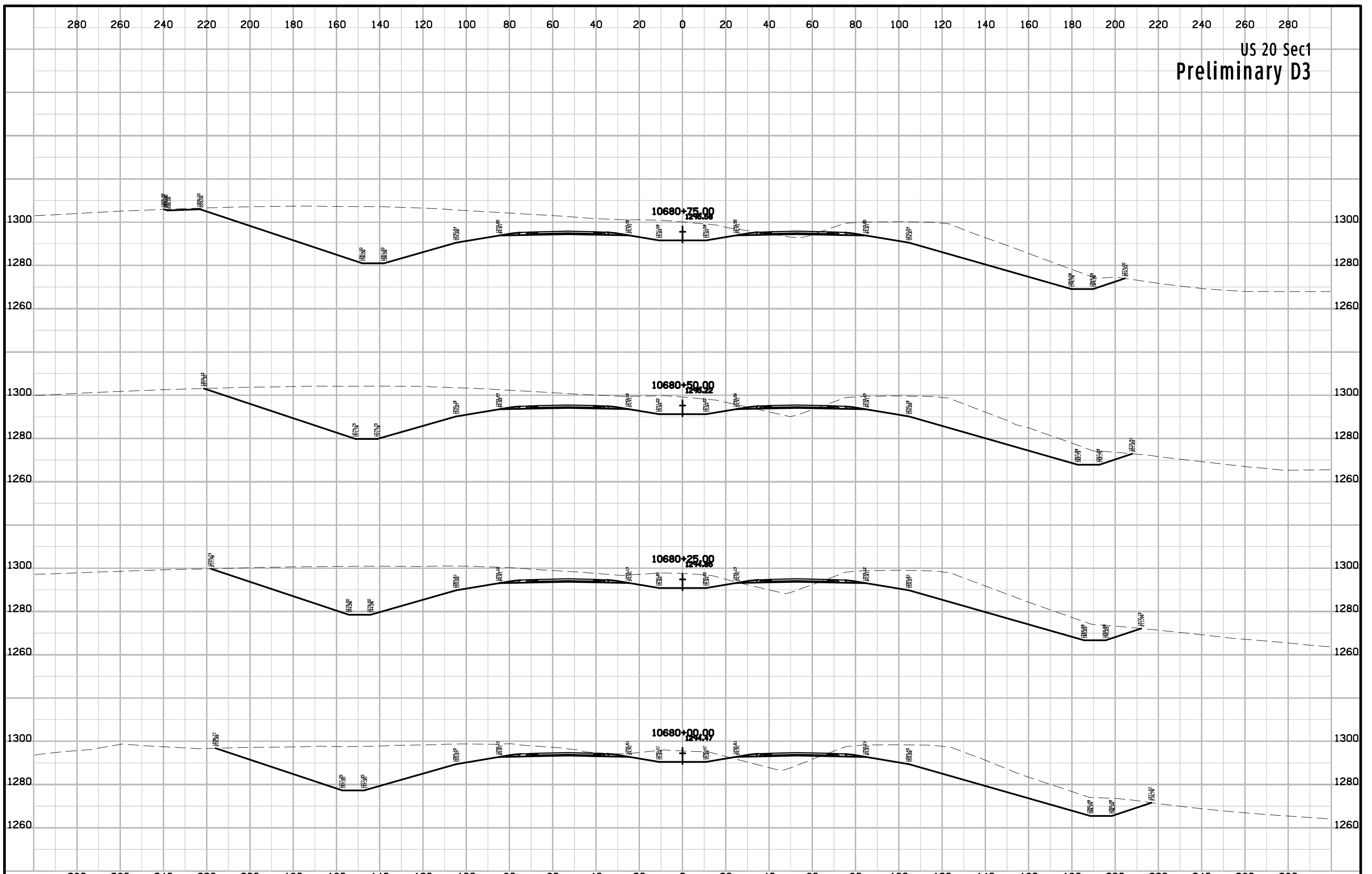


US 20 Sec1
Preliminary D3

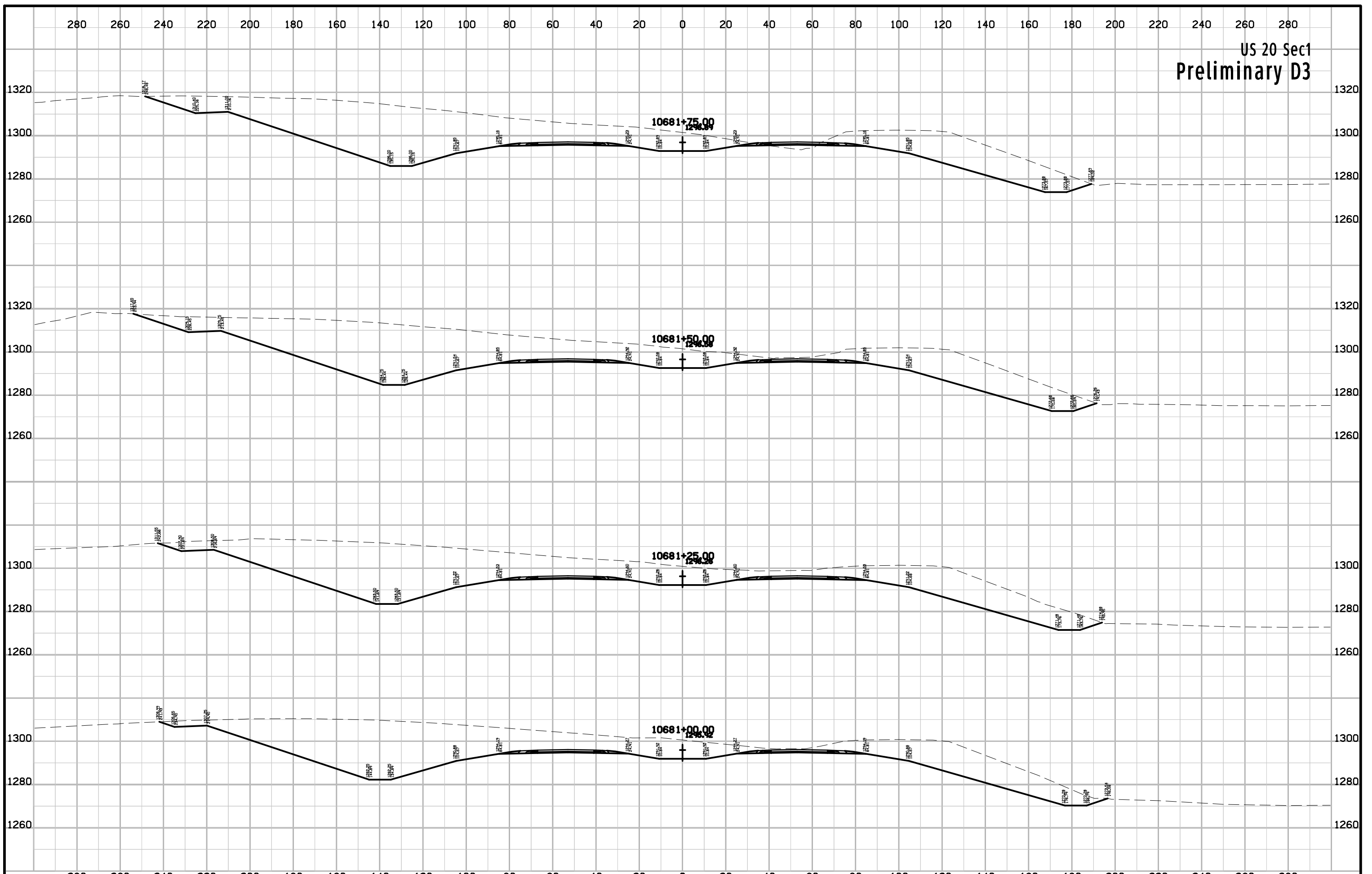


US 20 Sec1
Preliminary D3

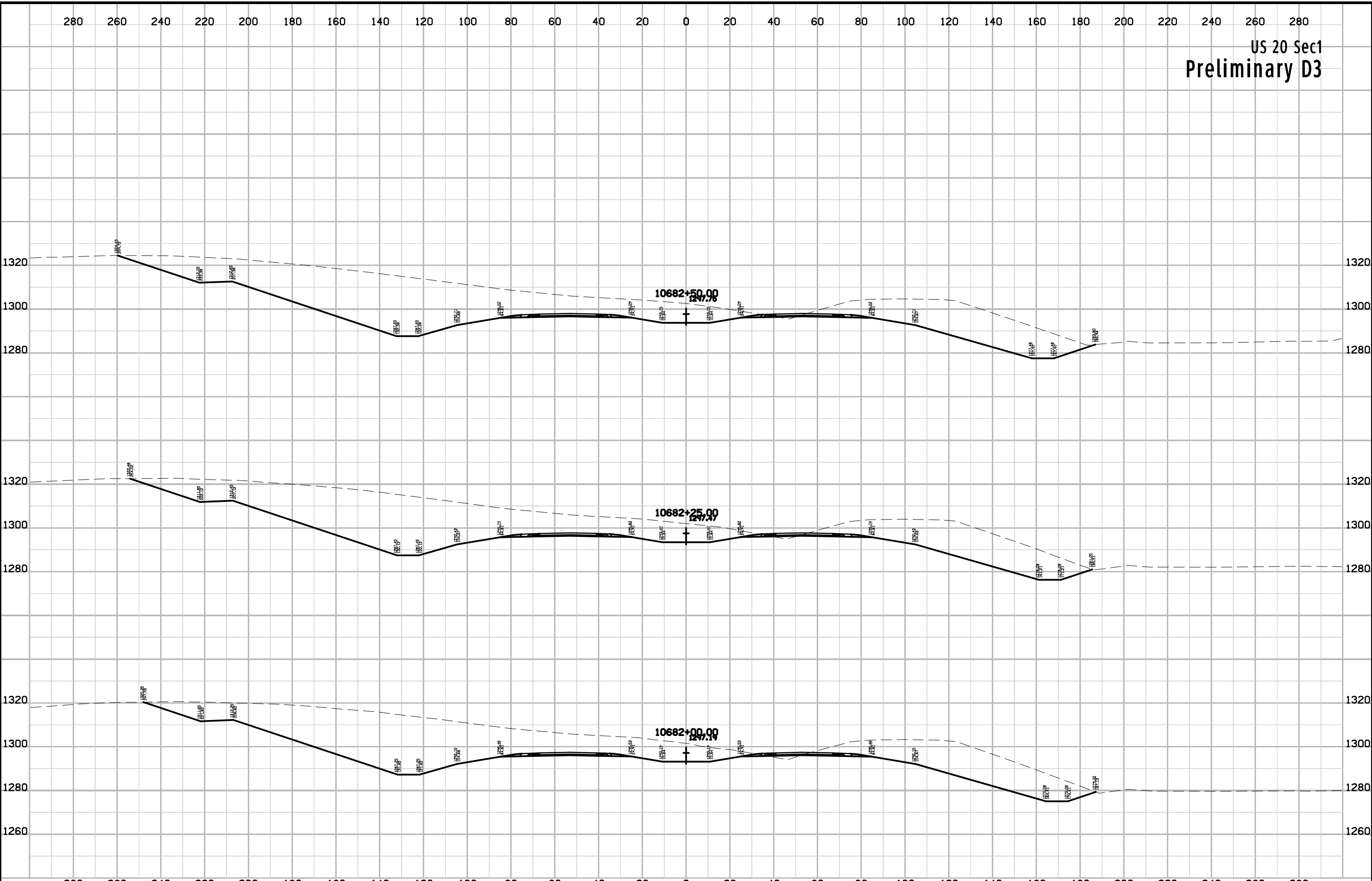
US 20 Sec1
Preliminary D3



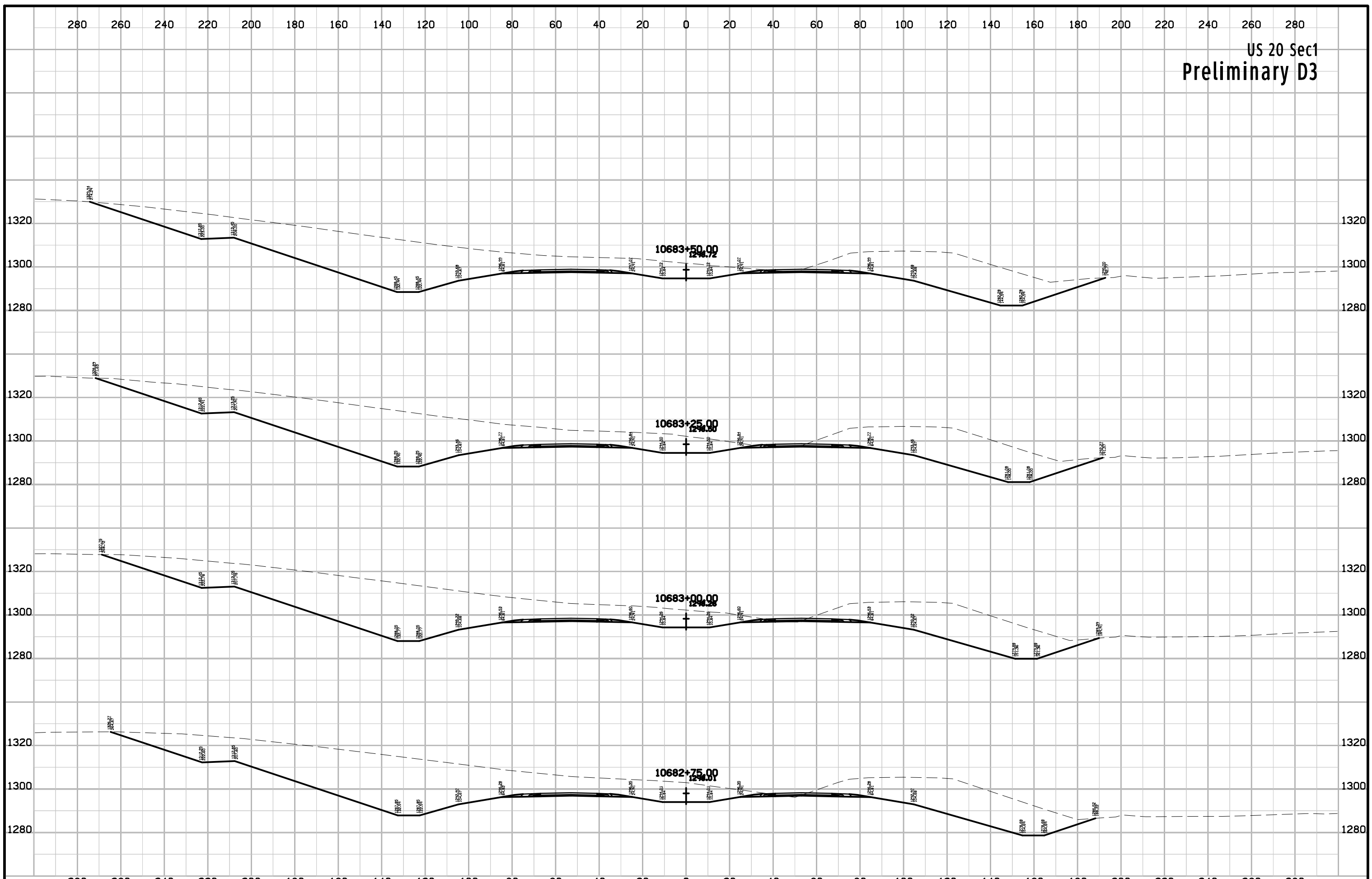
US 20 Sec1
Preliminary D3



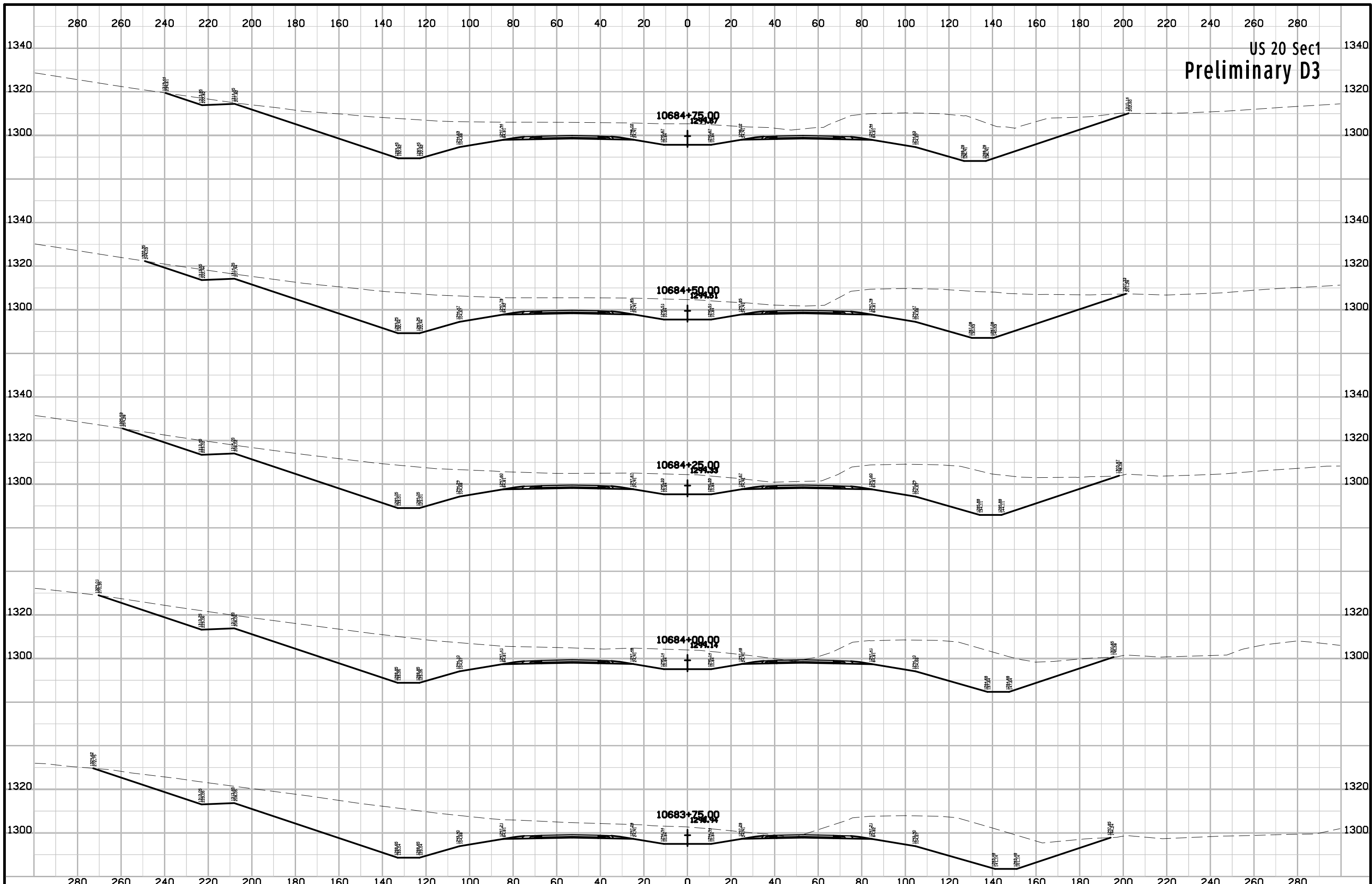
US 20 Sec1
Preliminary D3



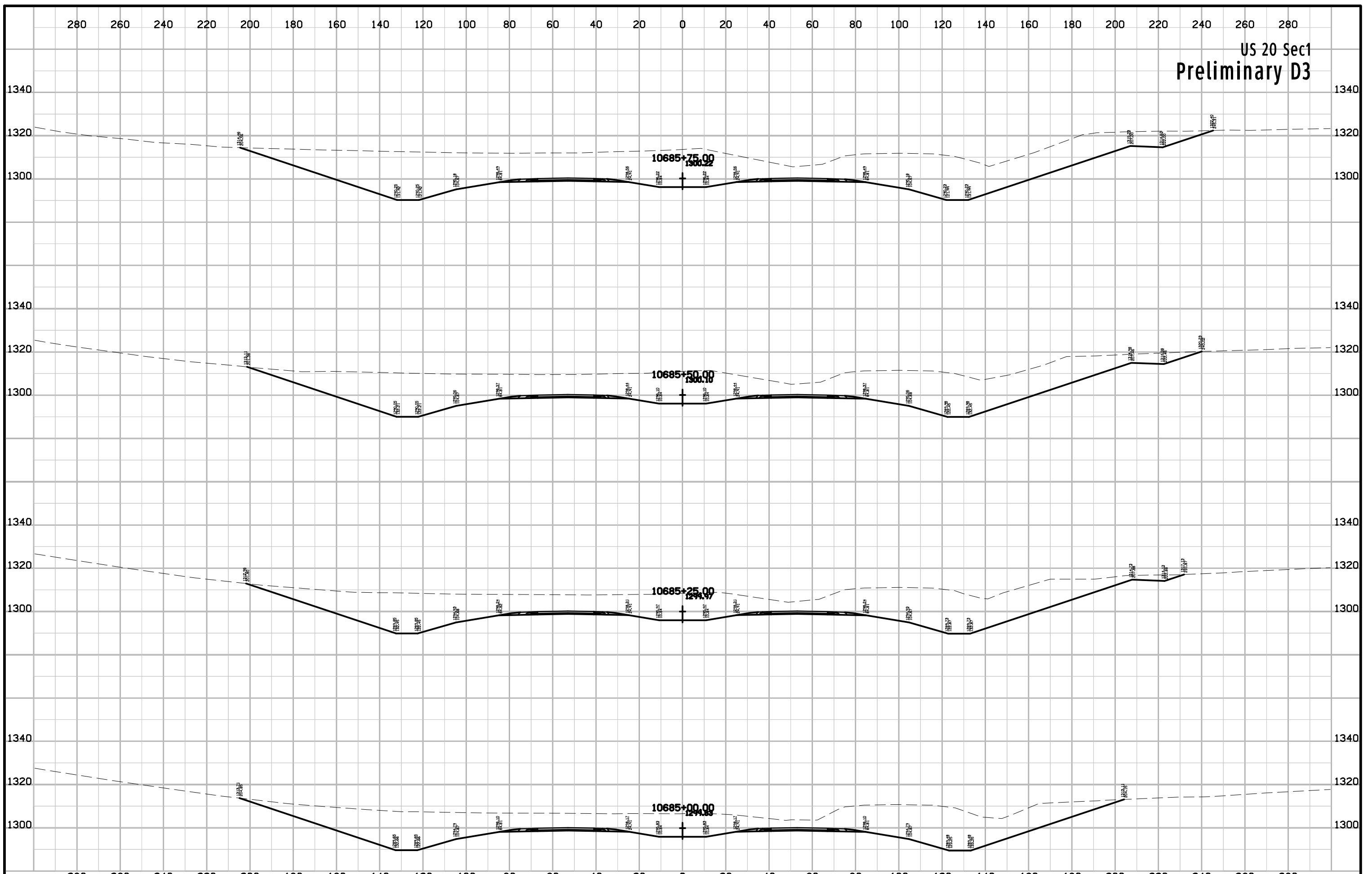
US 20 Sec1
Preliminary D3



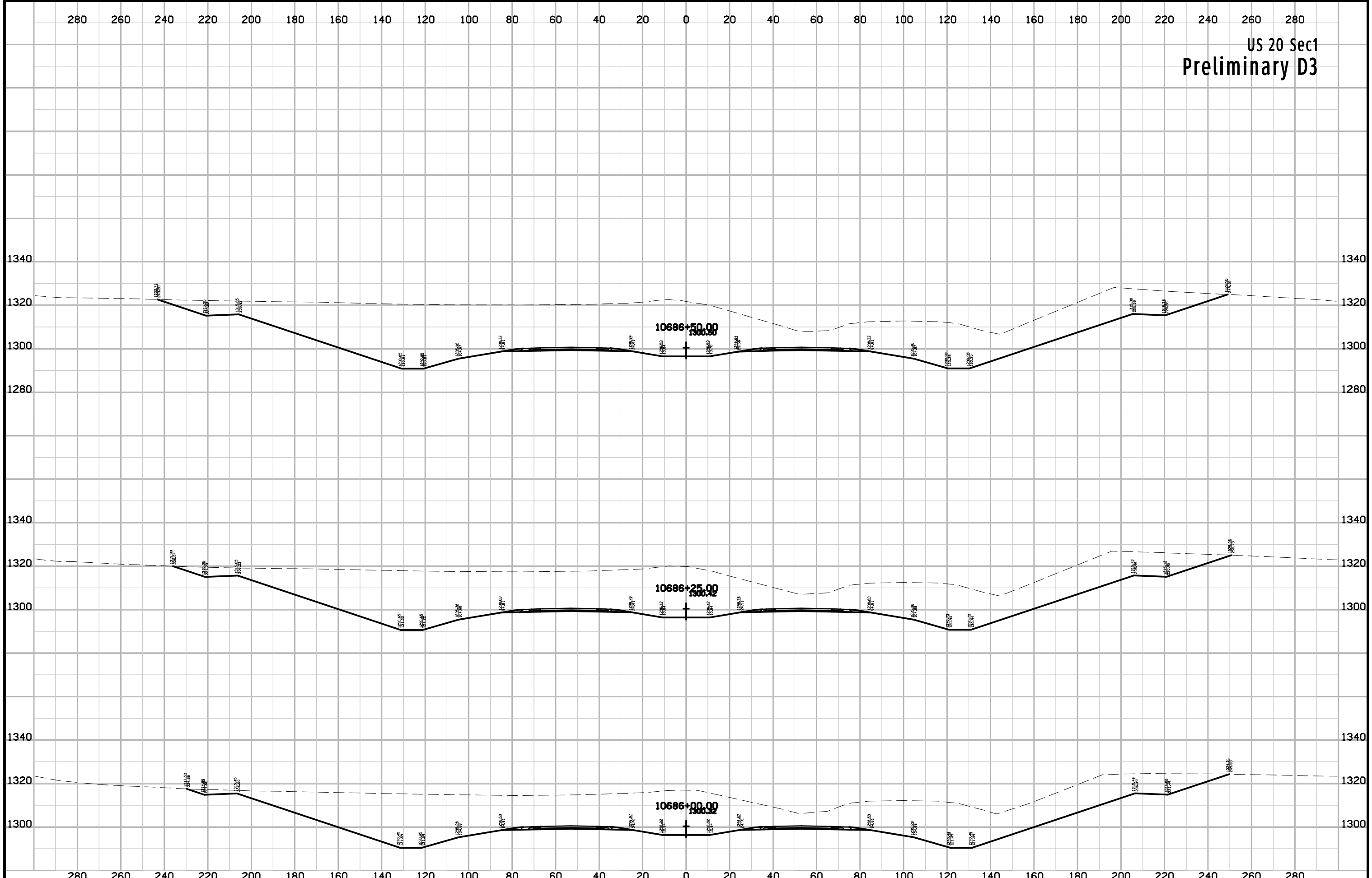
US 20 Sec1
Preliminary D3



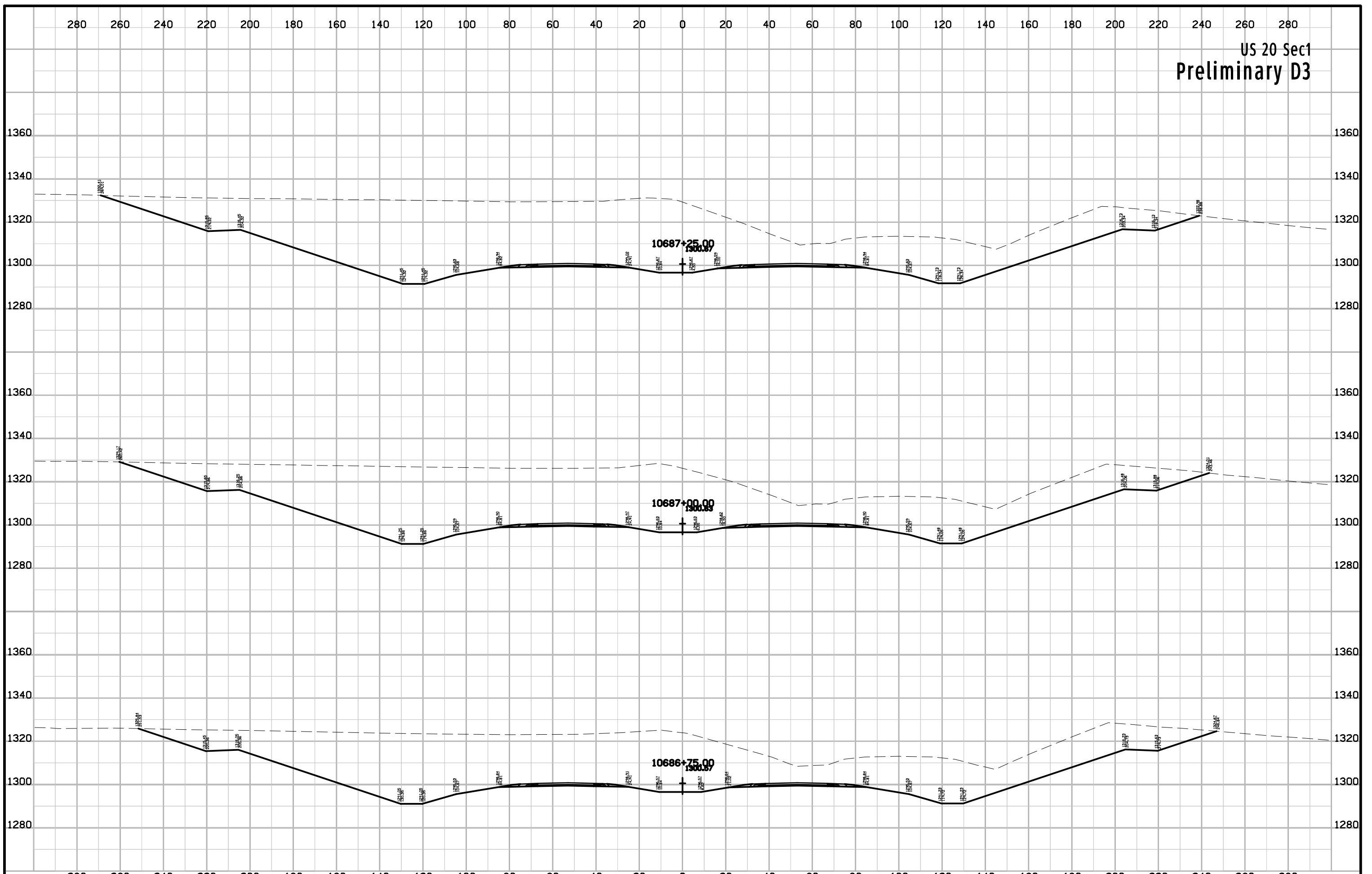
US 20 Sec1
Preliminary D3



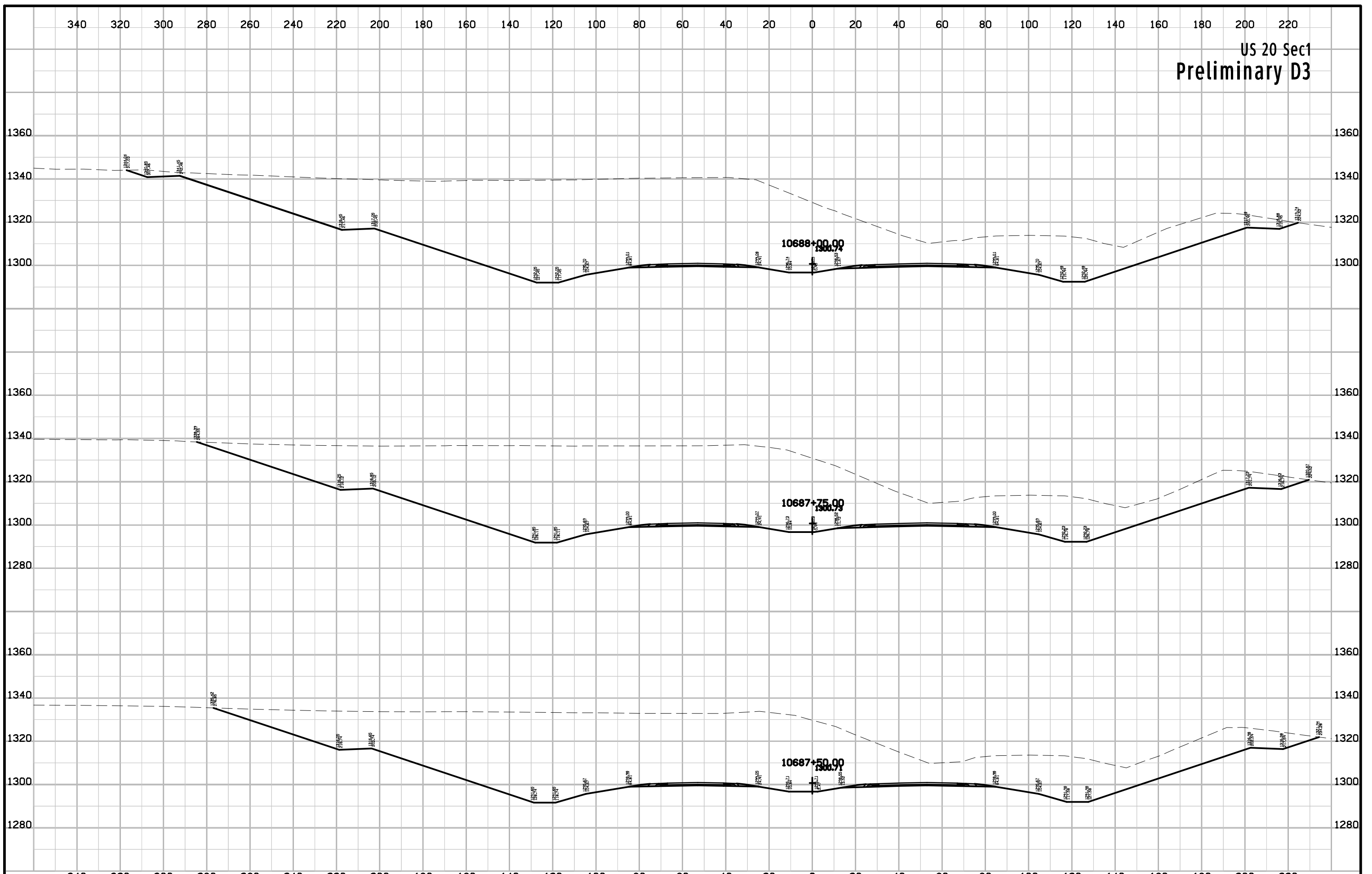
US 20 Sec1
Preliminary D3



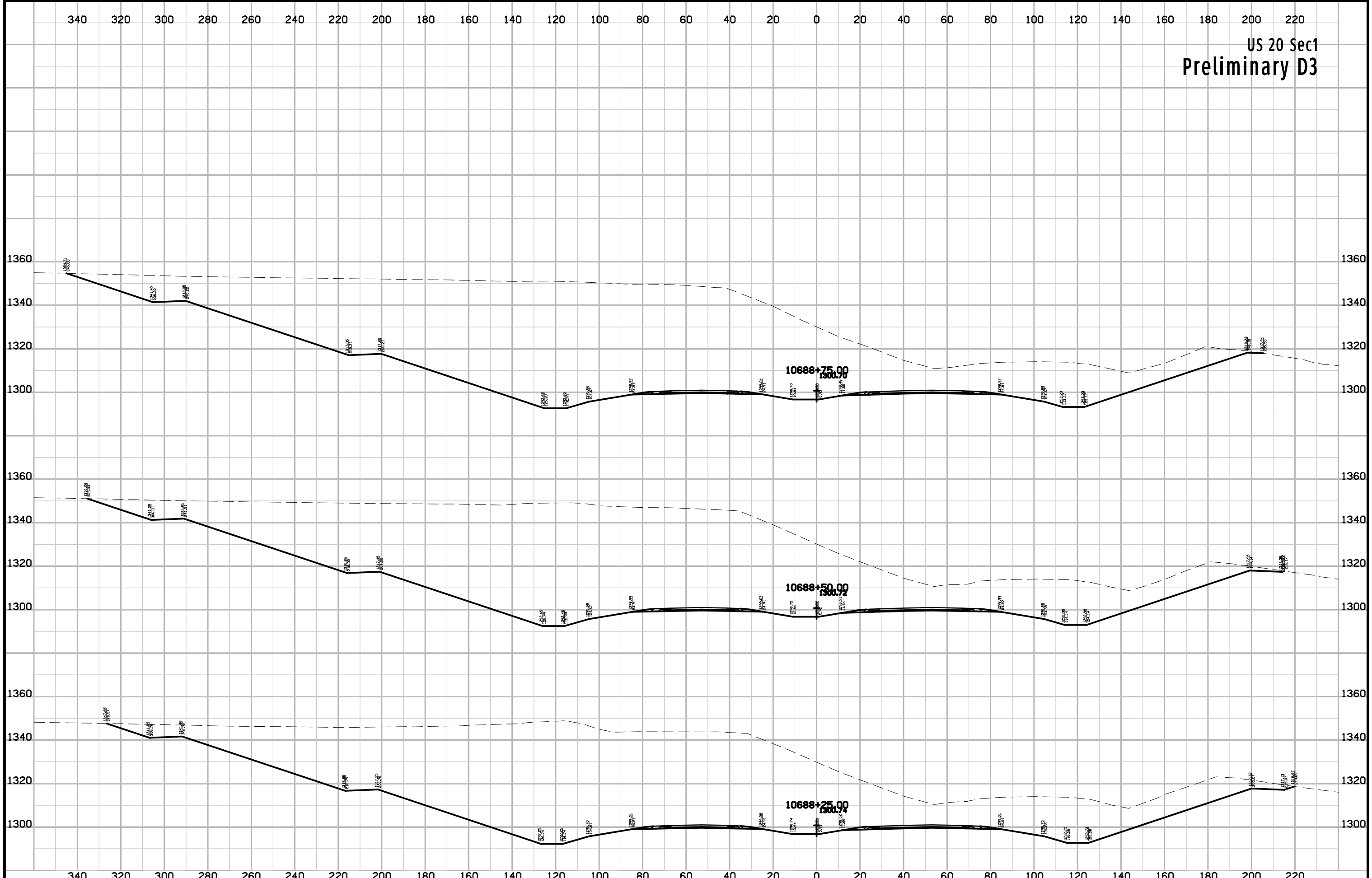
US 20 Sec1
Preliminary D3



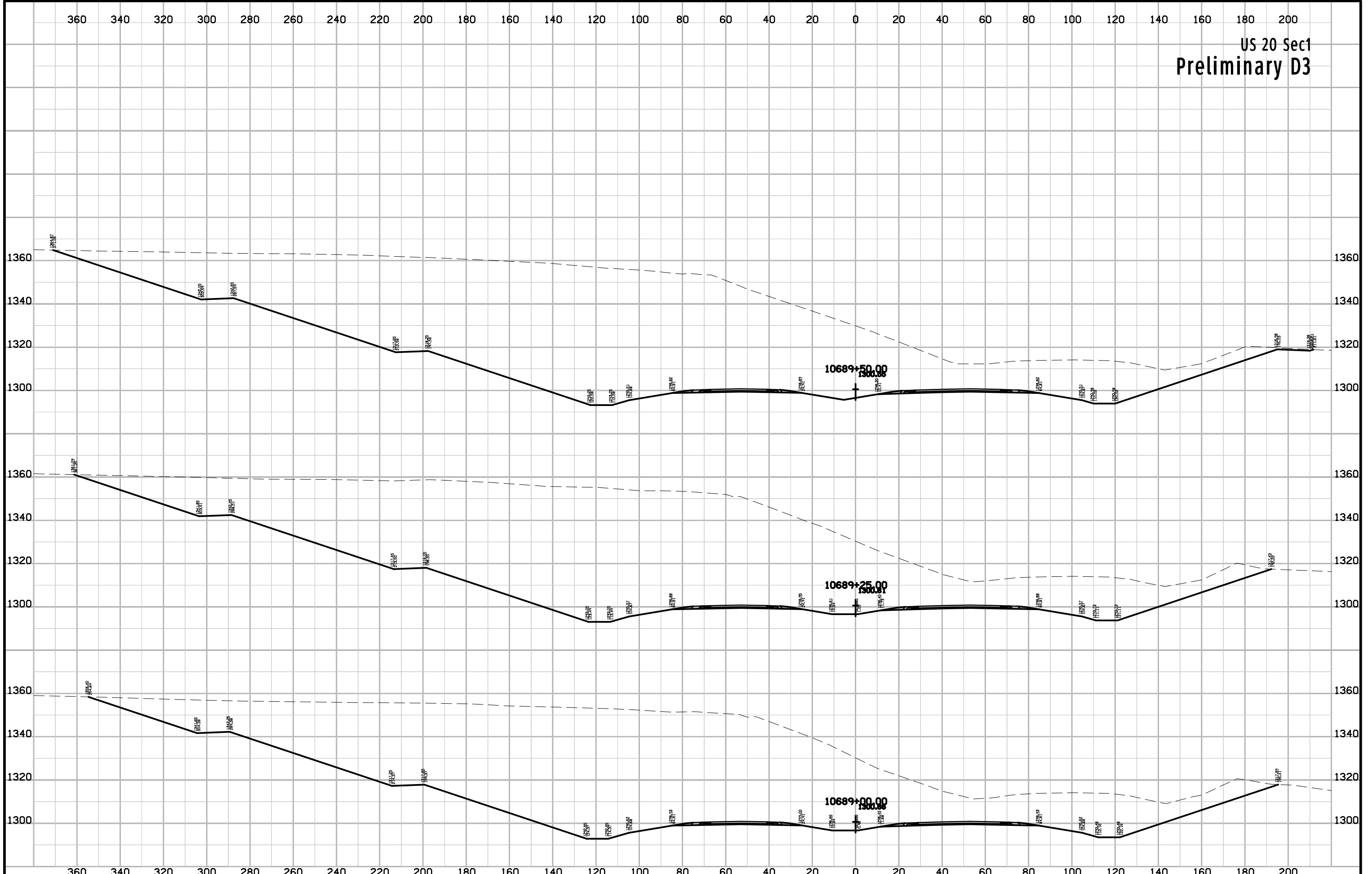
US 20 Sec1
Preliminary D3



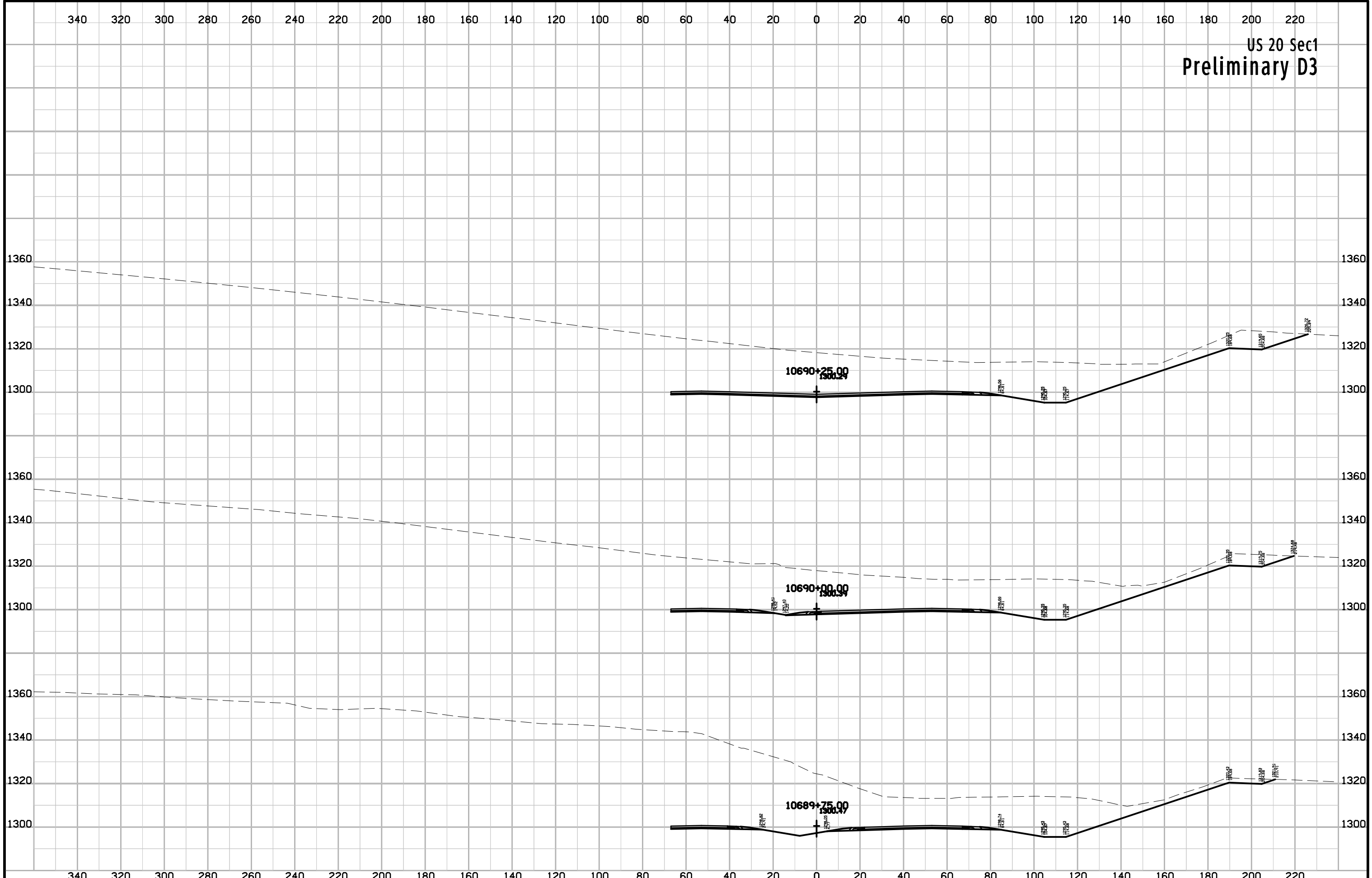
US 20 Sec1
Preliminary D3



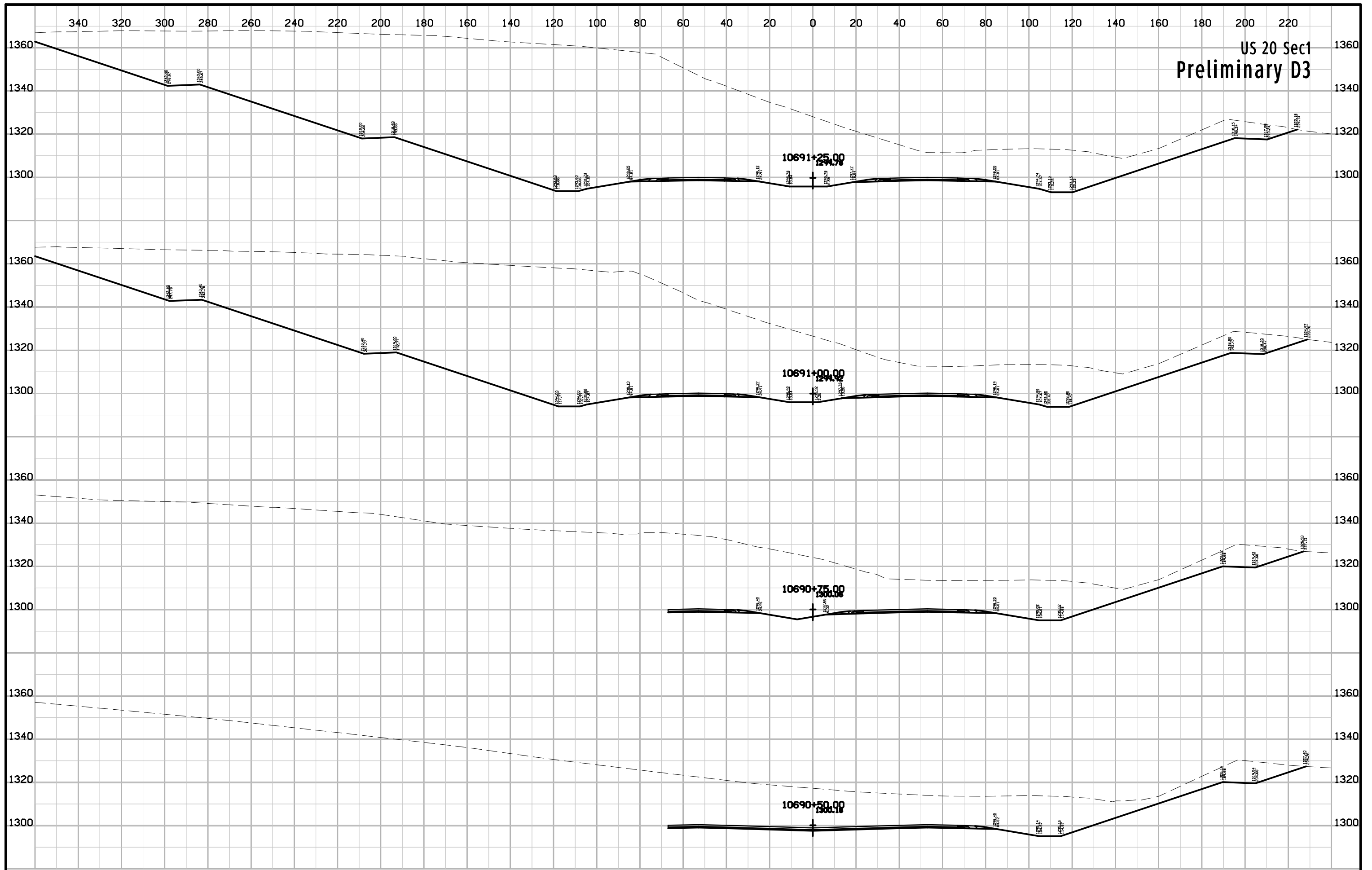
US 20 Sec1
Preliminary D3



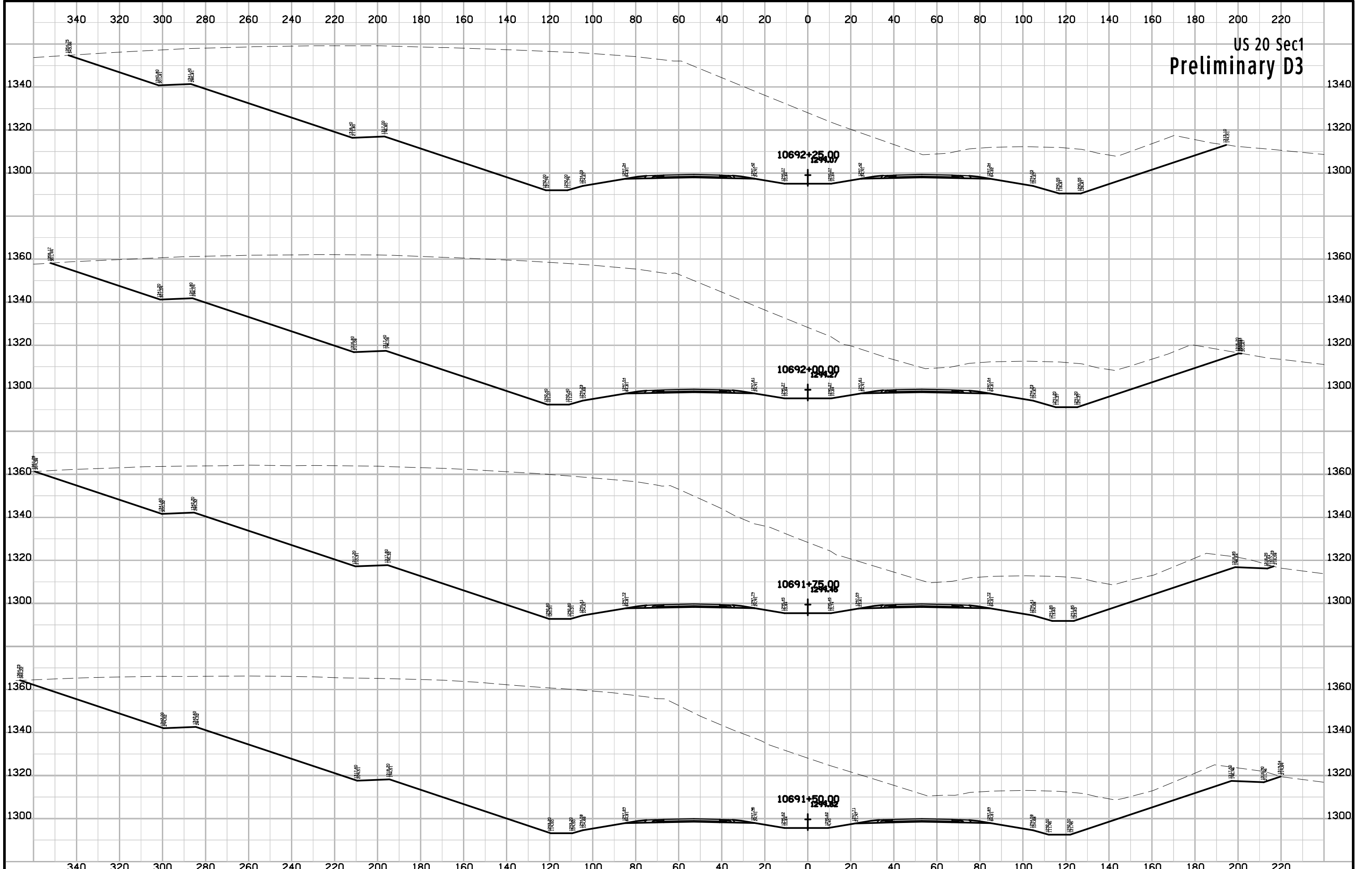
US 20 Sec1
Preliminary D3



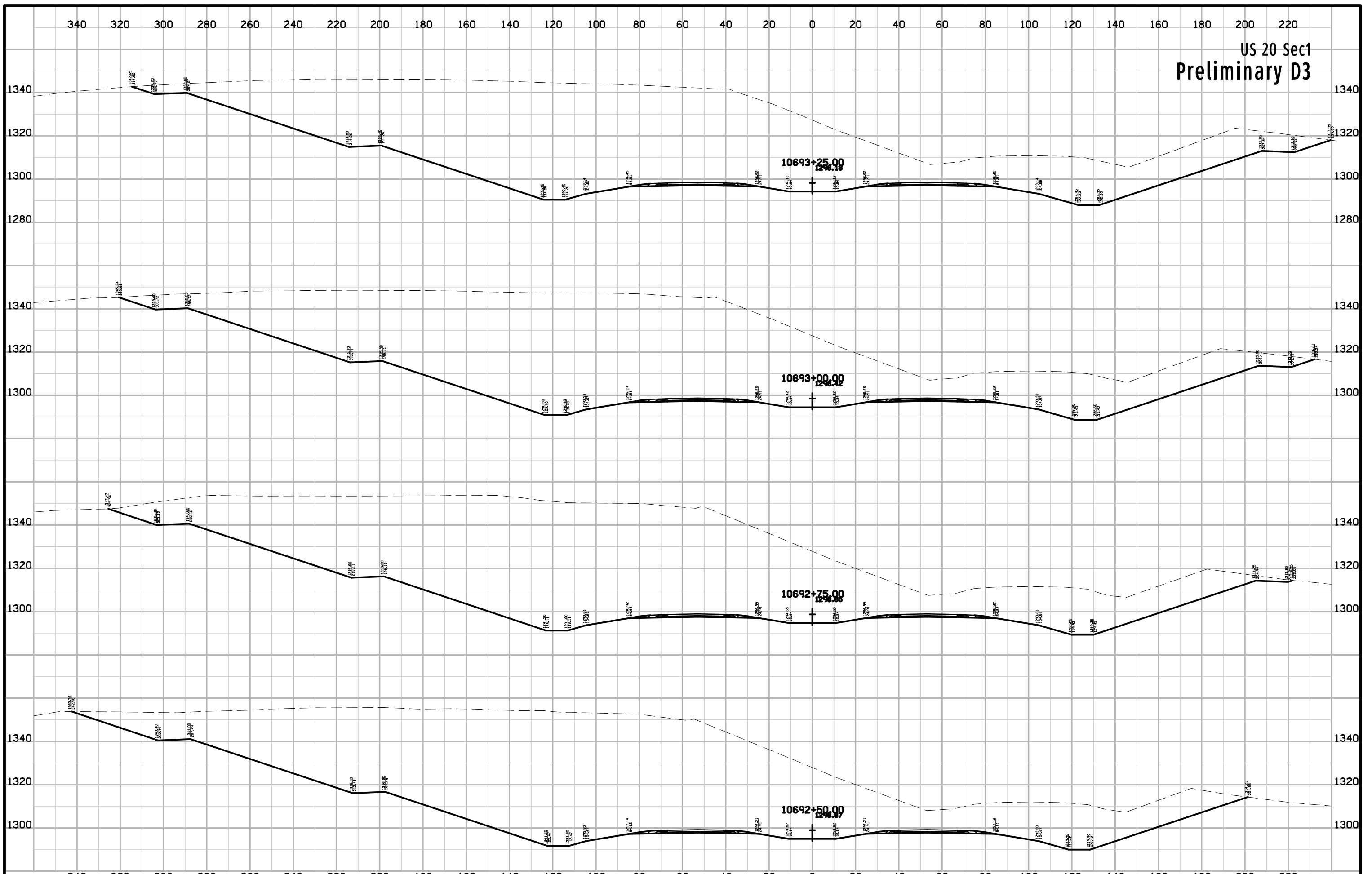
US 20 Sec1
Preliminary D3



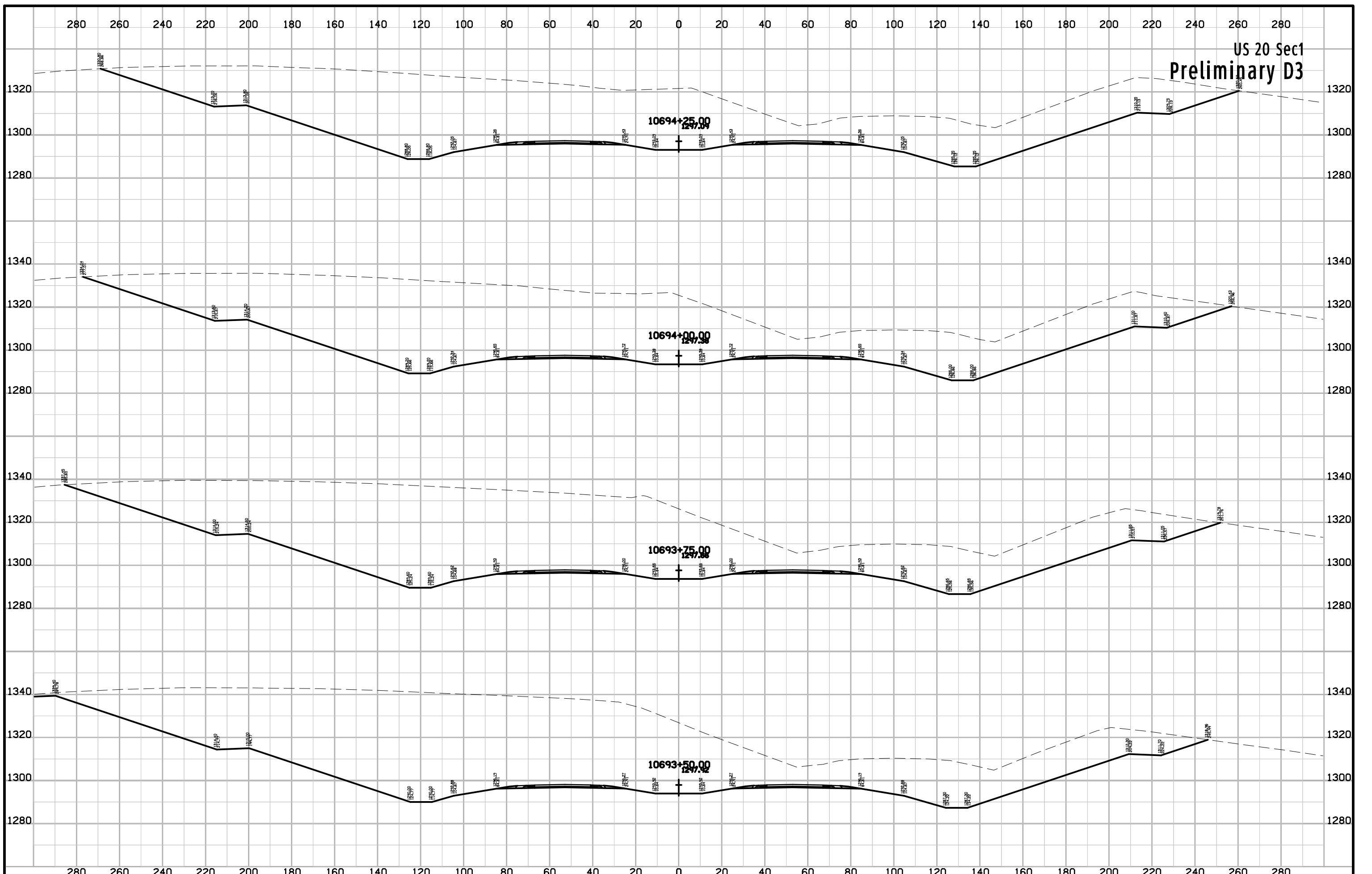
US 20 Sec1
Preliminary D3



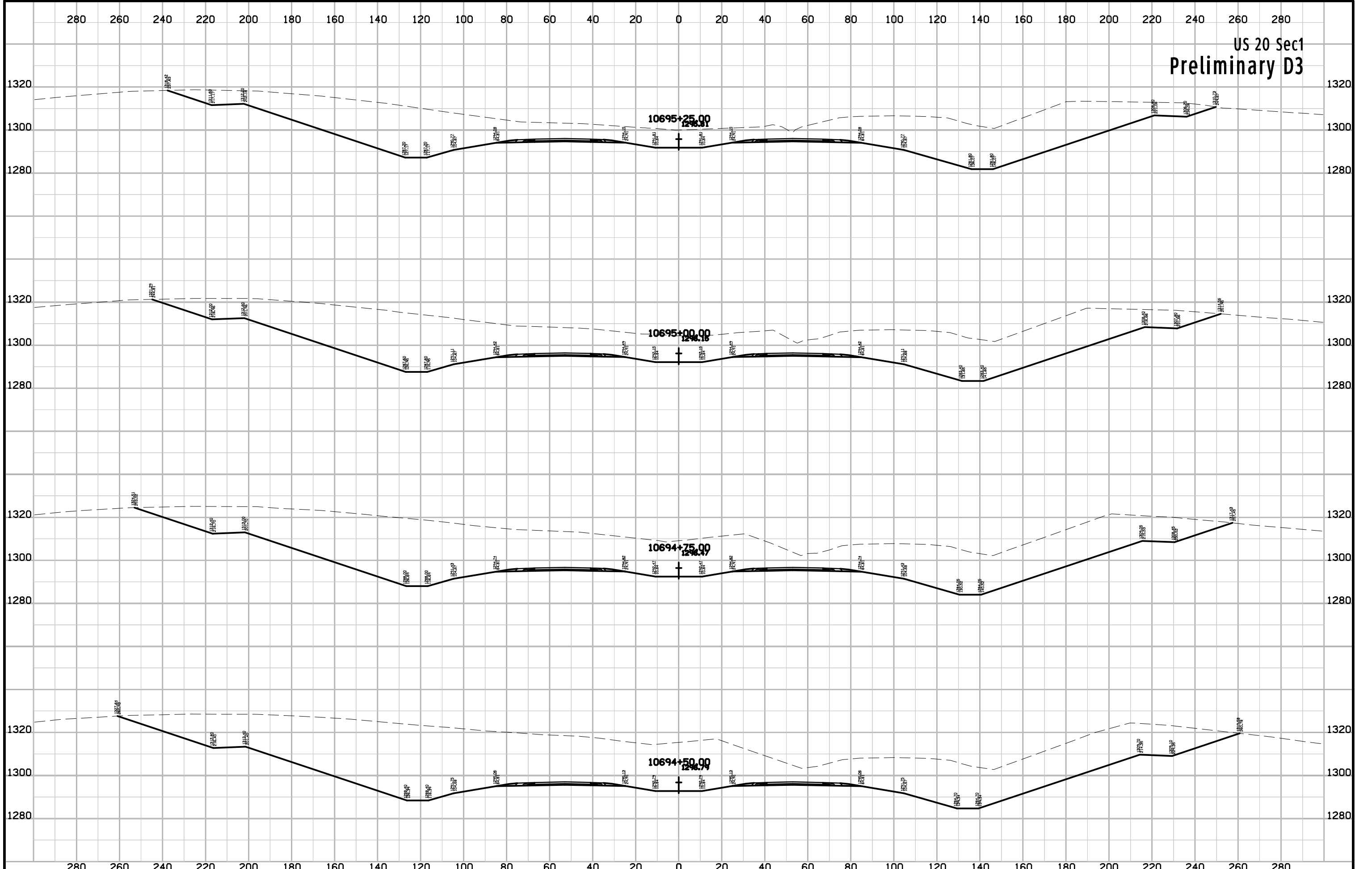
US 20 Sec1
Preliminary D3



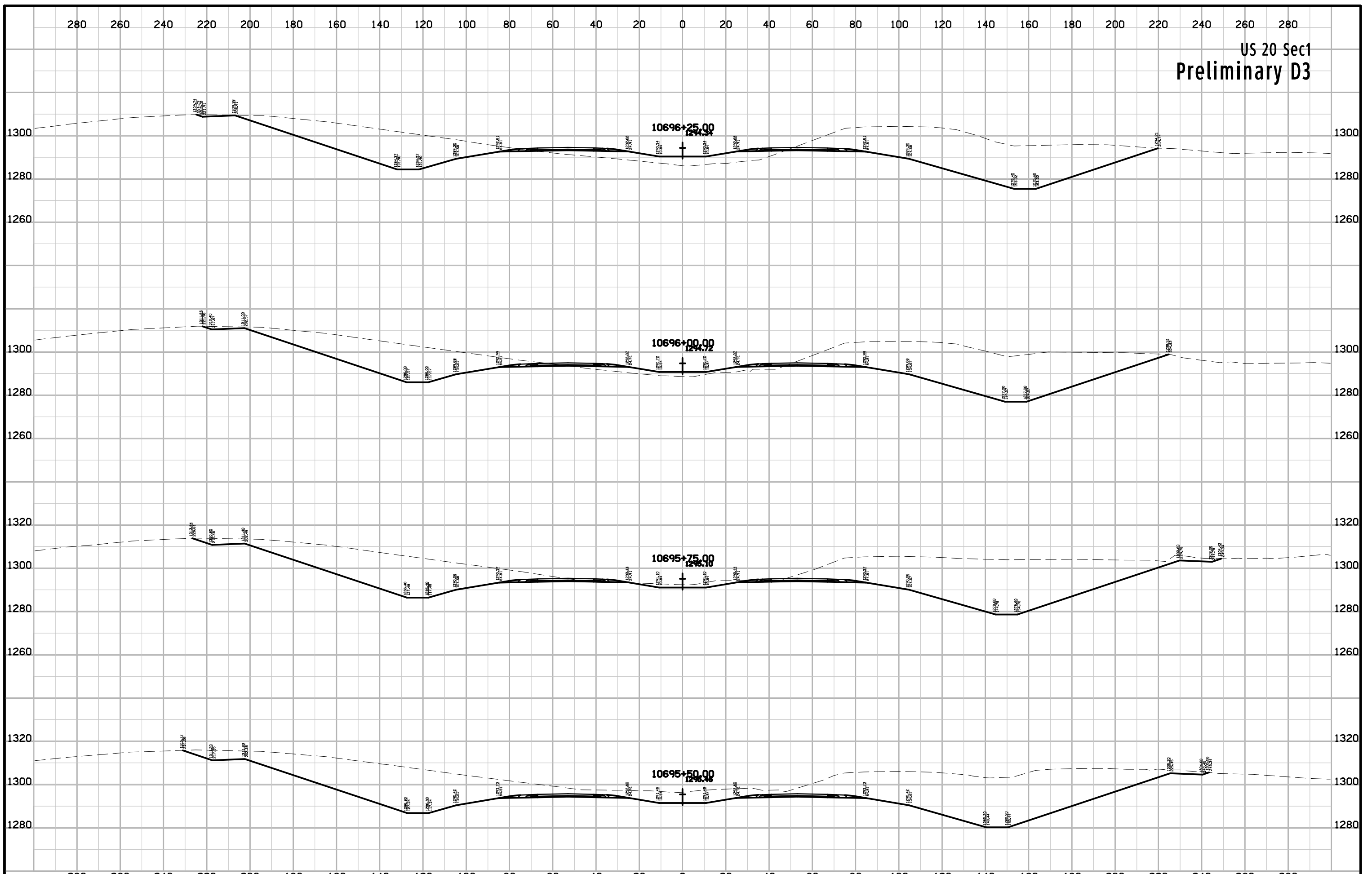
US 20 Sec1
Preliminary D3



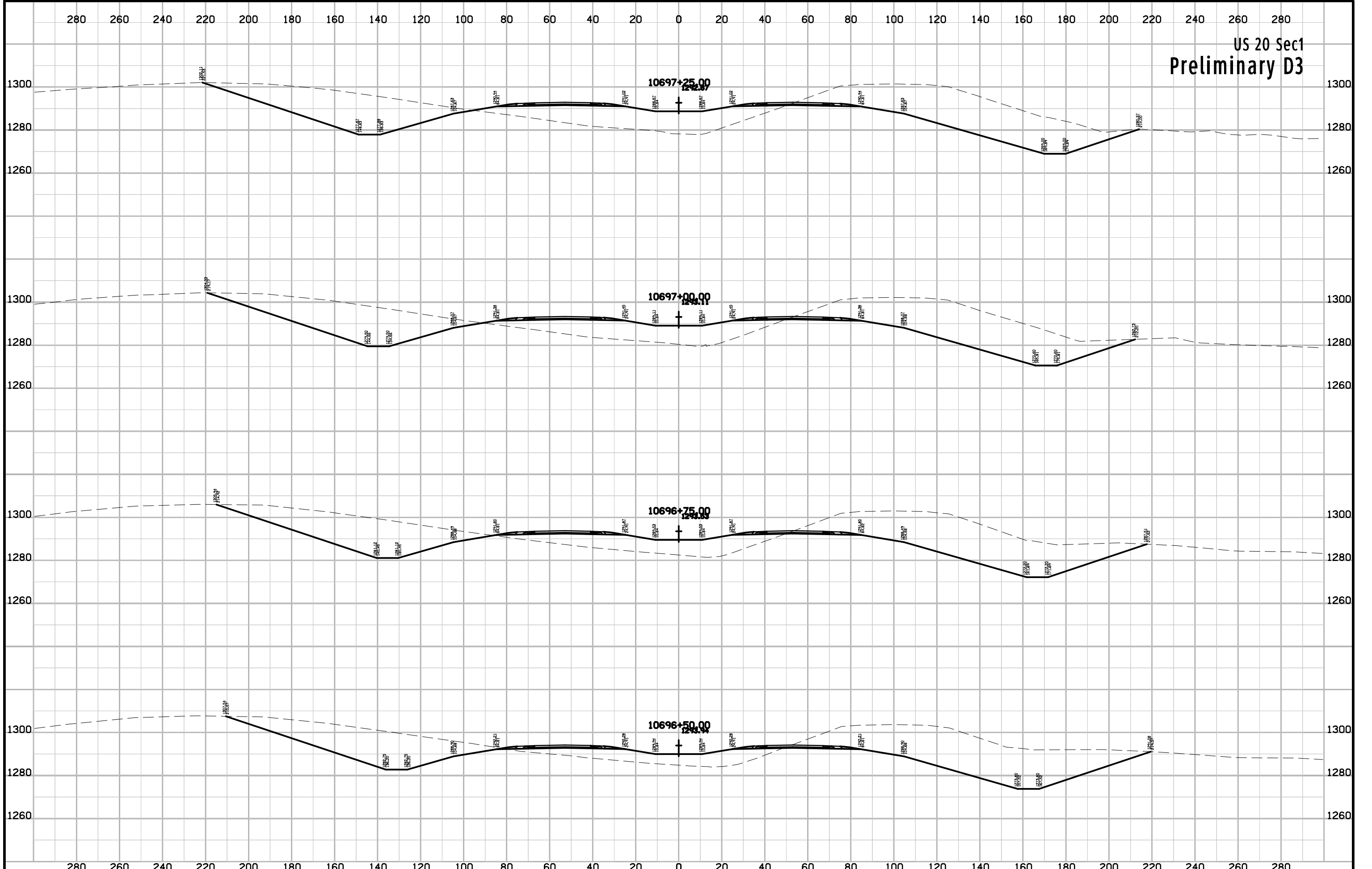
US 20 Sec1
Preliminary D3



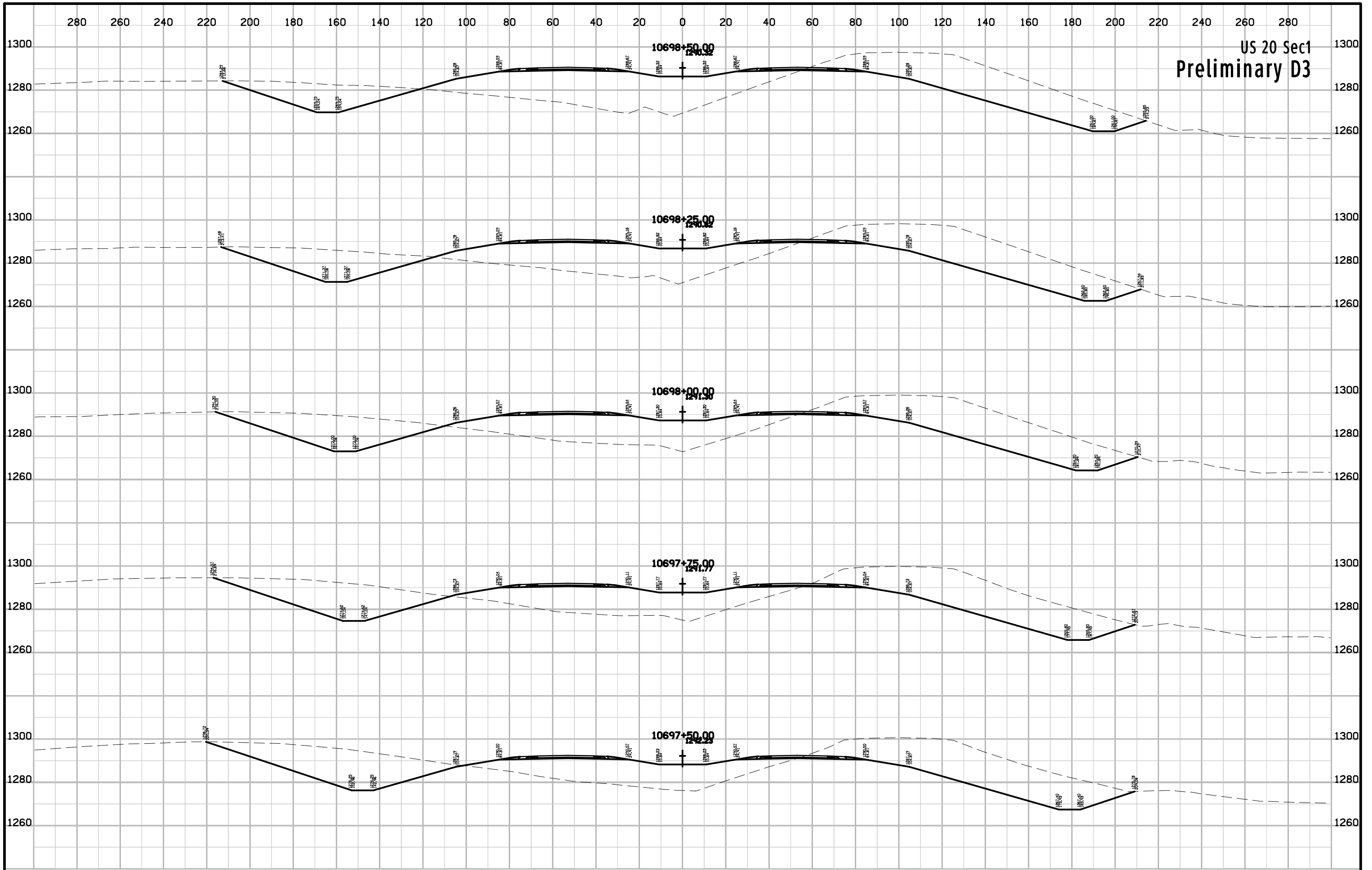
US 20 Sec1
Preliminary D3



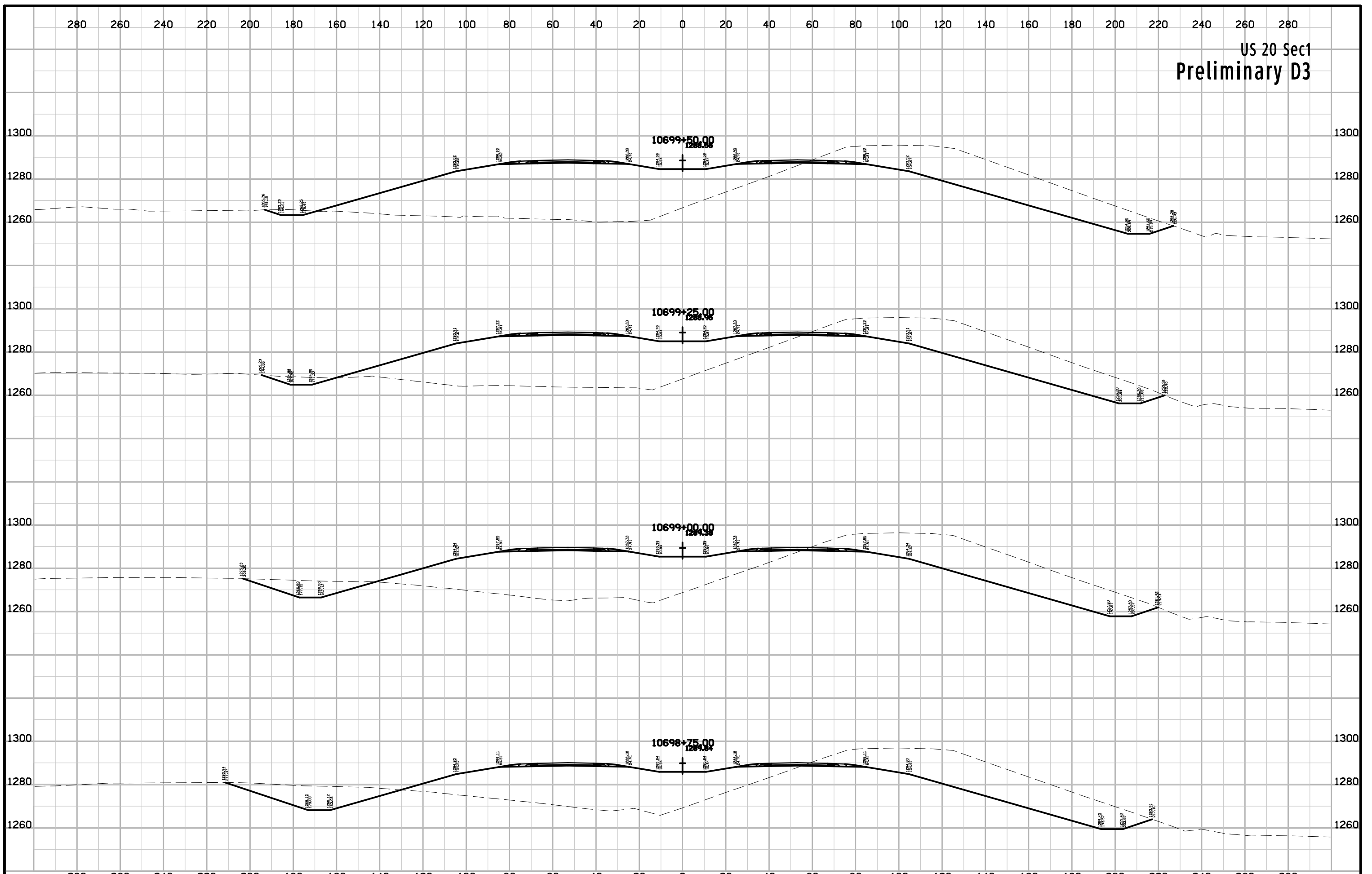
US 20 Sec1
Preliminary D3



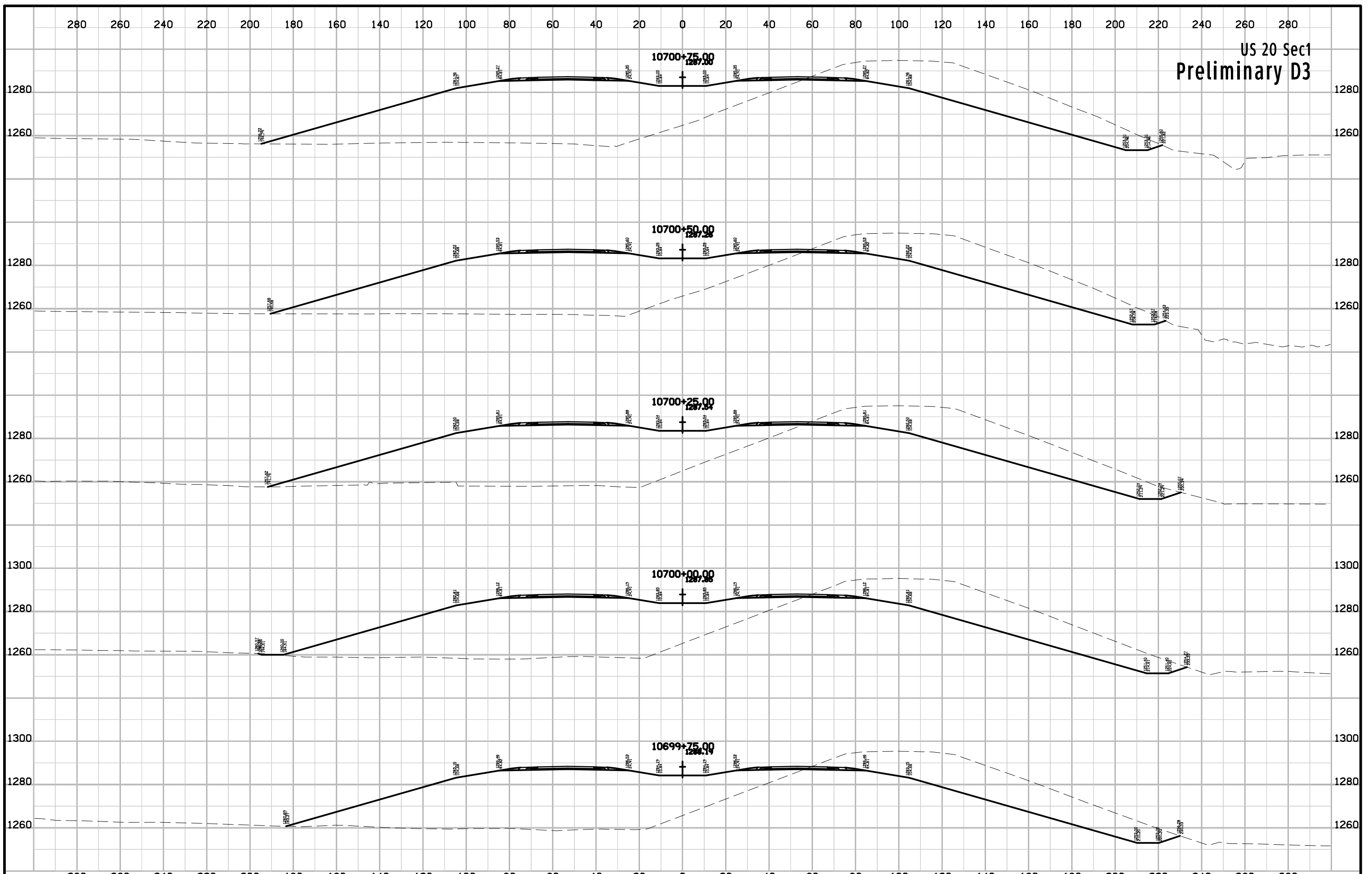
US 20 Sec1
Preliminary D3



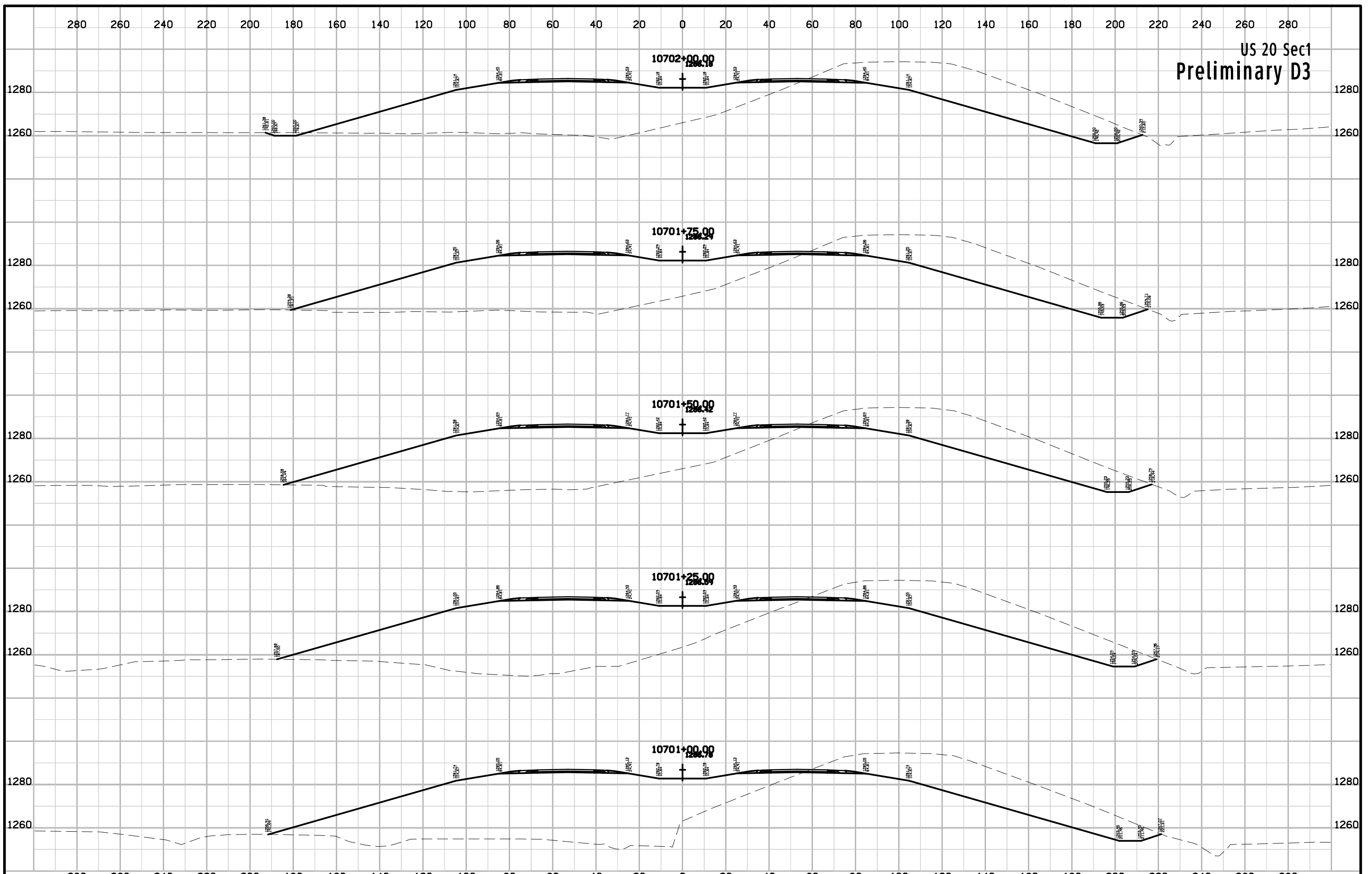
US 20 Sec1
Preliminary D3



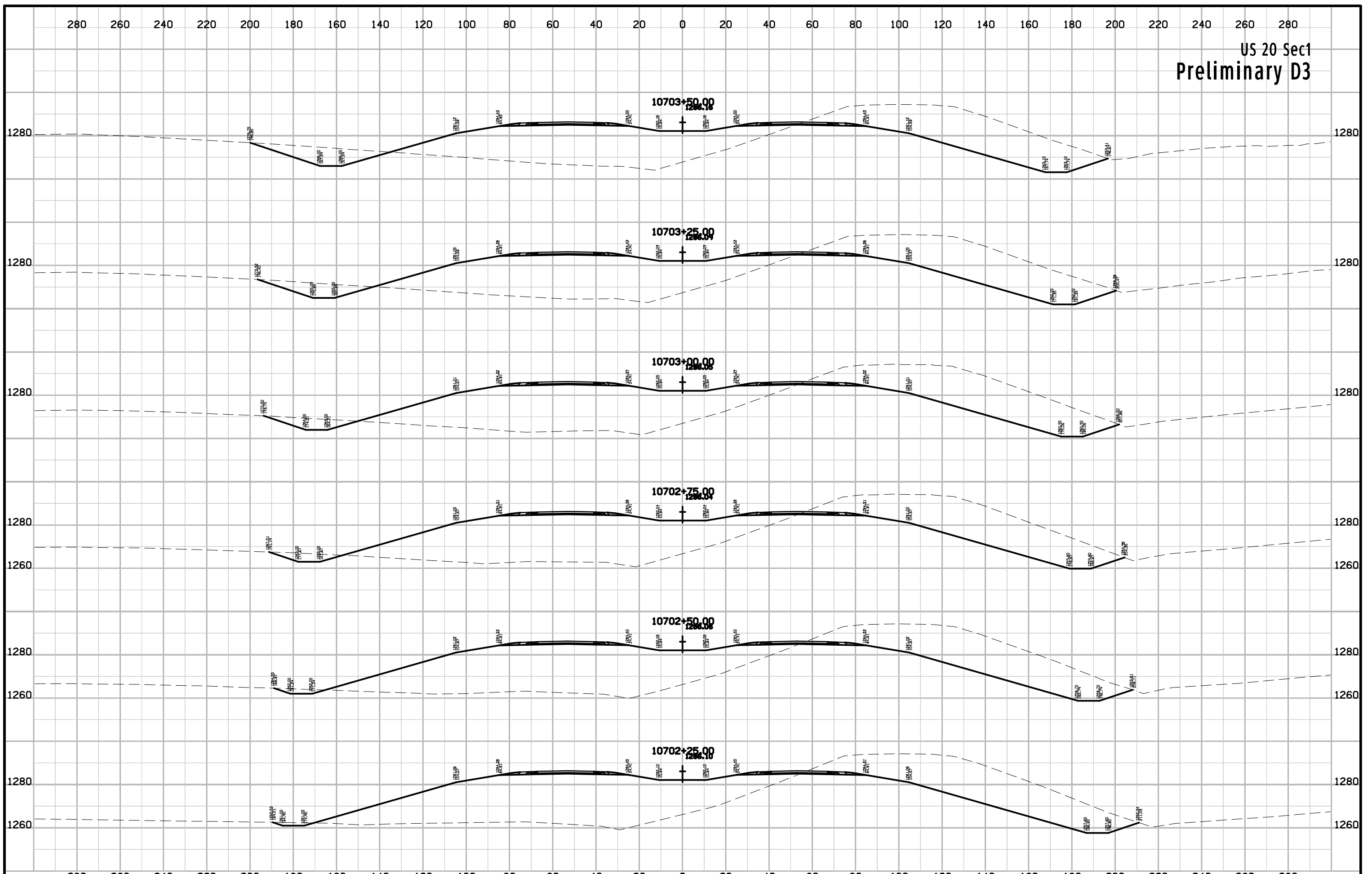
US 20 Sec1
Preliminary D3



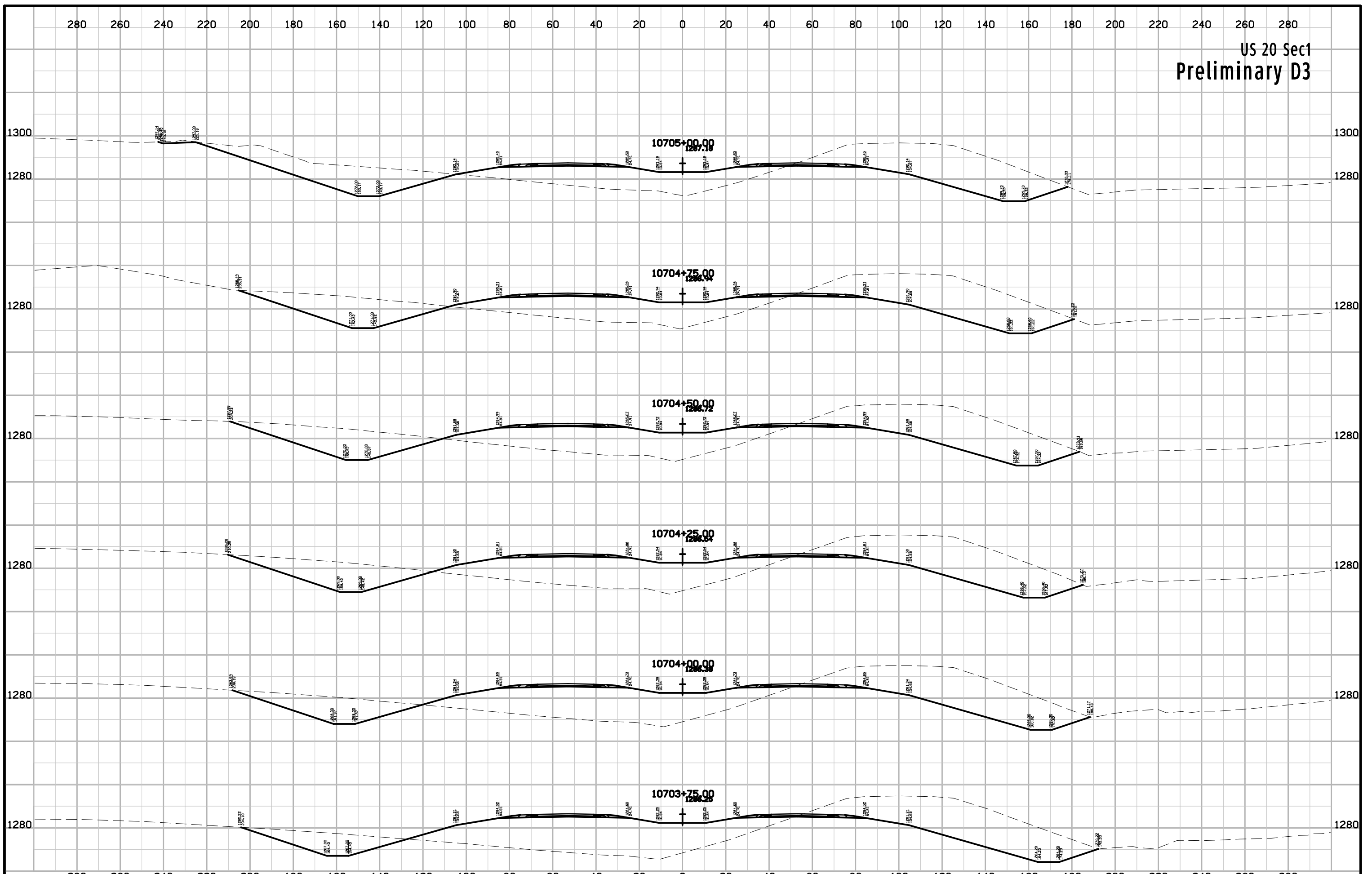
US 20 Sec1
Preliminary D3



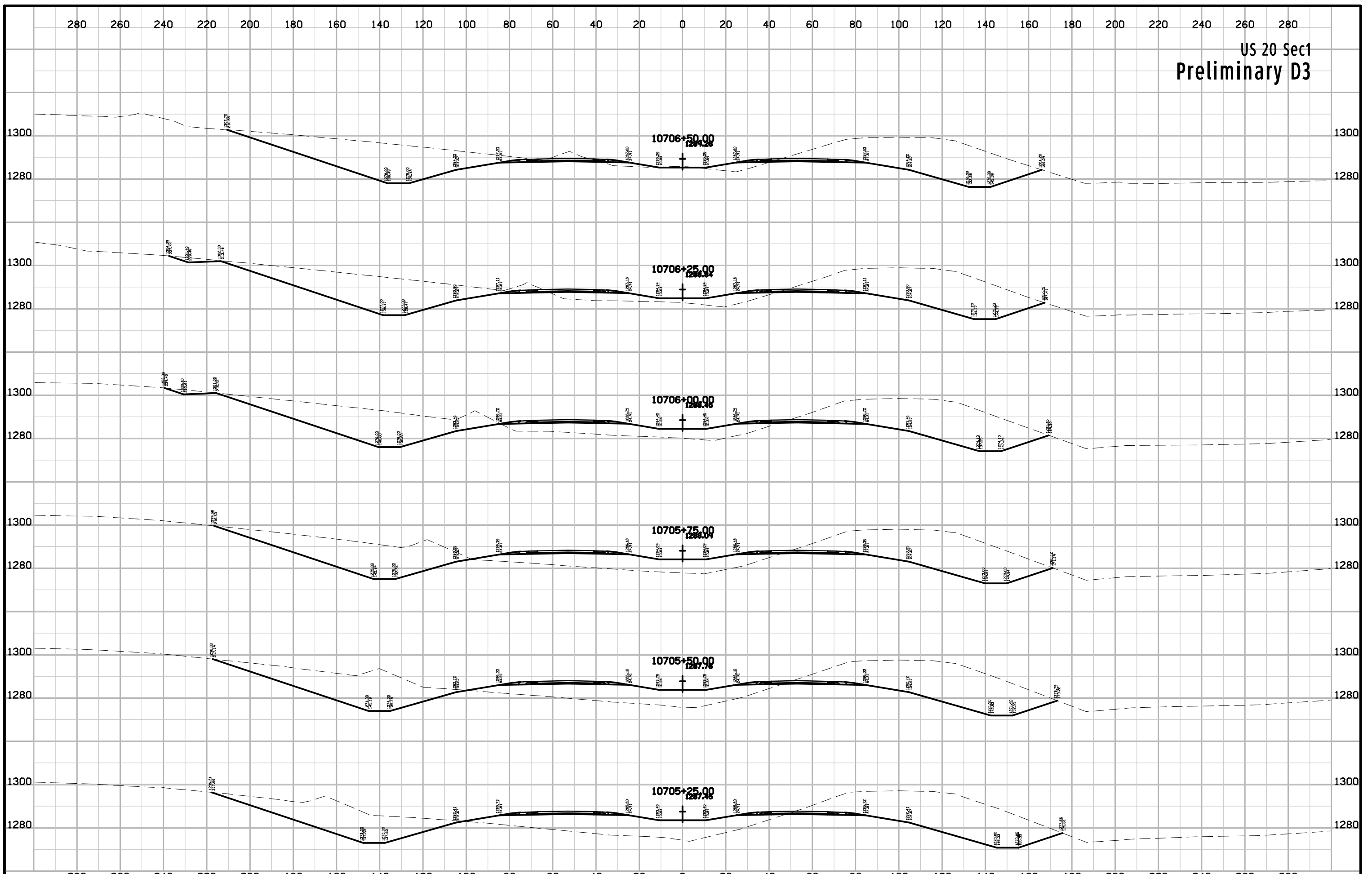
US 20 Sec1
Preliminary D3



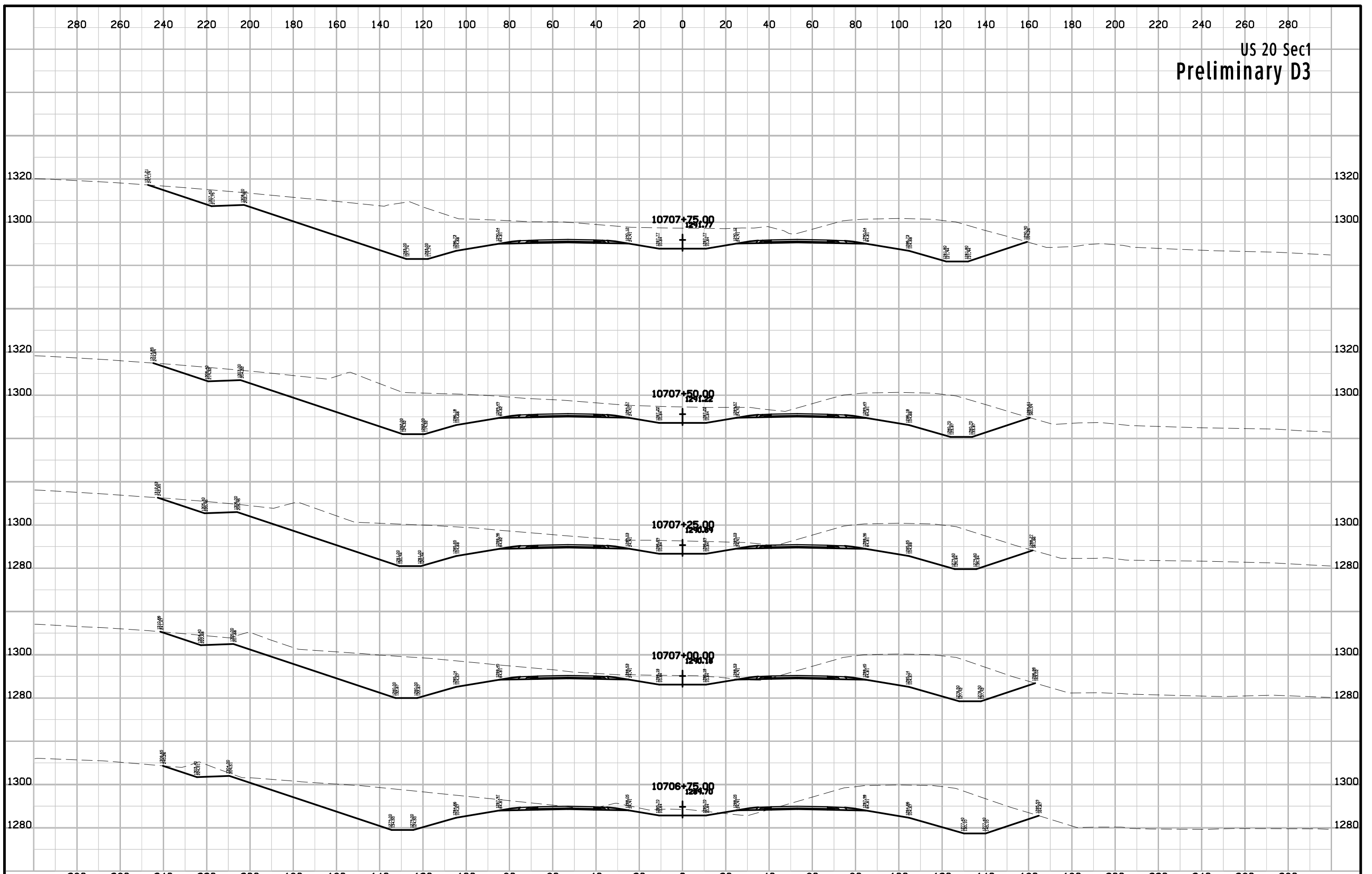
US 20 Sec1
Preliminary D3



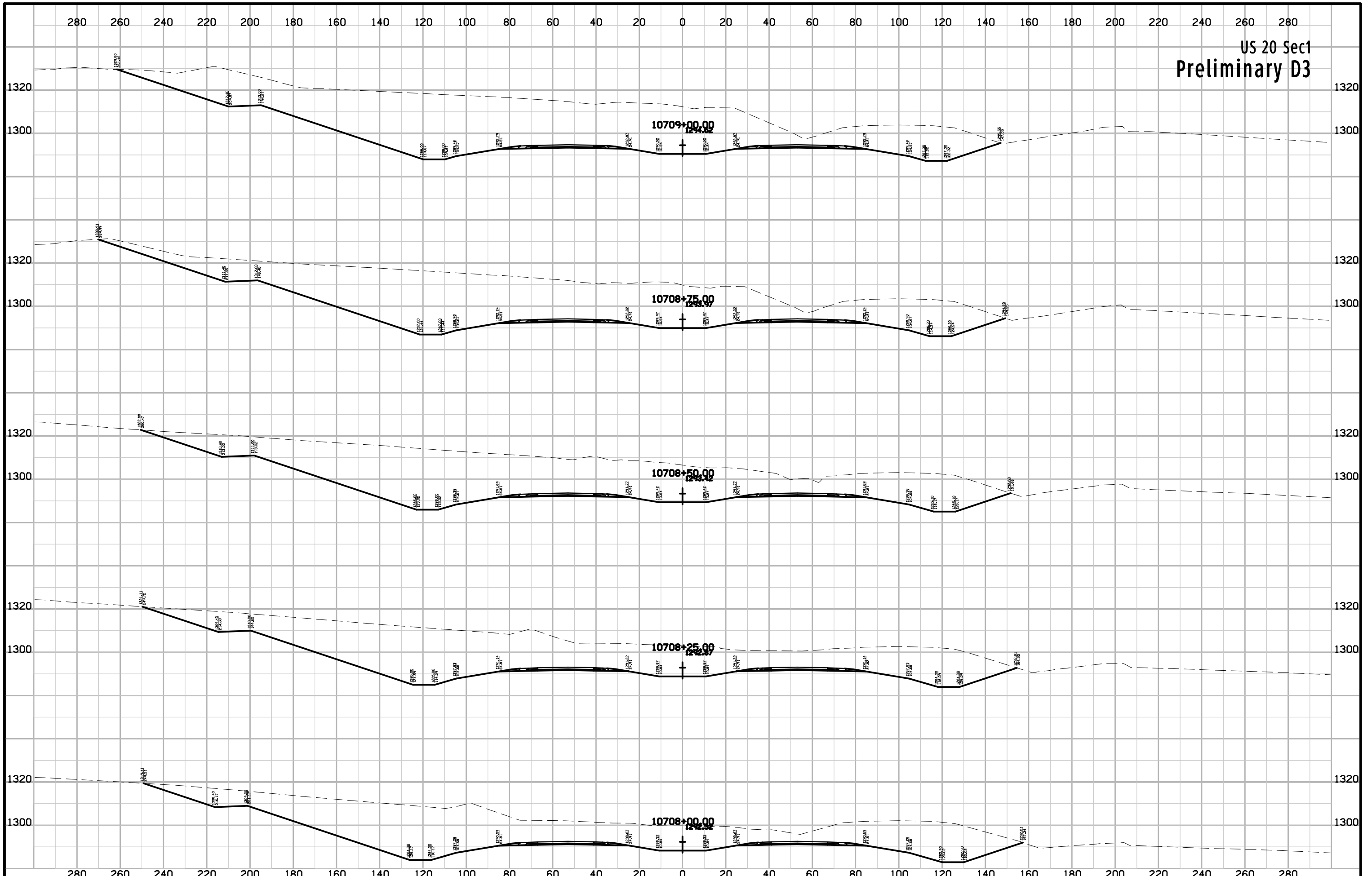
US 20 Sec1
Preliminary D3



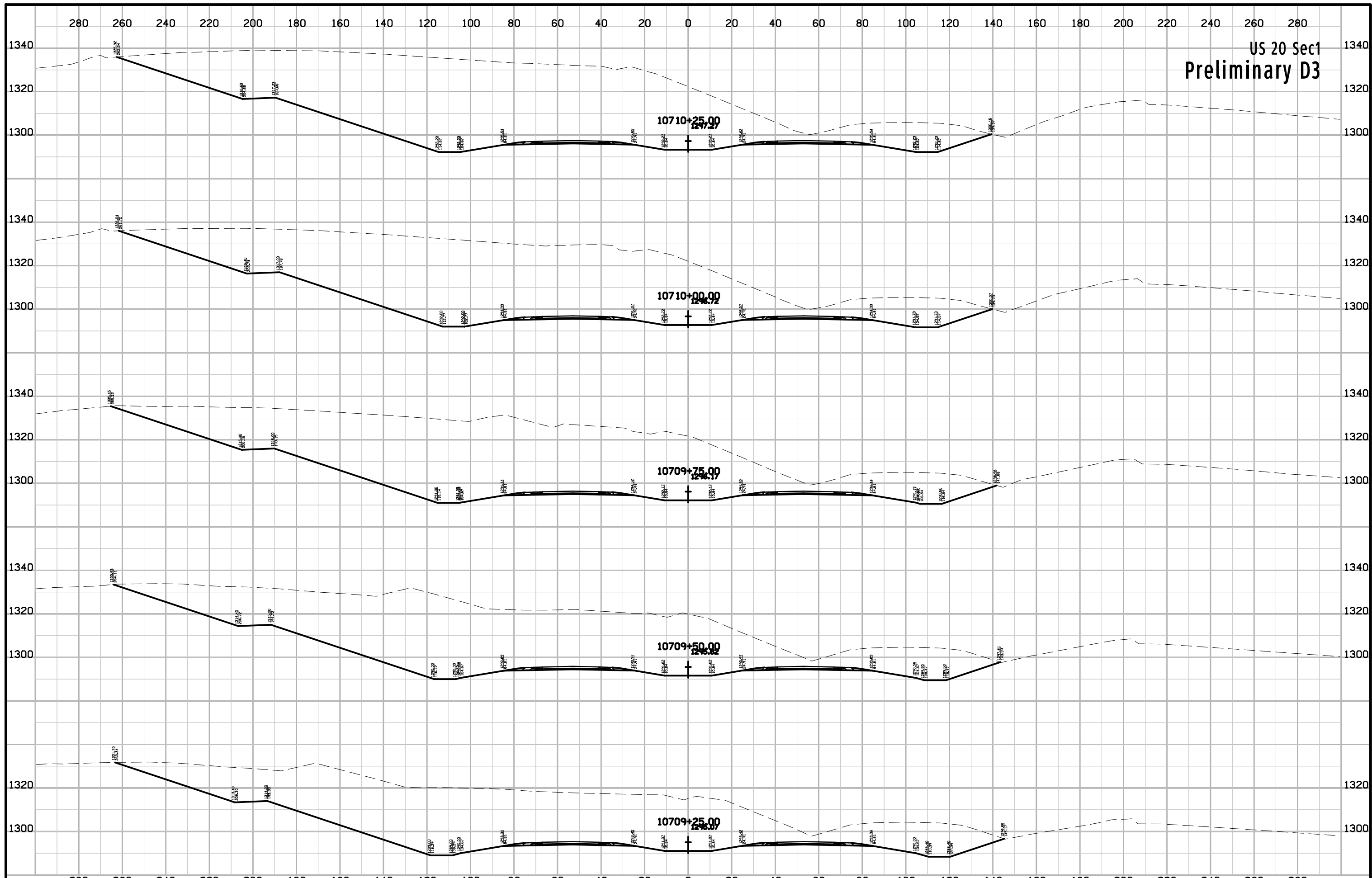
US 20 Sec1
Preliminary D3

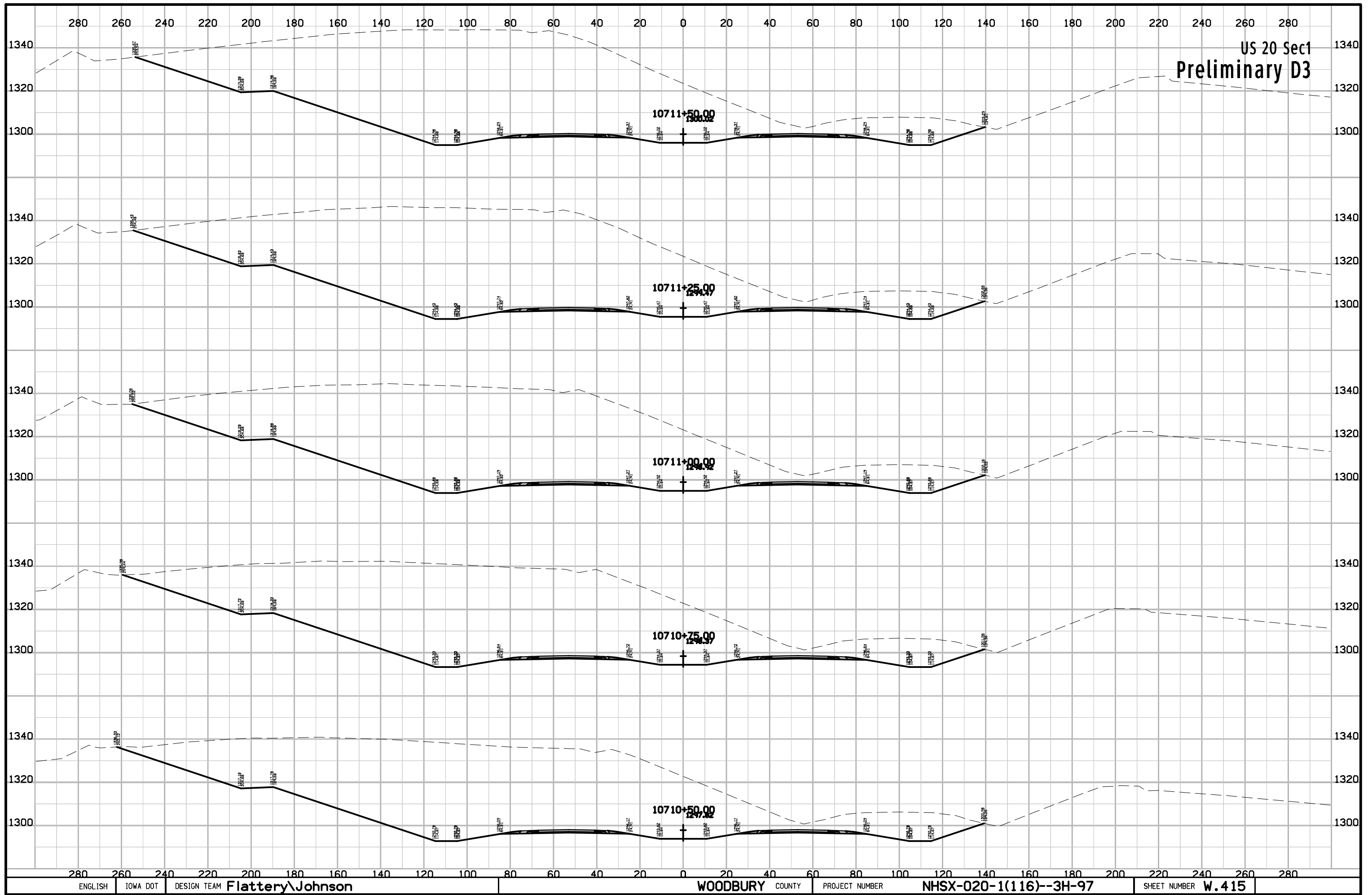


US 20 Sec1
Preliminary D3

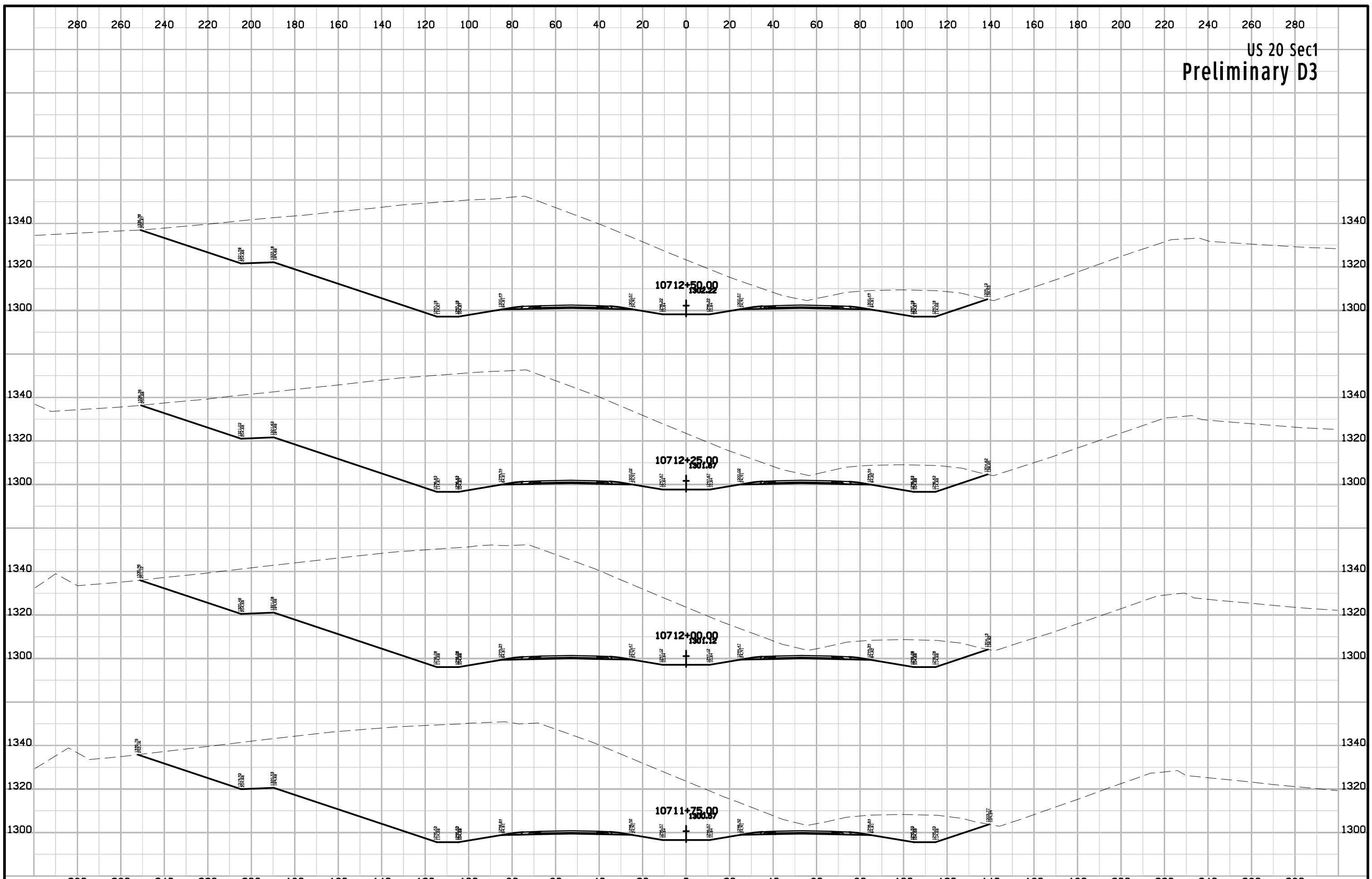


US 20 Sec1
Preliminary D3

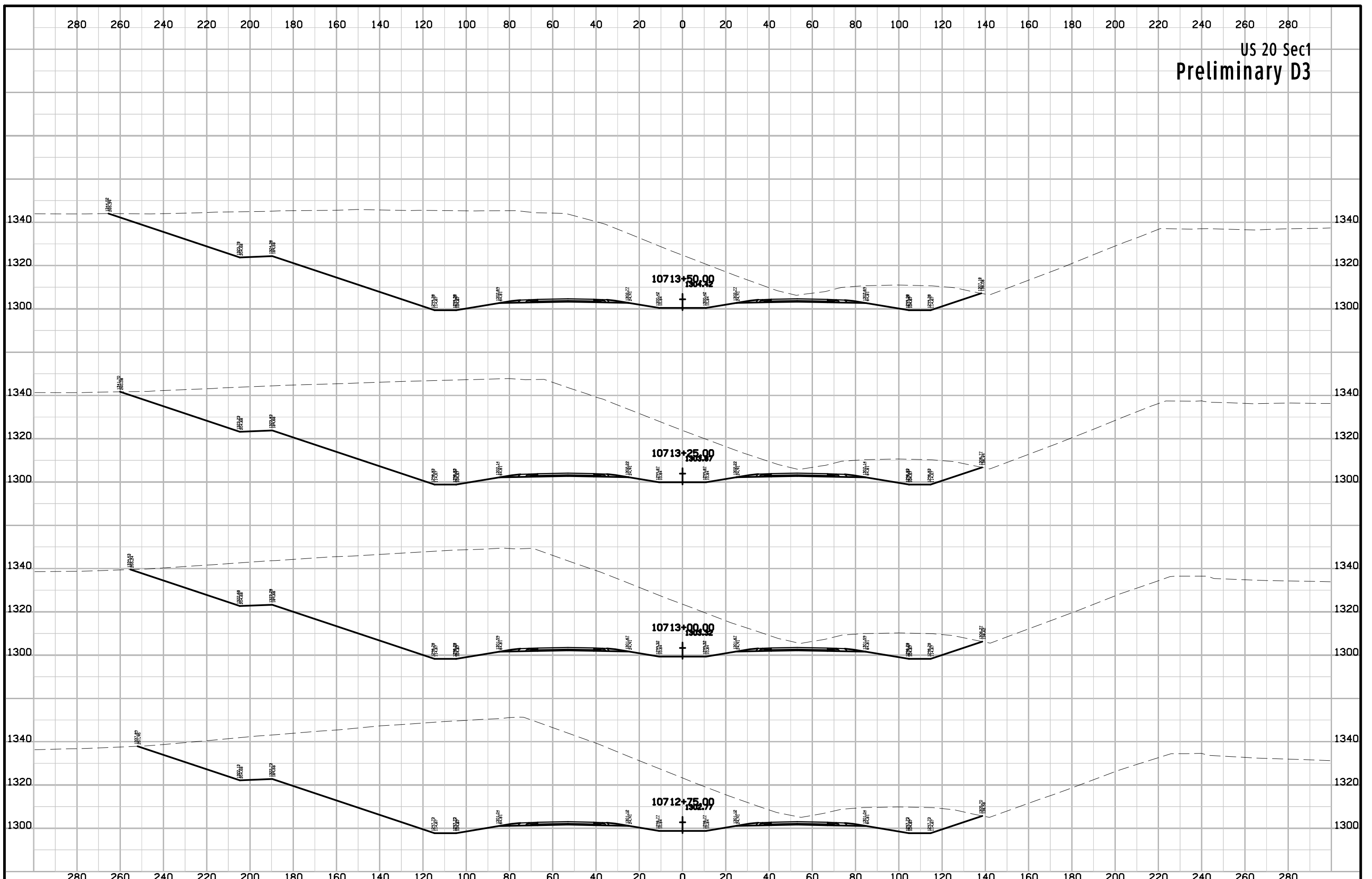




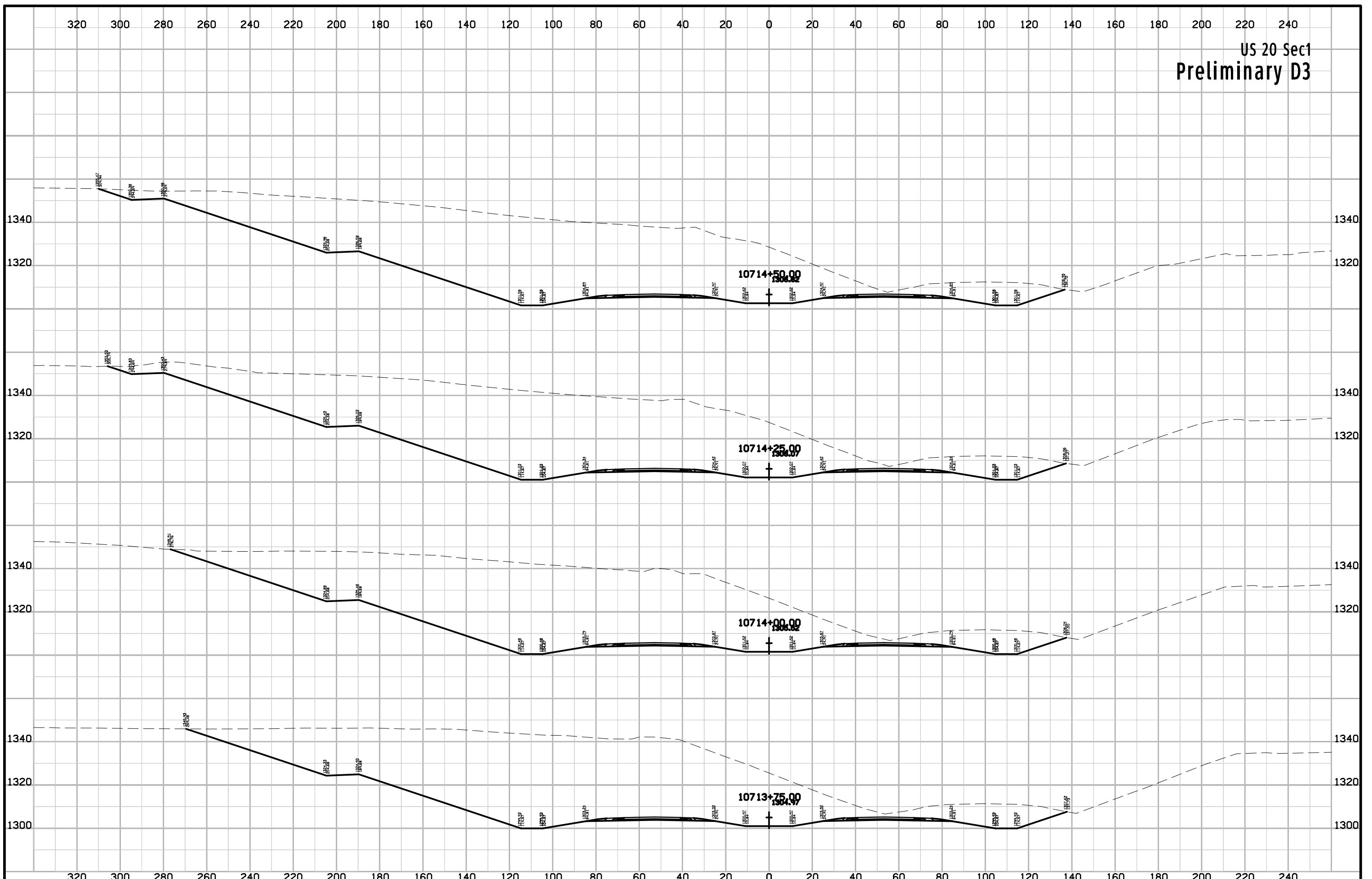
US 20 Sec1
Preliminary D3



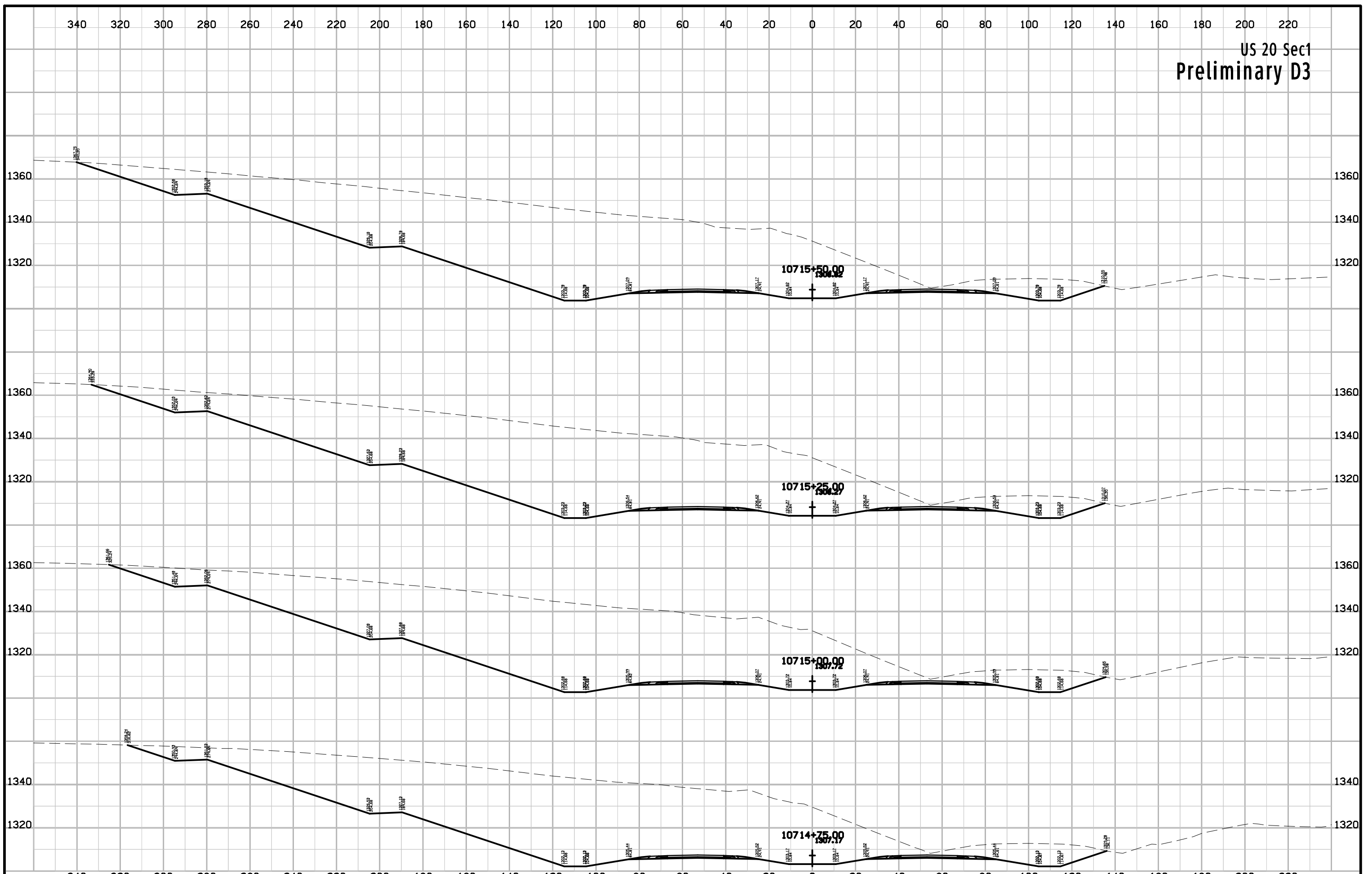
US 20 Sec1
Preliminary D3



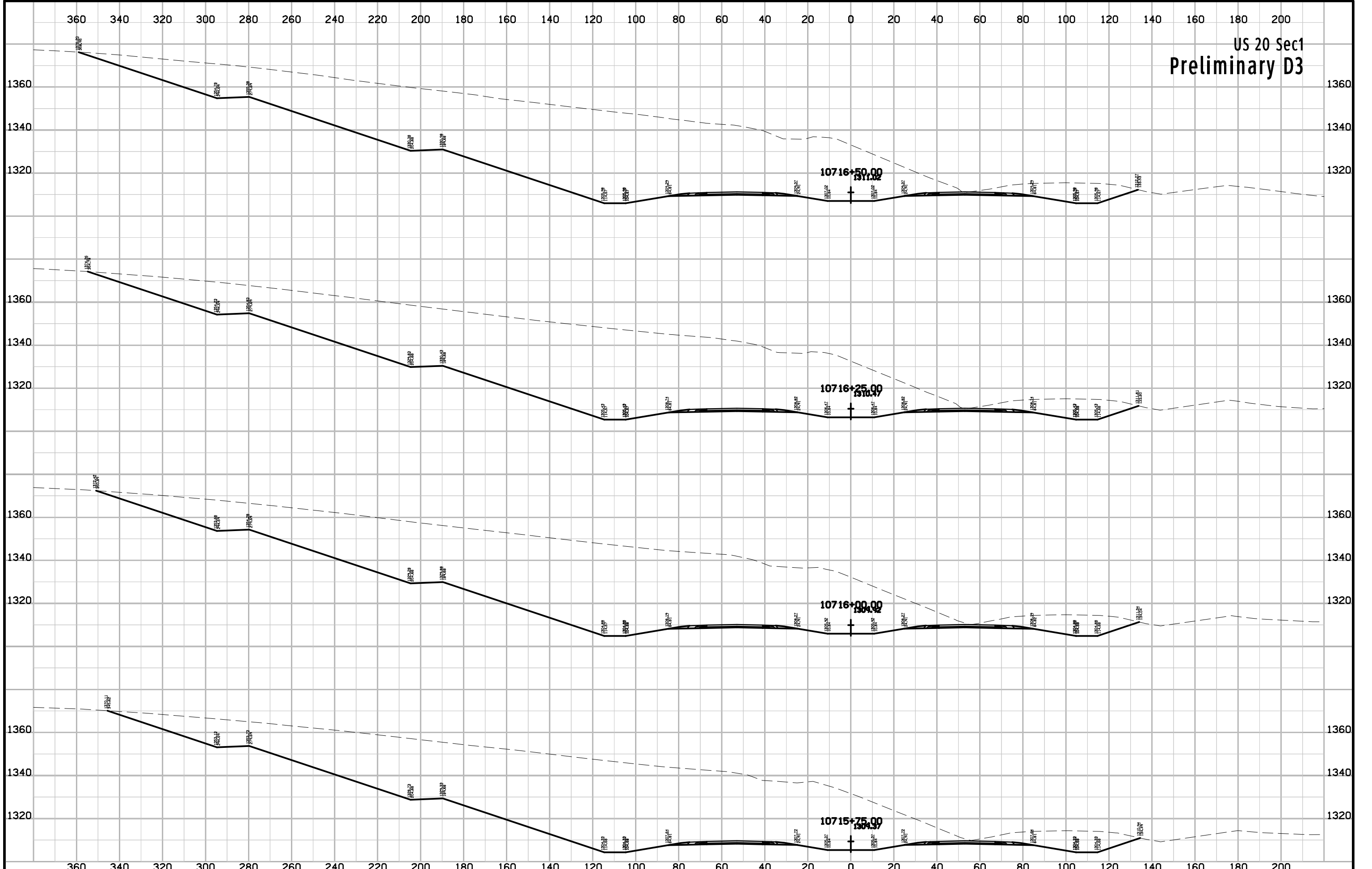
US 20 Sec1
Preliminary D3



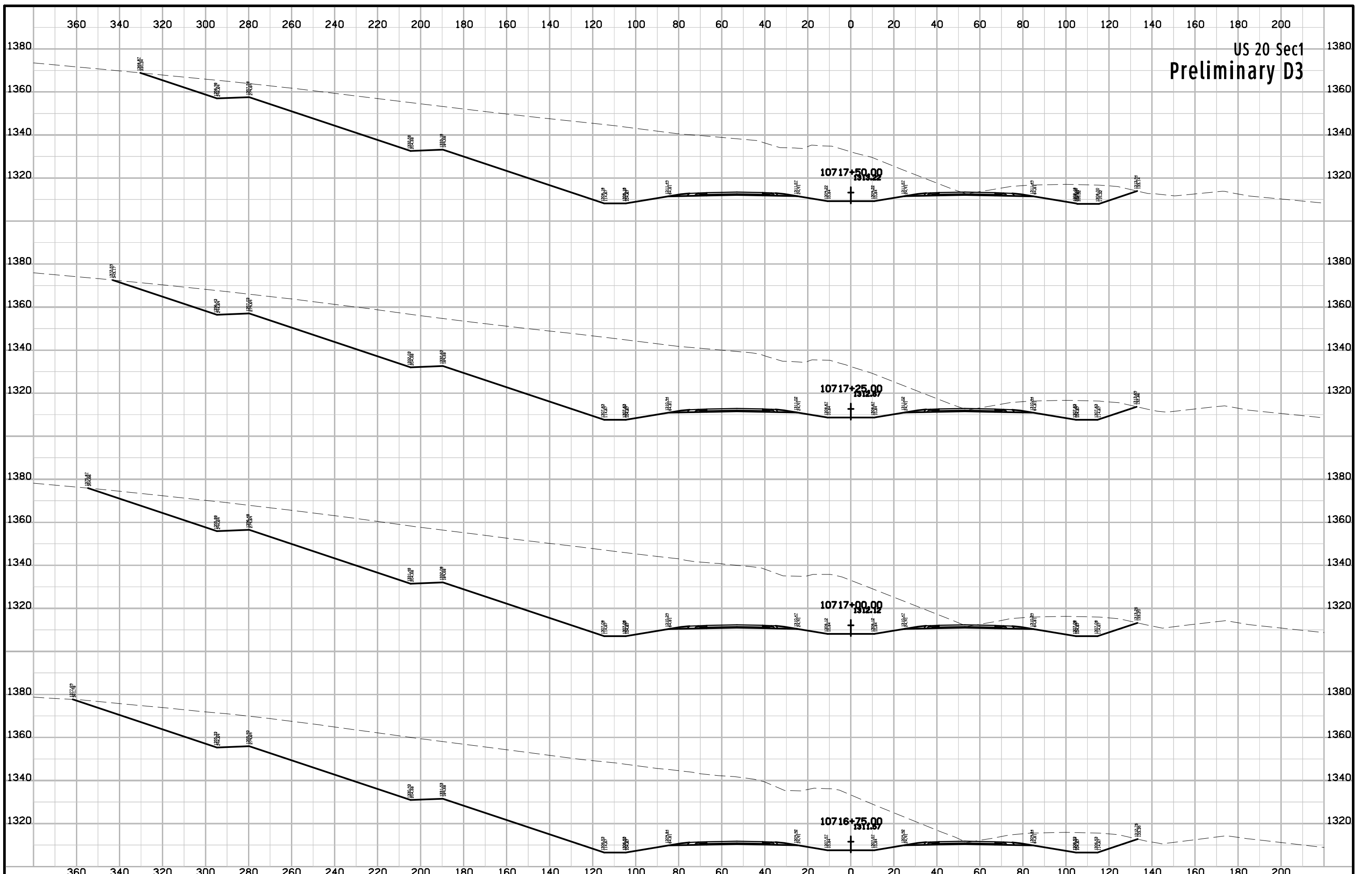
US 20 Sec1
Preliminary D3



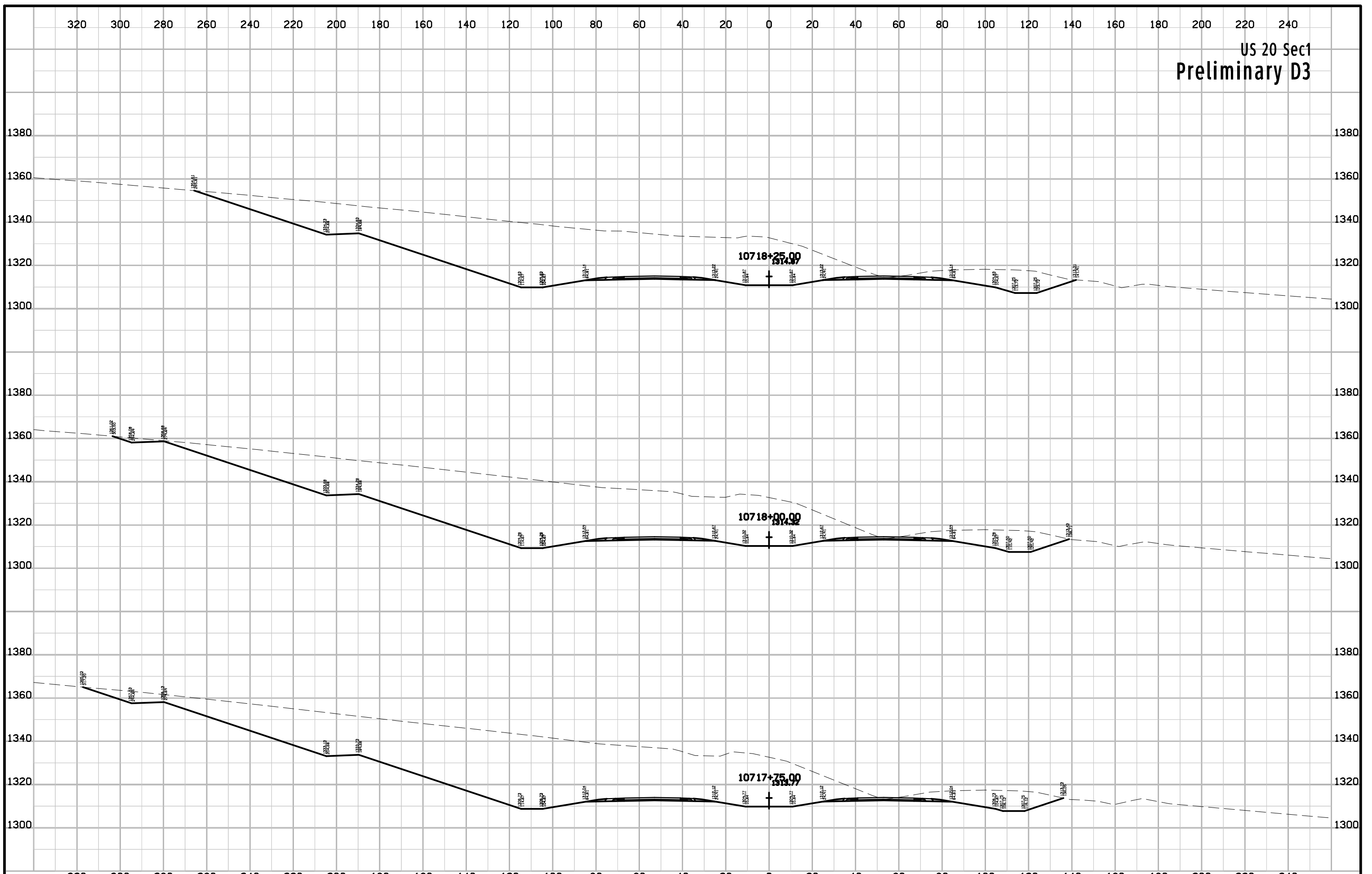
US 20 Sec1
Preliminary D3



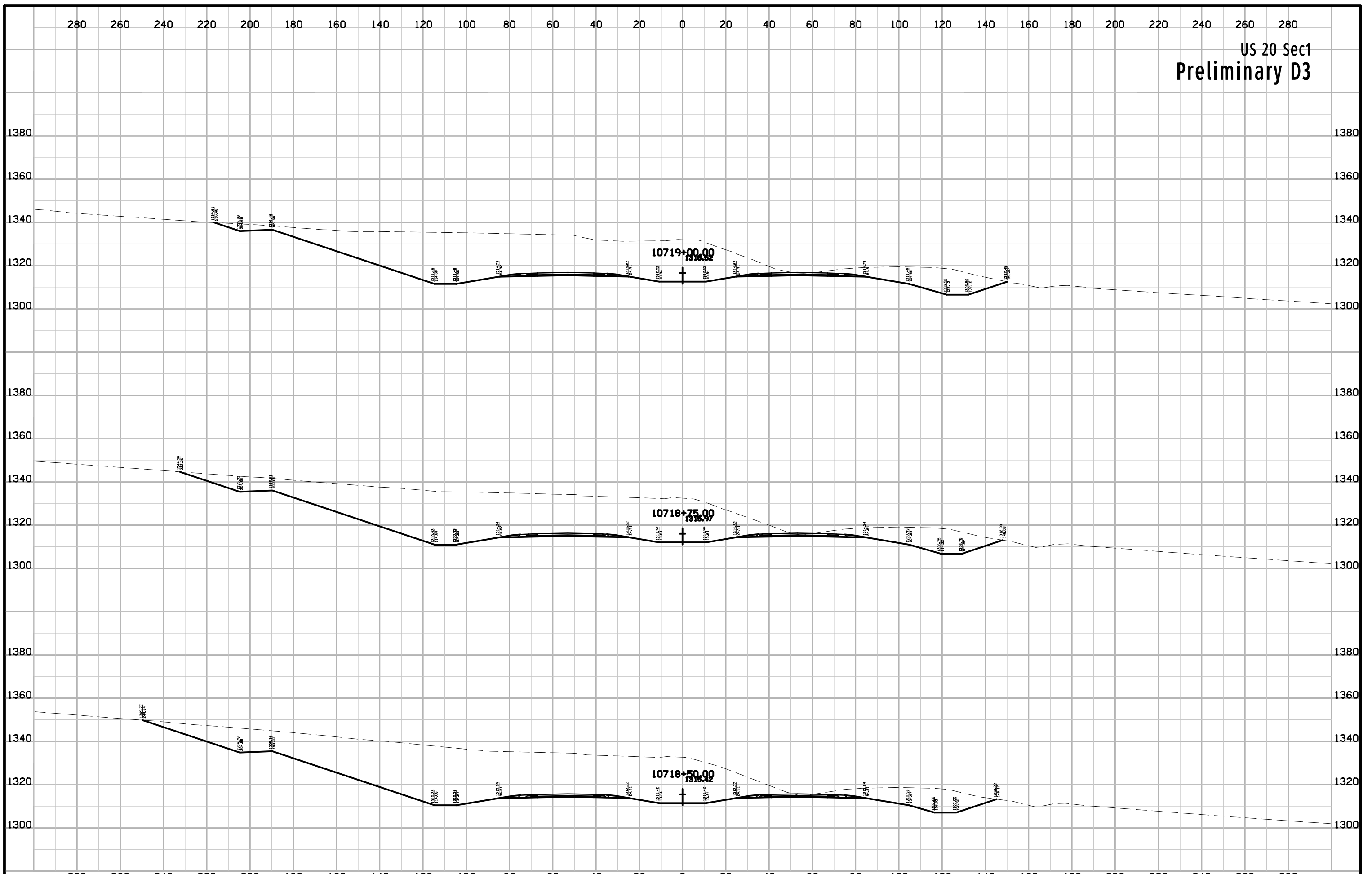
US 20 Sec1
Preliminary D3



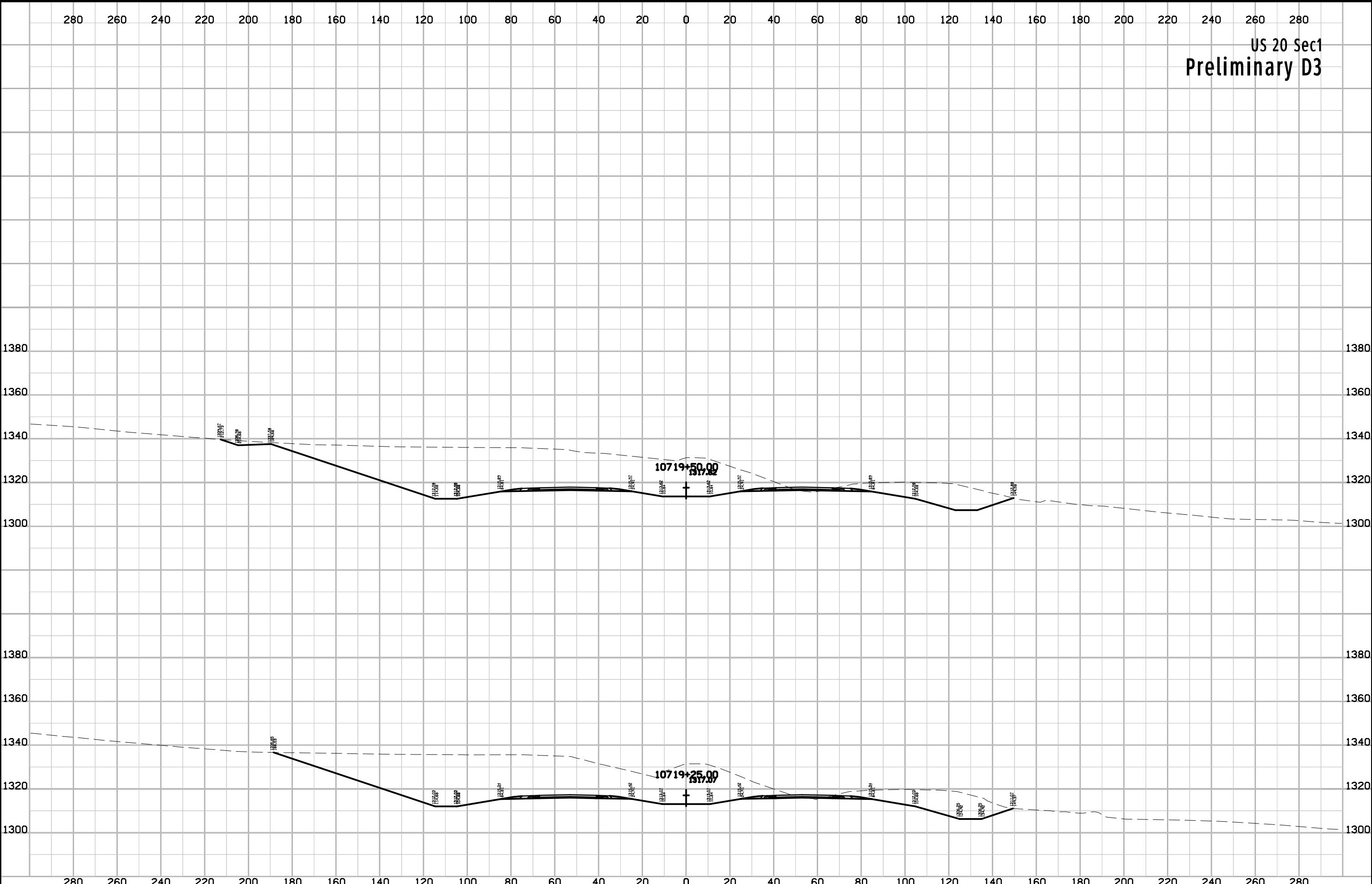
US 20 Sec1
Preliminary D3



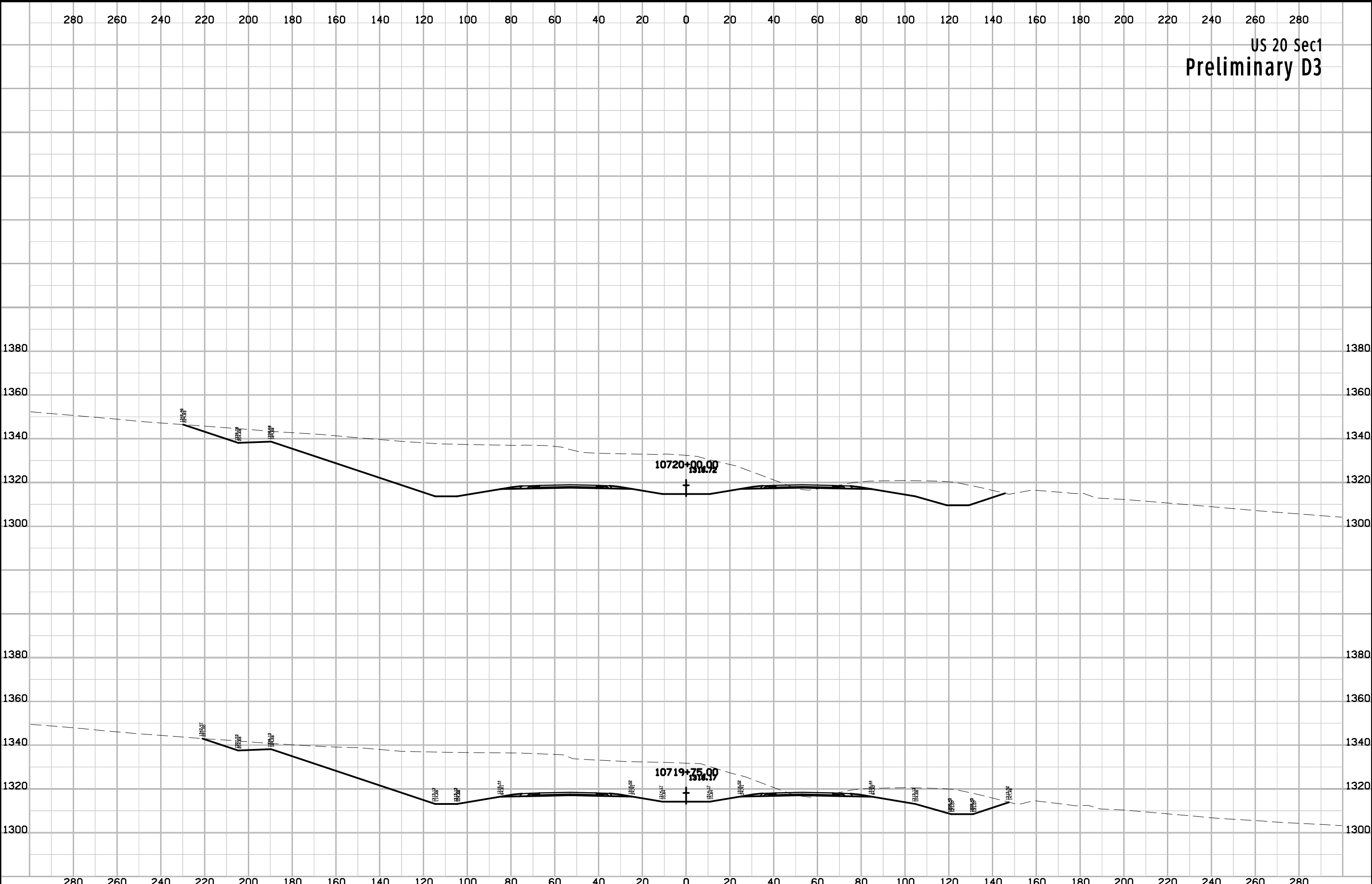
US 20 Sec1
Preliminary D3



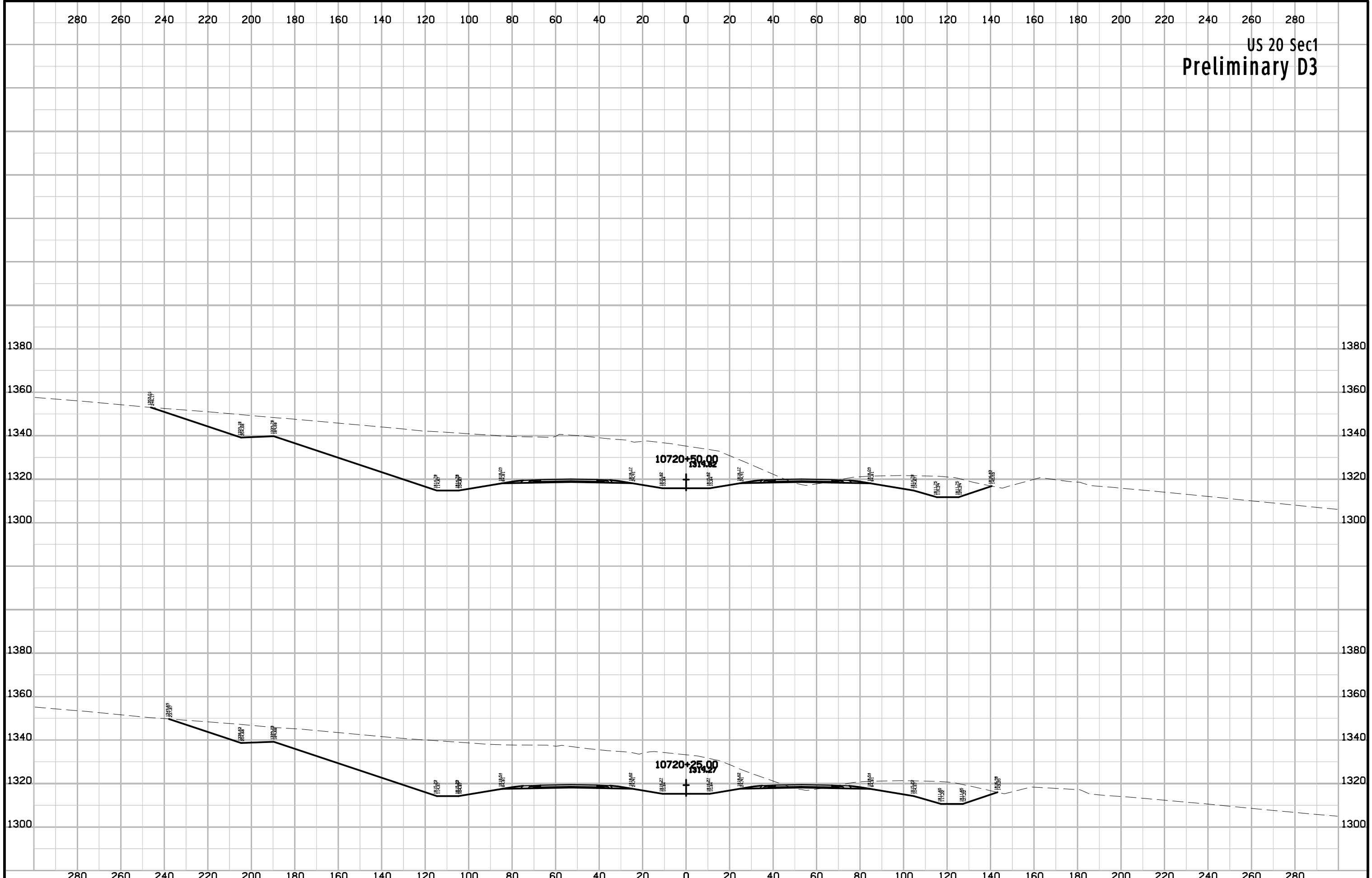
US 20 Sec1
Preliminary D3



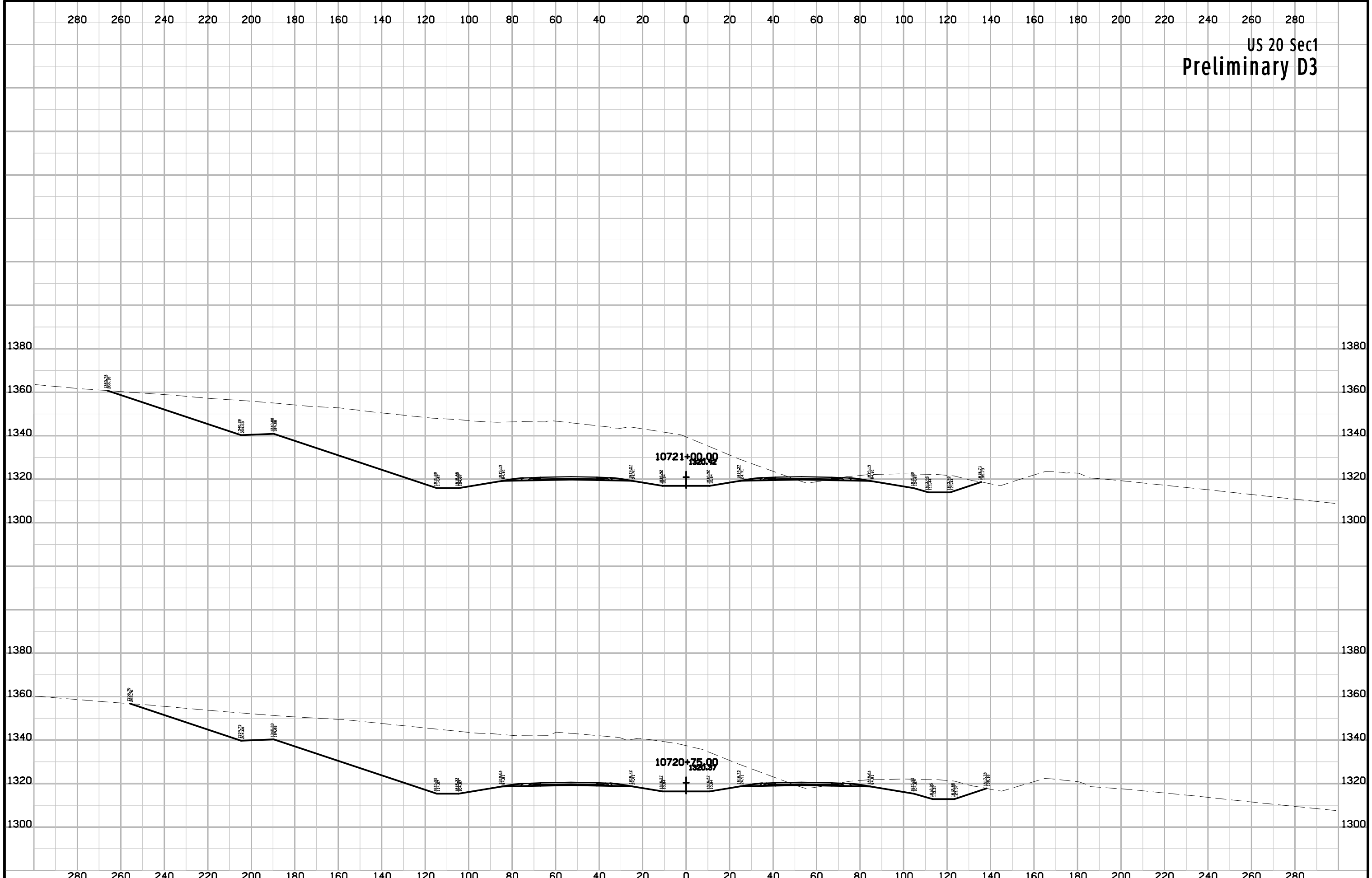
US 20 Sec1
Preliminary D3



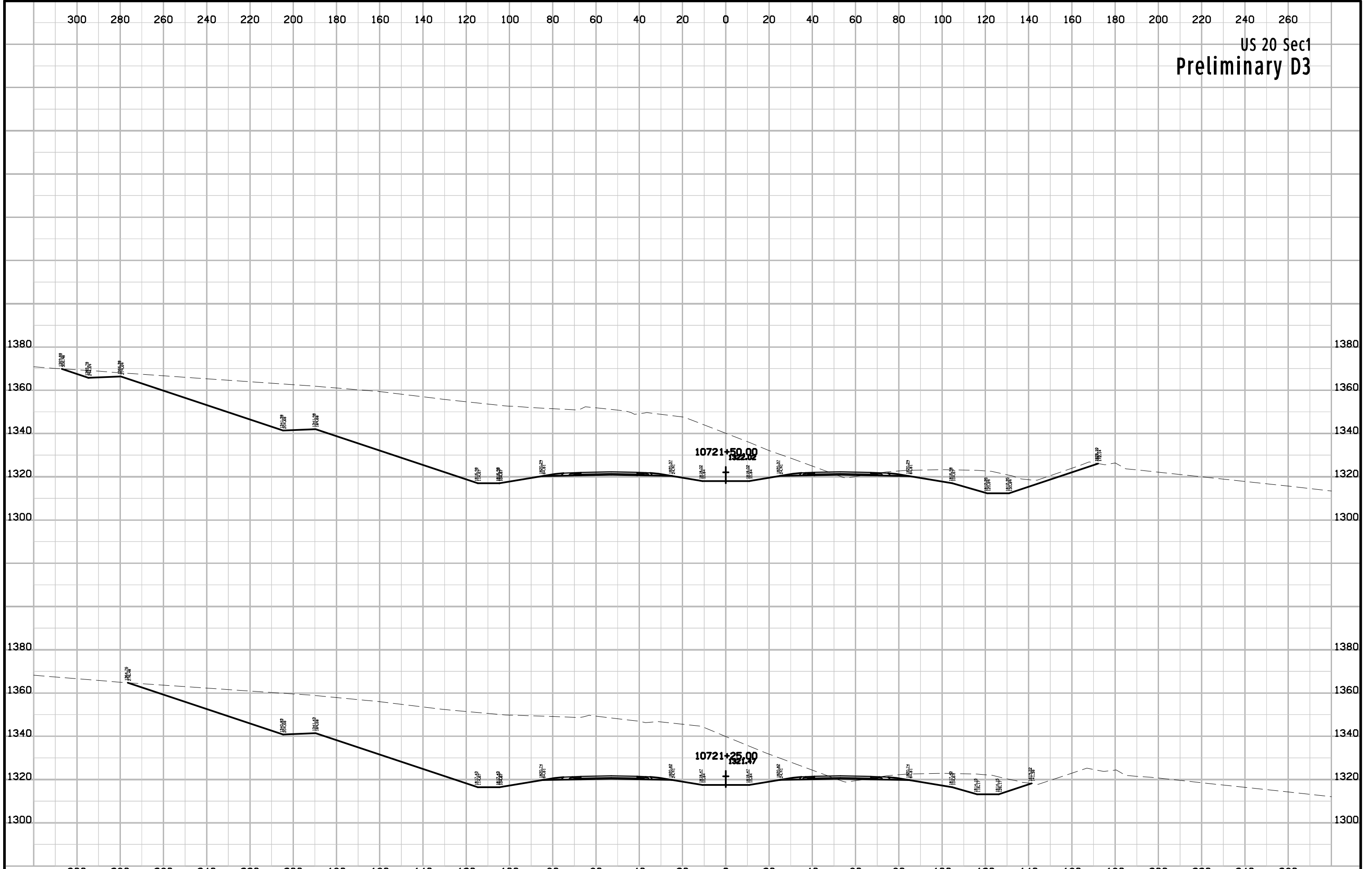
US 20 Sec1
Preliminary D3



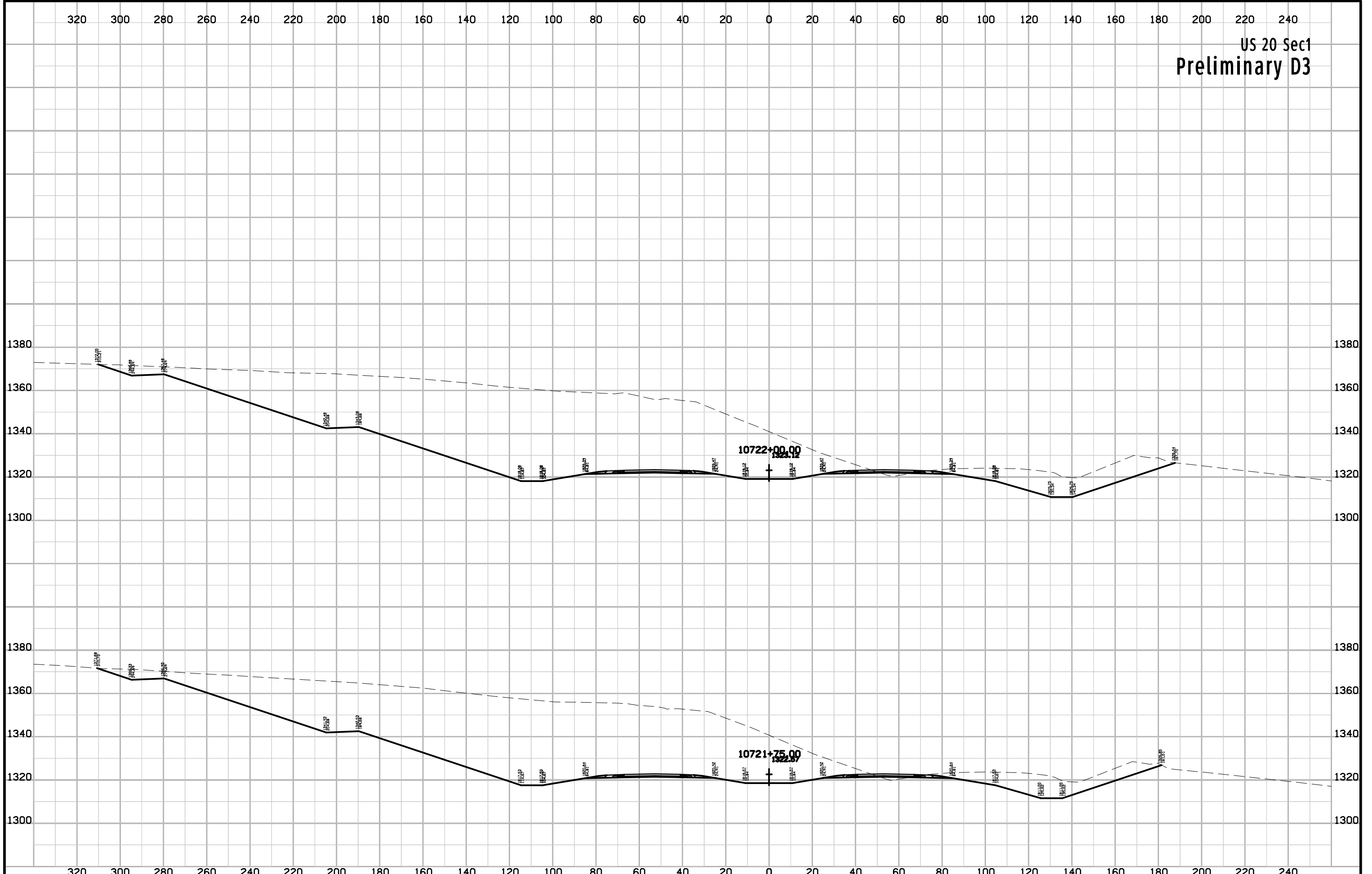
US 20 Sec1
Preliminary D3



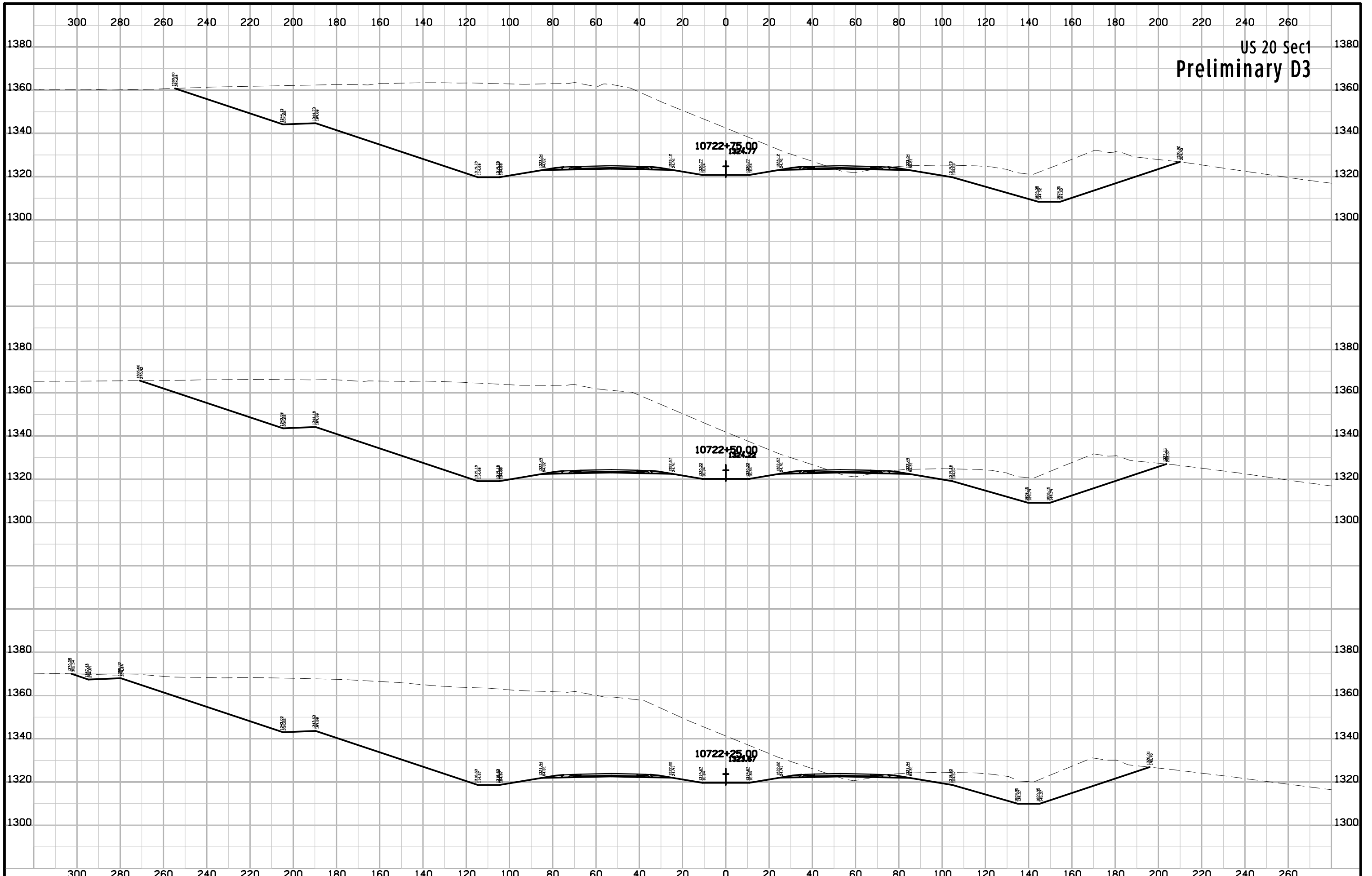
US 20 Sec1
Preliminary D3



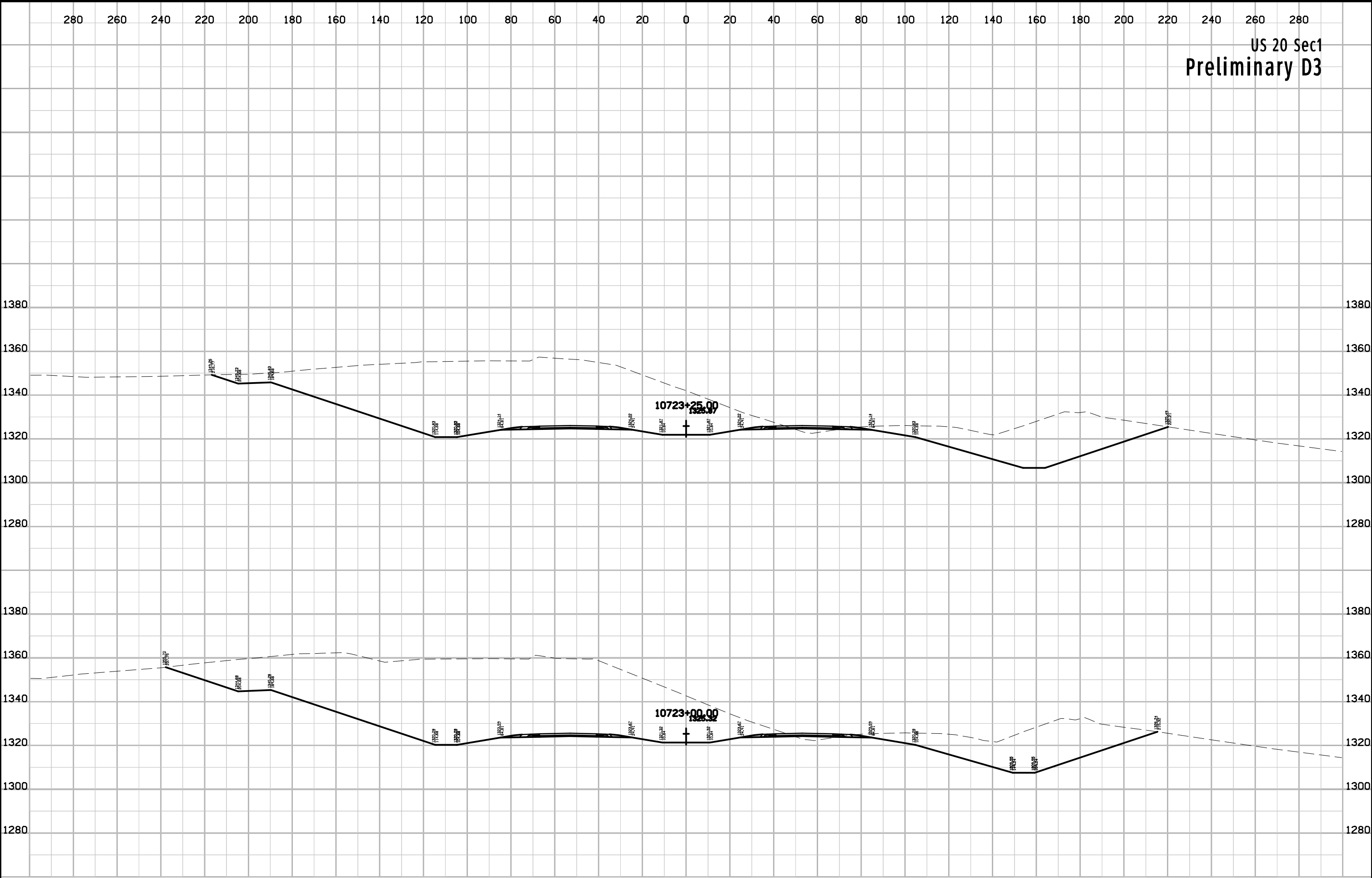
US 20 Sec1
Preliminary D3



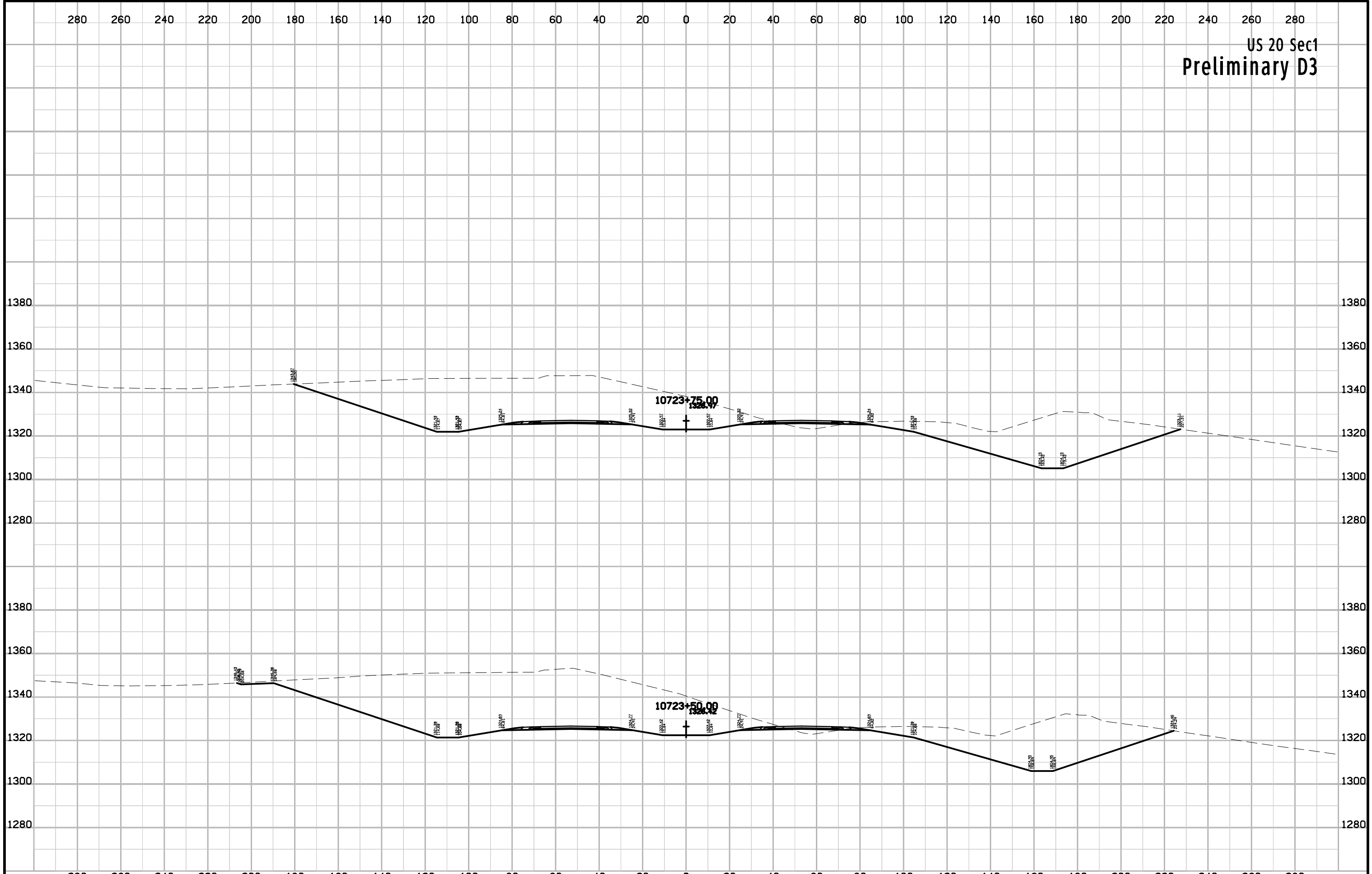
US 20 Sec1
Preliminary D3



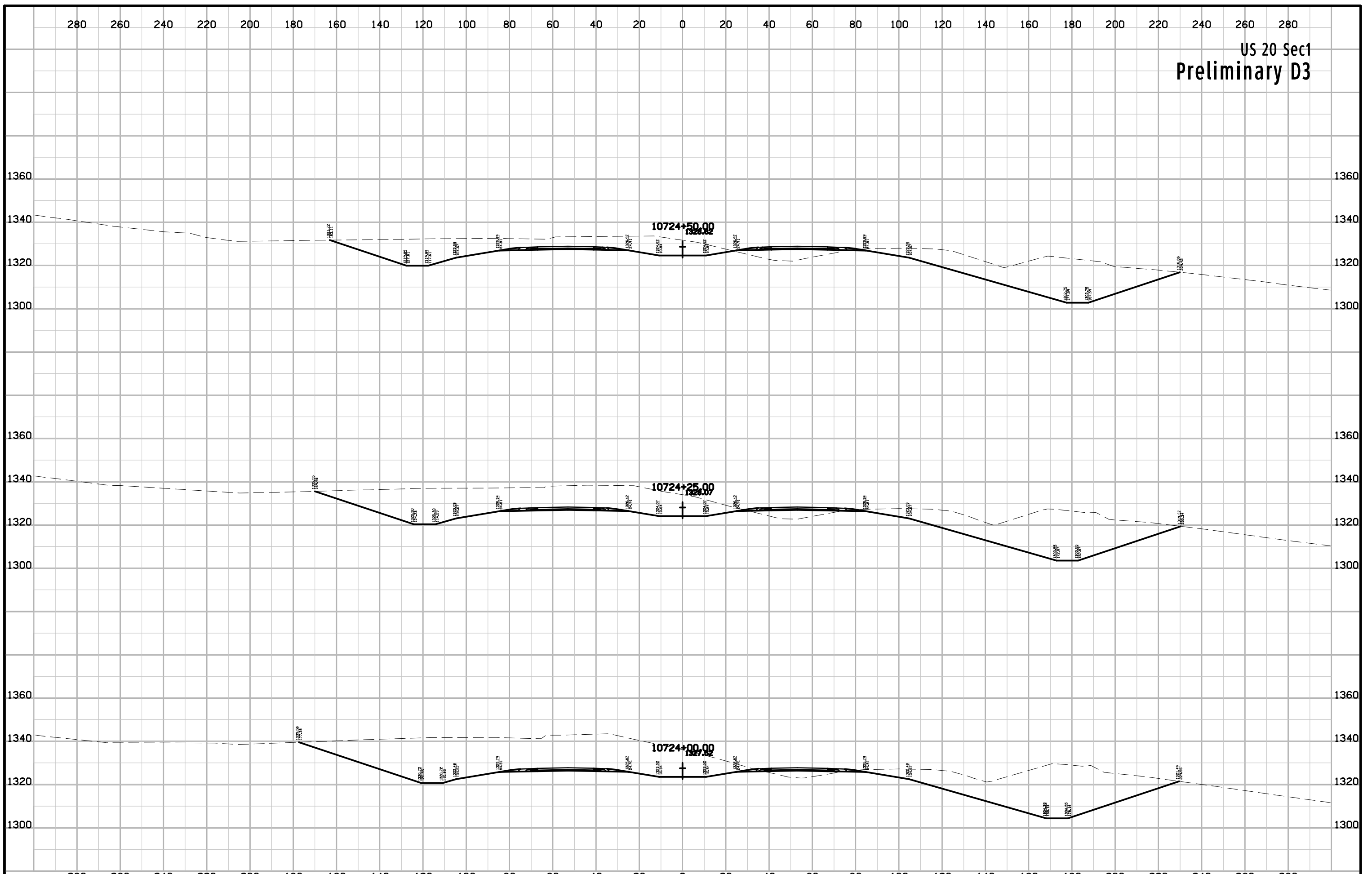
US 20 Sec1
Preliminary D3



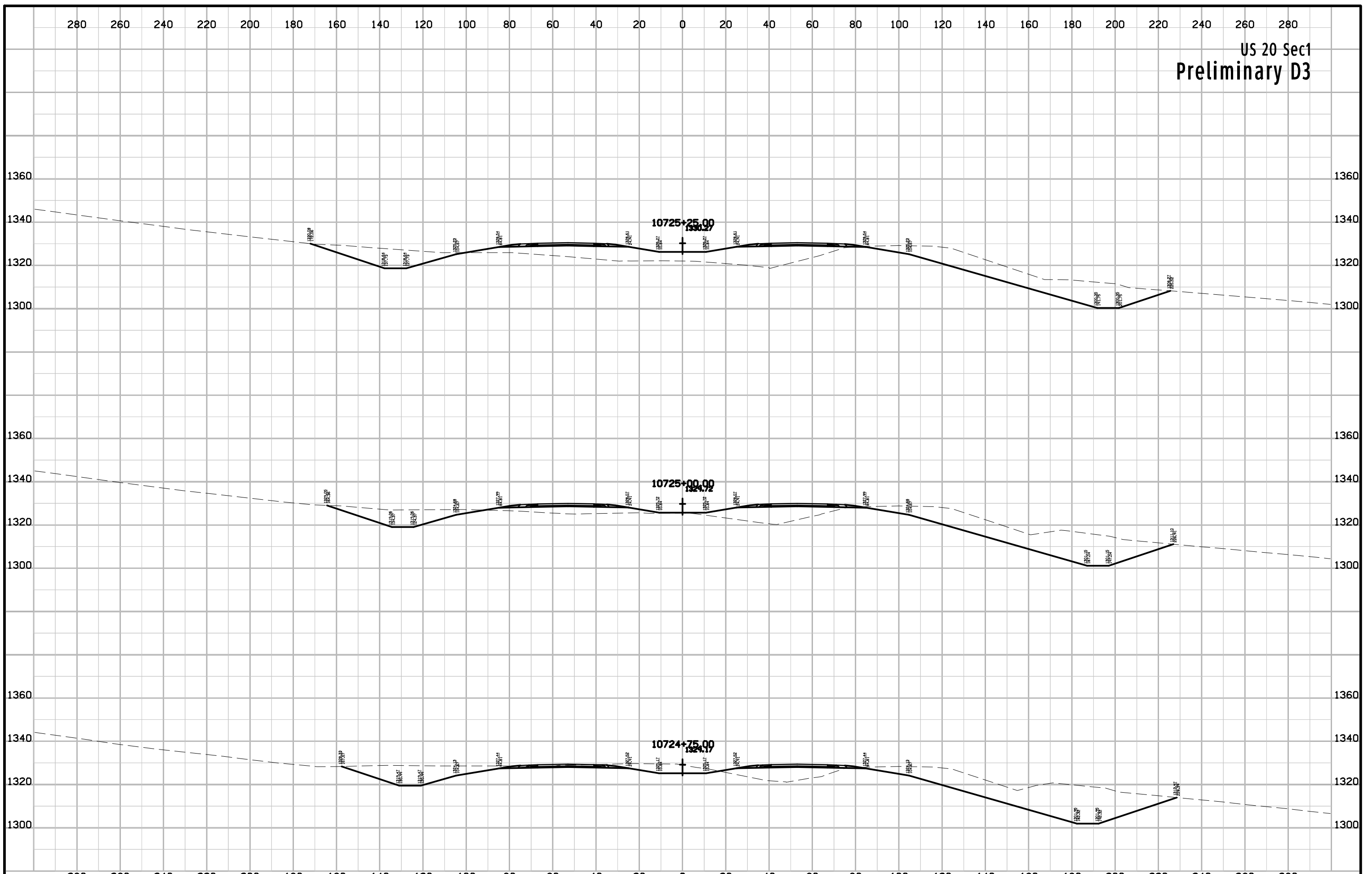
US 20 Sec1
Preliminary D3



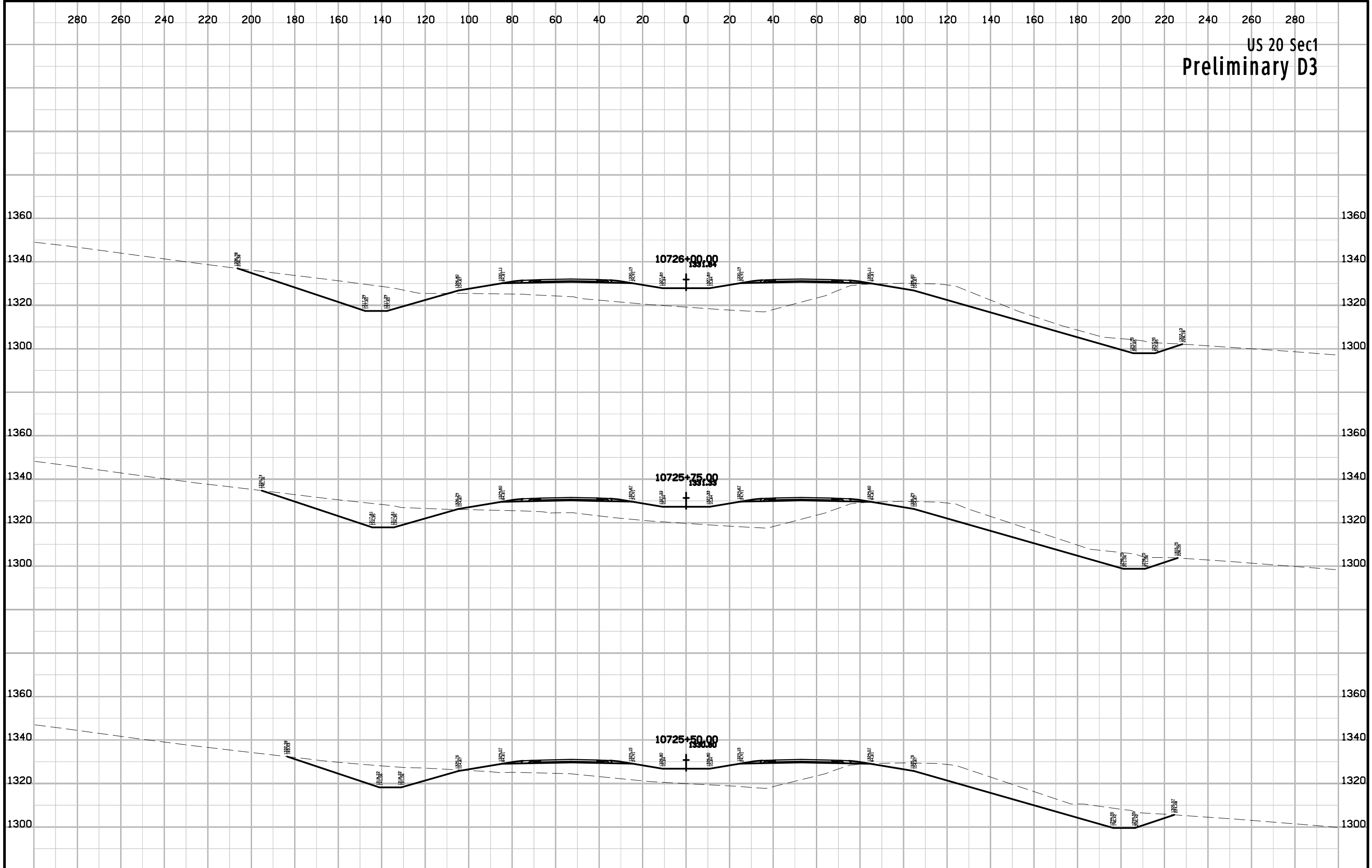
US 20 Sec1
Preliminary D3



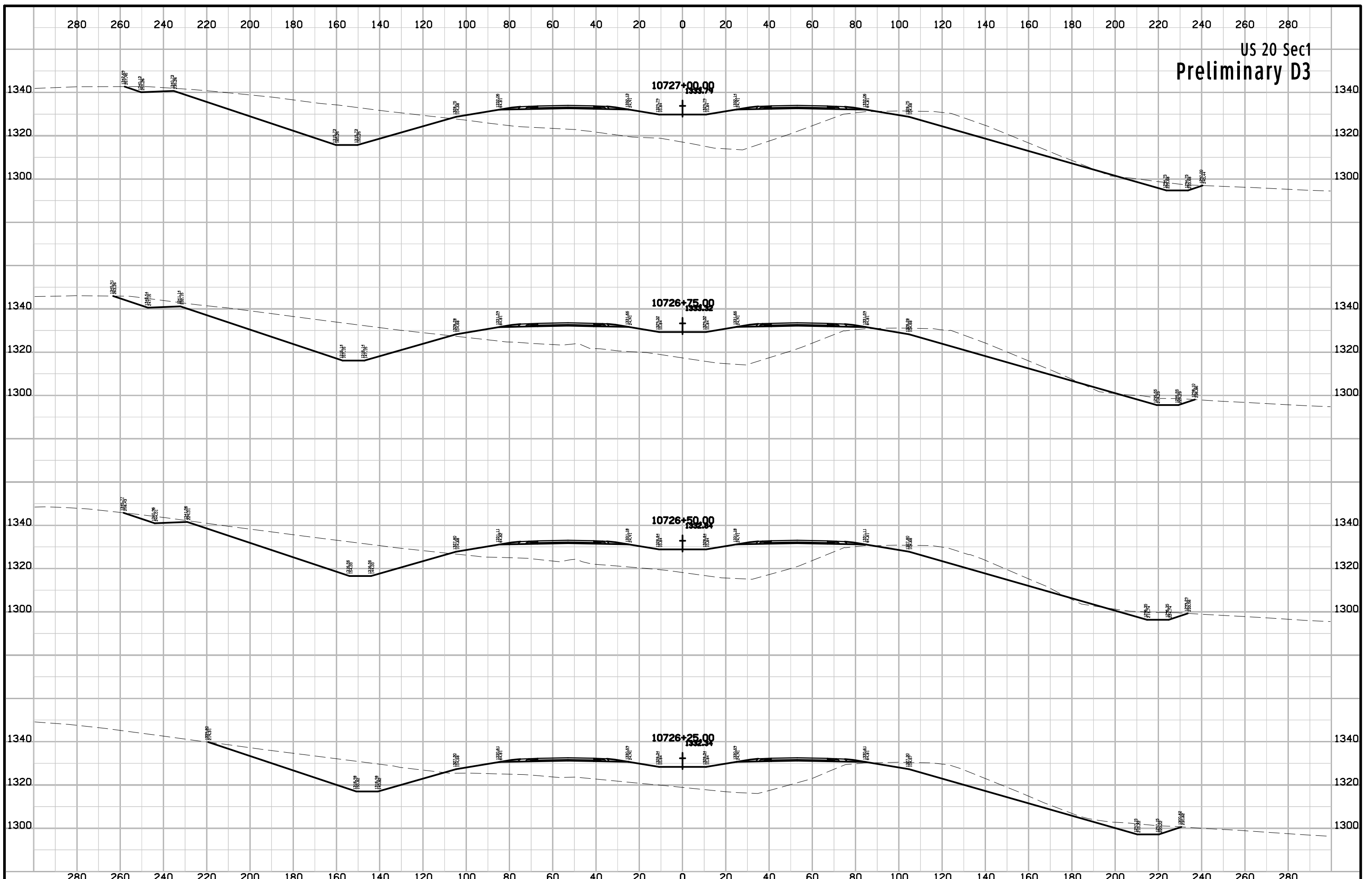
US 20 Sec1
Preliminary D3

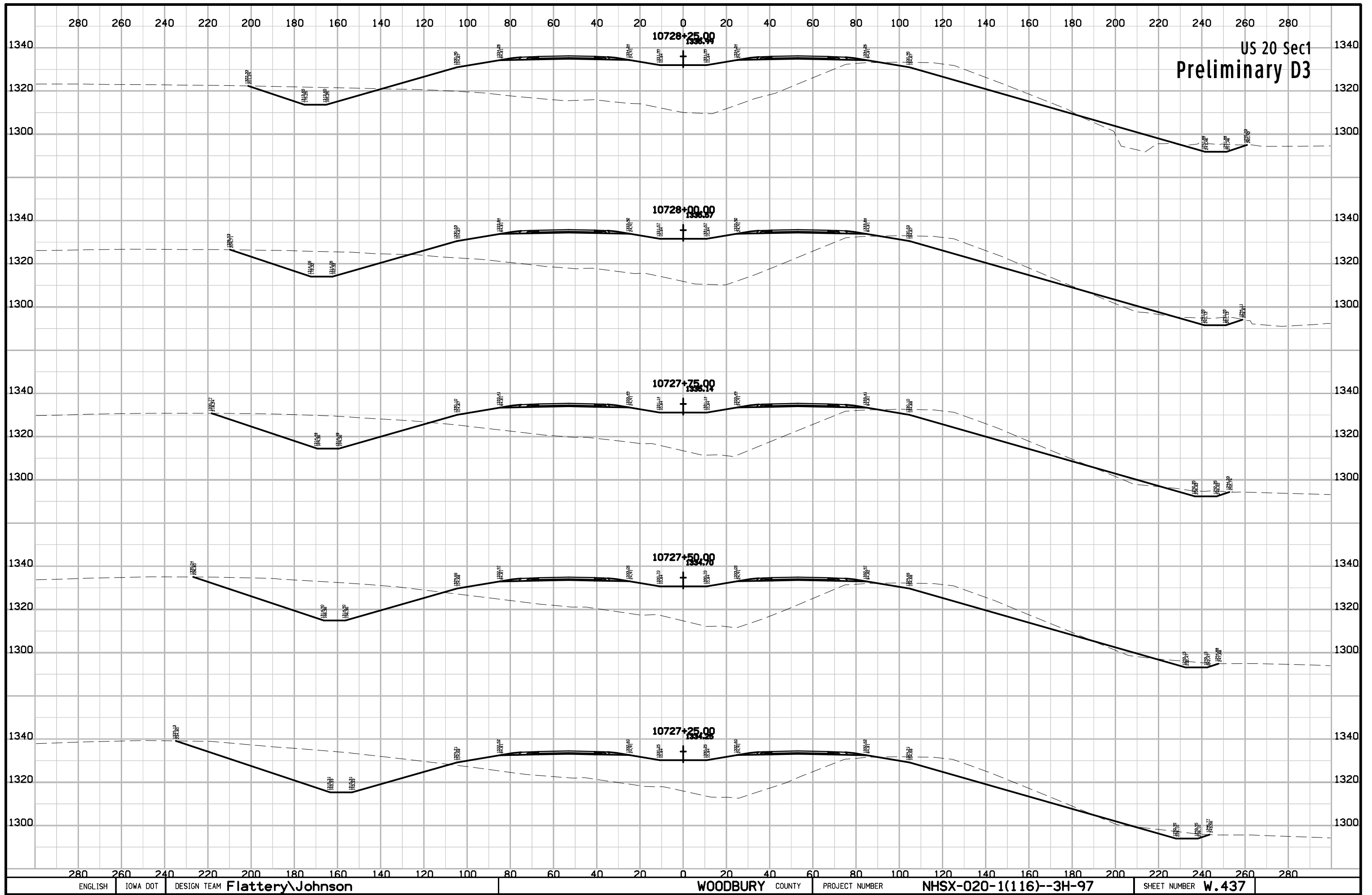


US 20 Sec1
Preliminary D3



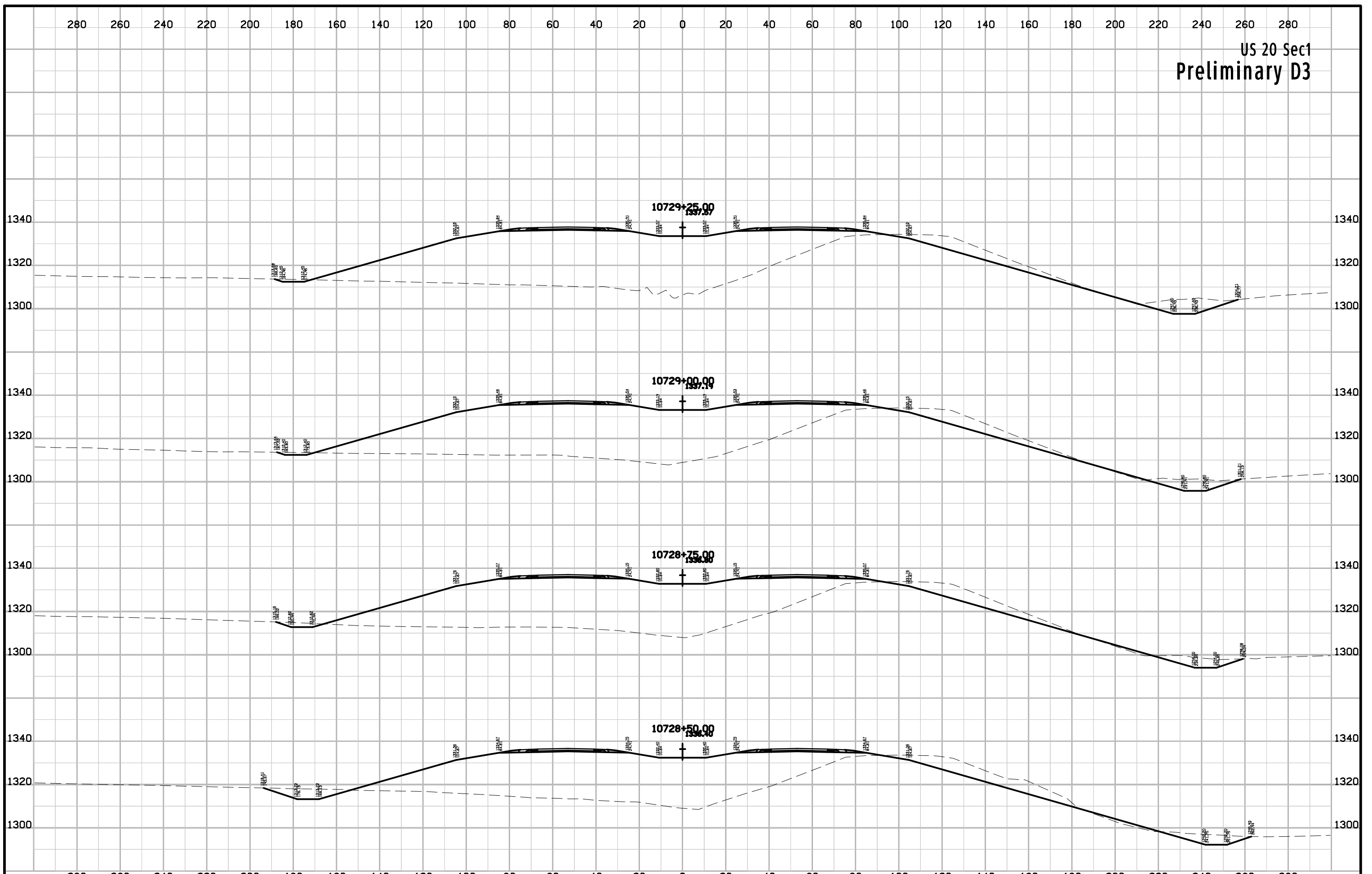
US 20 Sec1
Preliminary D3



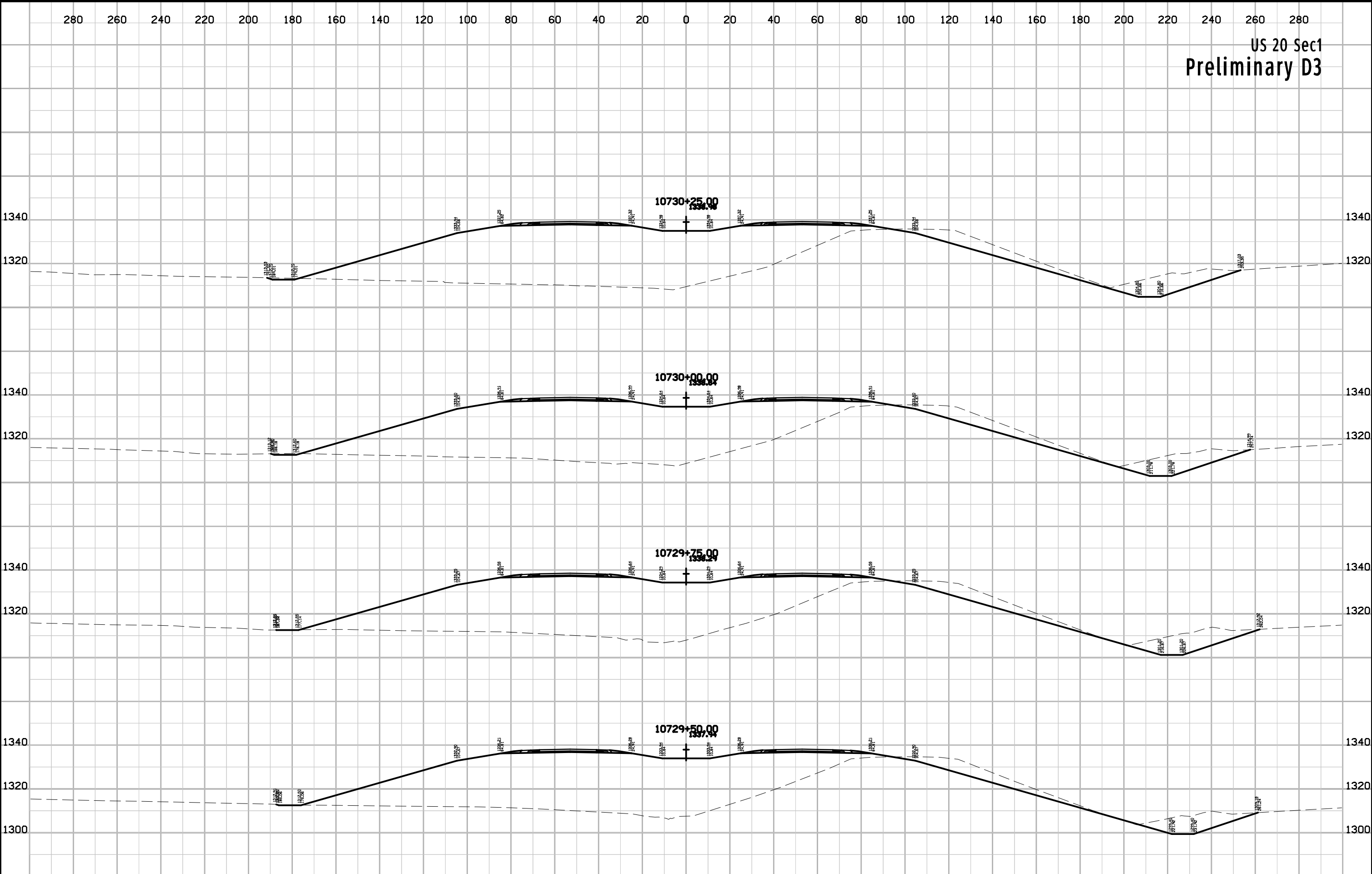


US 20 Sec1
Preliminary D3

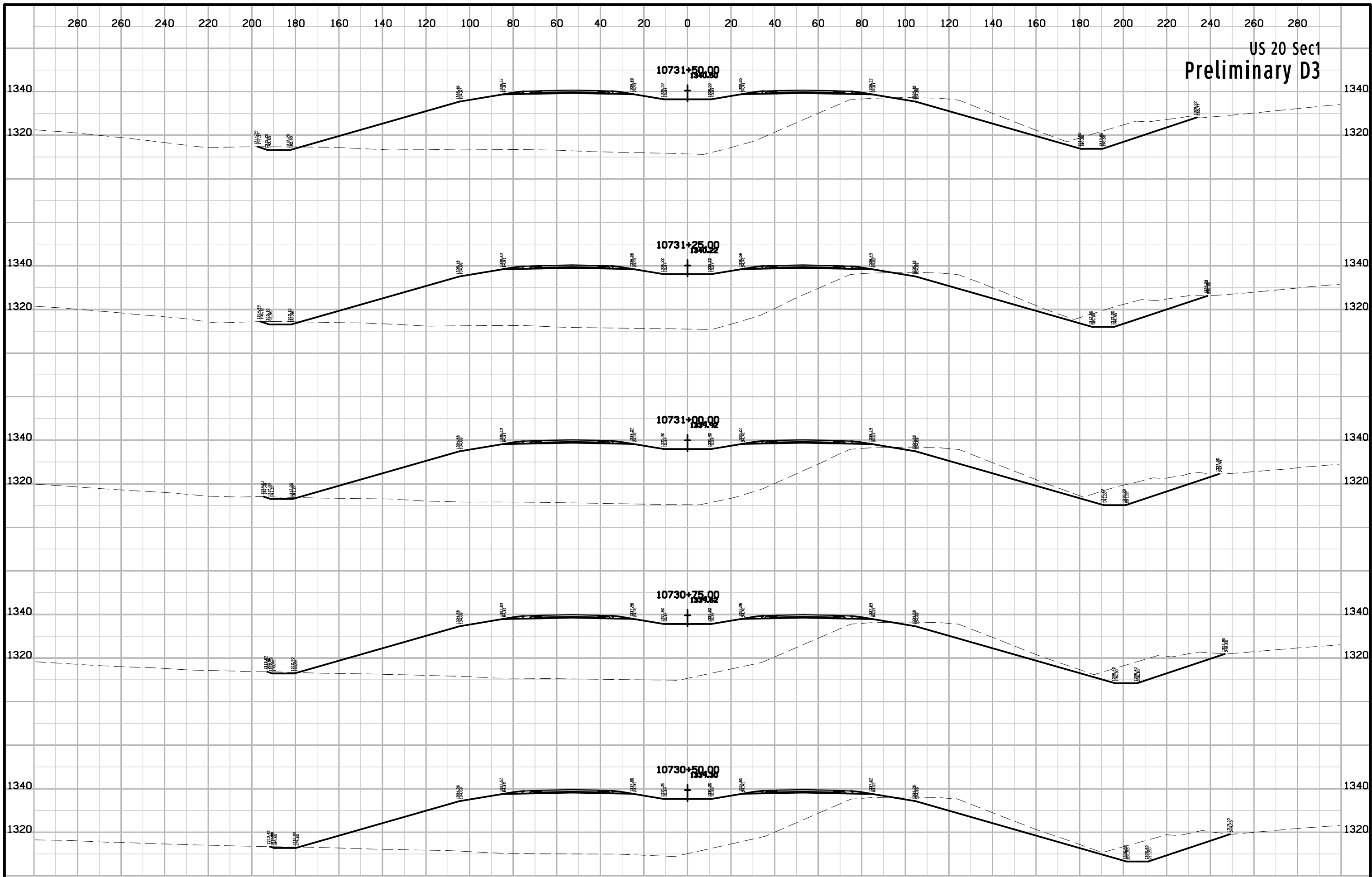
US 20 Sec1
Preliminary D3



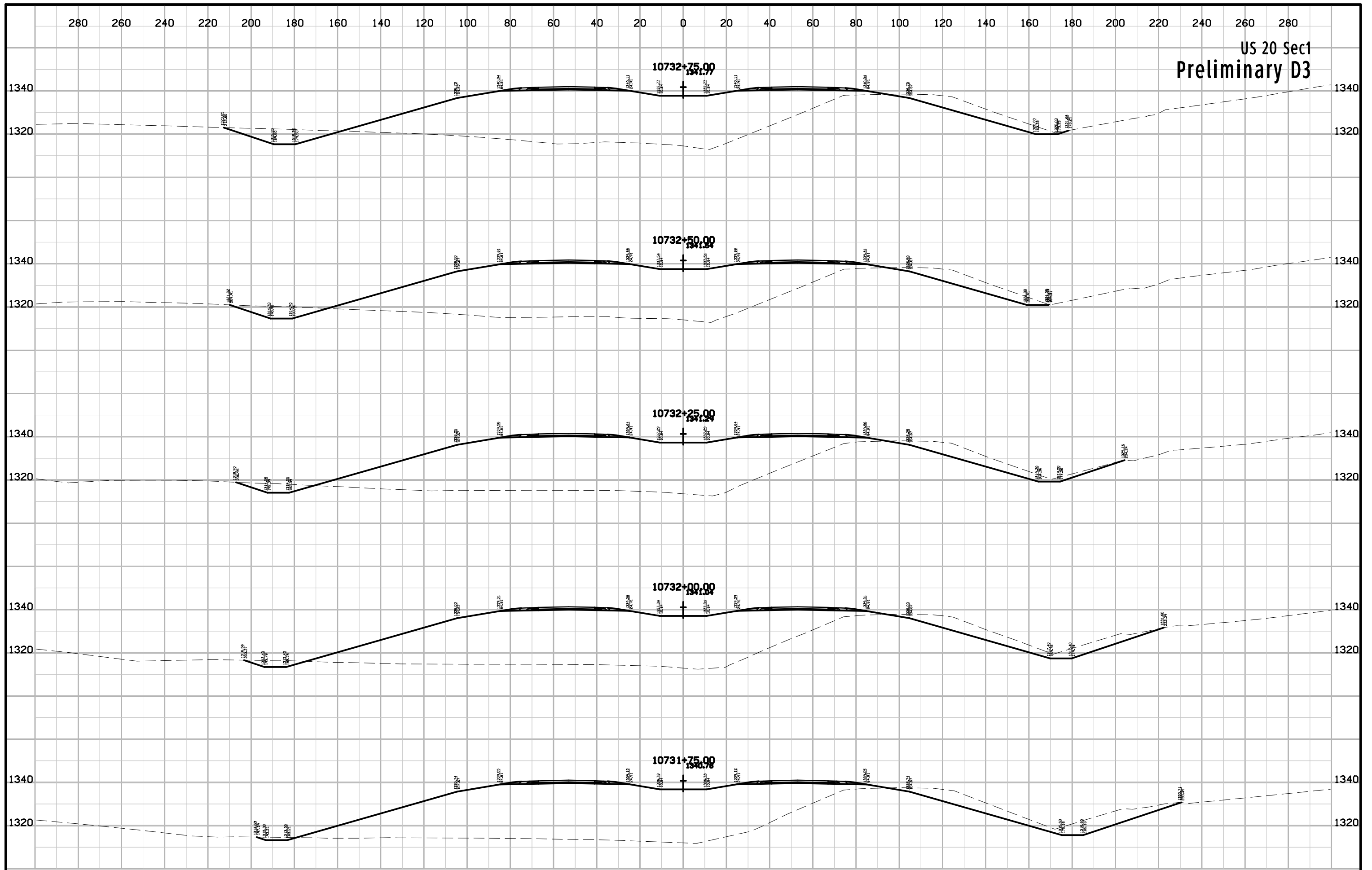
US 20 Sec1
Preliminary D3



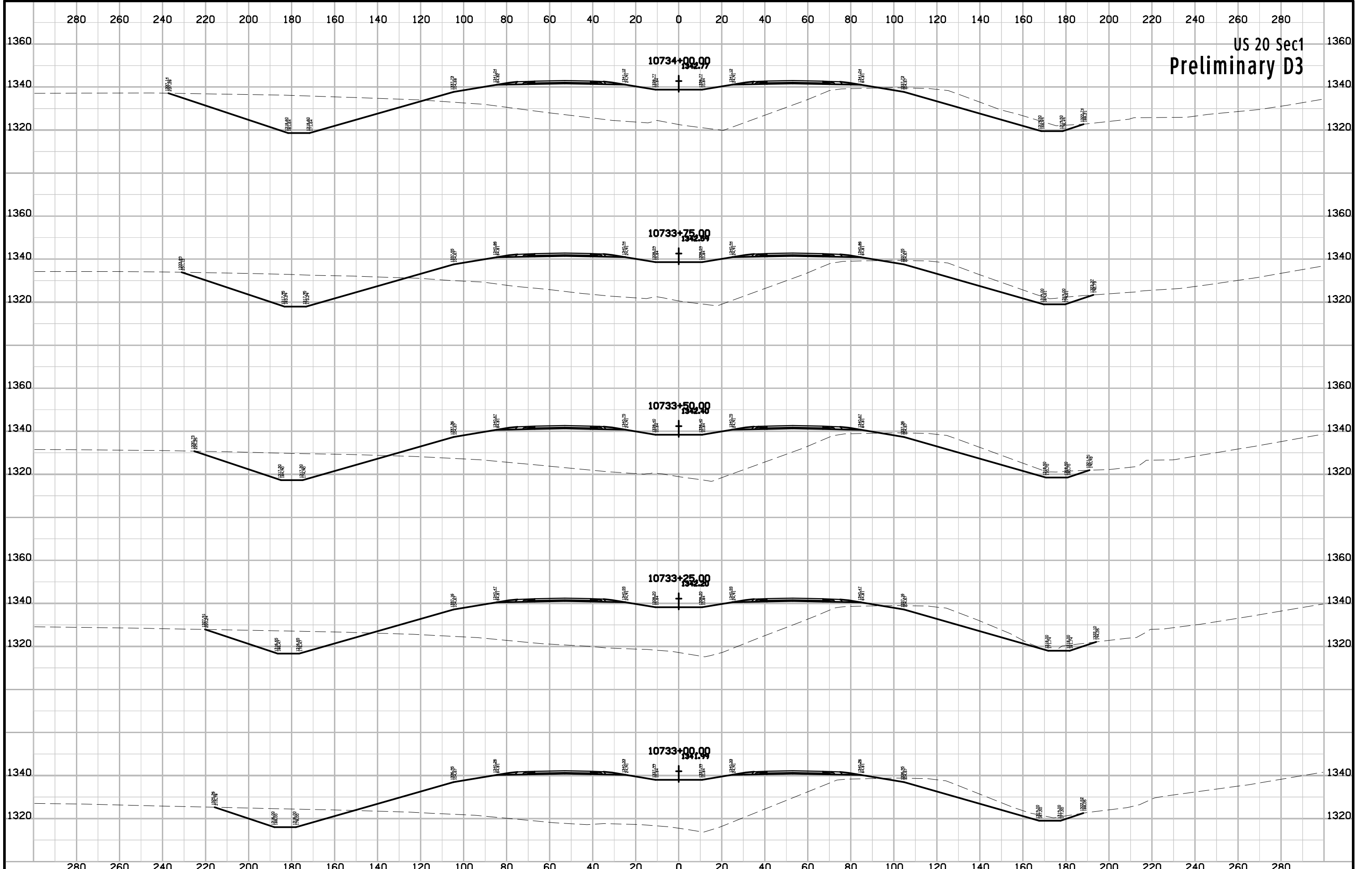
US 20 Sec1
Preliminary D3



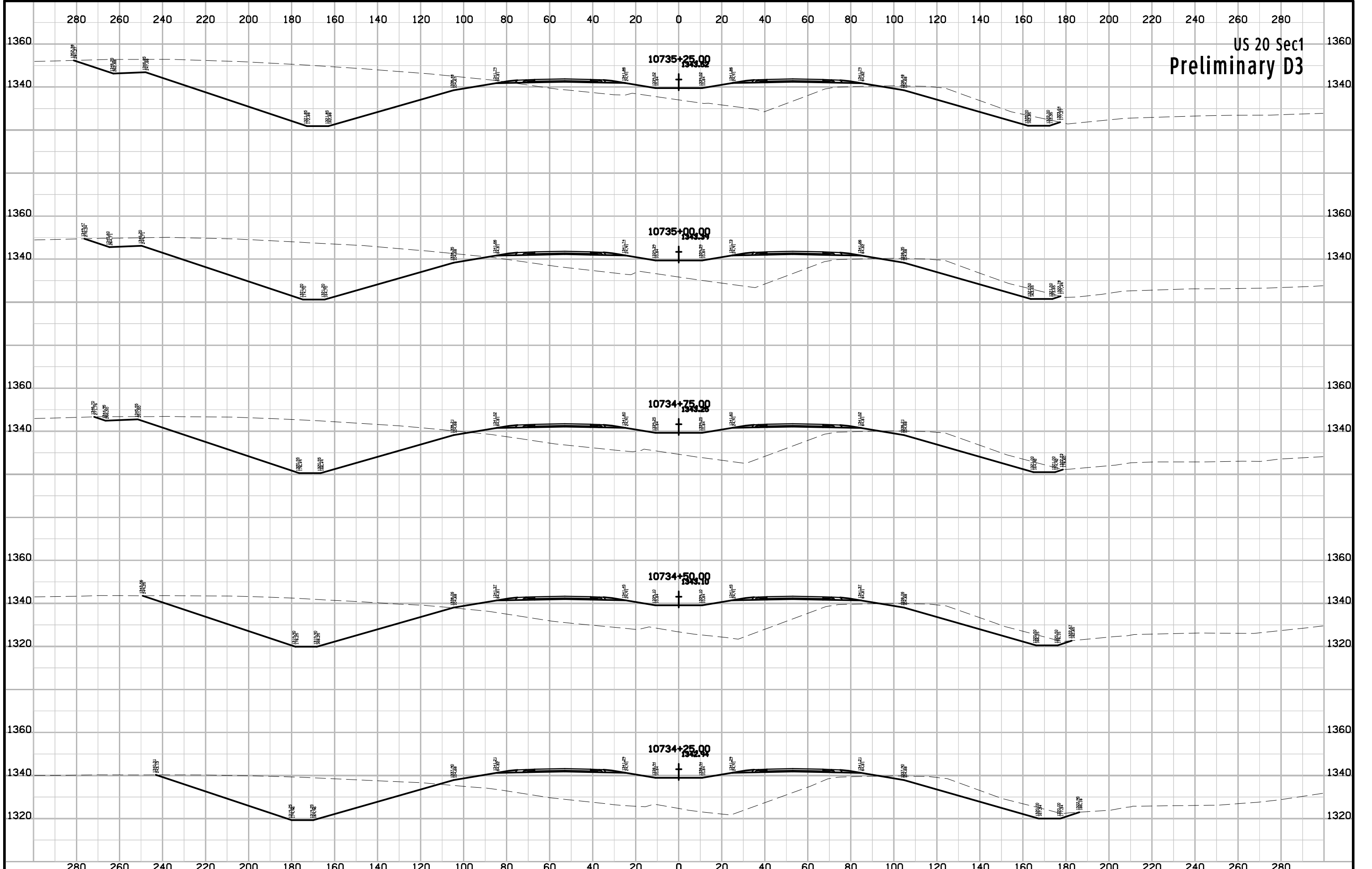
US 20 Sec1
Preliminary D3



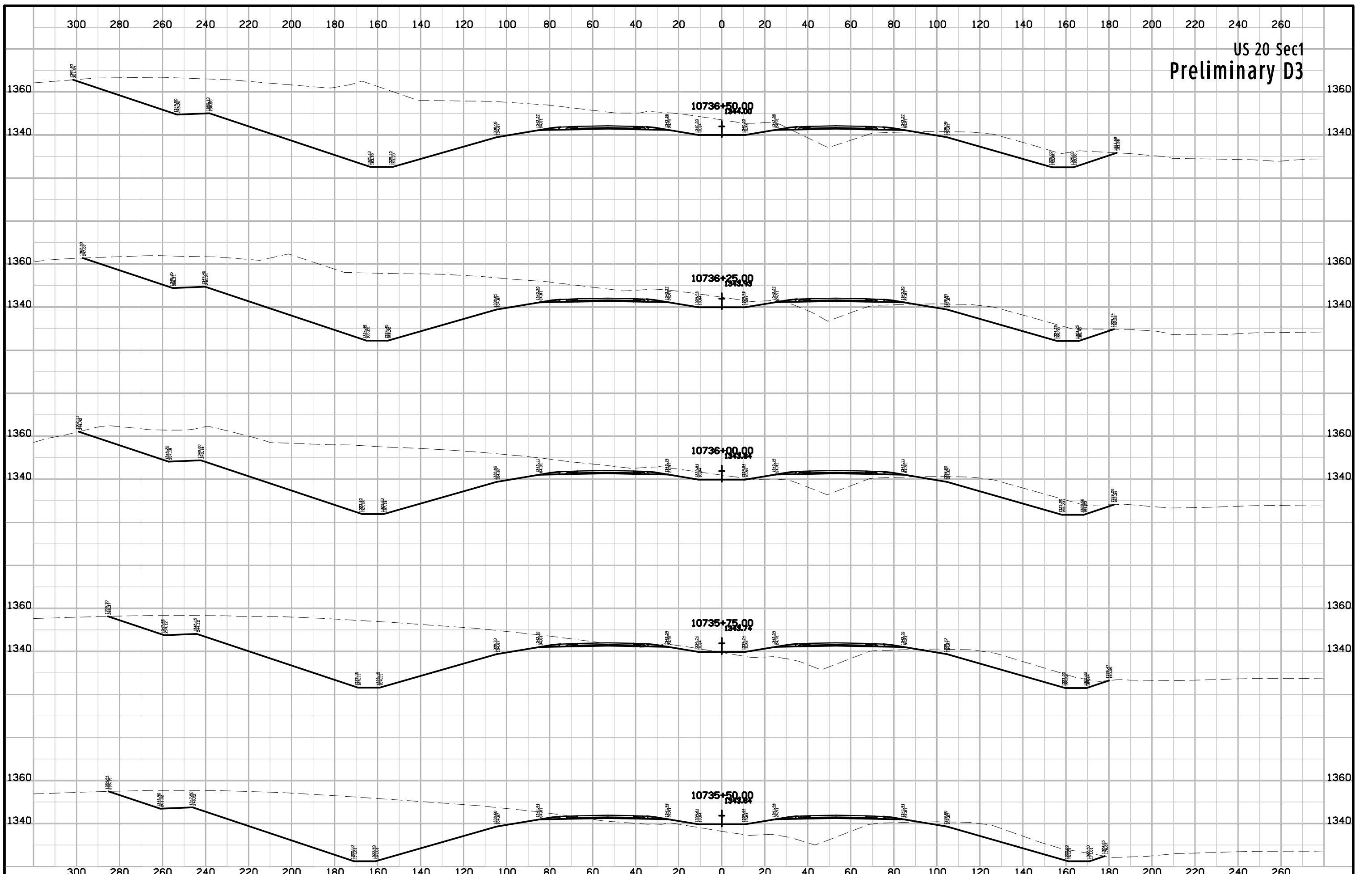
US 20 Sec1
Preliminary D3



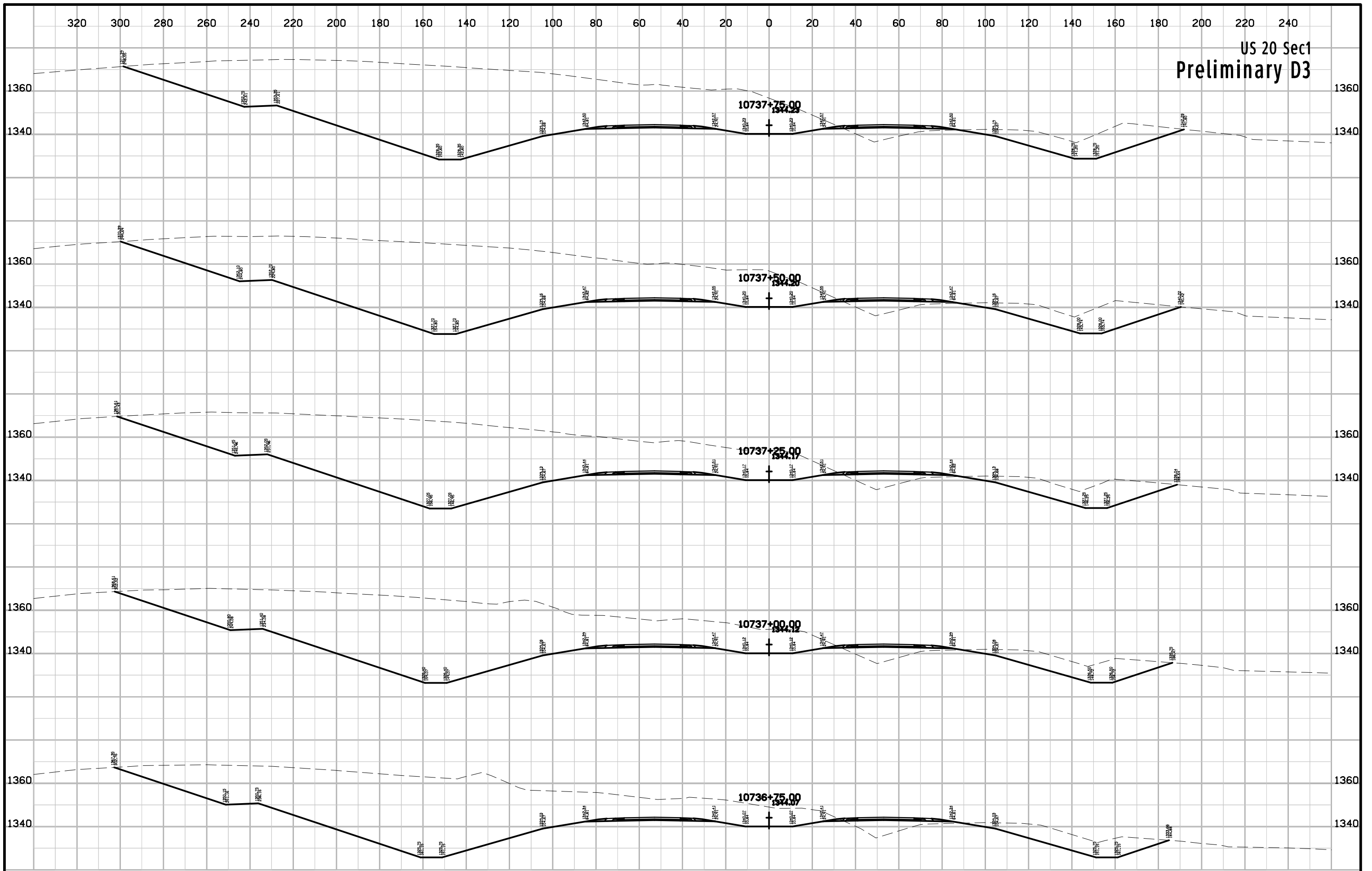
US 20 Sec1
Preliminary D3



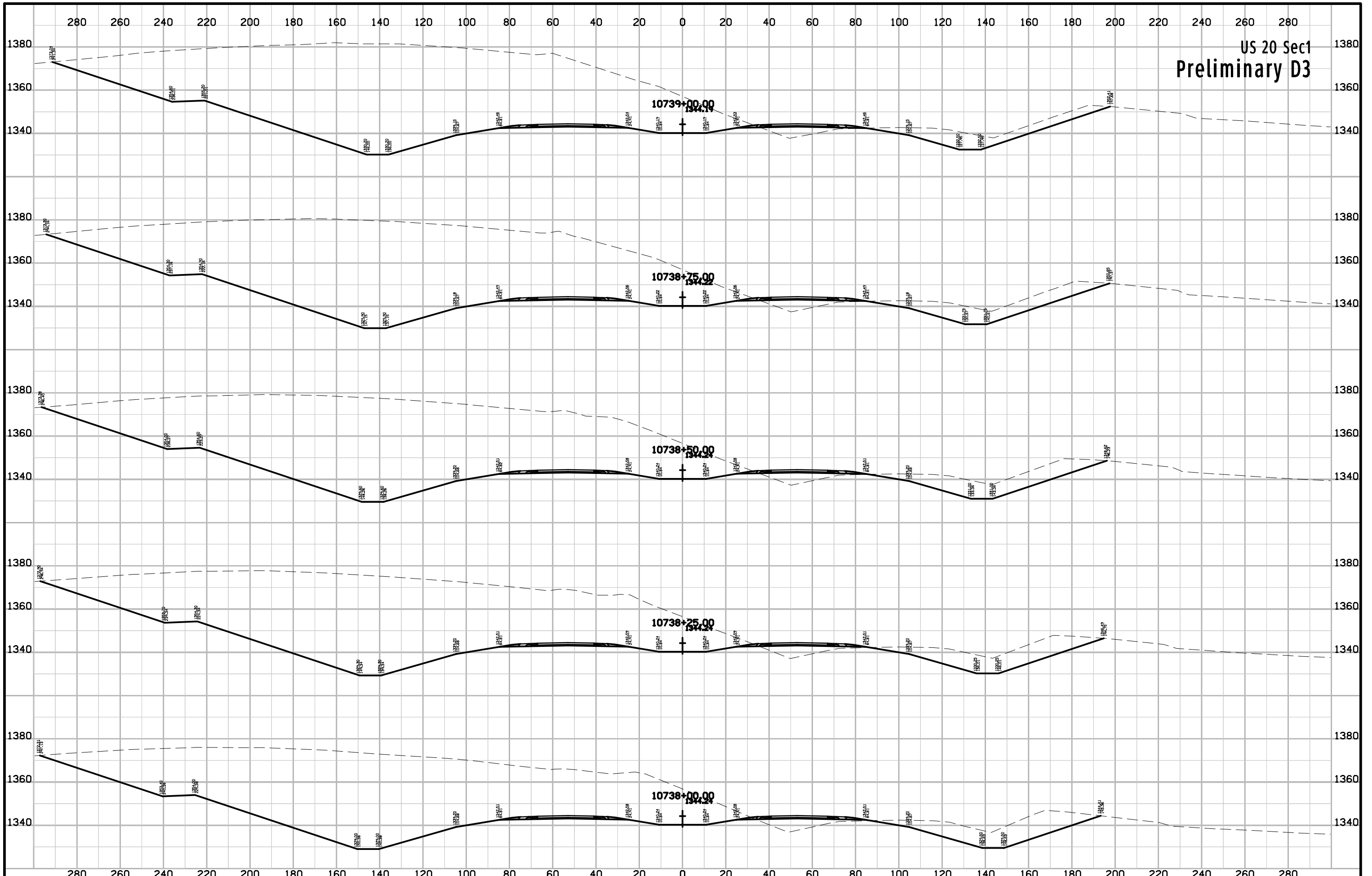
US 20 Sec1
Preliminary D3

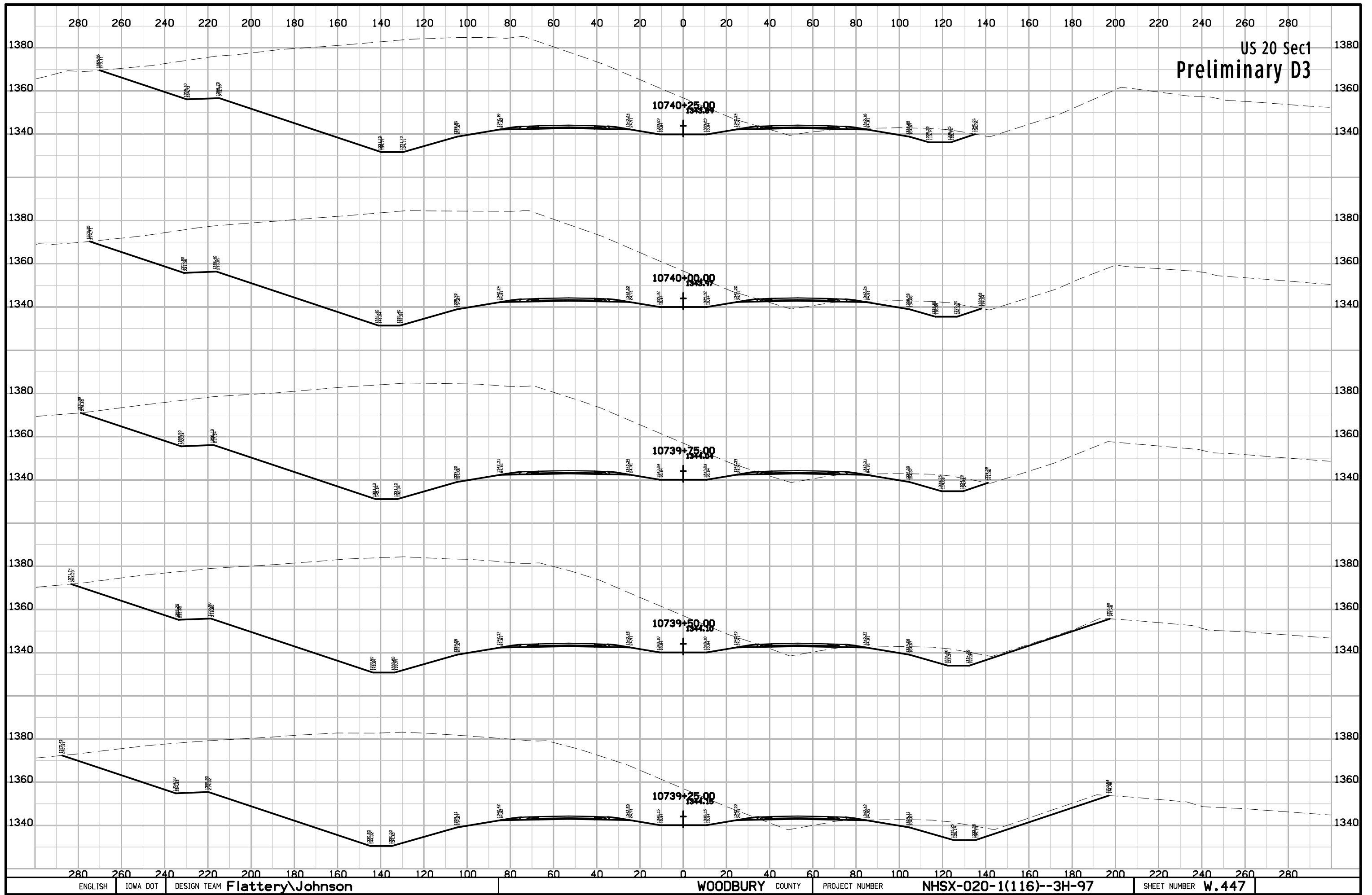


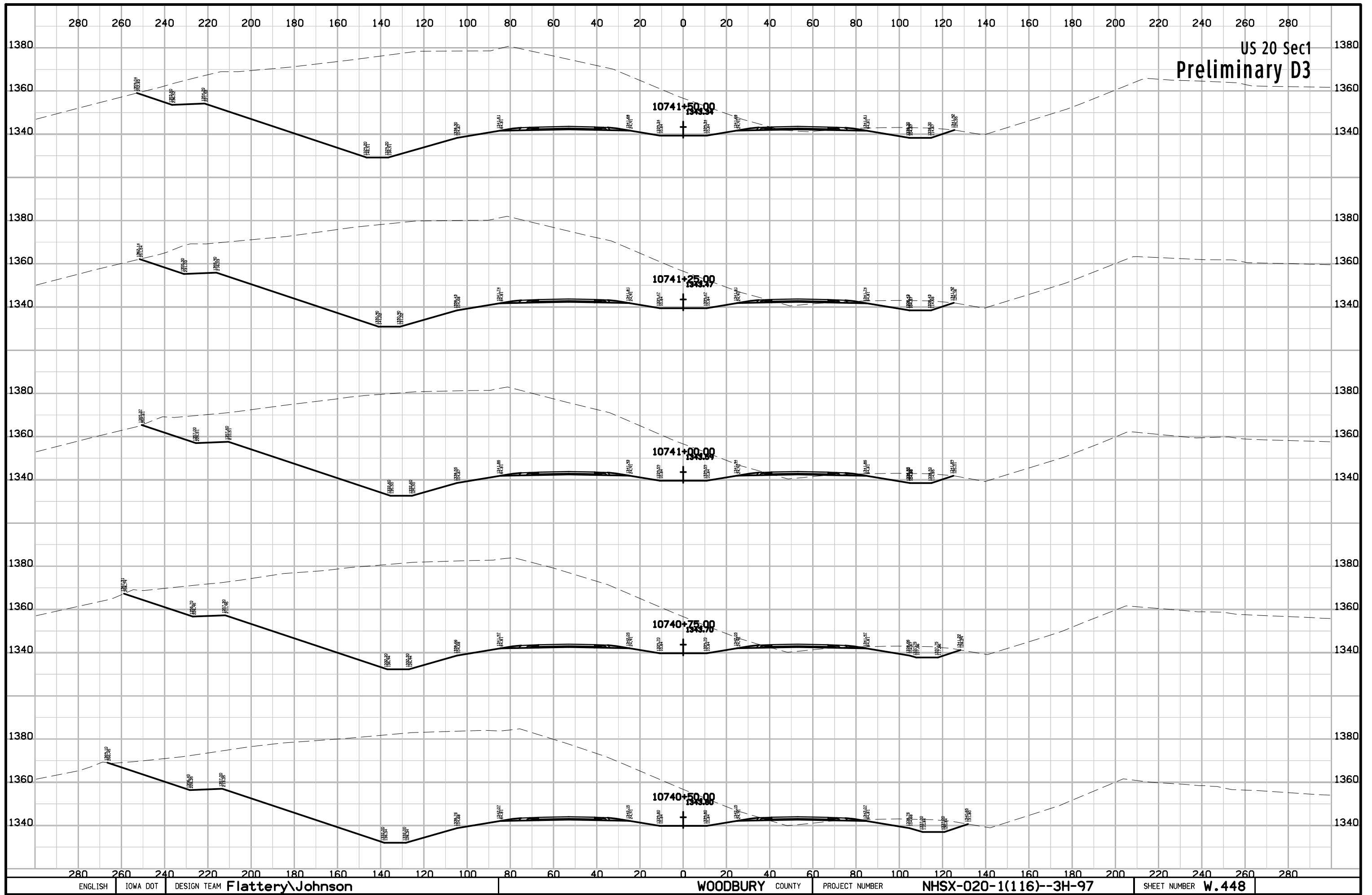
US 20 Sec1
Preliminary D3



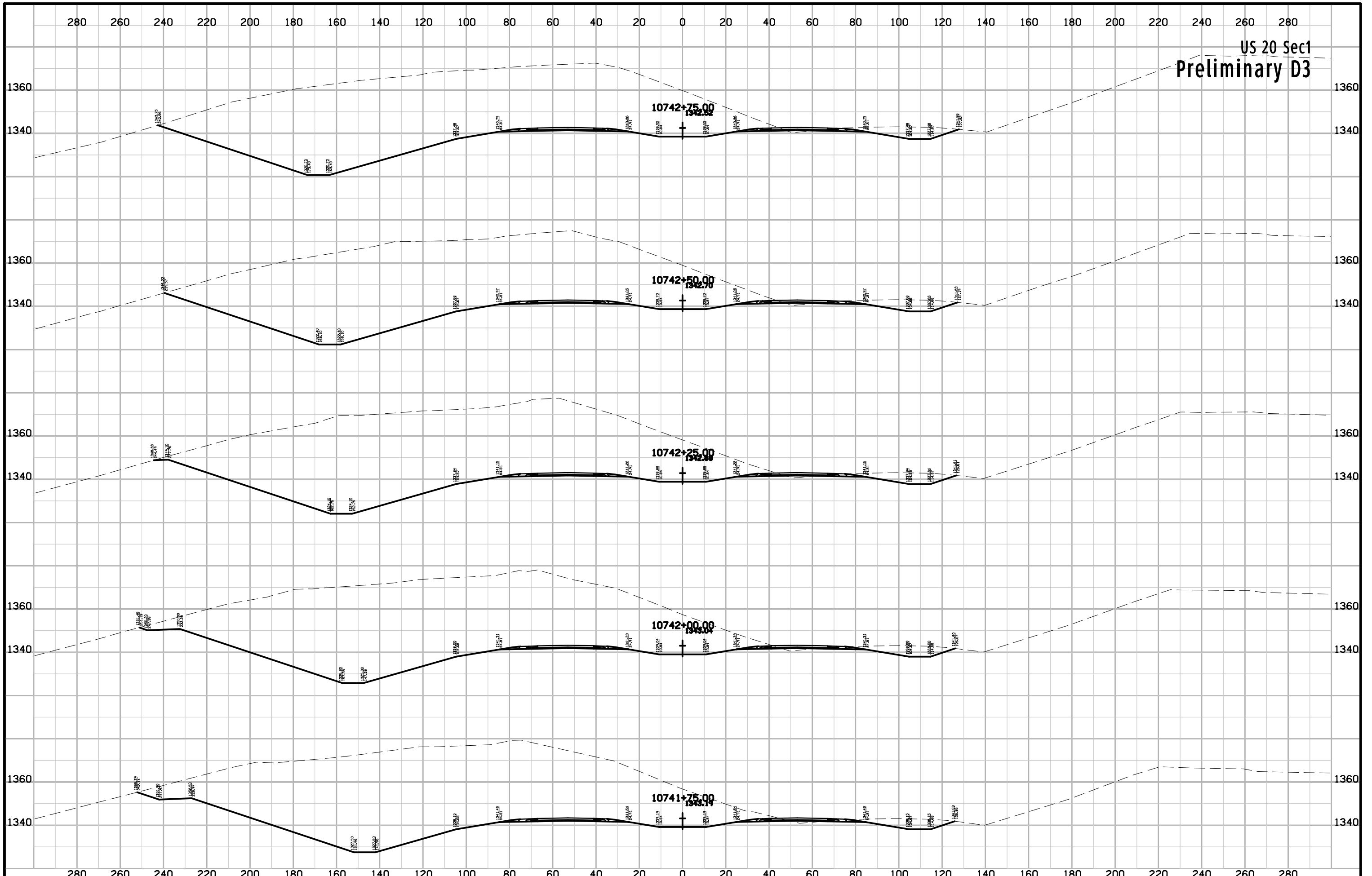
US 20 Sec1
Preliminary D3



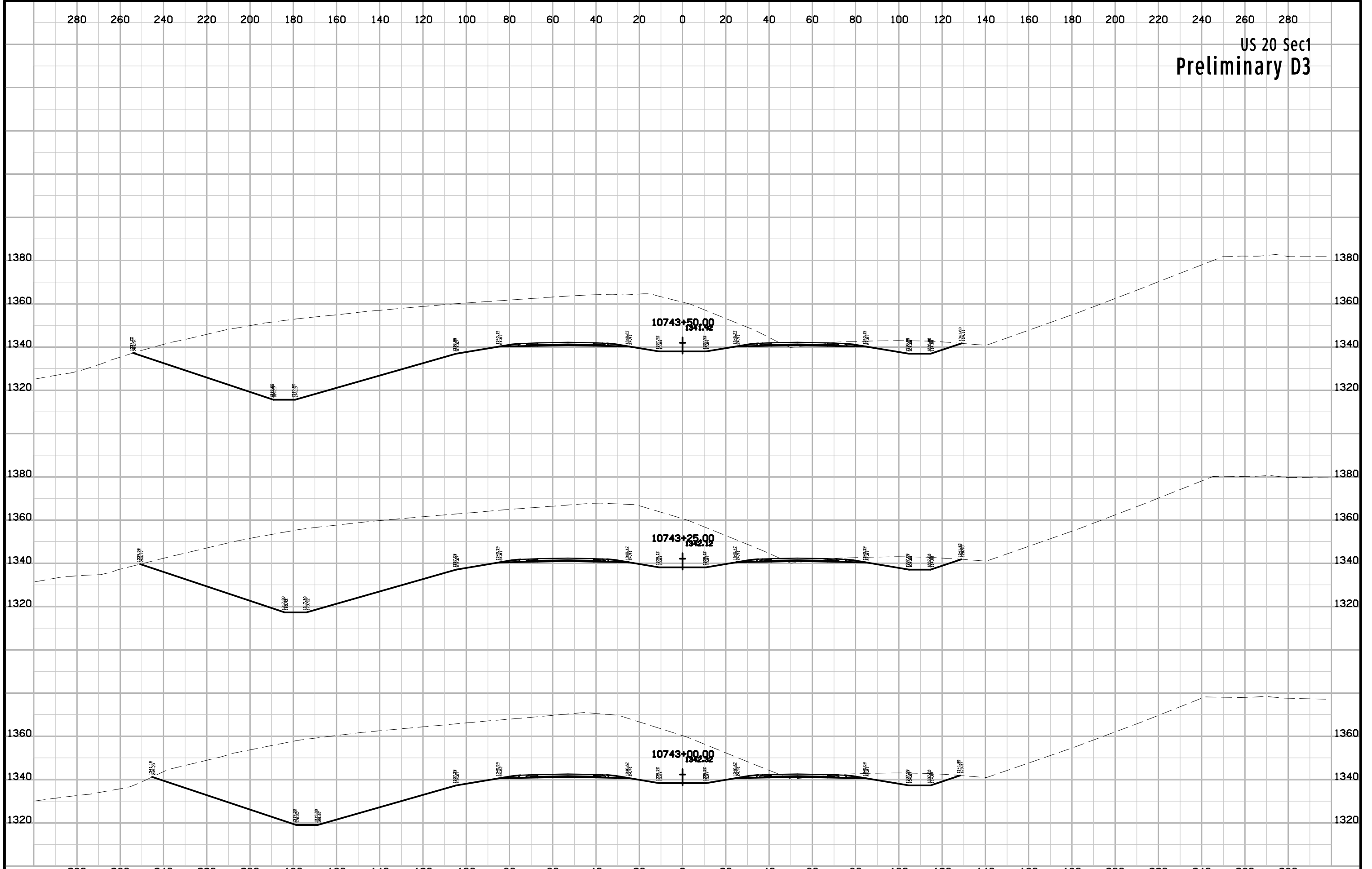




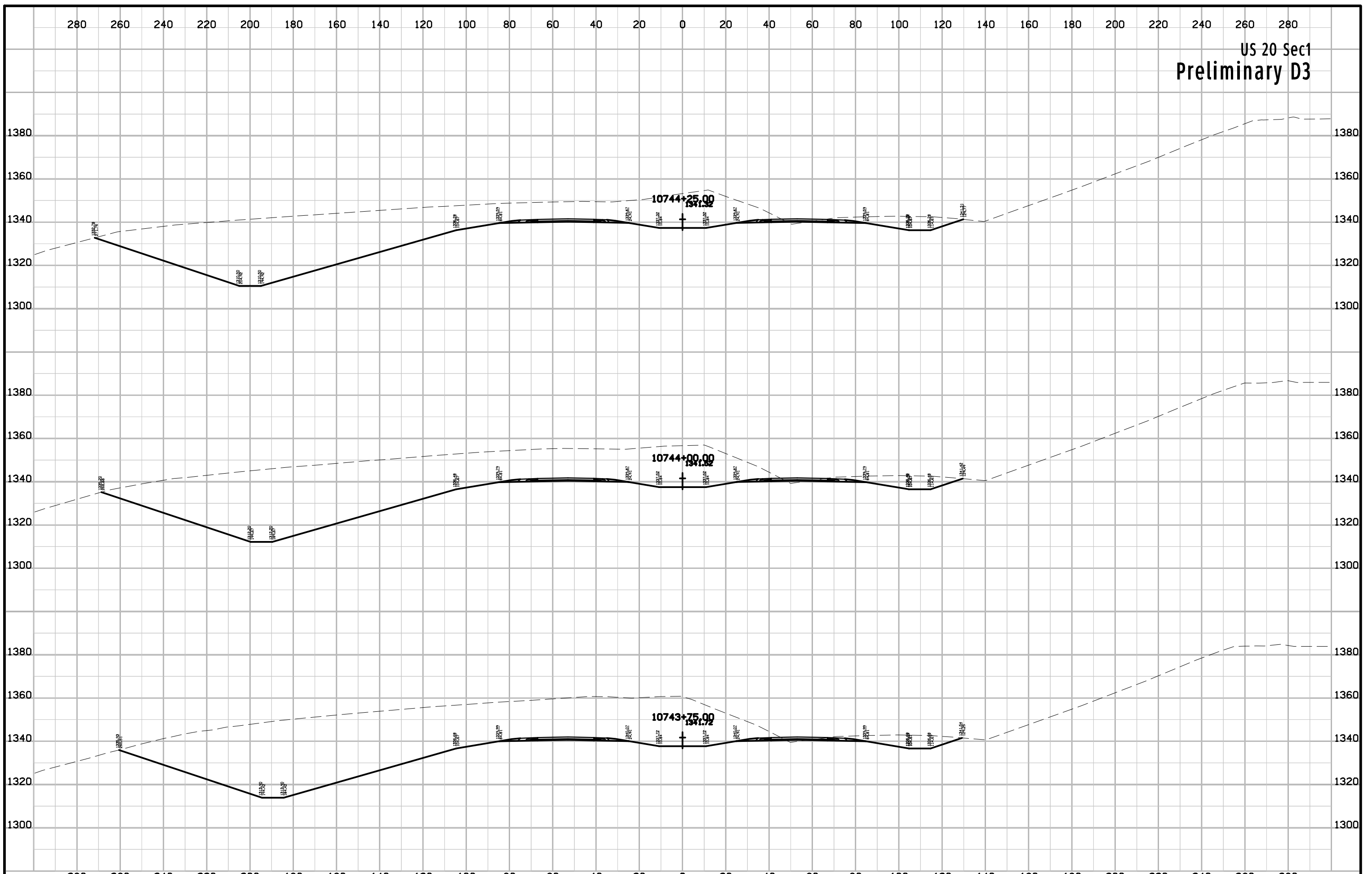
US 20 Sec1
Preliminary D3



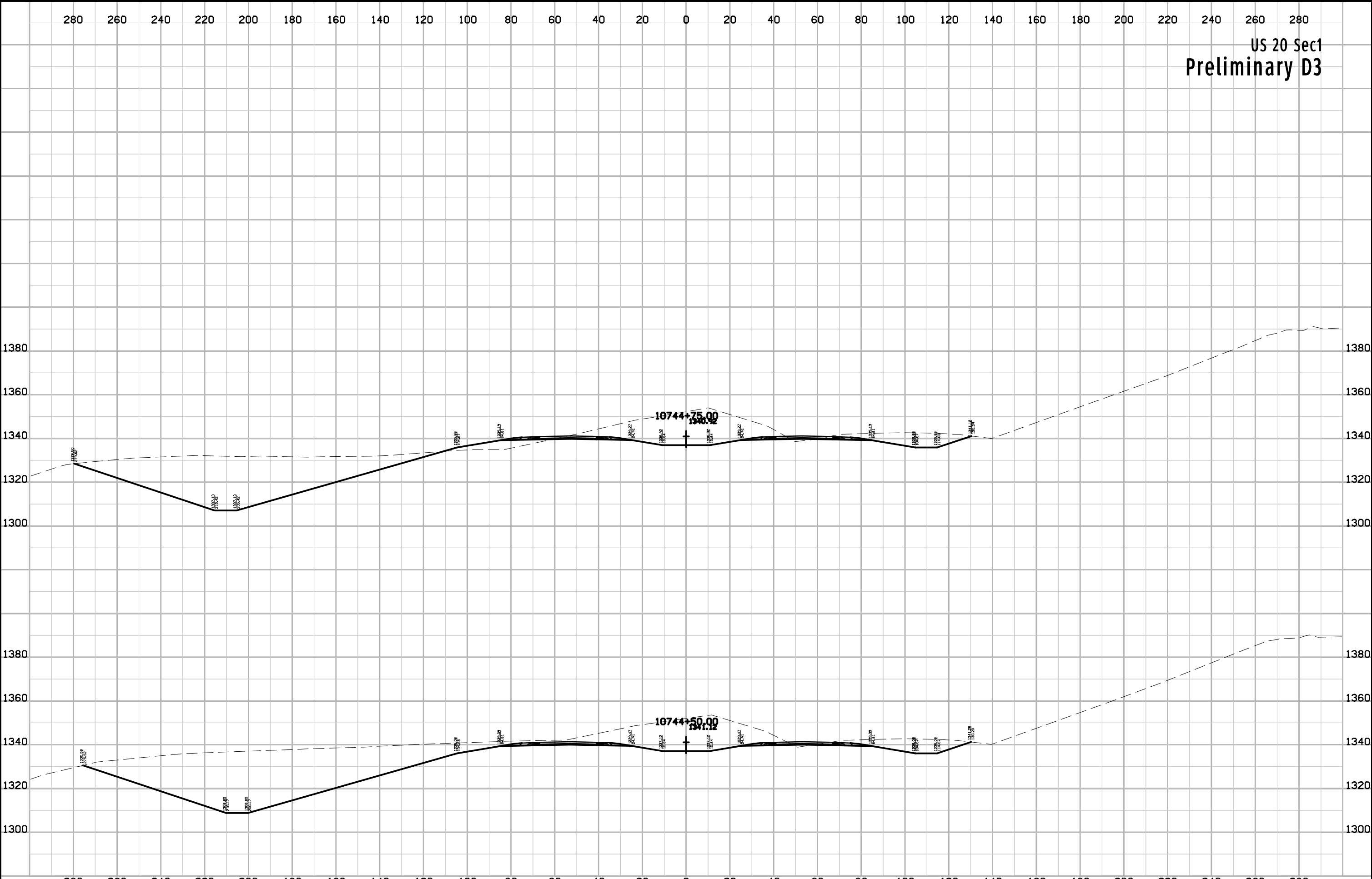
US 20 Sec1
Preliminary D3



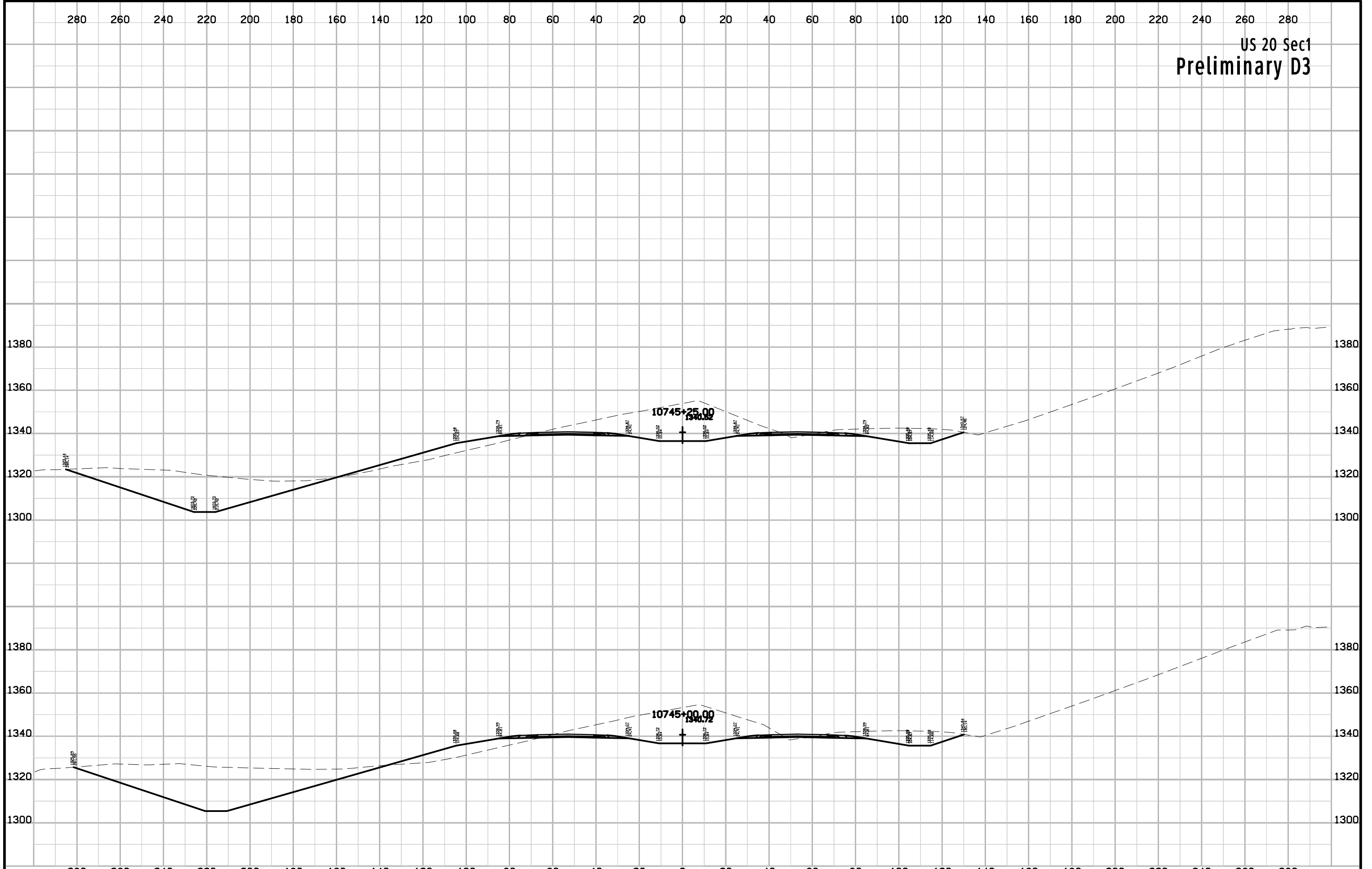
US 20 Sec1
Preliminary D3



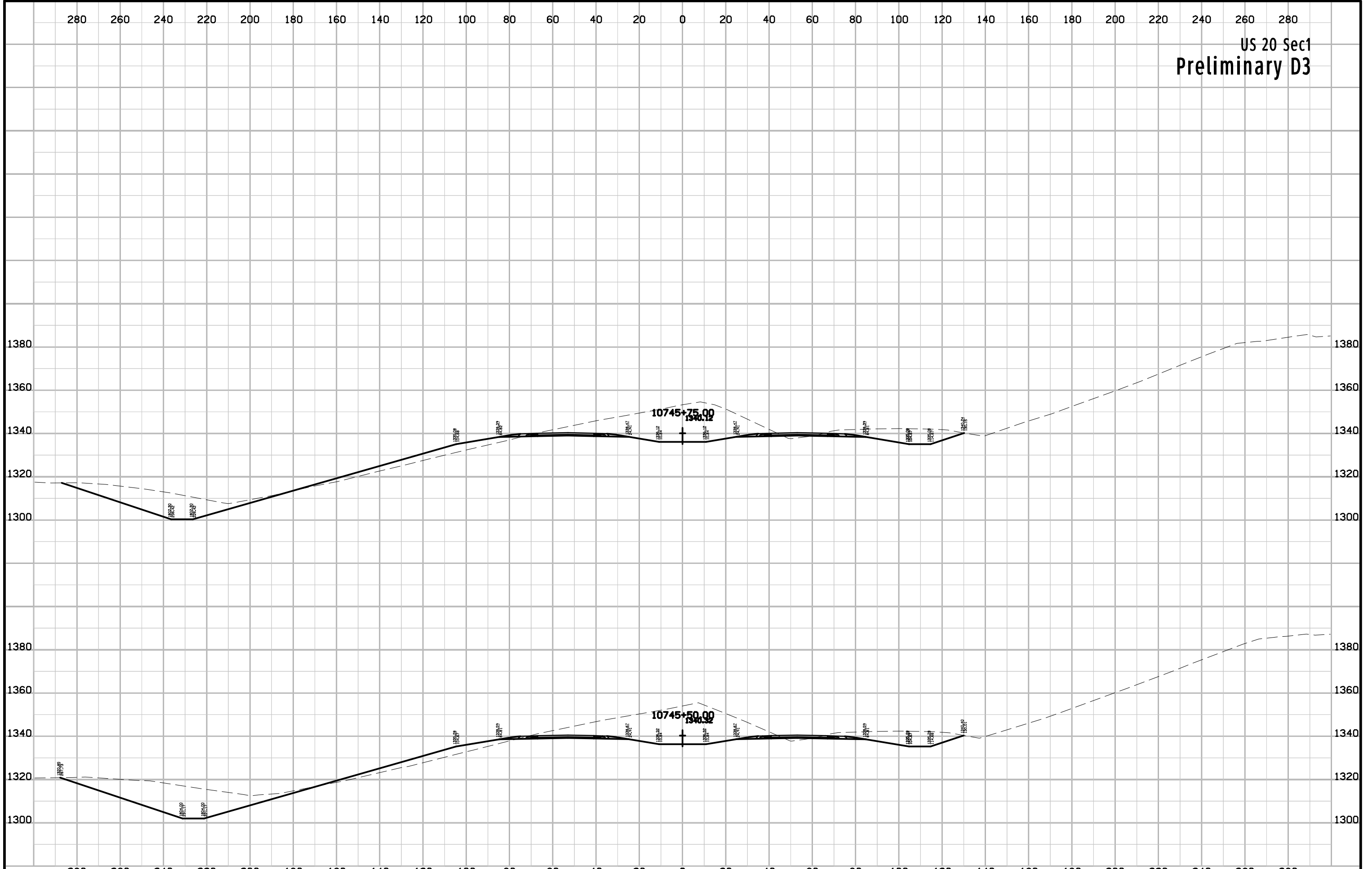
US 20 Sec1
Preliminary D3



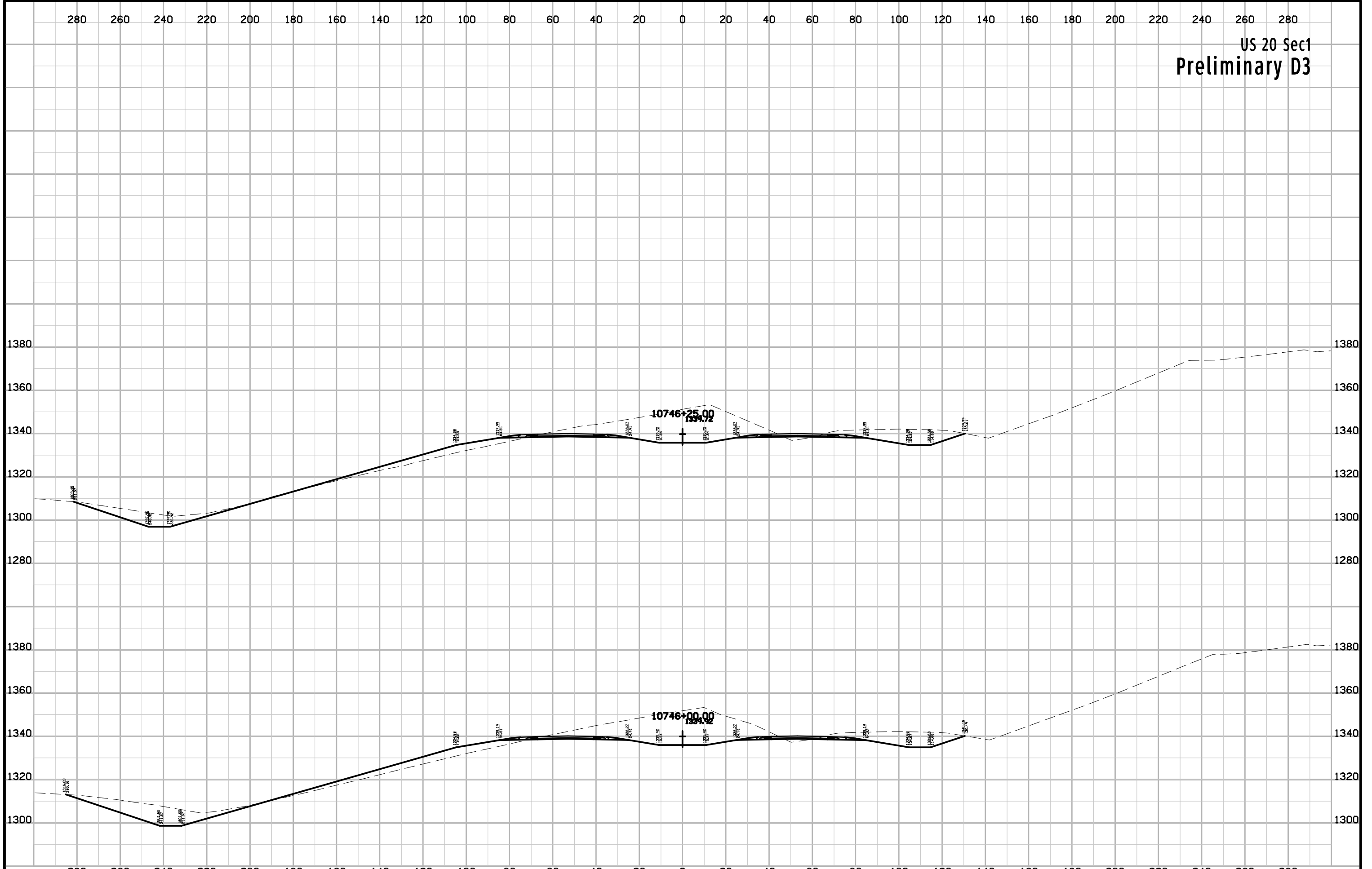
US 20 Sec1
Preliminary D3



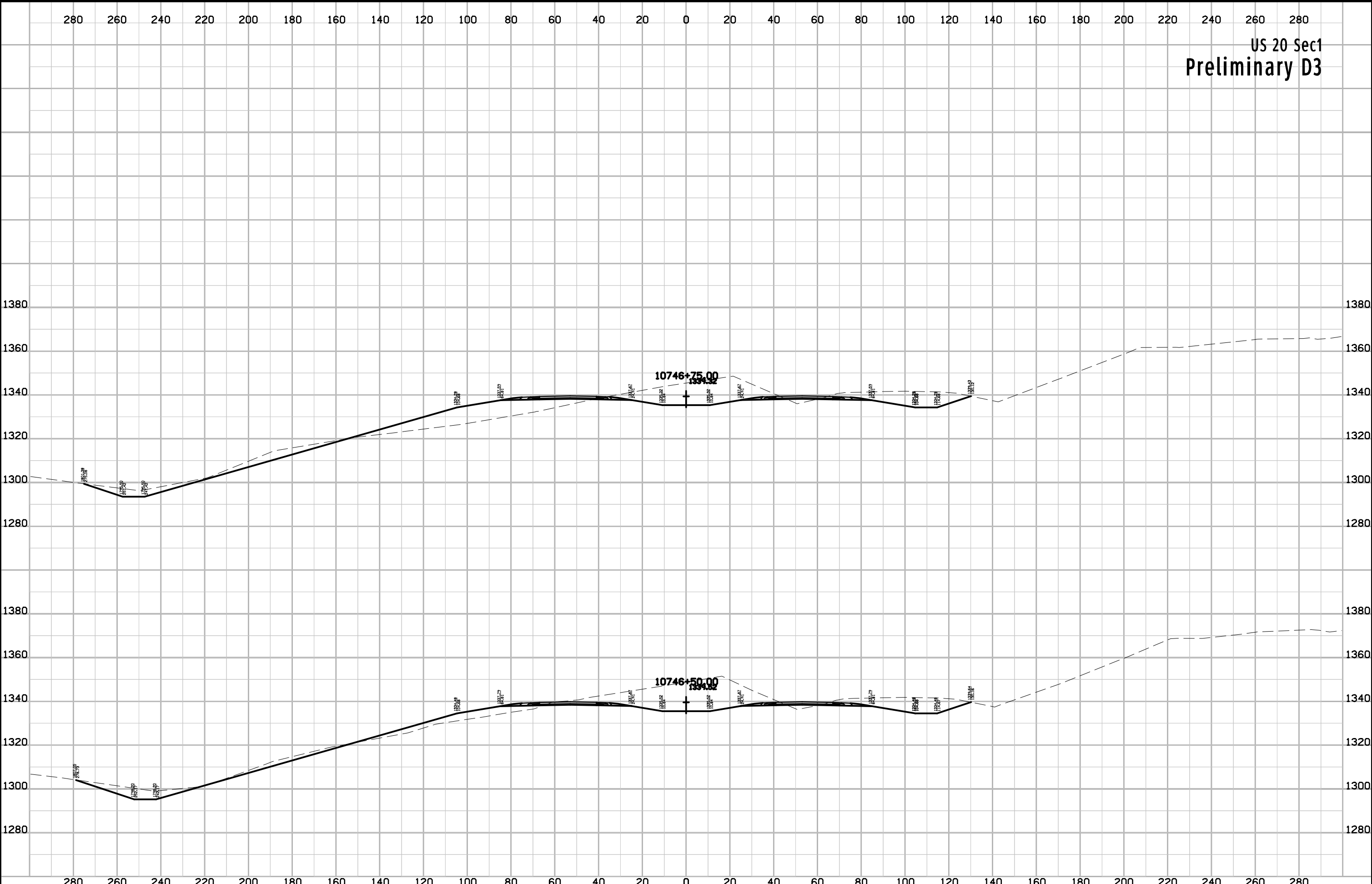
US 20 Sec1
Preliminary D3



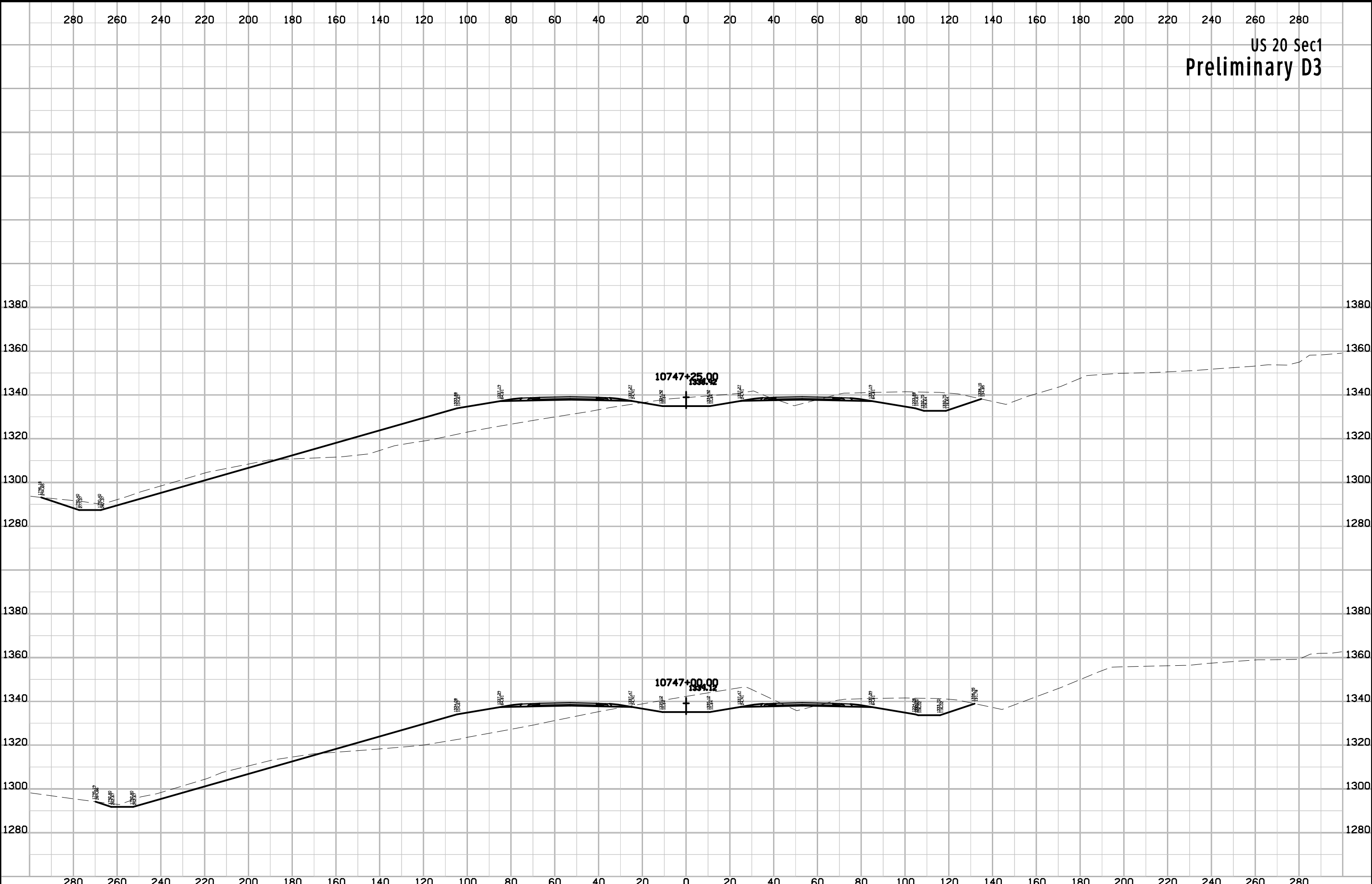
US 20 Sec1
Preliminary D3



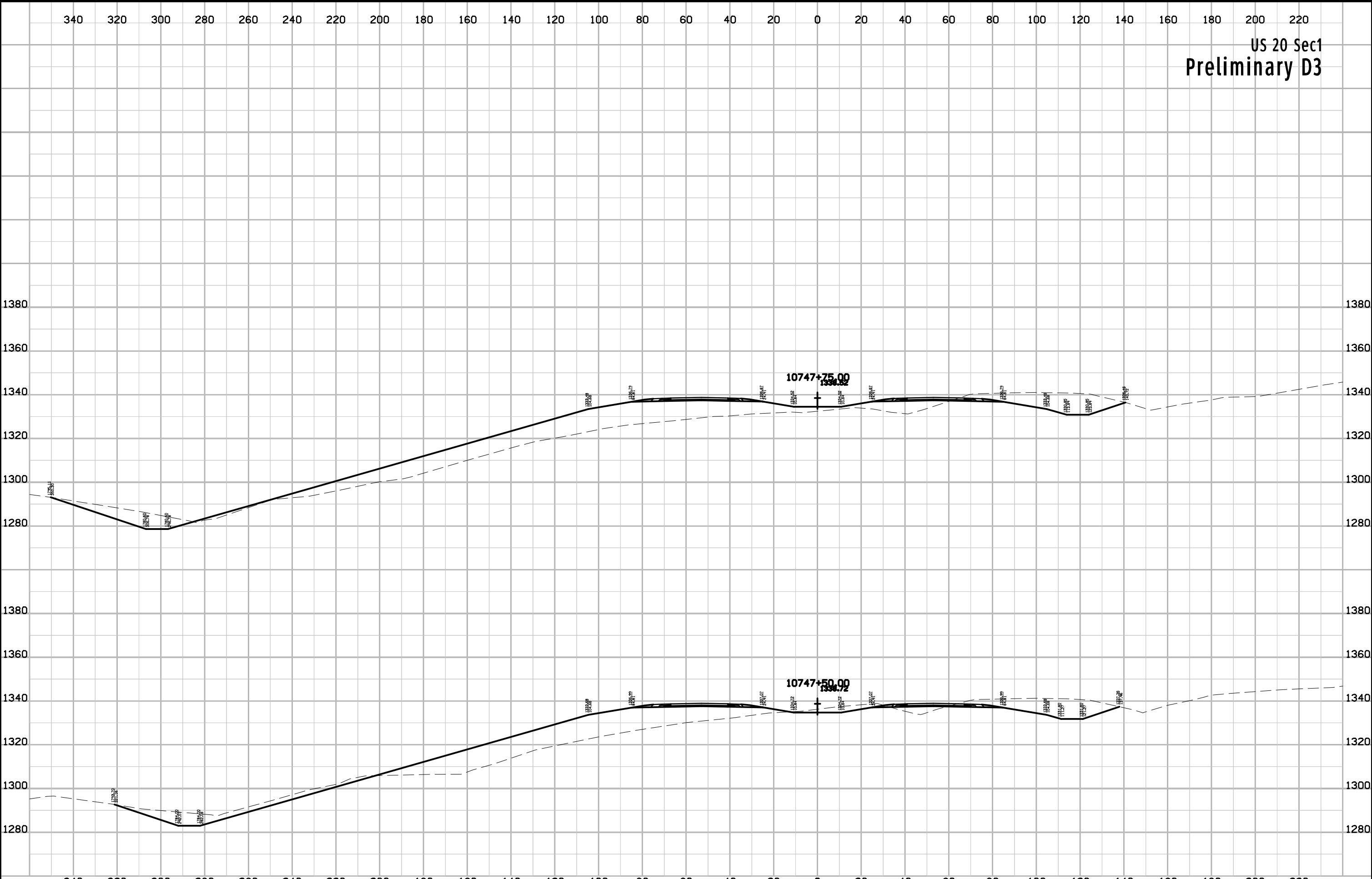
US 20 Sec1
Preliminary D3



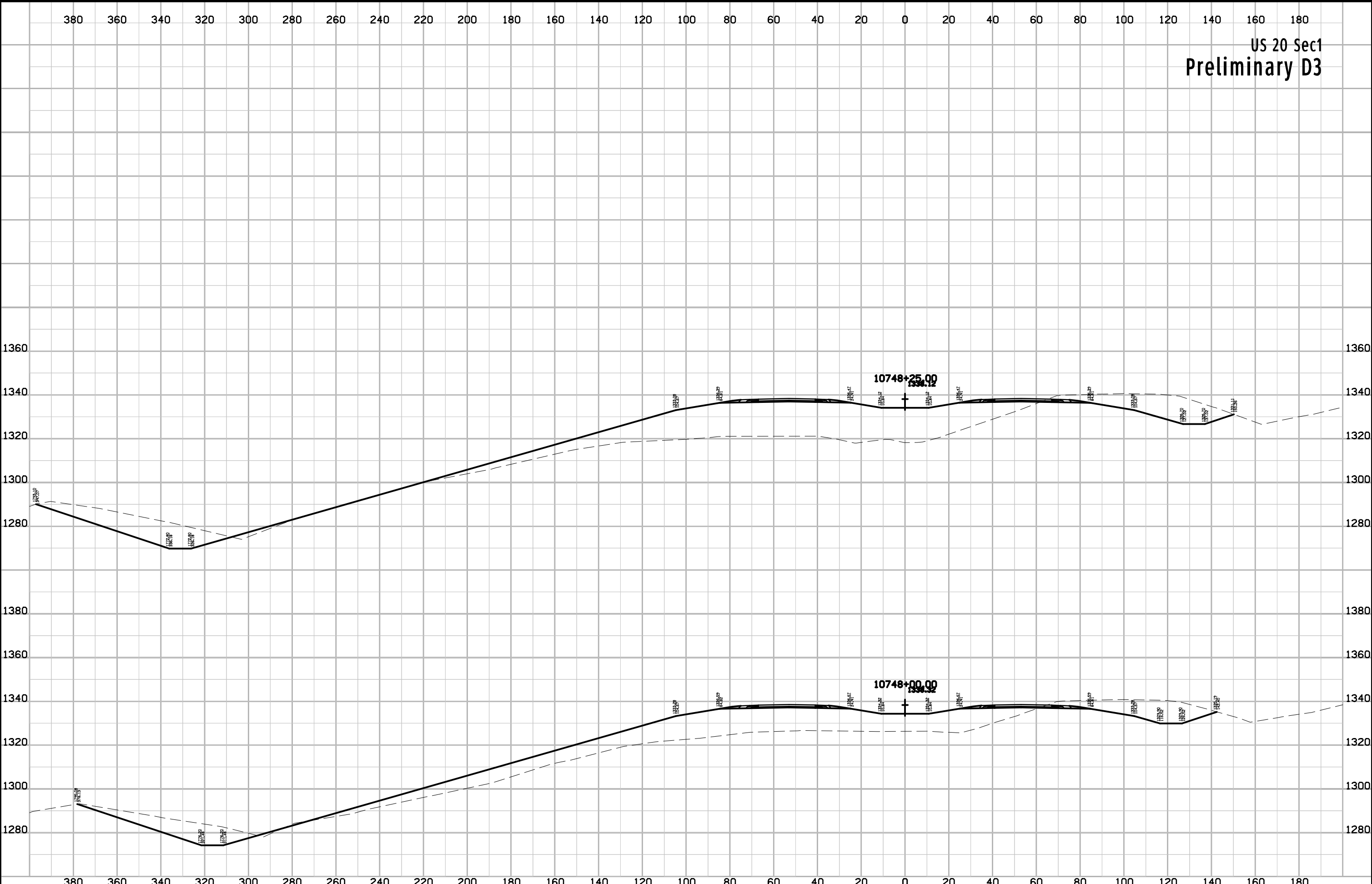
US 20 Sec1
Preliminary D3



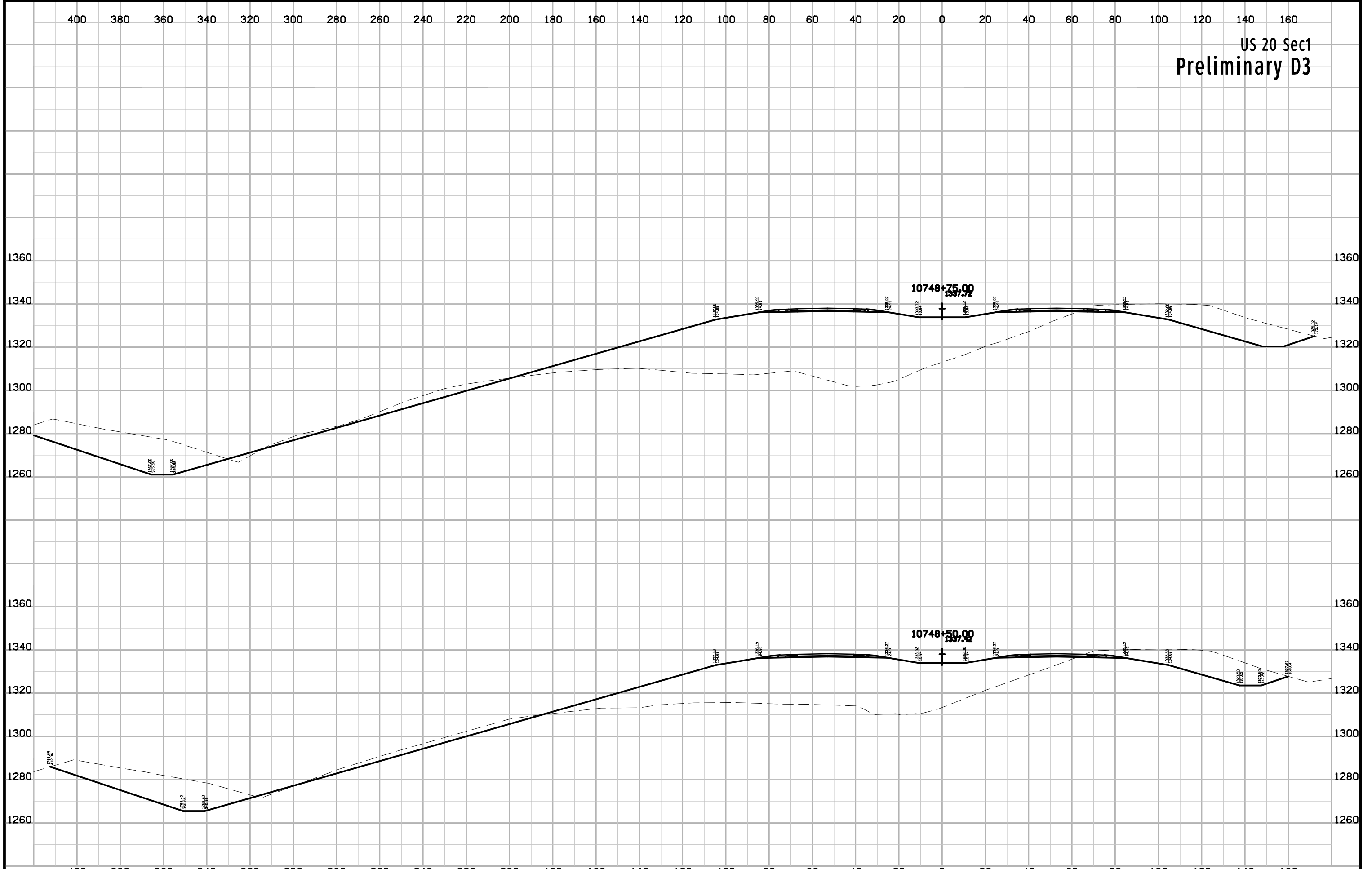
US 20 Sec1
Preliminary D3



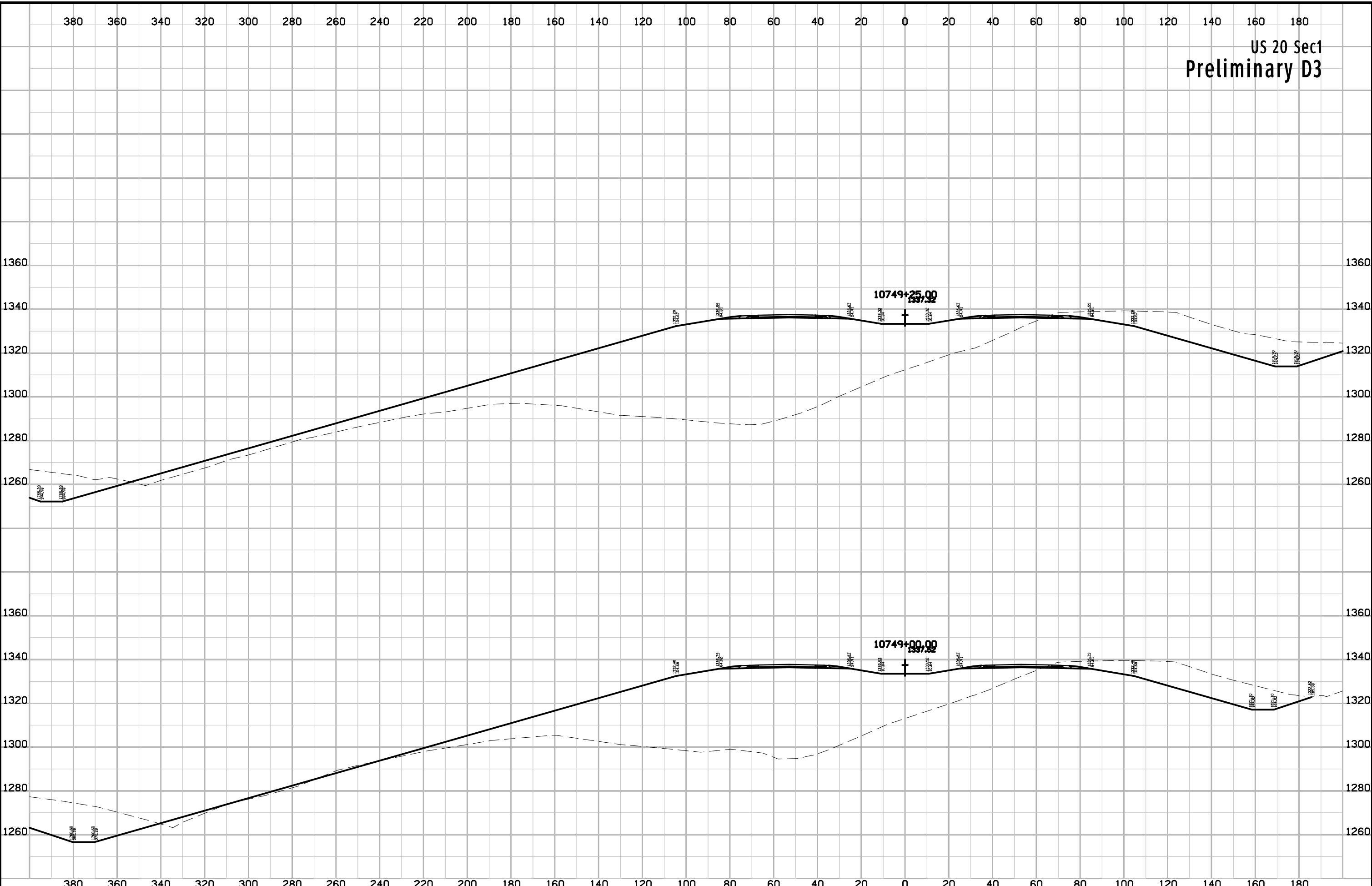
US 20 Sec1
Preliminary D3



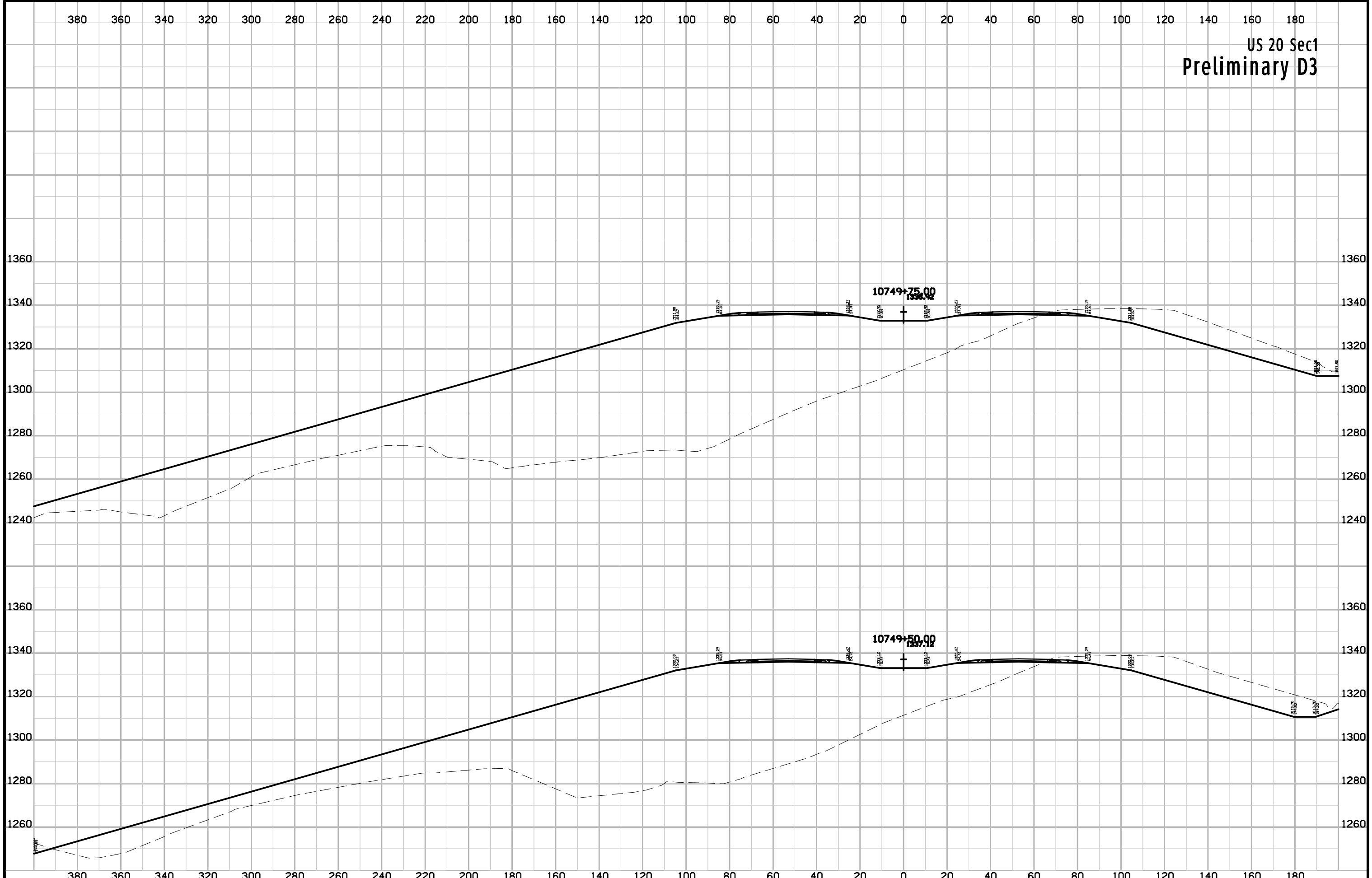
US 20 Sec1
Preliminary D3



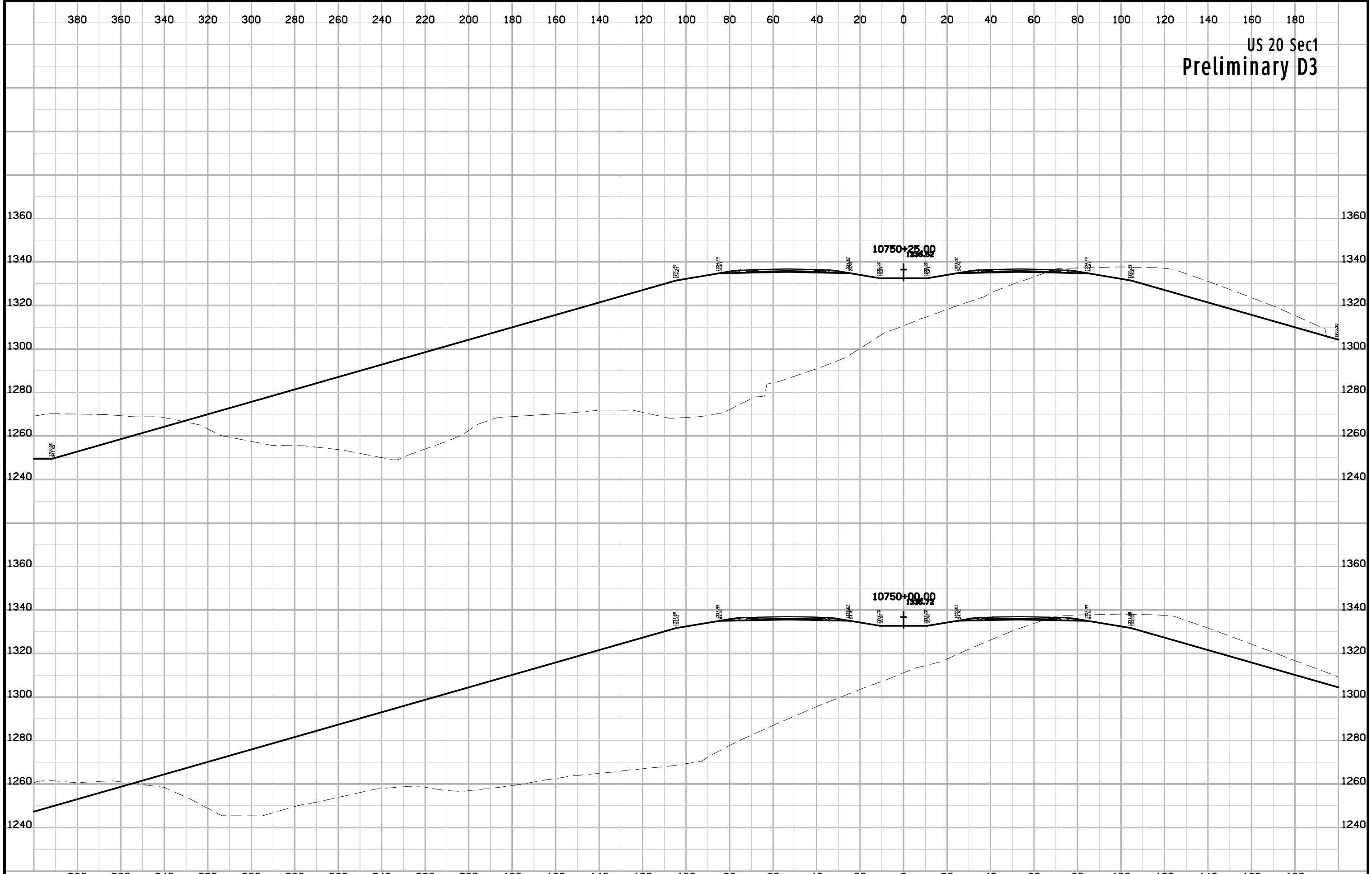
US 20 Sec1
Preliminary D3

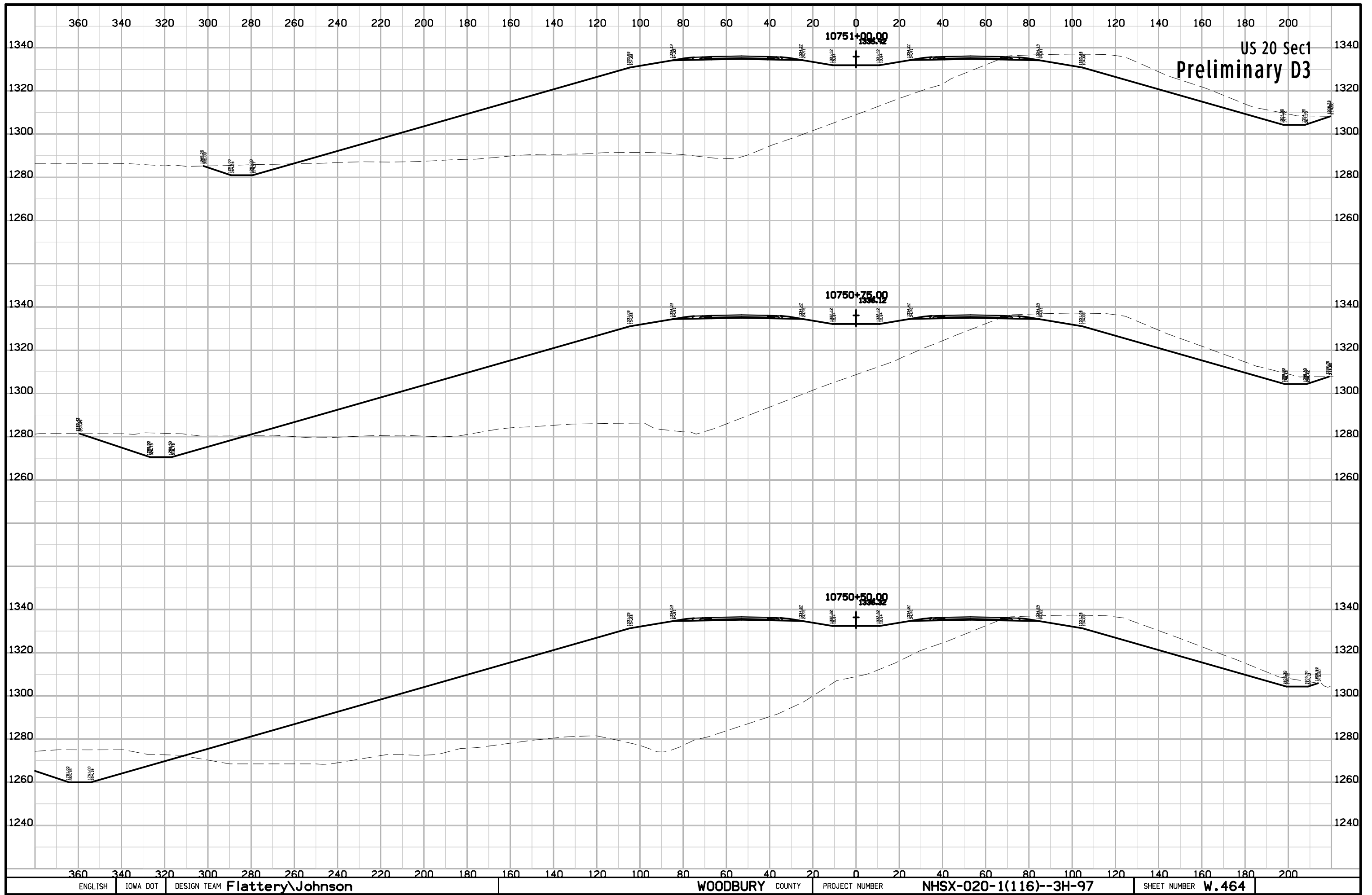


US 20 Sec1
Preliminary D3



US 20 Sec1
Preliminary D3



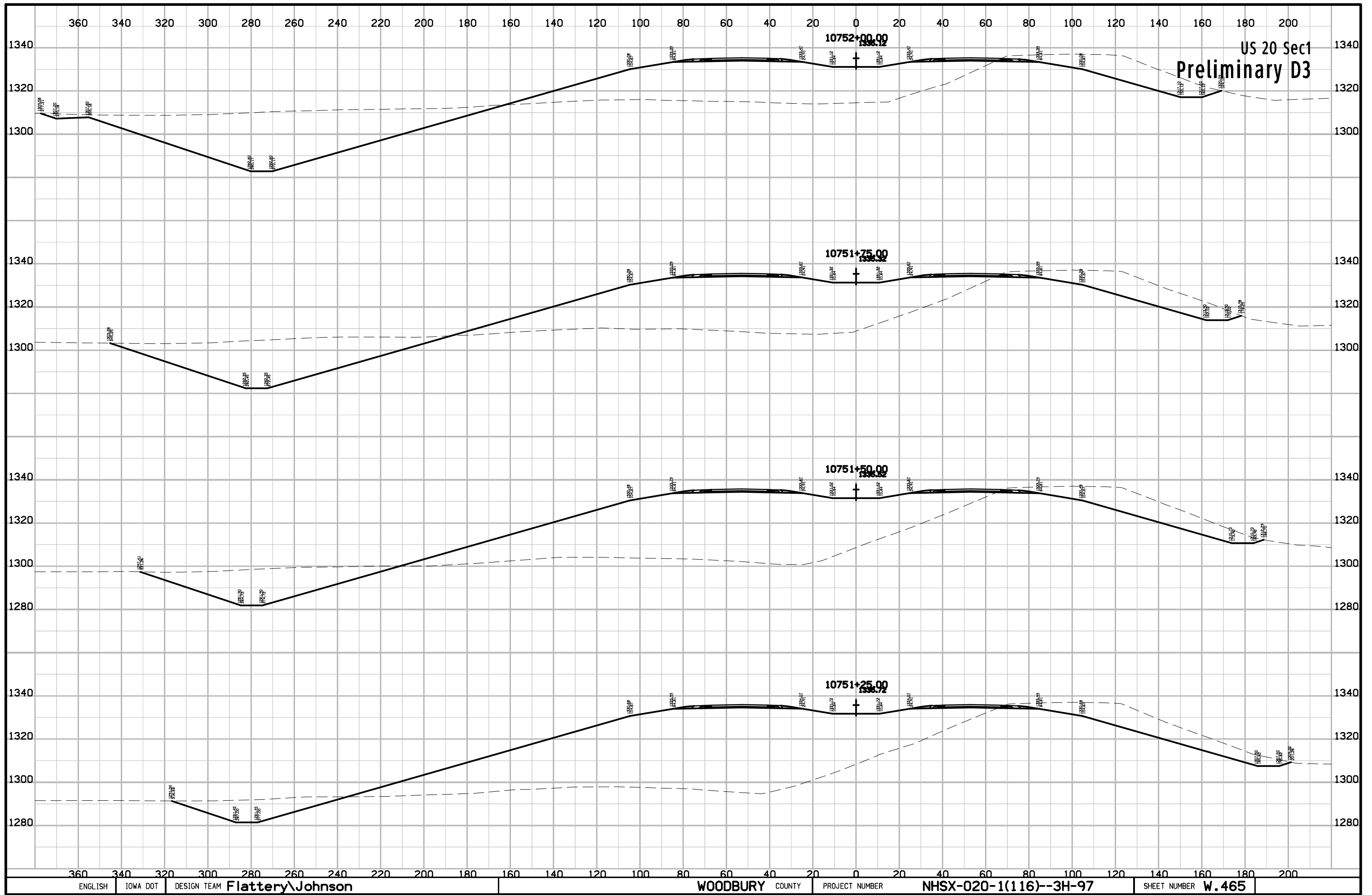


US 20 Sec1
Preliminary D3

10751+00.00
1336.12

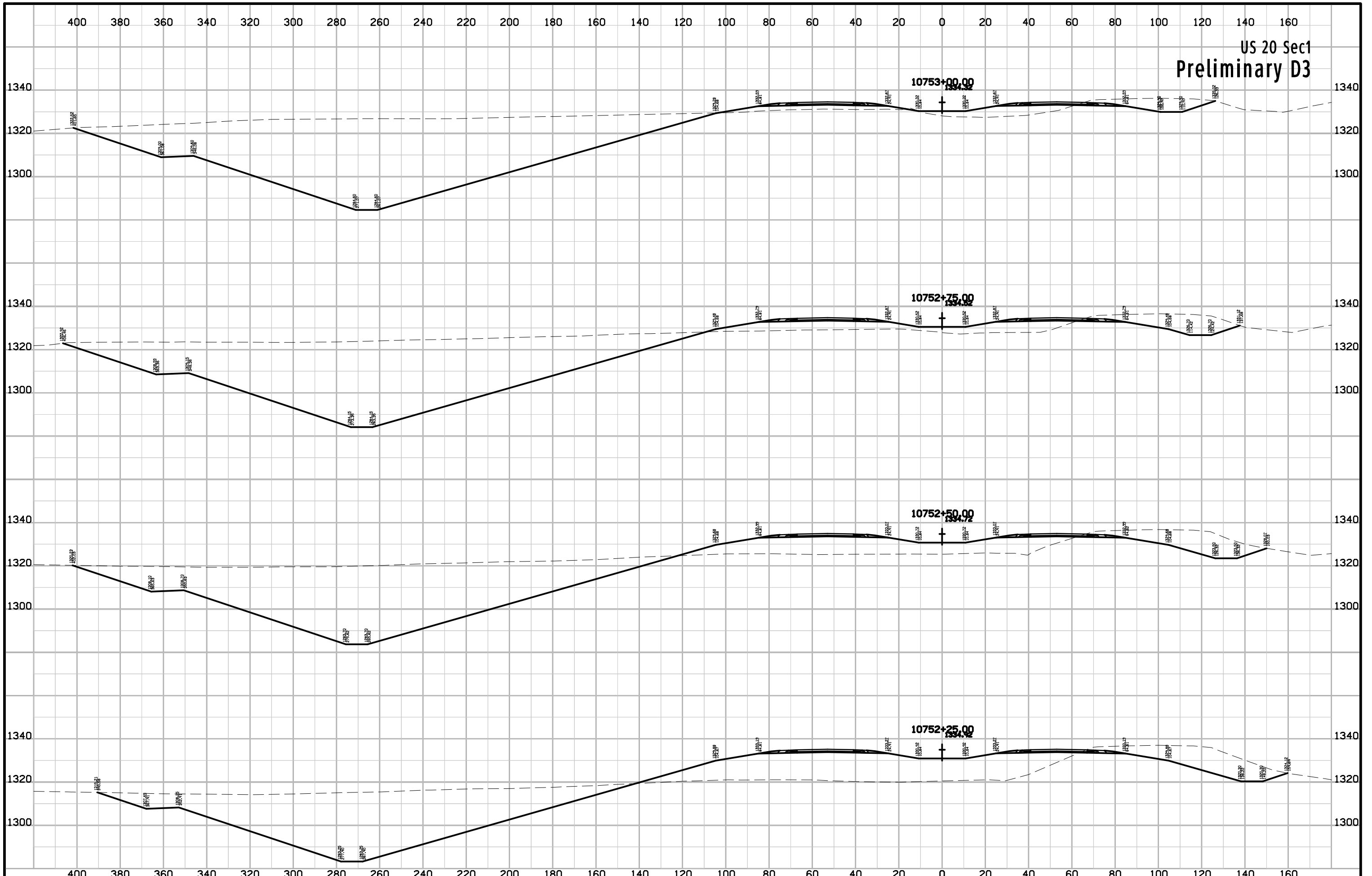
10750+75.00
1334.12

10750+50.00
1334.32

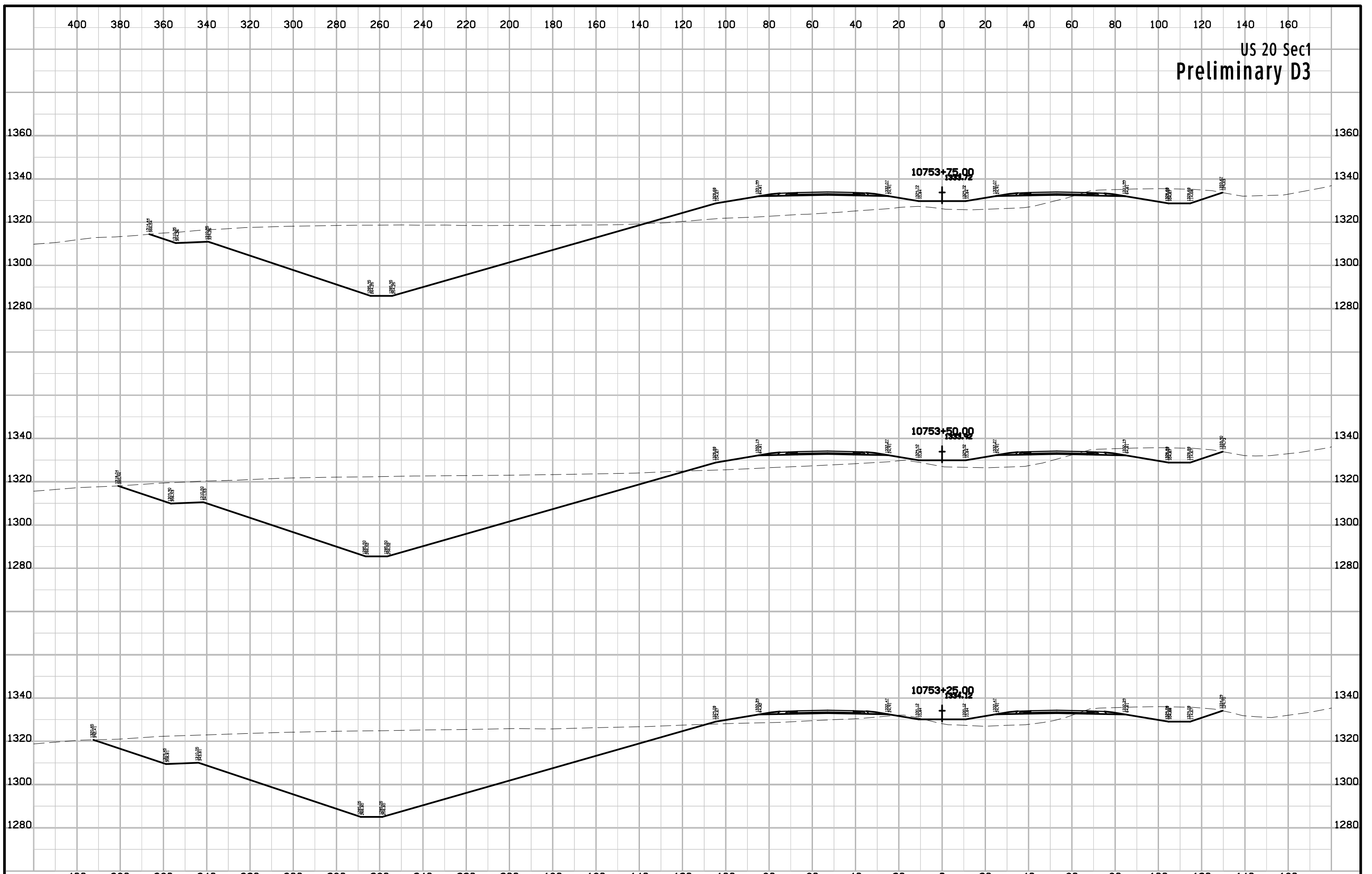


US 20 Sec1
Preliminary D3

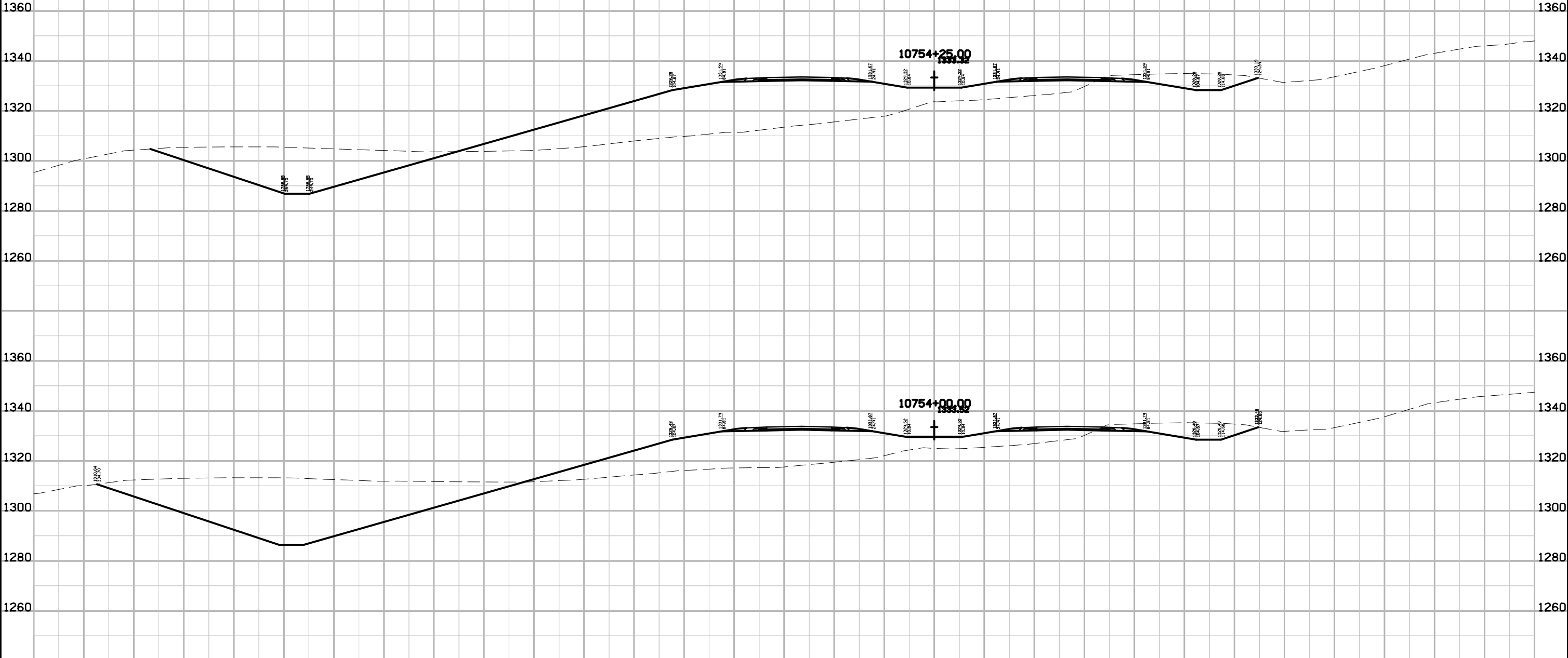
US 20 Sec1
Preliminary D3



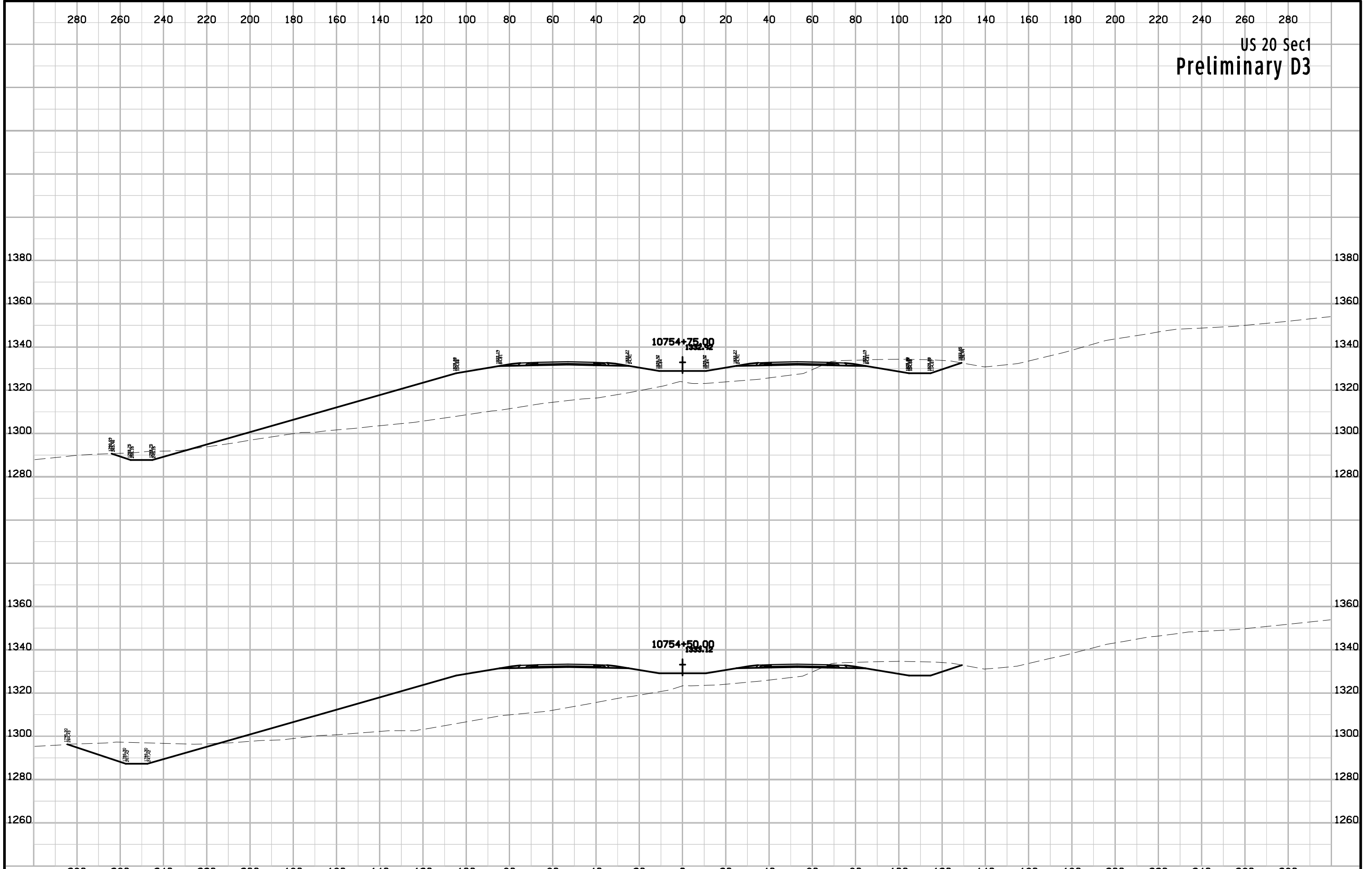
US 20 Sec1
Preliminary D3



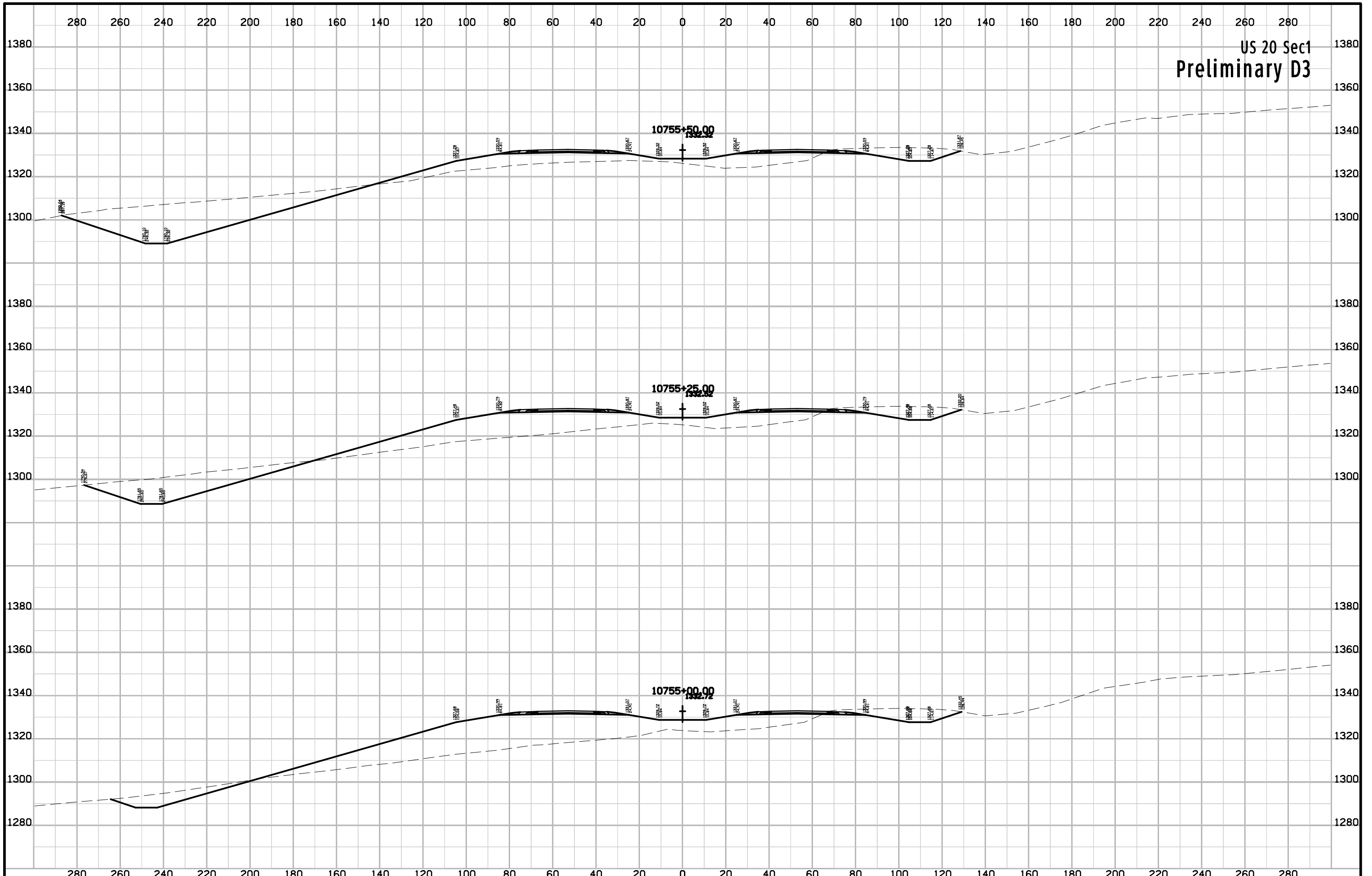
US 20 Sec1
Preliminary D3



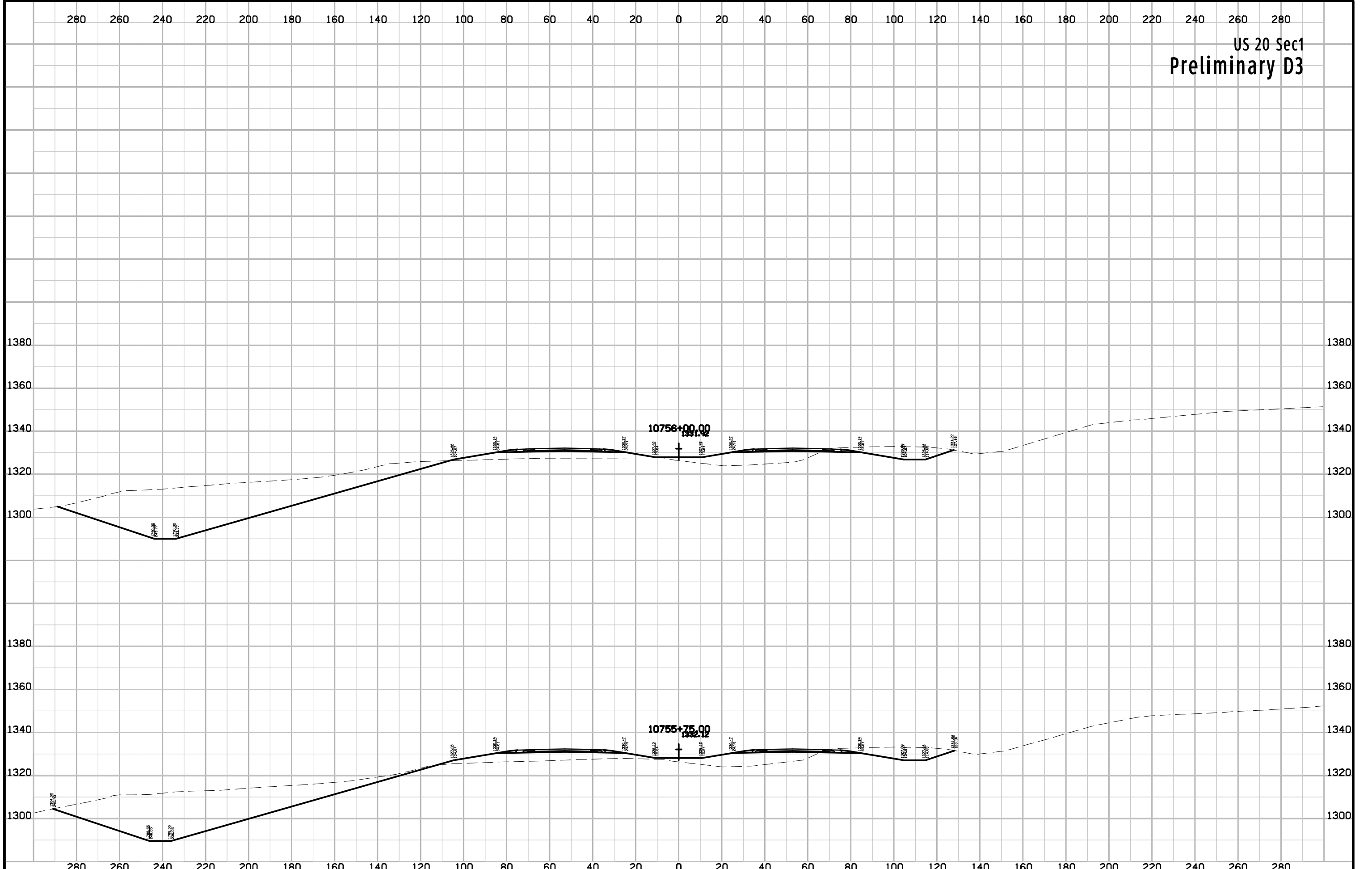
US 20 Sec1
Preliminary D3



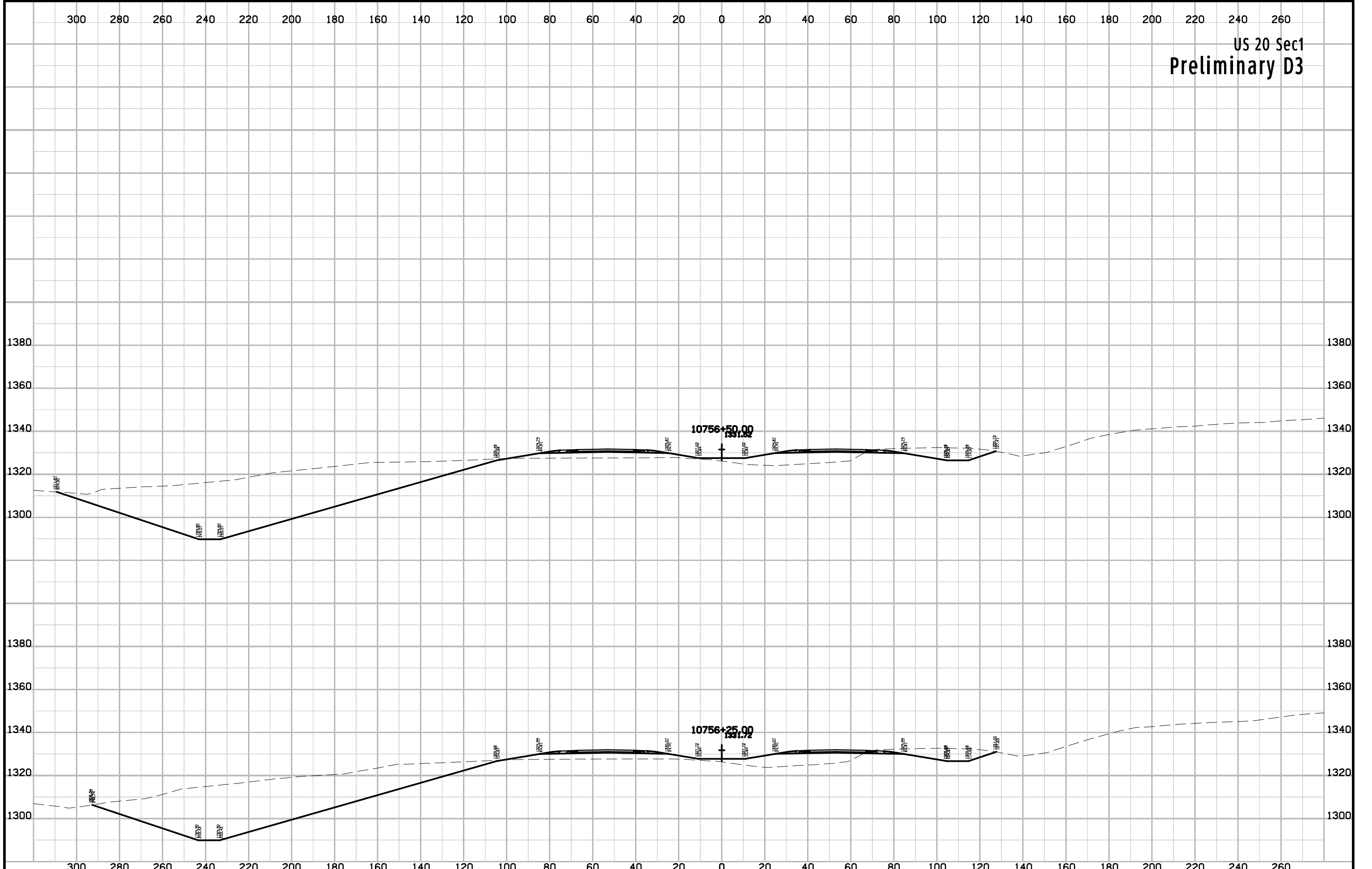
US 20 Sec1
Preliminary D3



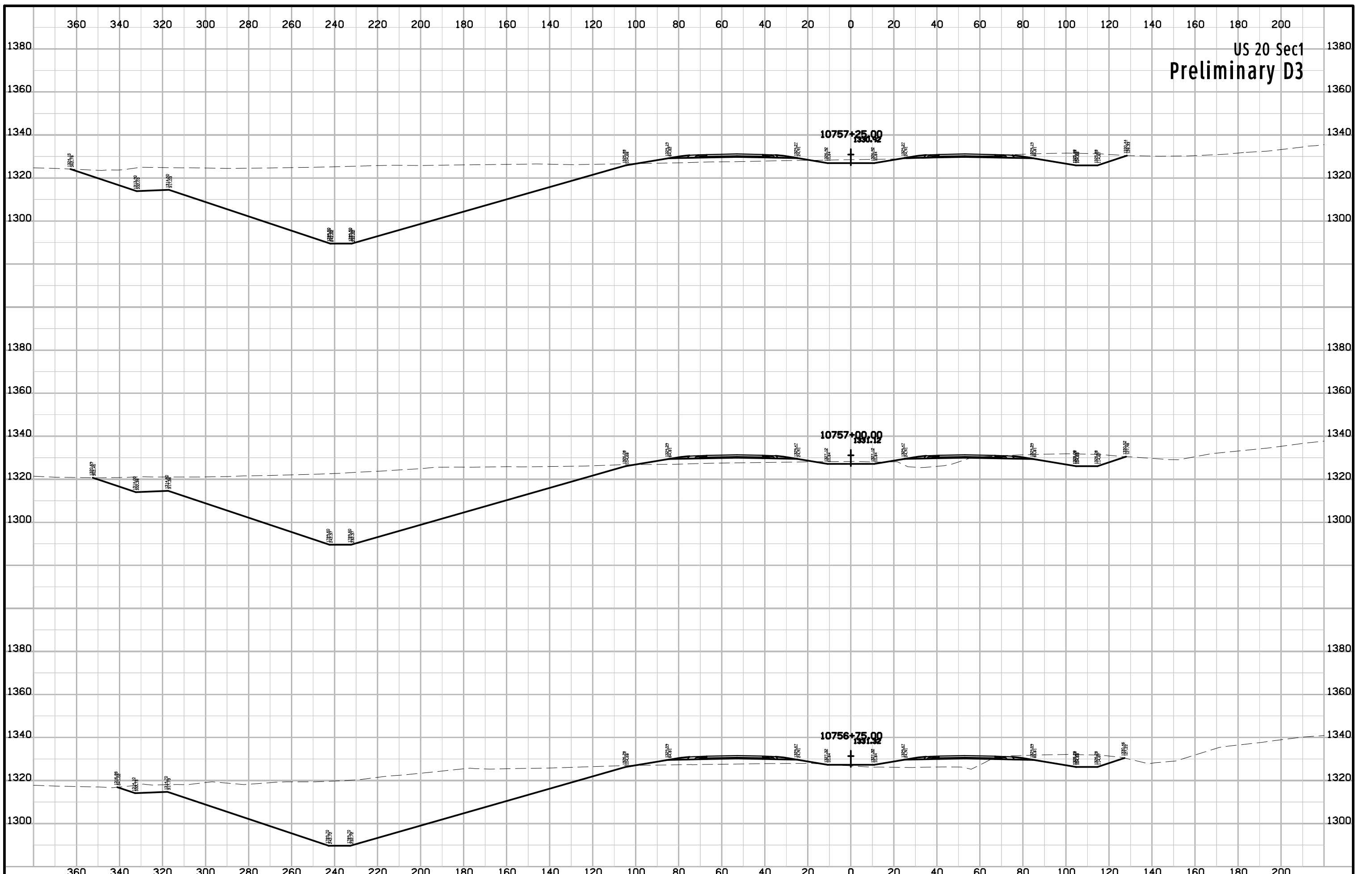
US 20 Sec1
Preliminary D3



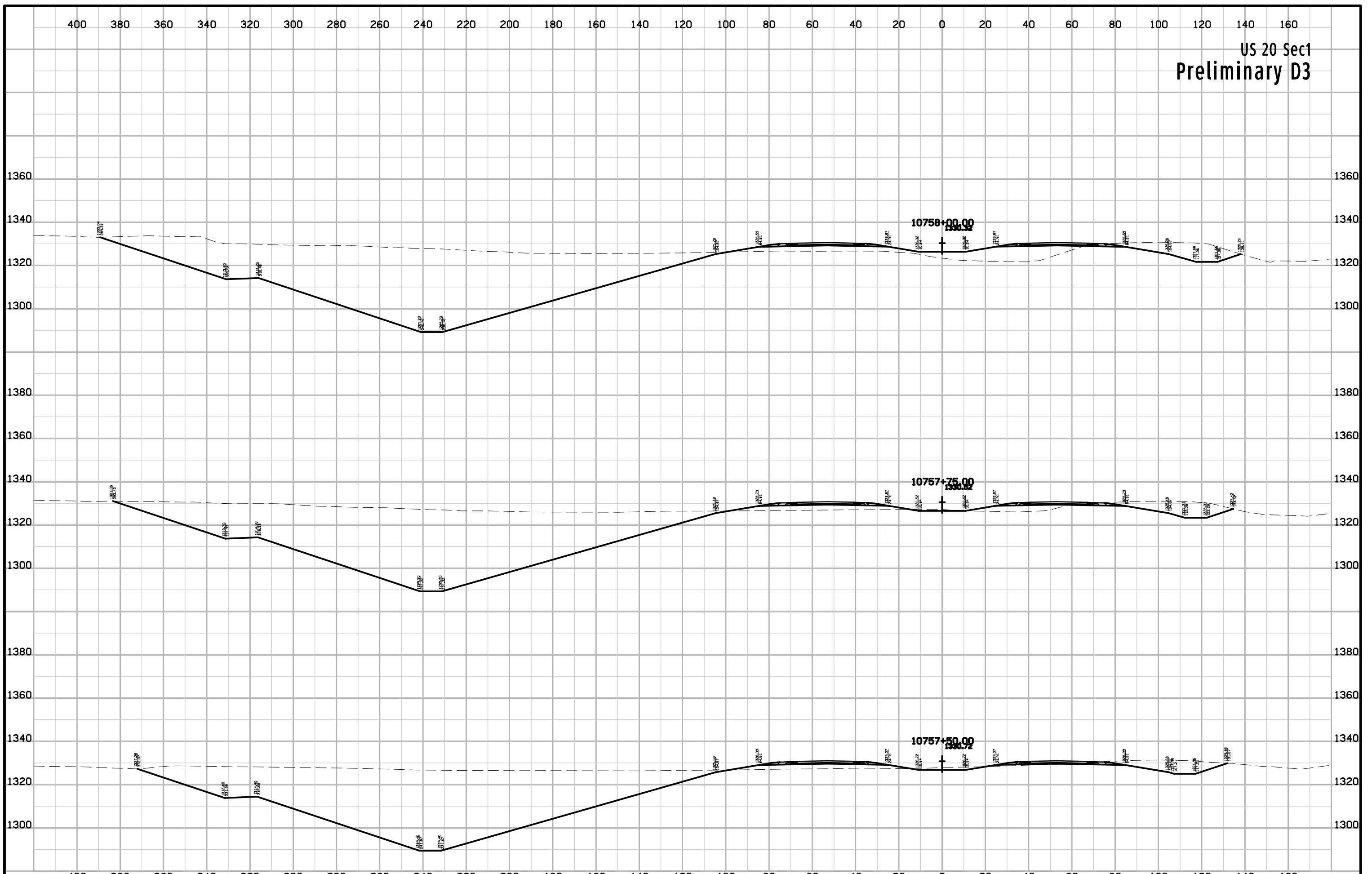
US 20 Sec1
Preliminary D3



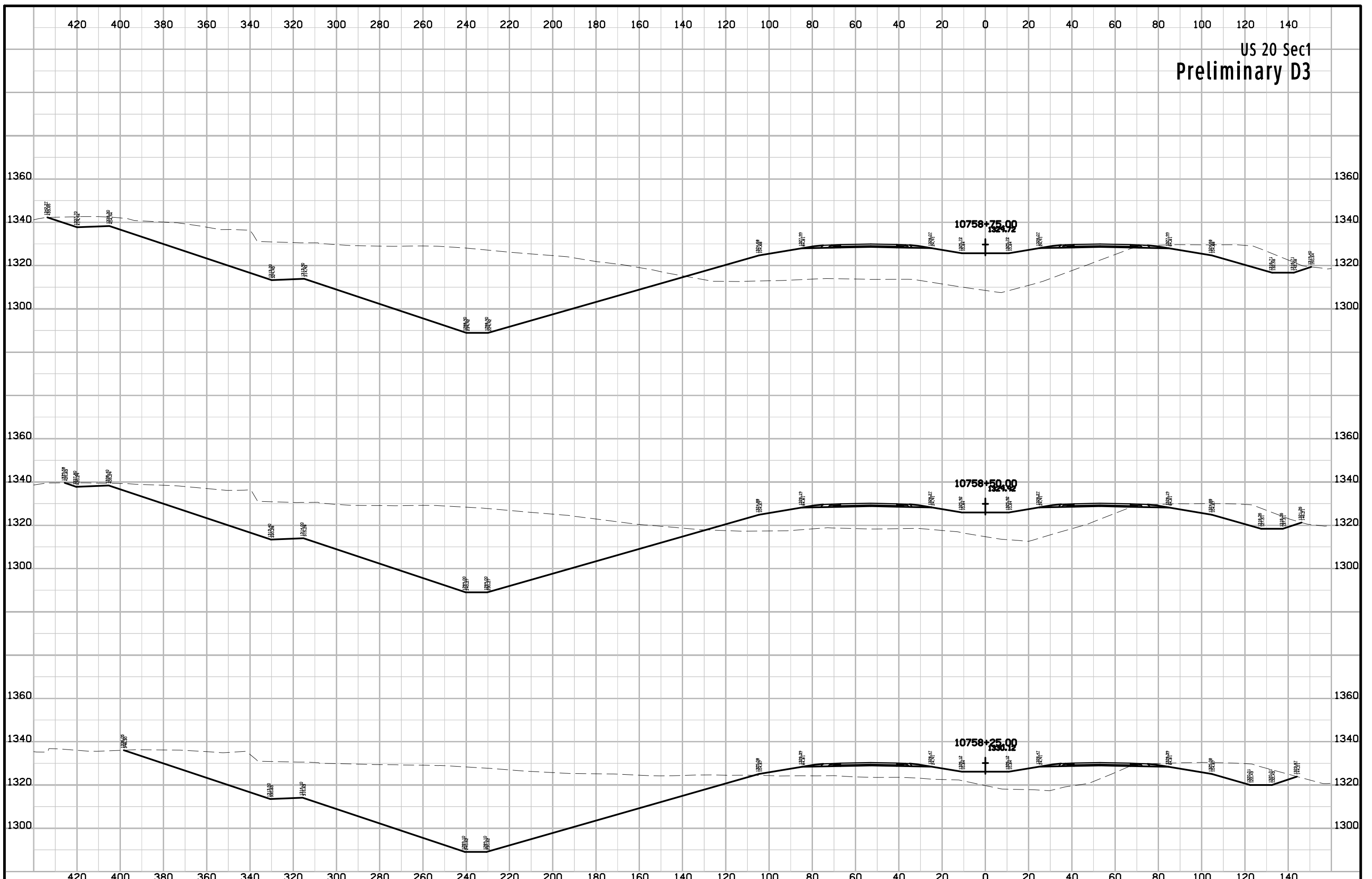
US 20 Sec1
Preliminary D3



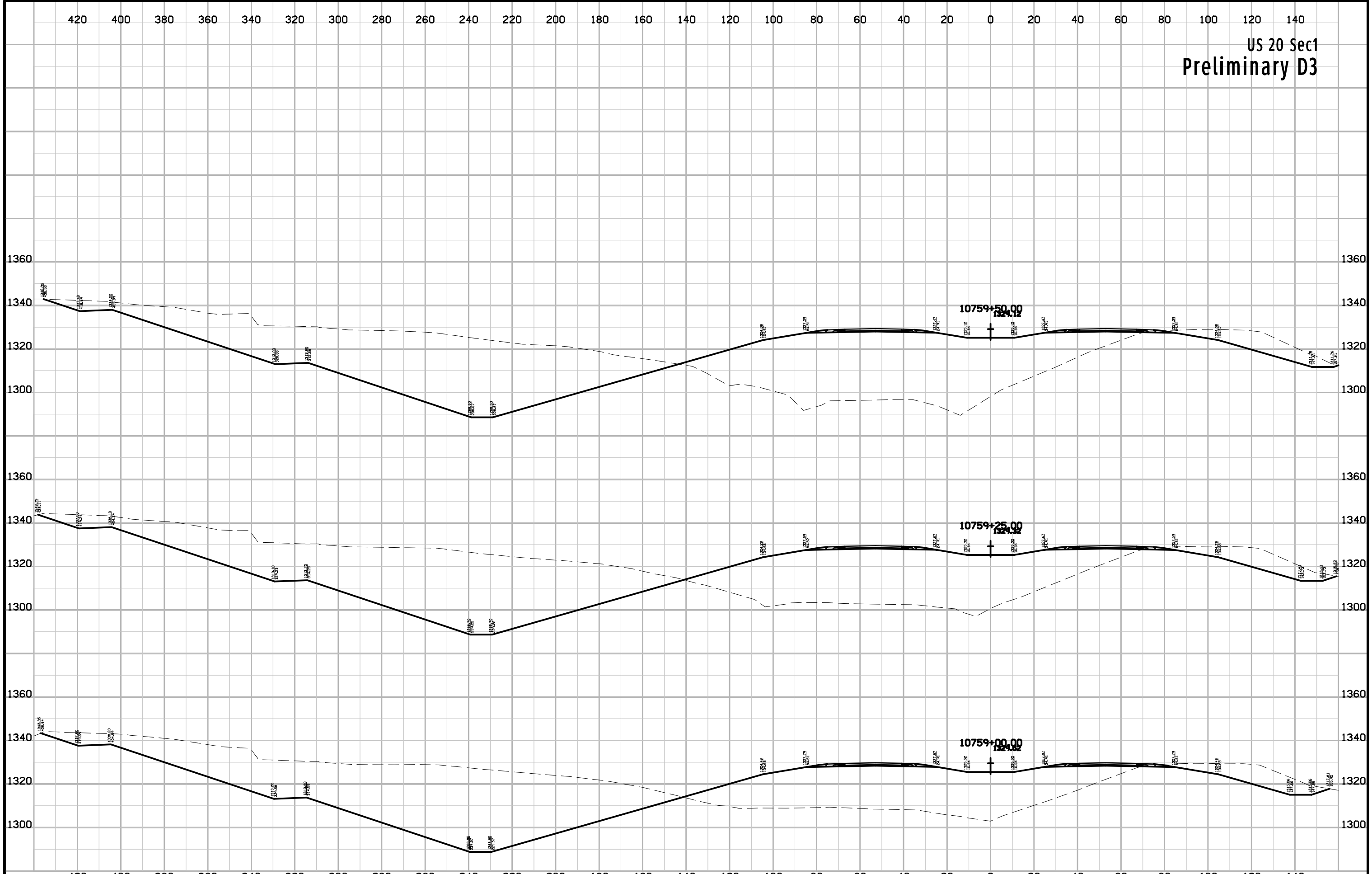
US 20 Sec1
Preliminary D3



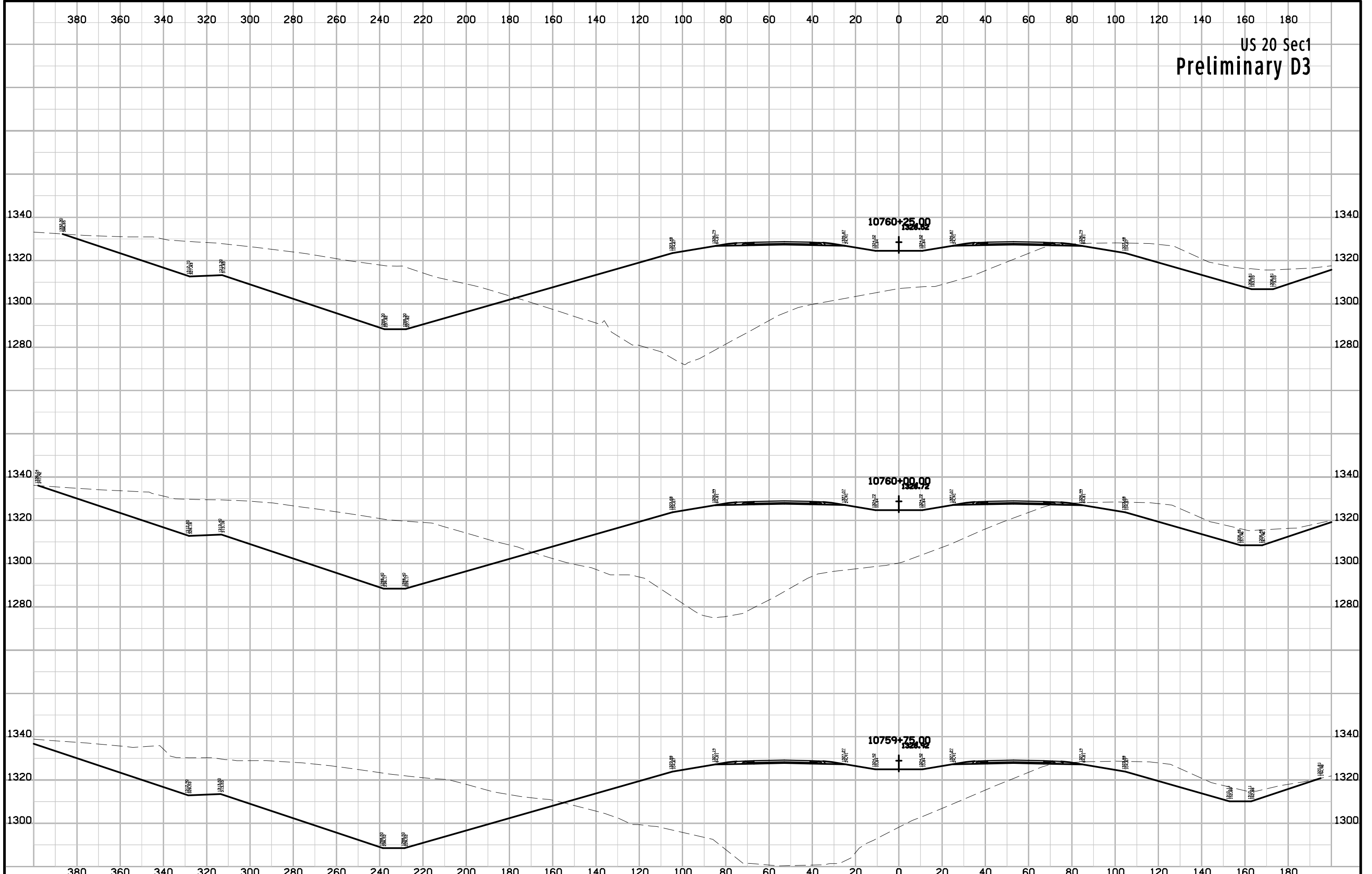
US 20 Sec1
Preliminary D3



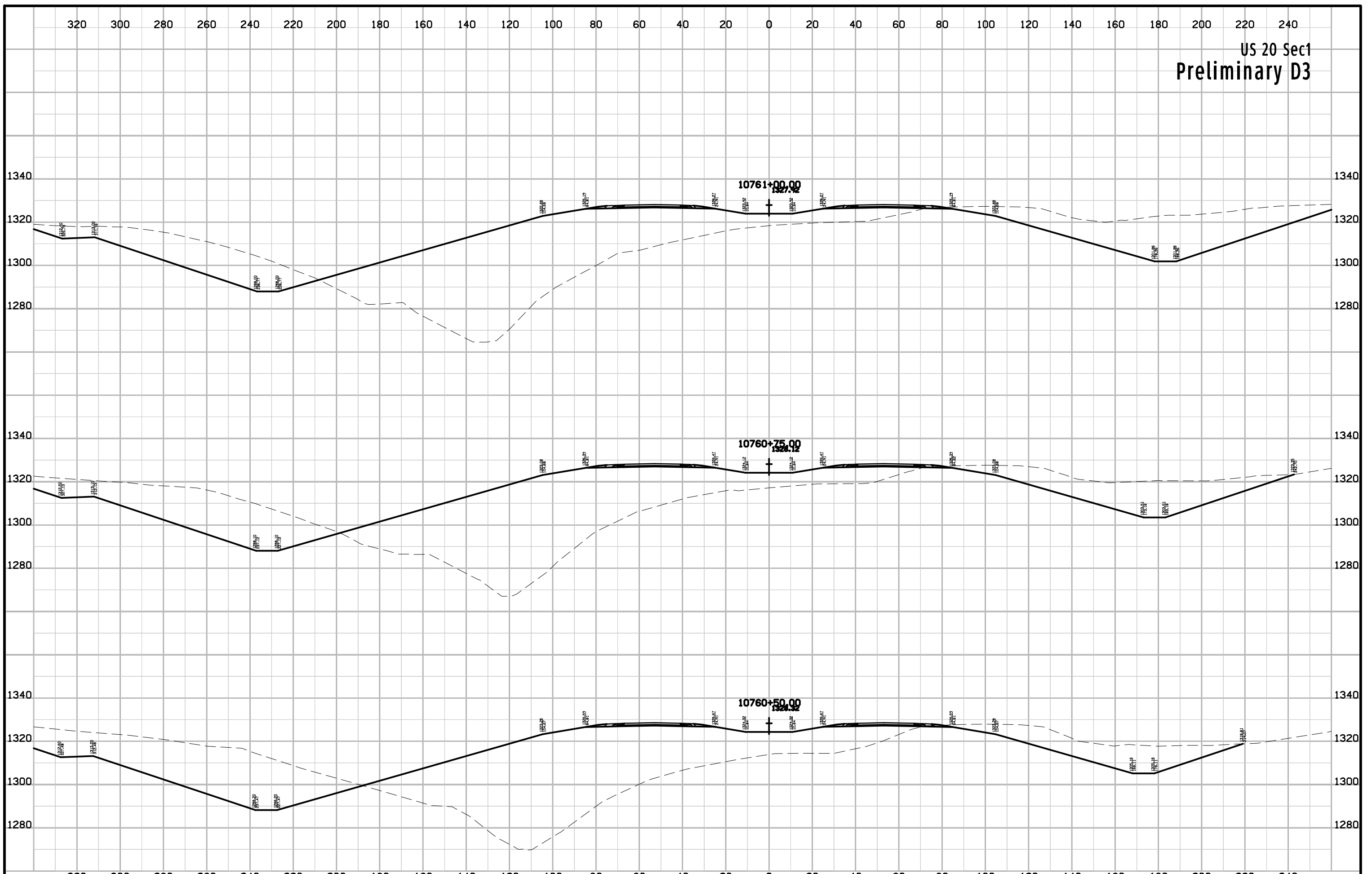
US 20 Sec1
Preliminary D3



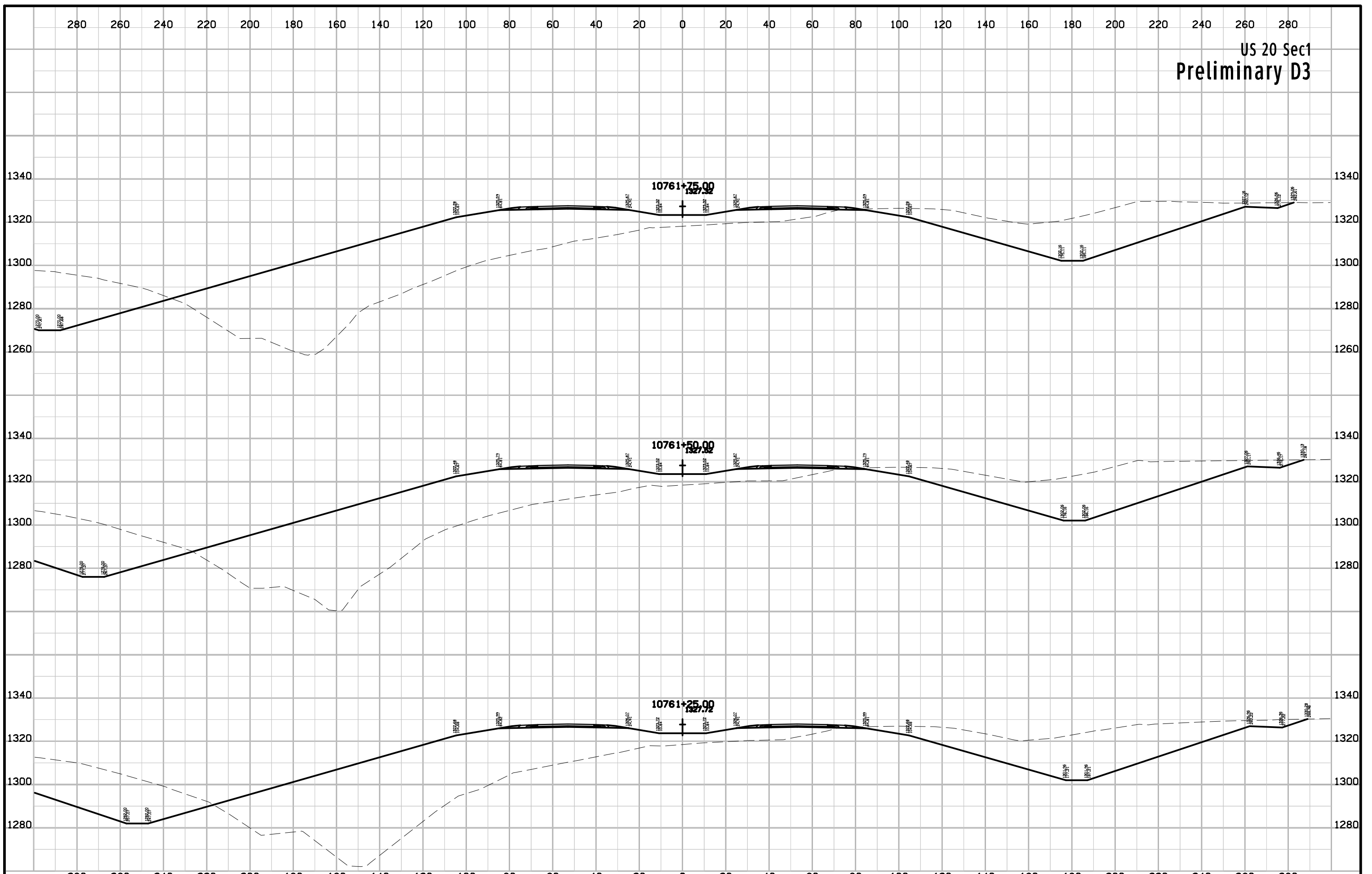
US 20 Sec1
Preliminary D3



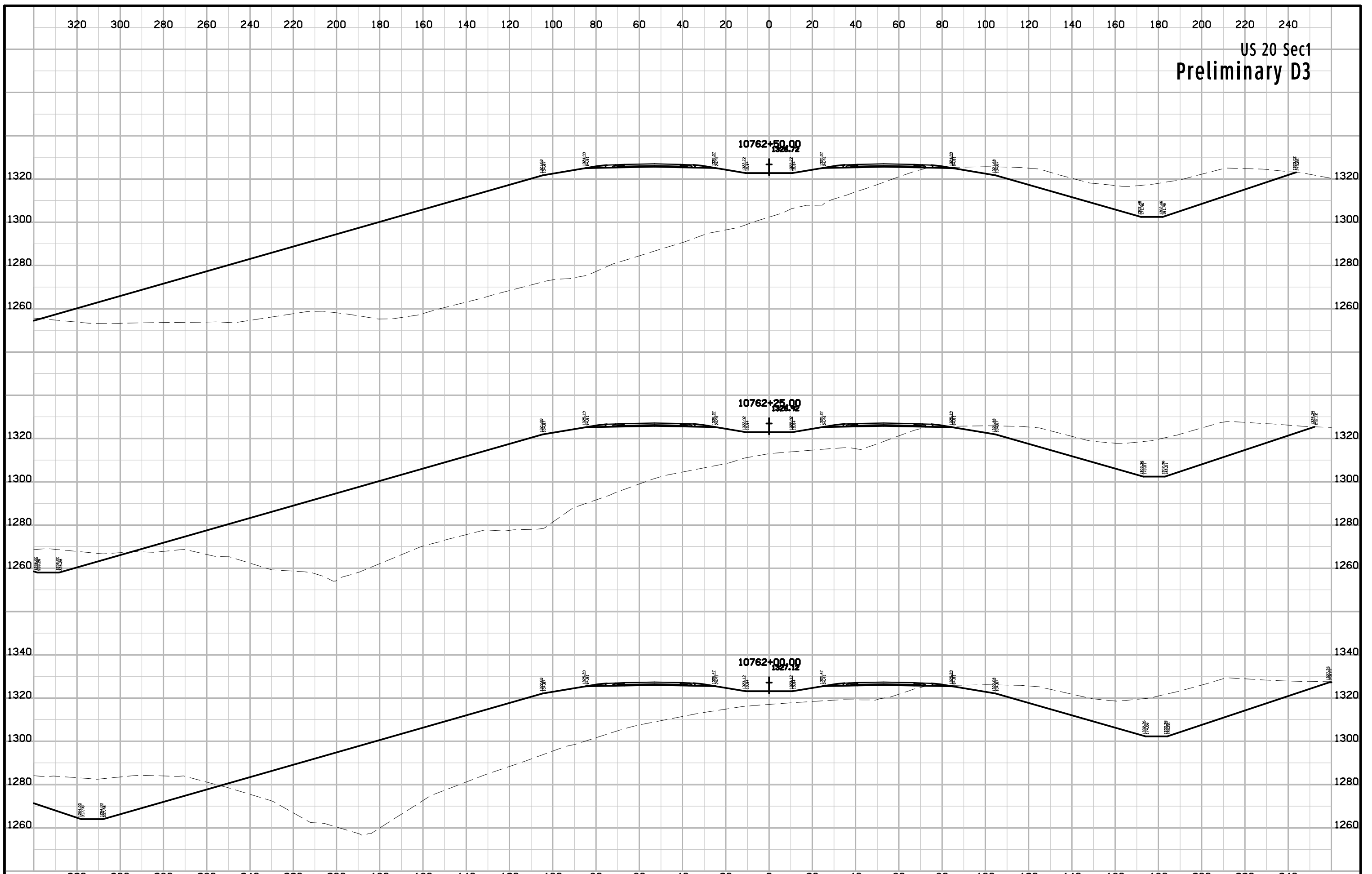
US 20 Sec1
Preliminary D3



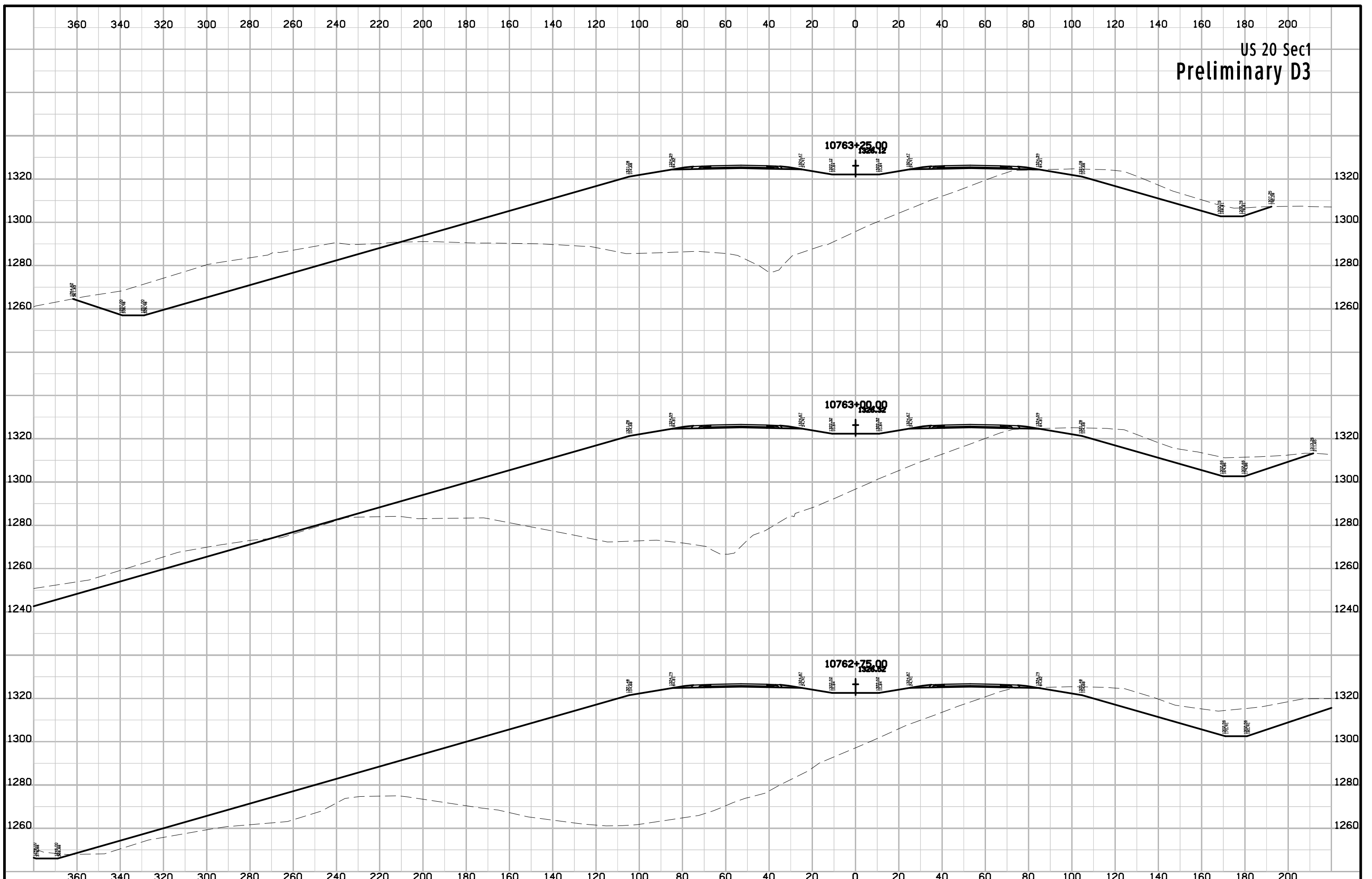
US 20 Sec1
Preliminary D3



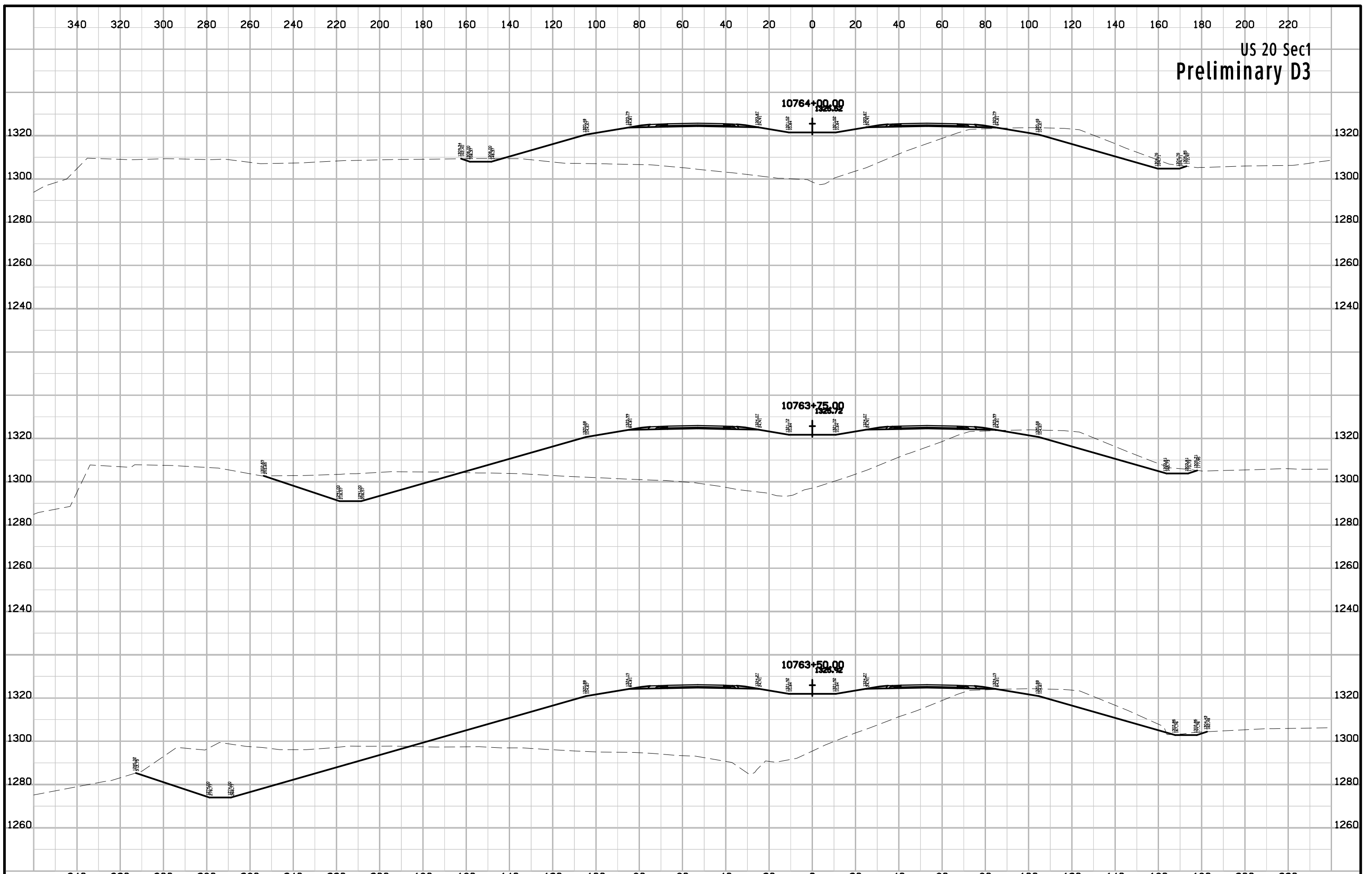
US 20 Sec1
Preliminary D3



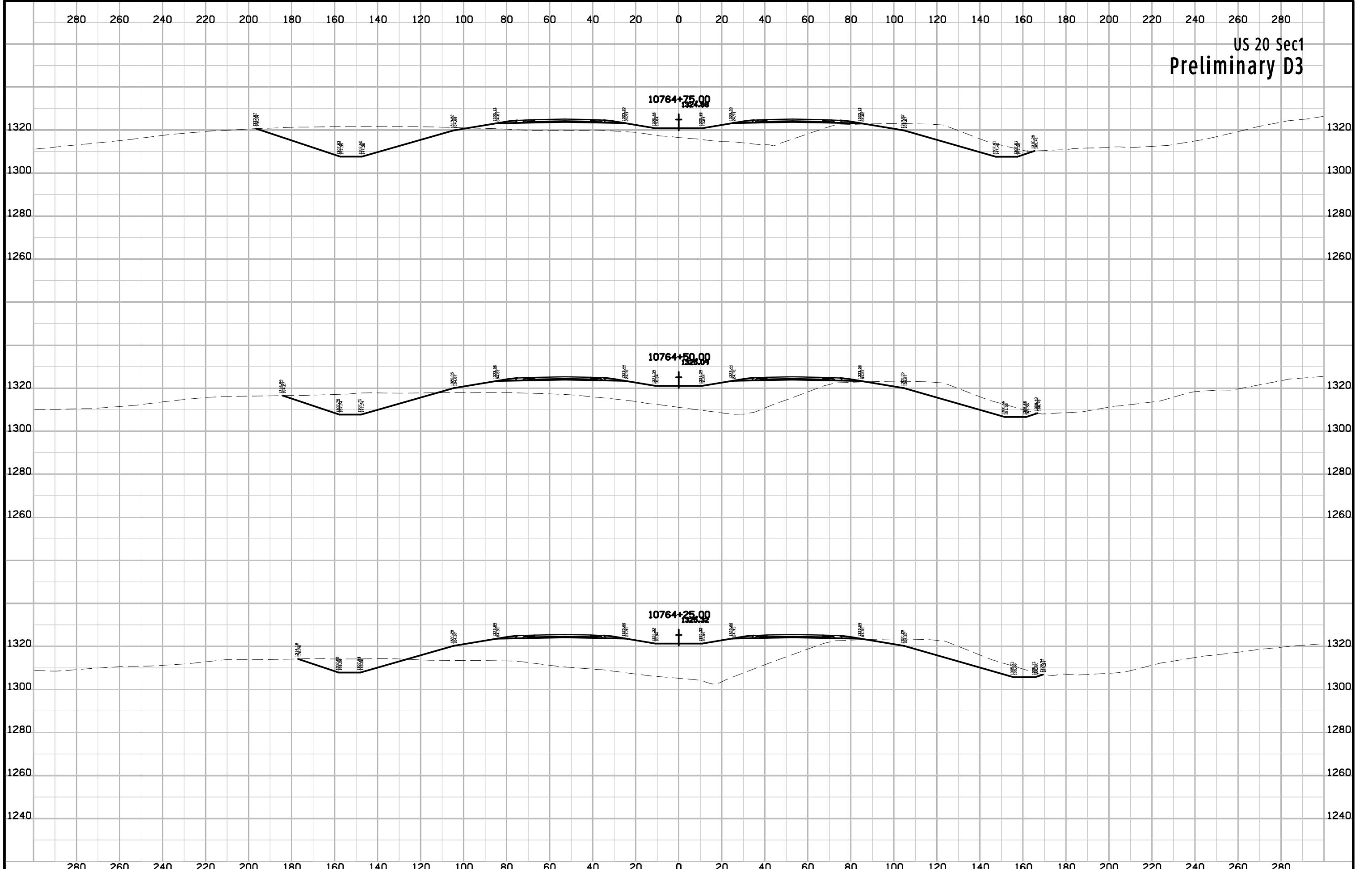
US 20 Sec1
Preliminary D3



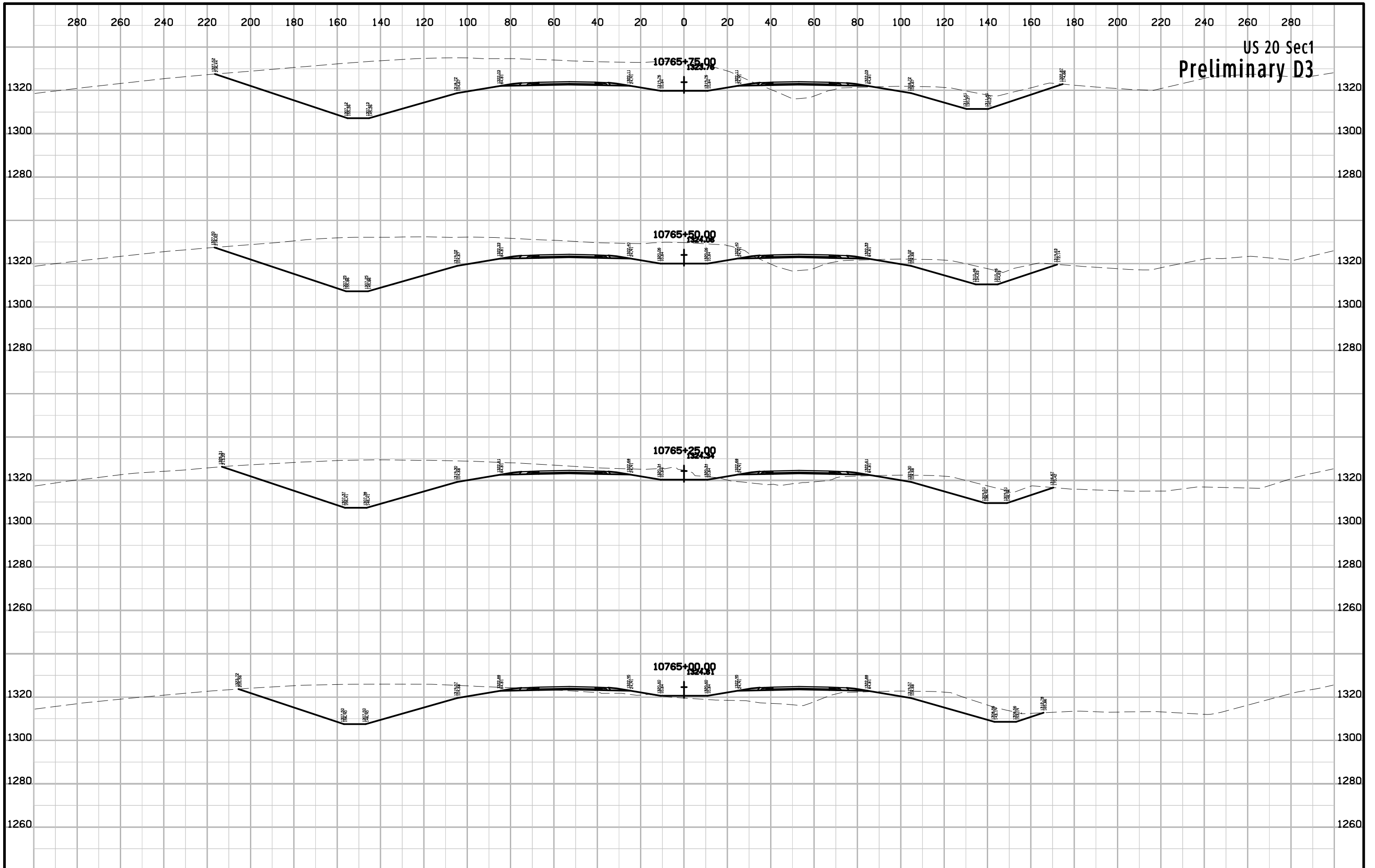
US 20 Sec1
Preliminary D3

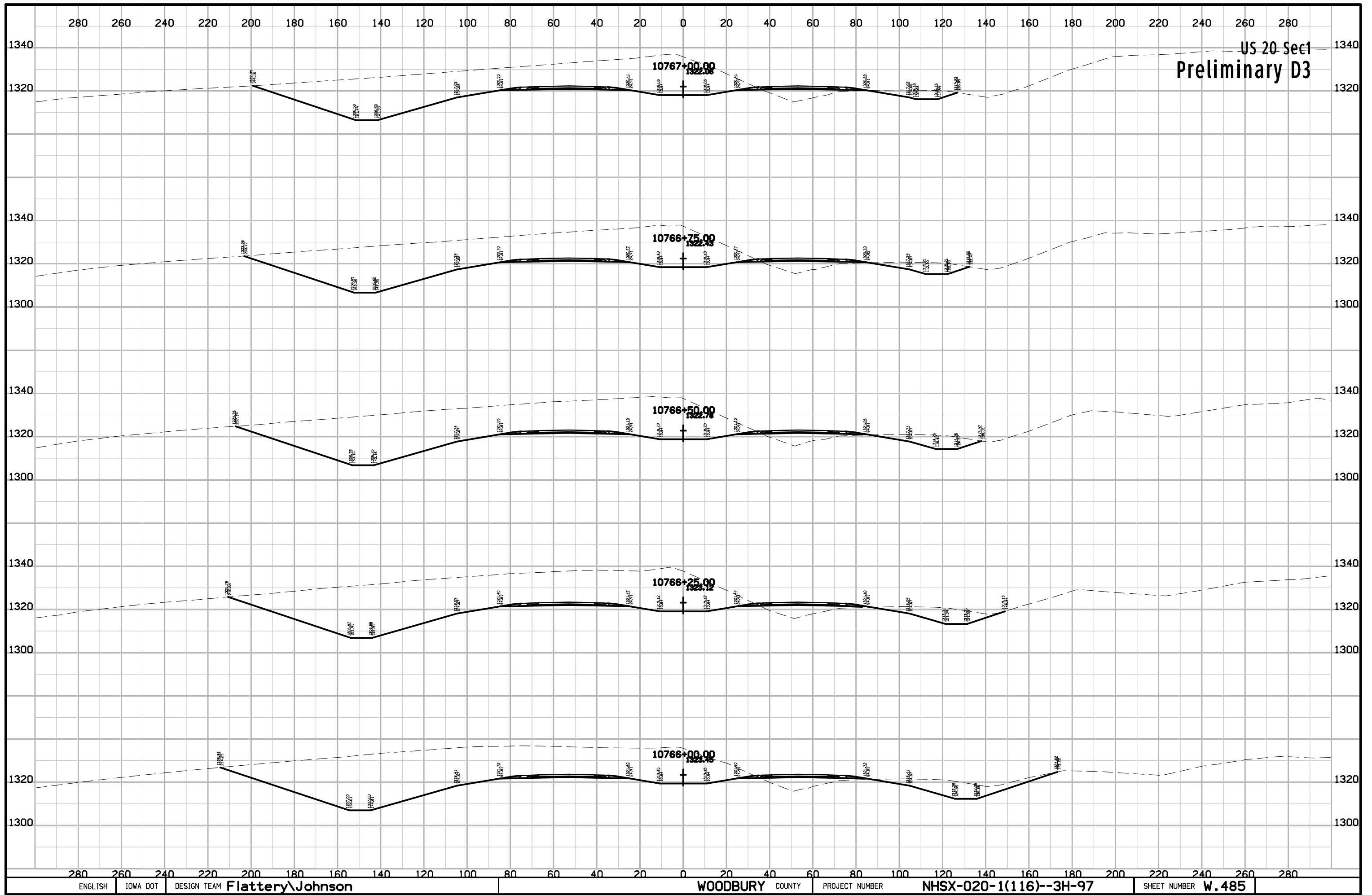


US 20 Sec1
Preliminary D3

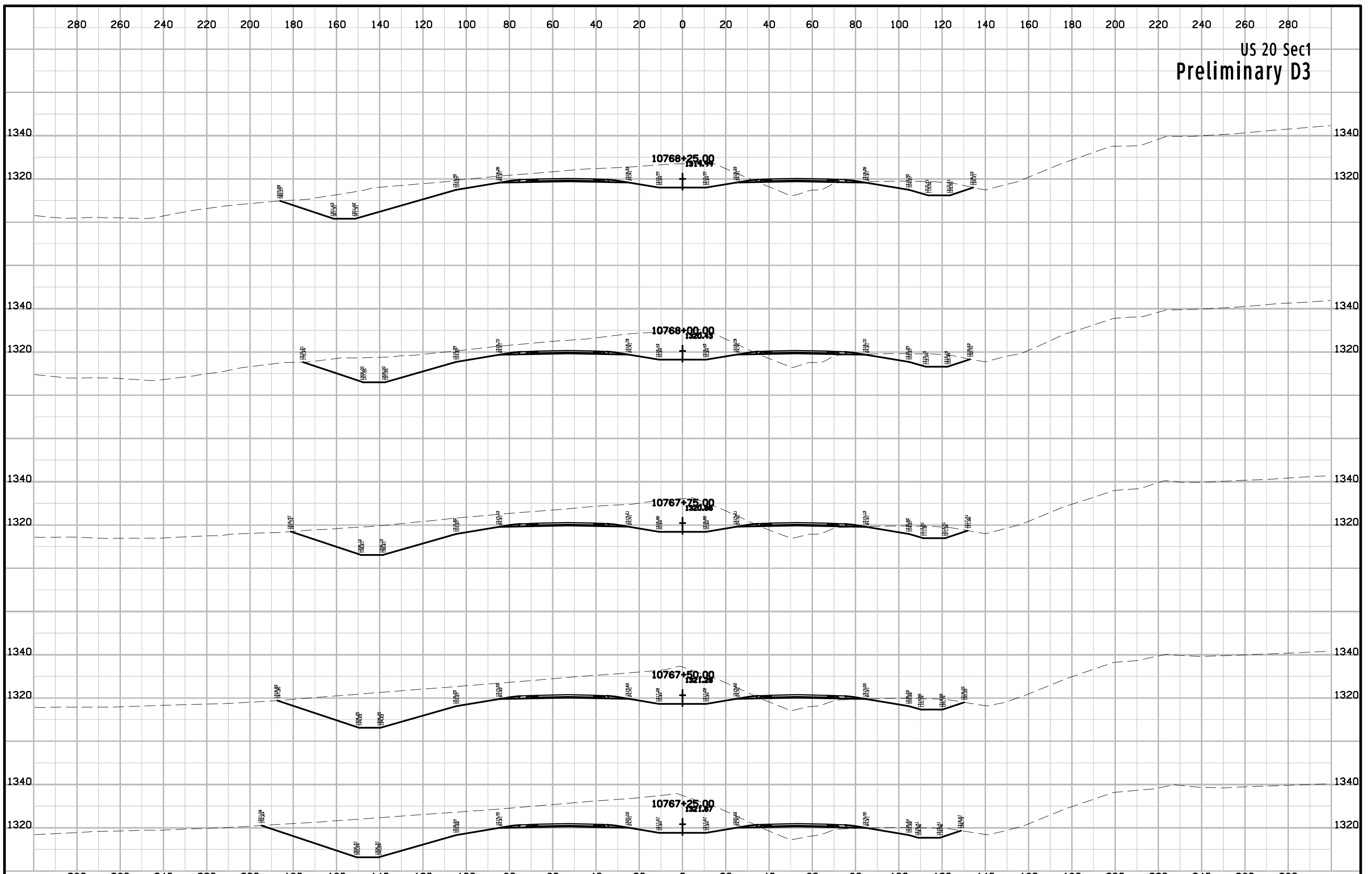


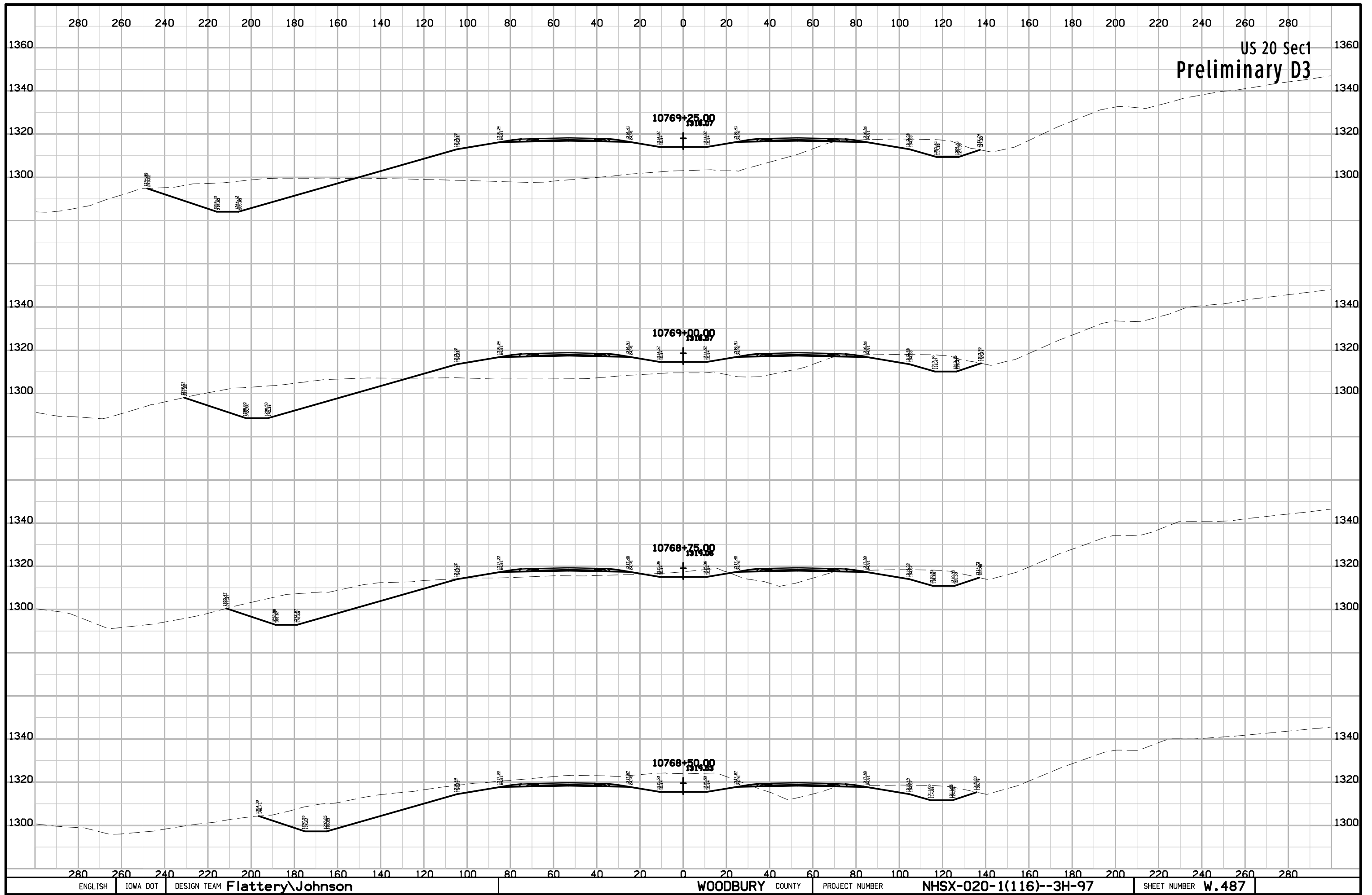
US 20 Sec1
Preliminary D3





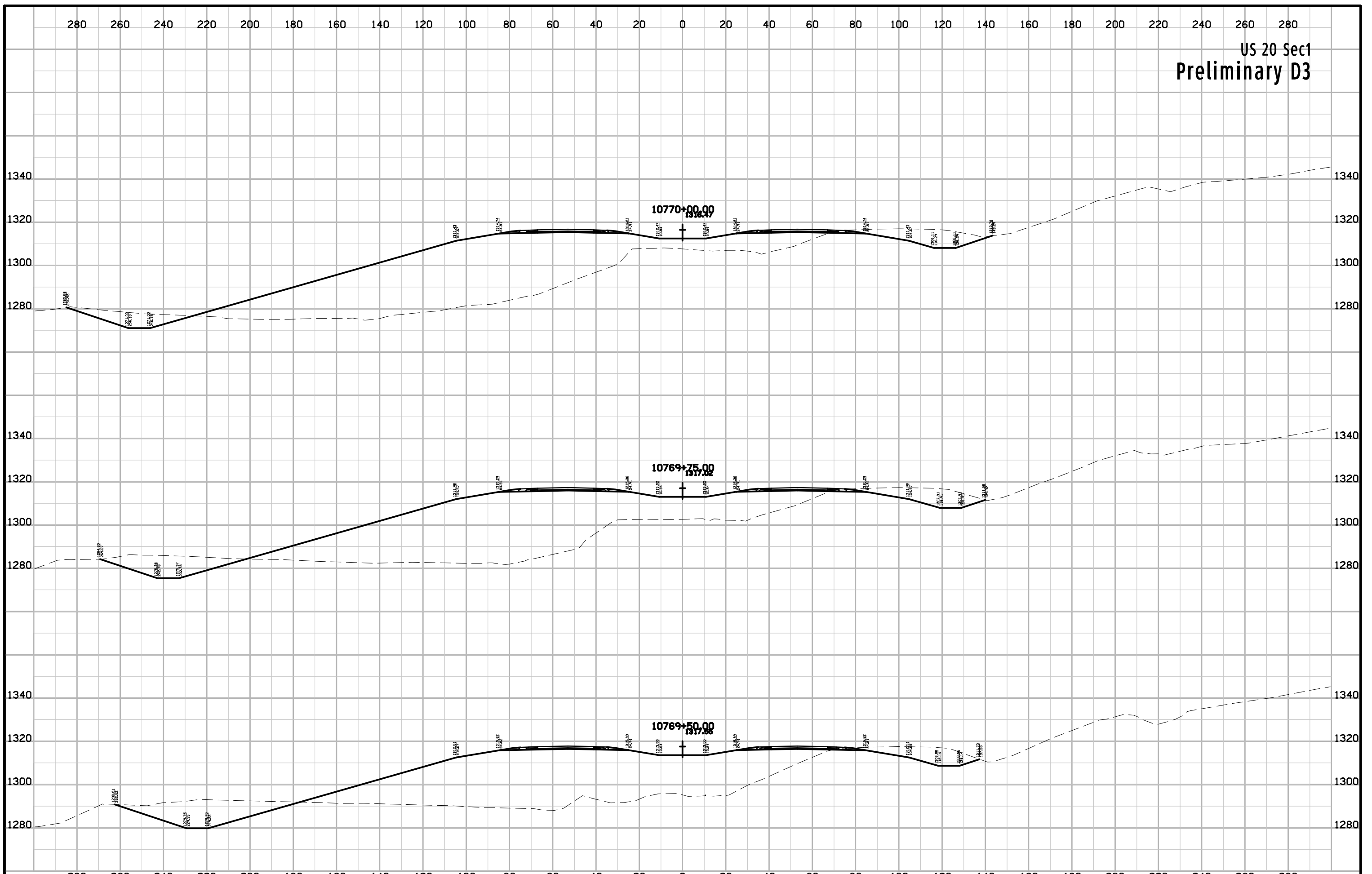
US 20 Sec1
Preliminary D3



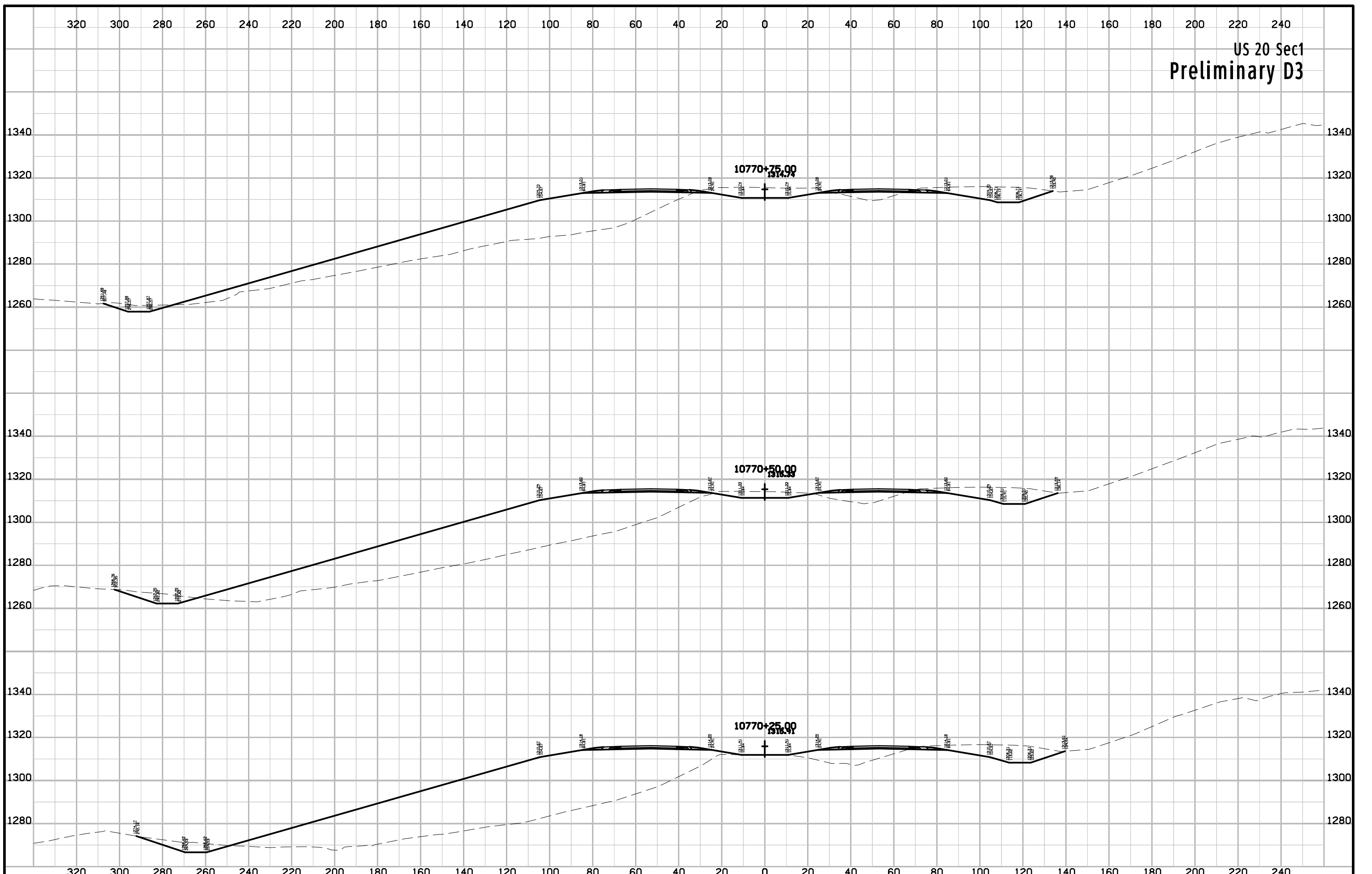


US 20 Sec1
Preliminary D3

US 20 Sec1
Preliminary D3



US 20 Sec1
Preliminary D3





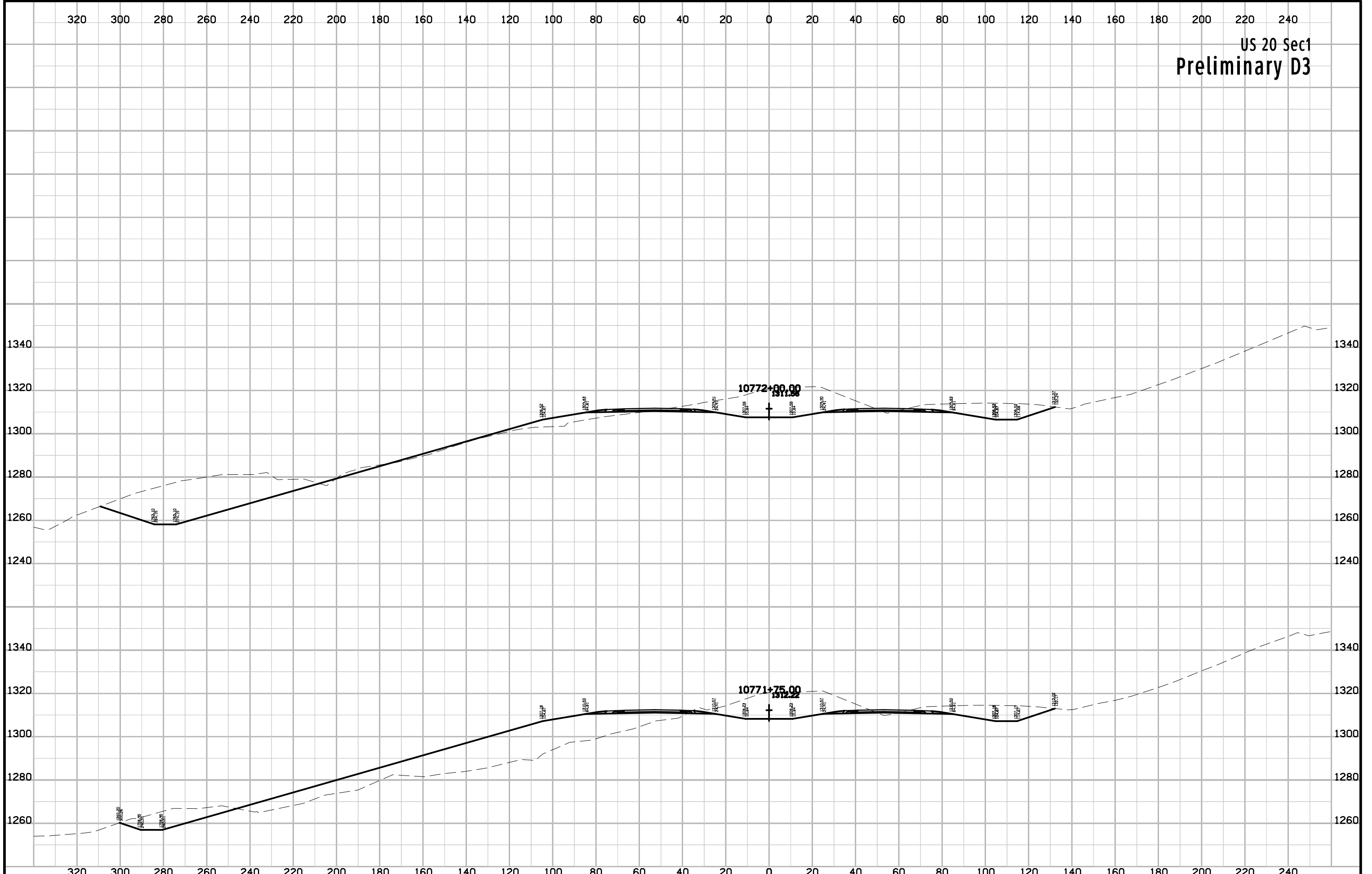
US 20 Sec1
Preliminary D3

10771+50.00

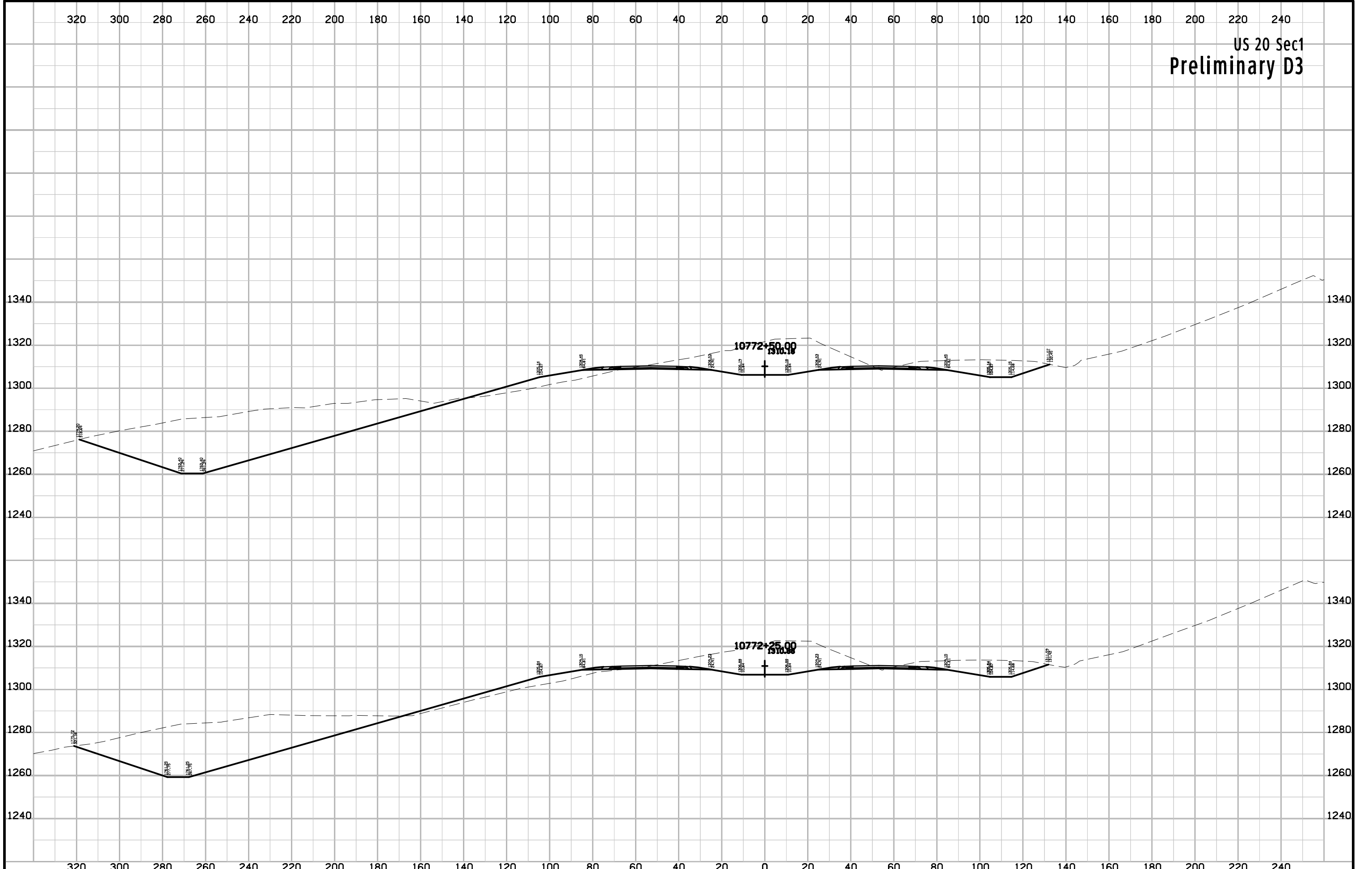
10771+25.00

10771+00.00

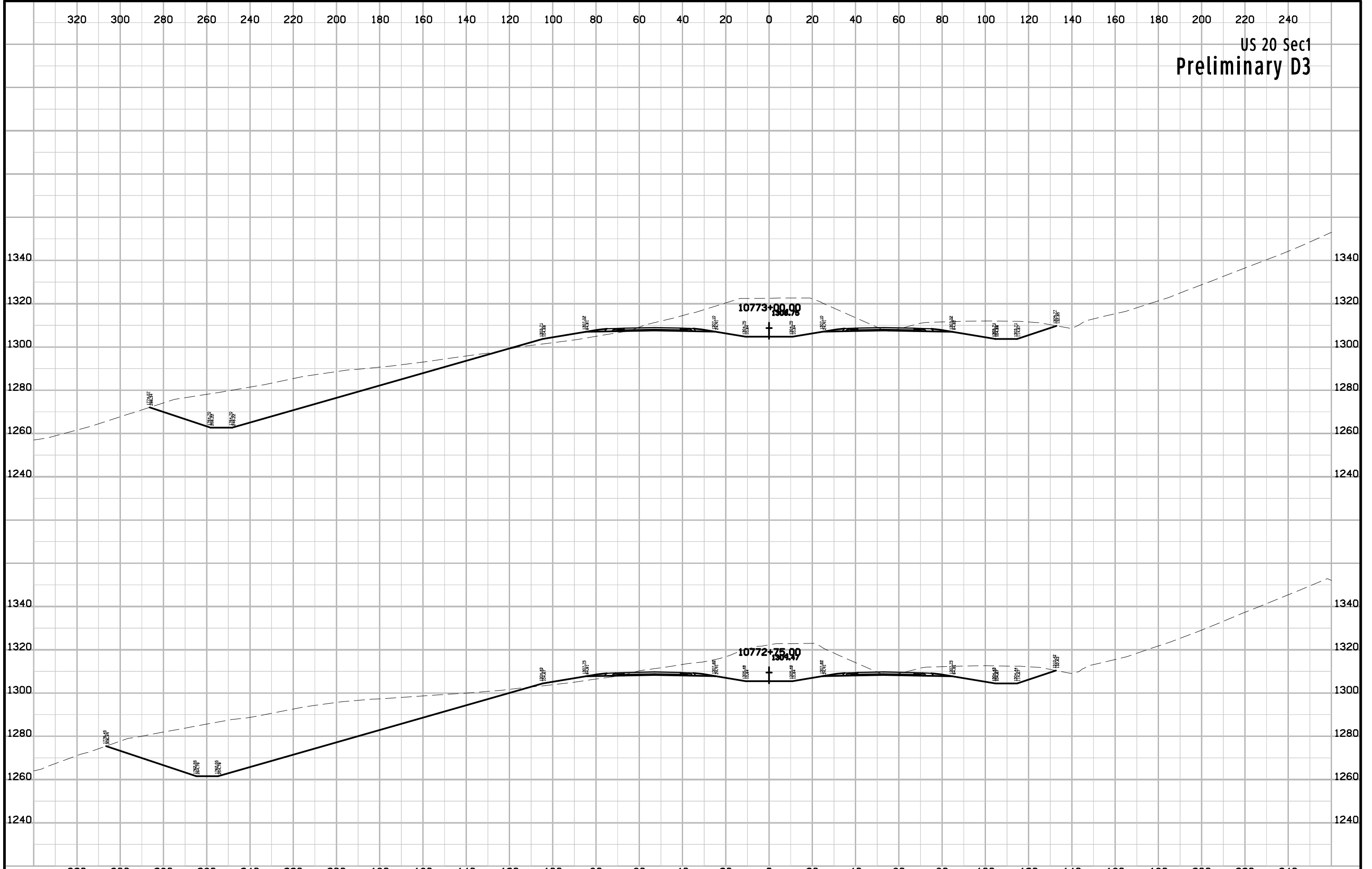
US 20 Sec1
Preliminary D3



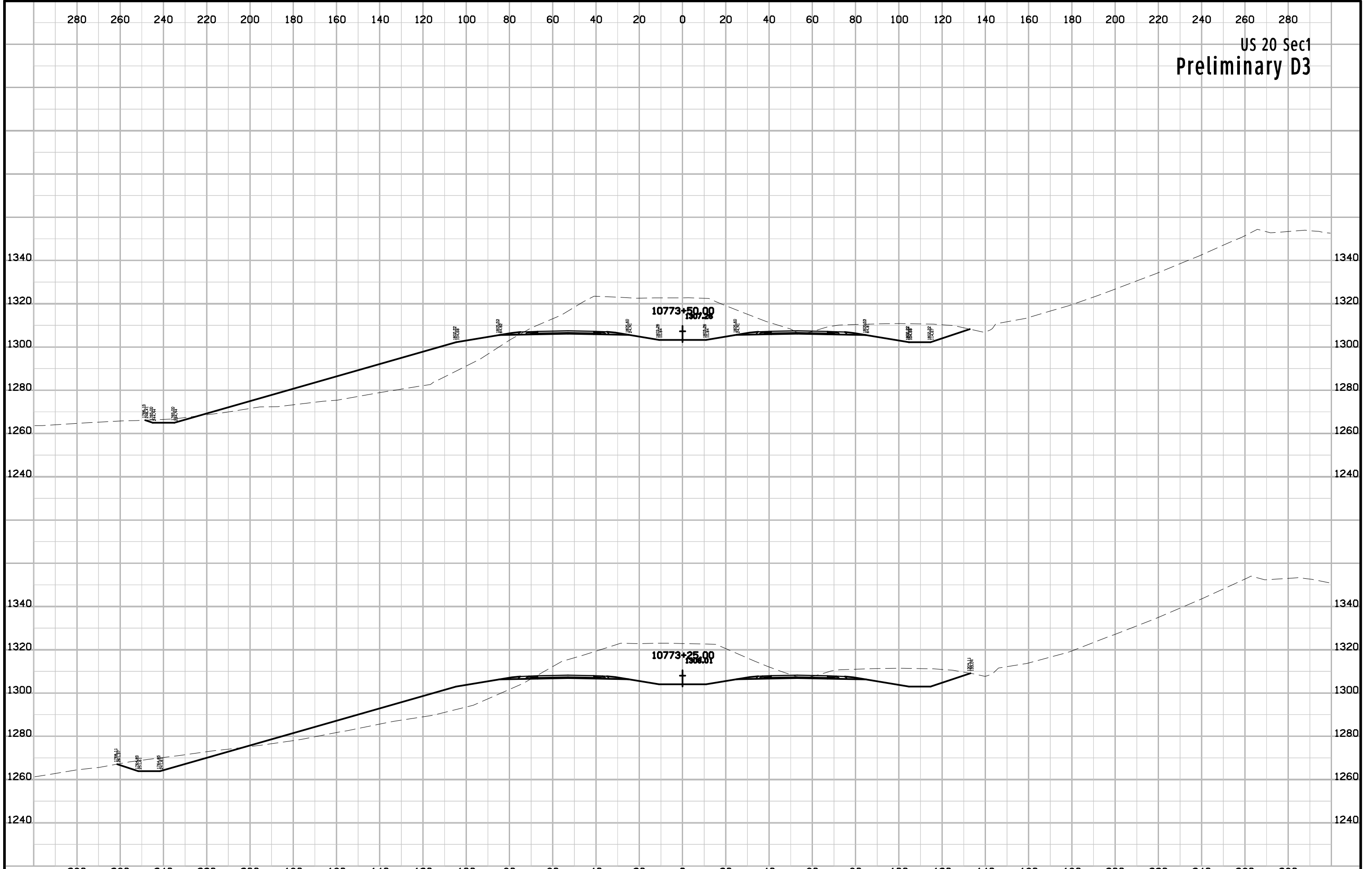
US 20 Sec1
Preliminary D3



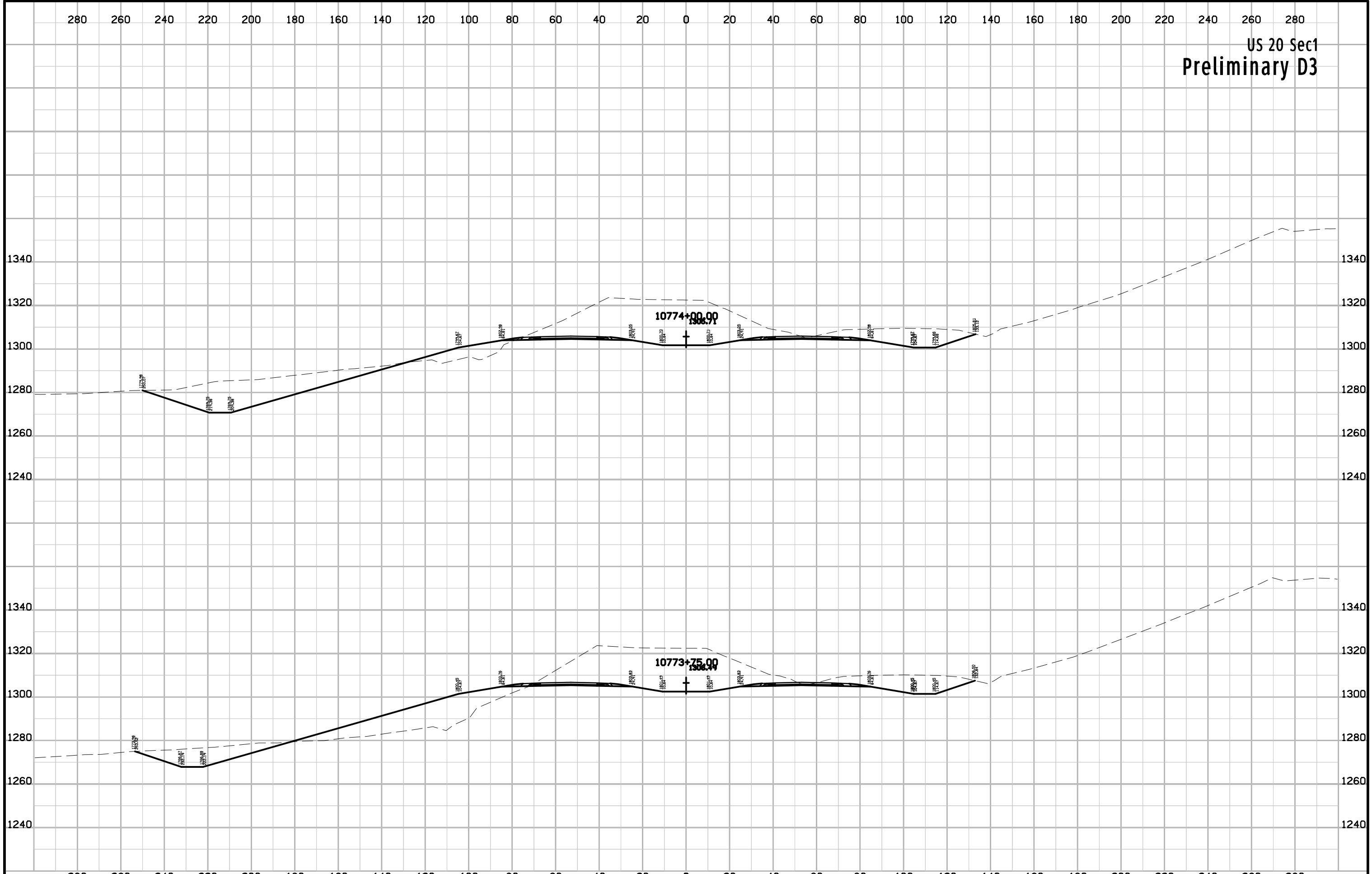
US 20 Sec1
Preliminary D3



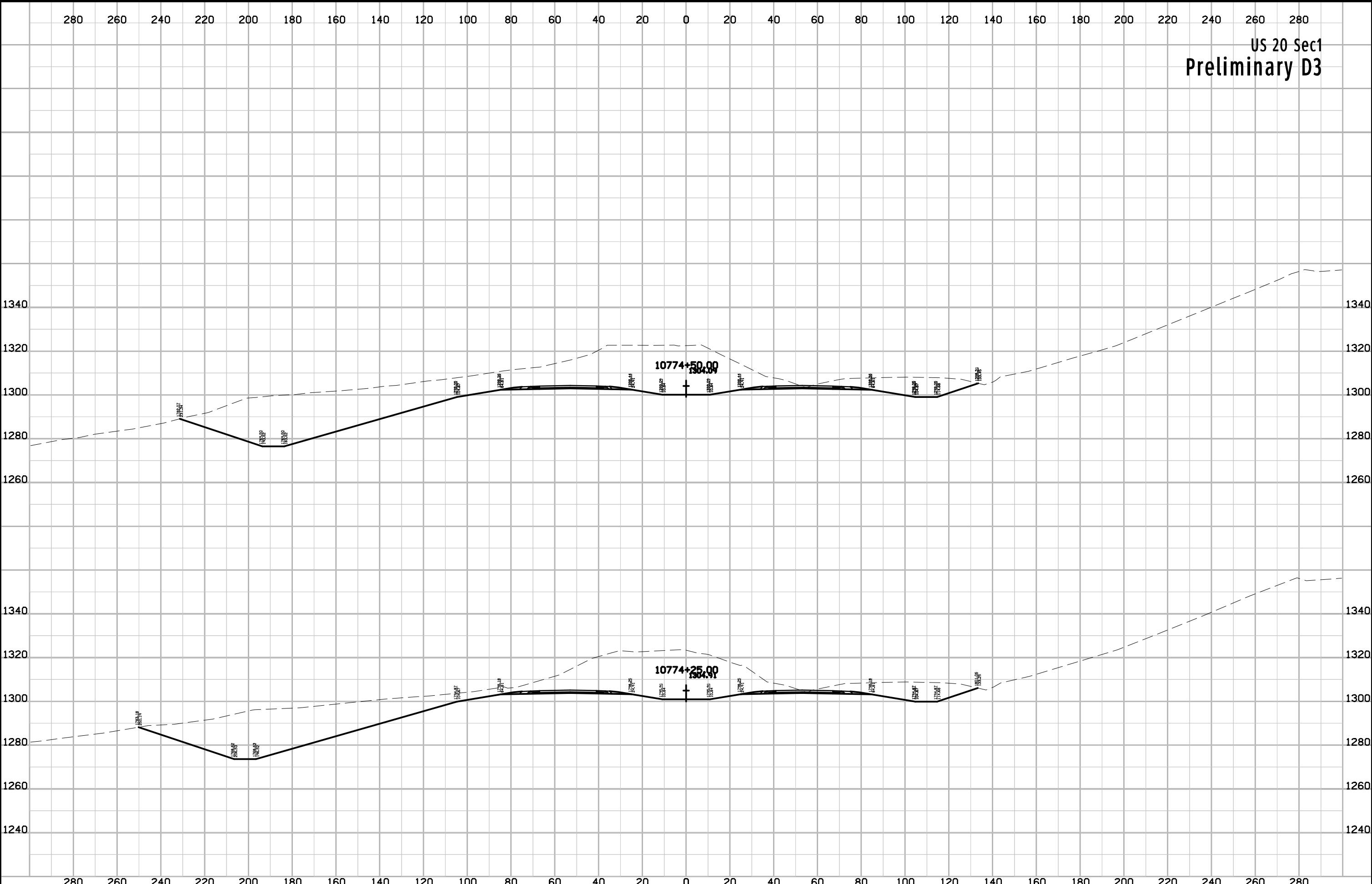
US 20 Sec1
Preliminary D3

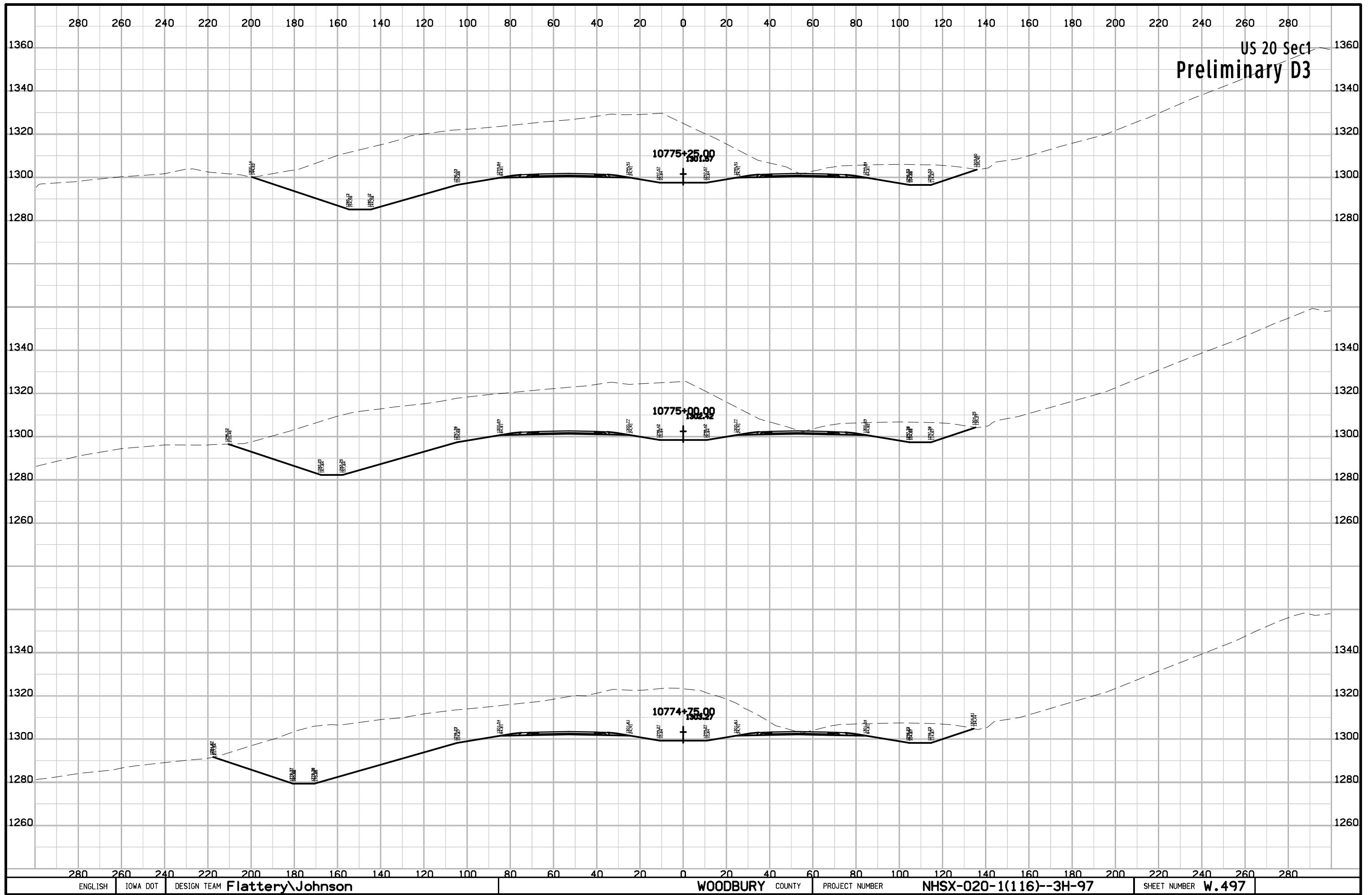


US 20 Sec1
Preliminary D3

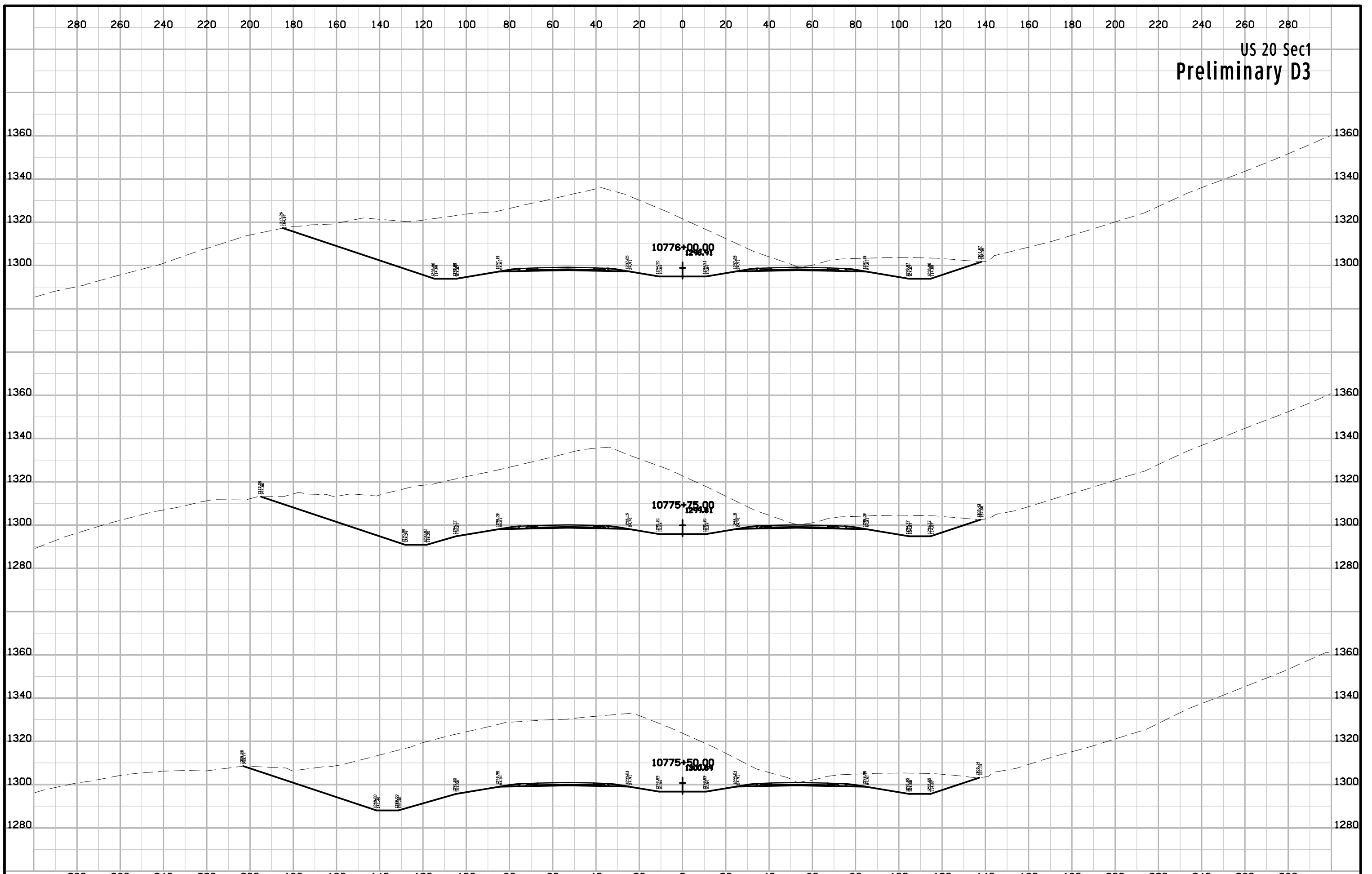


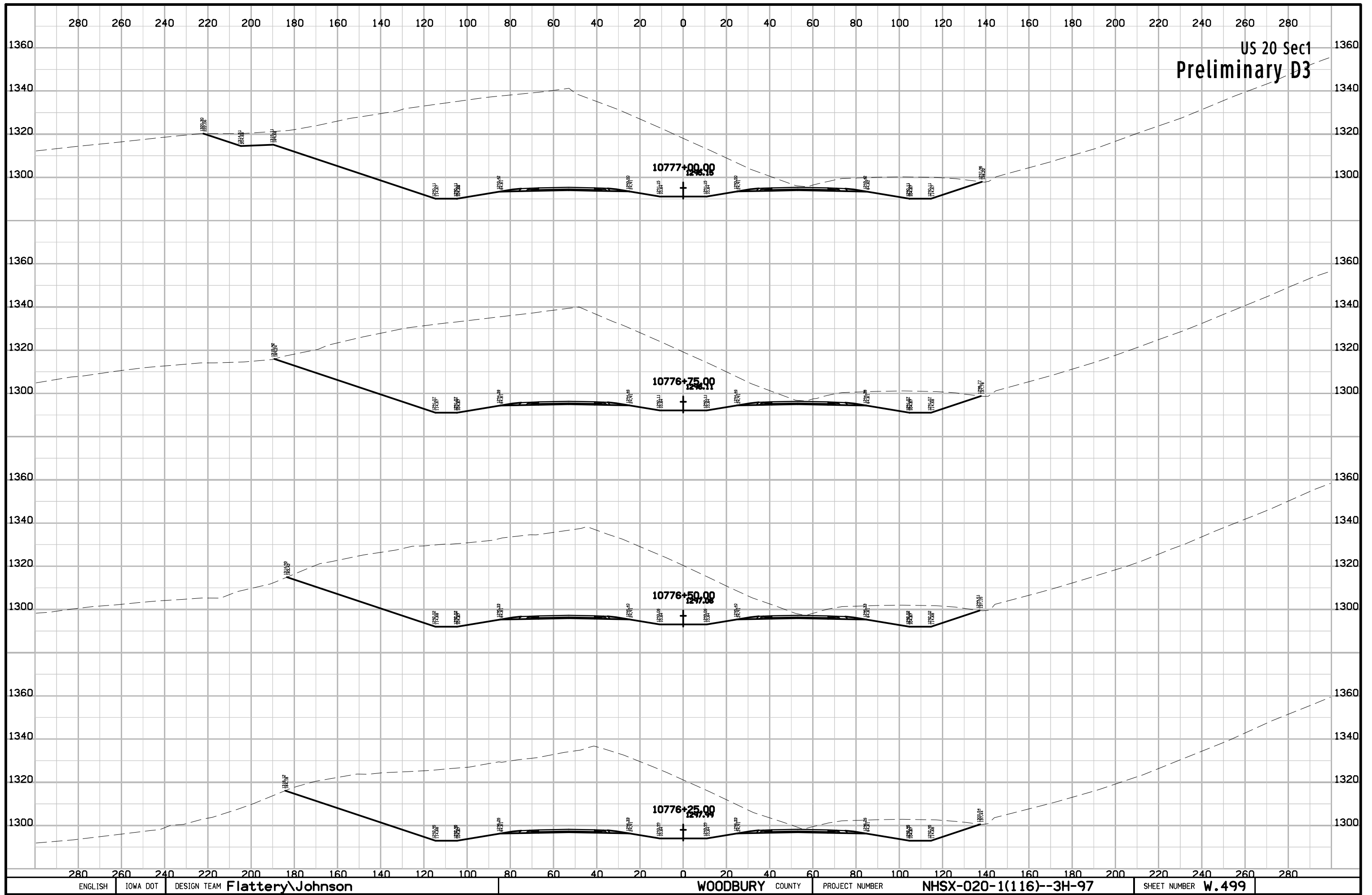
US 20 Sec1
Preliminary D3



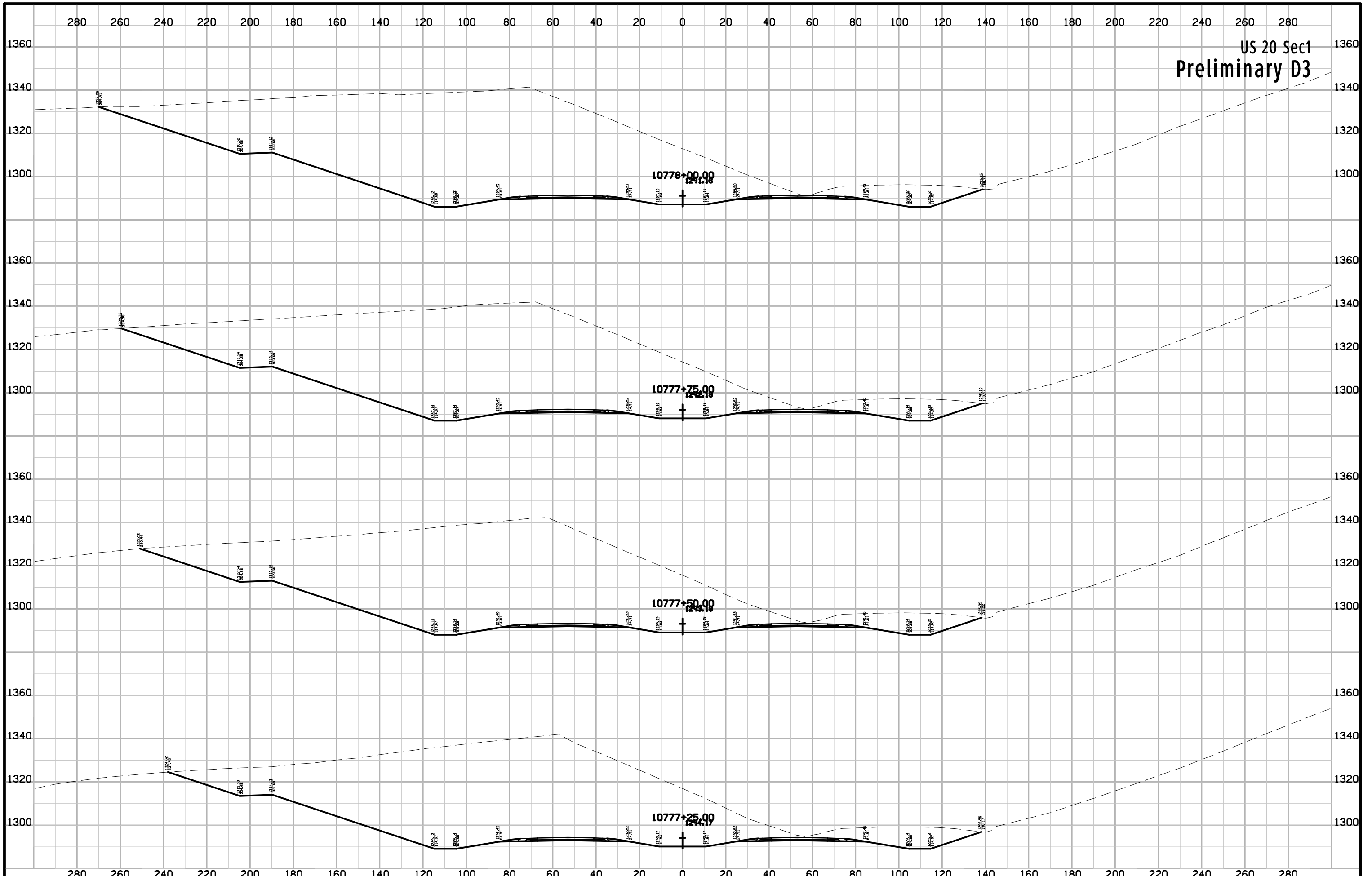


US 20 Sec1
Preliminary D3

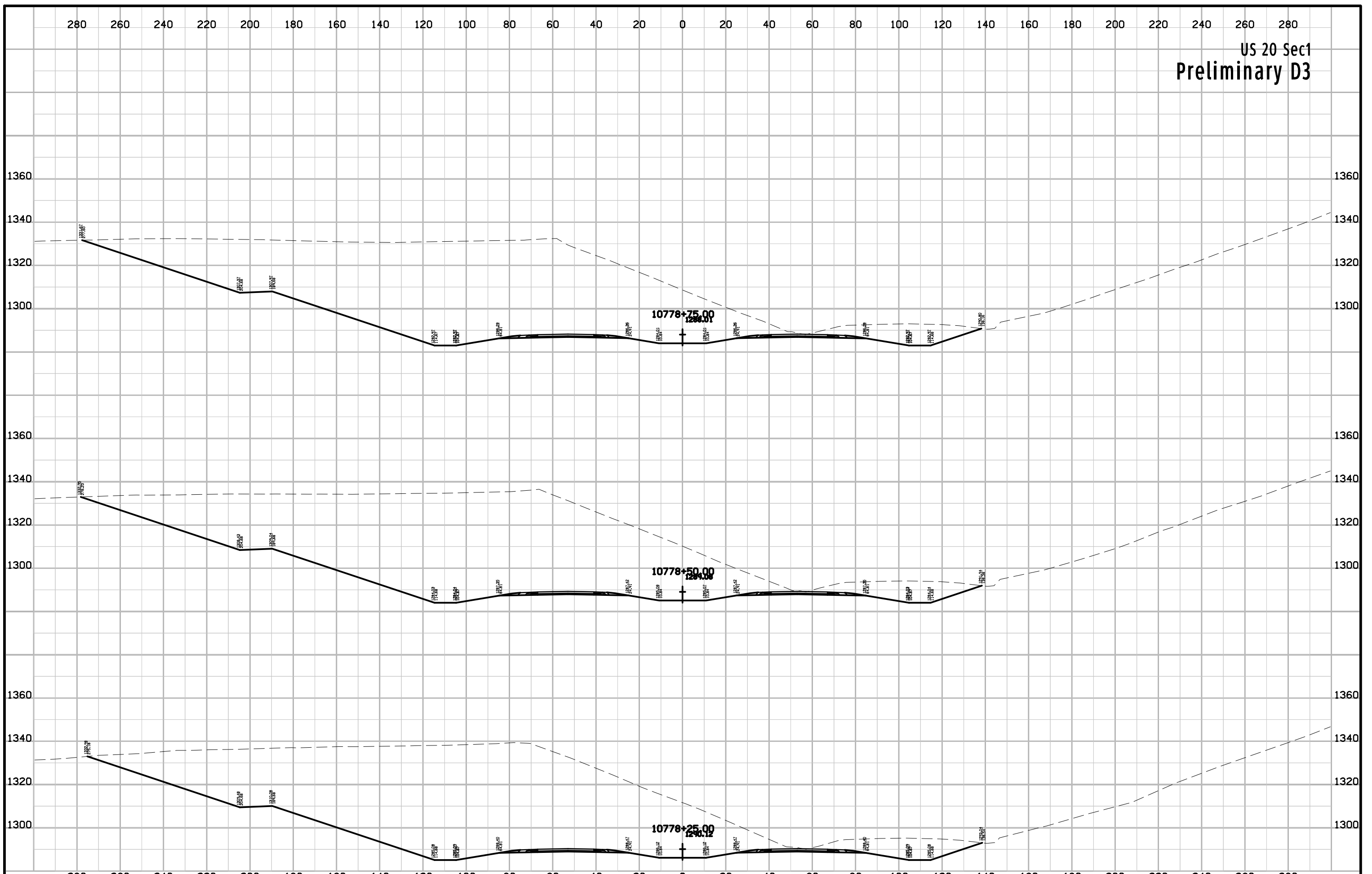




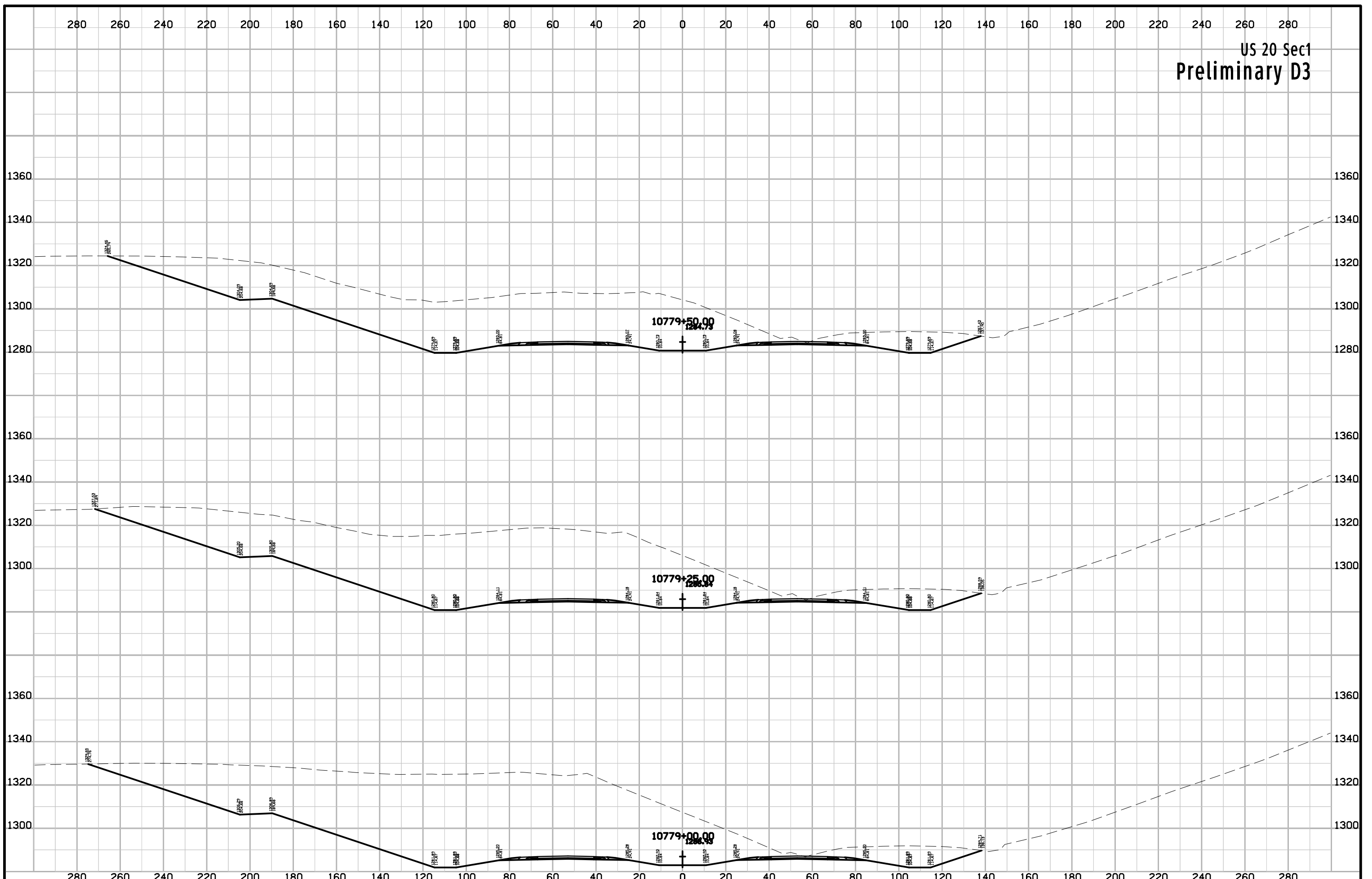
US 20 Sec1
Preliminary D3



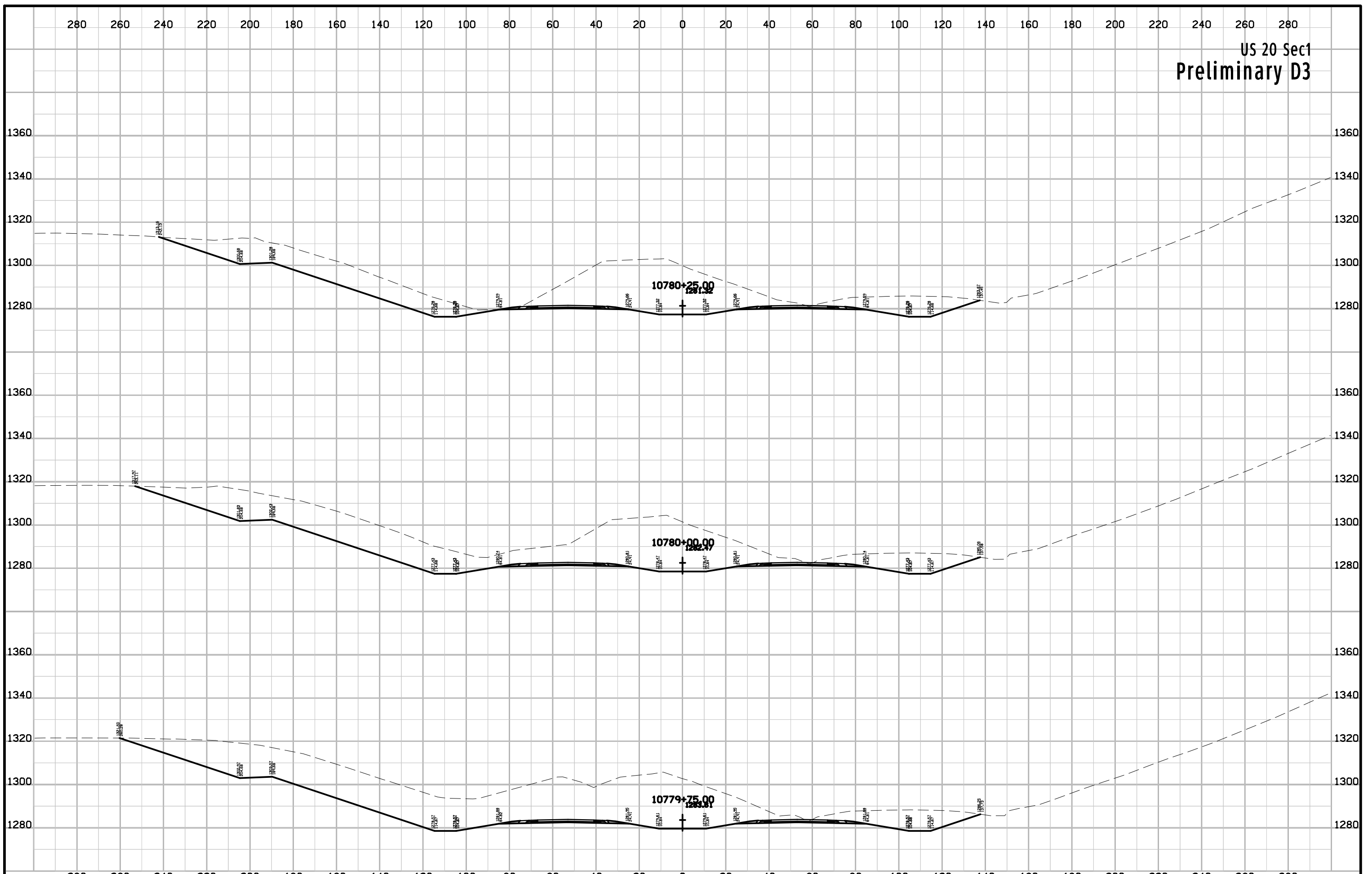
US 20 Sec1
Preliminary D3



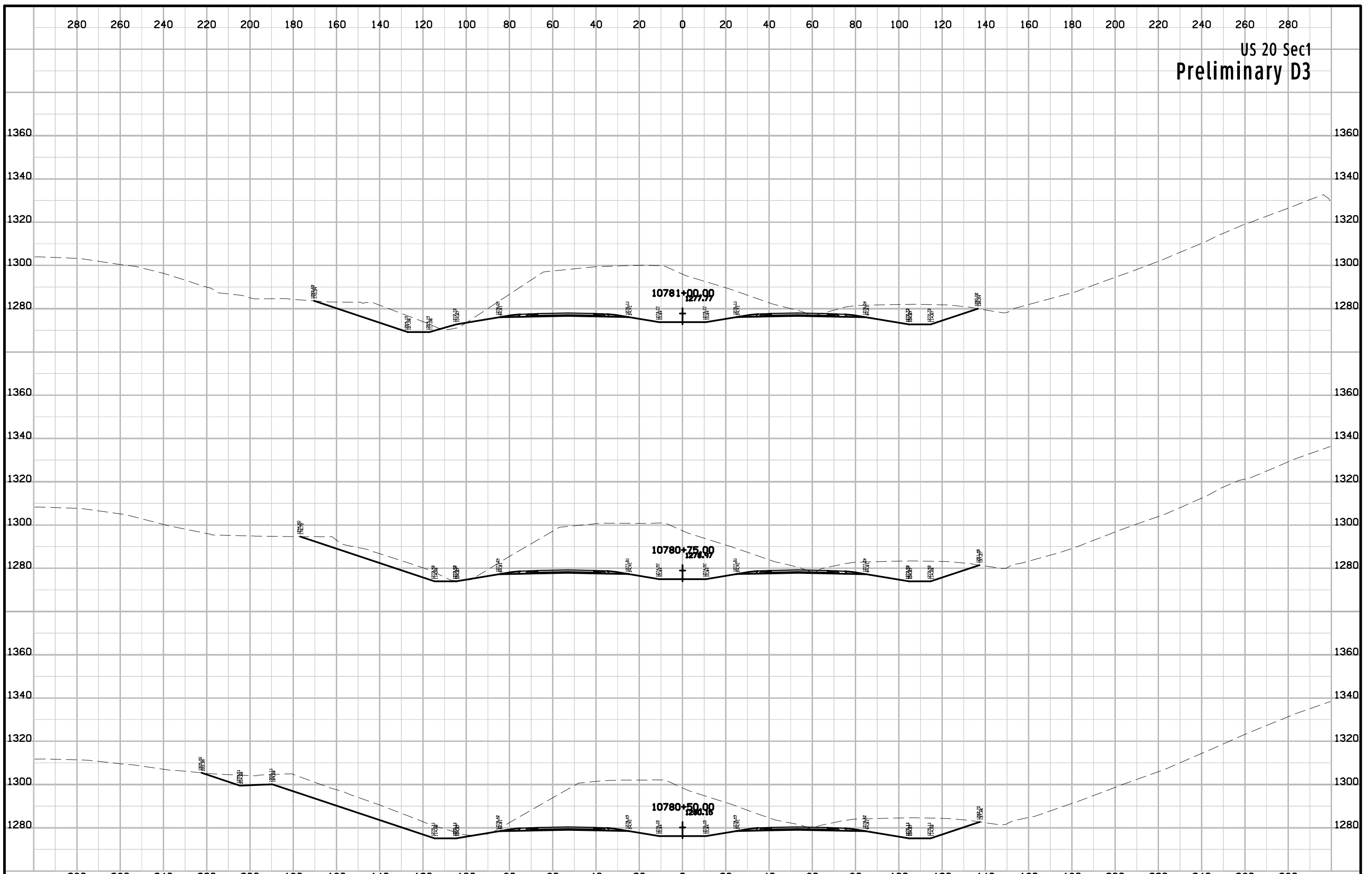
US 20 Sec1
Preliminary D3



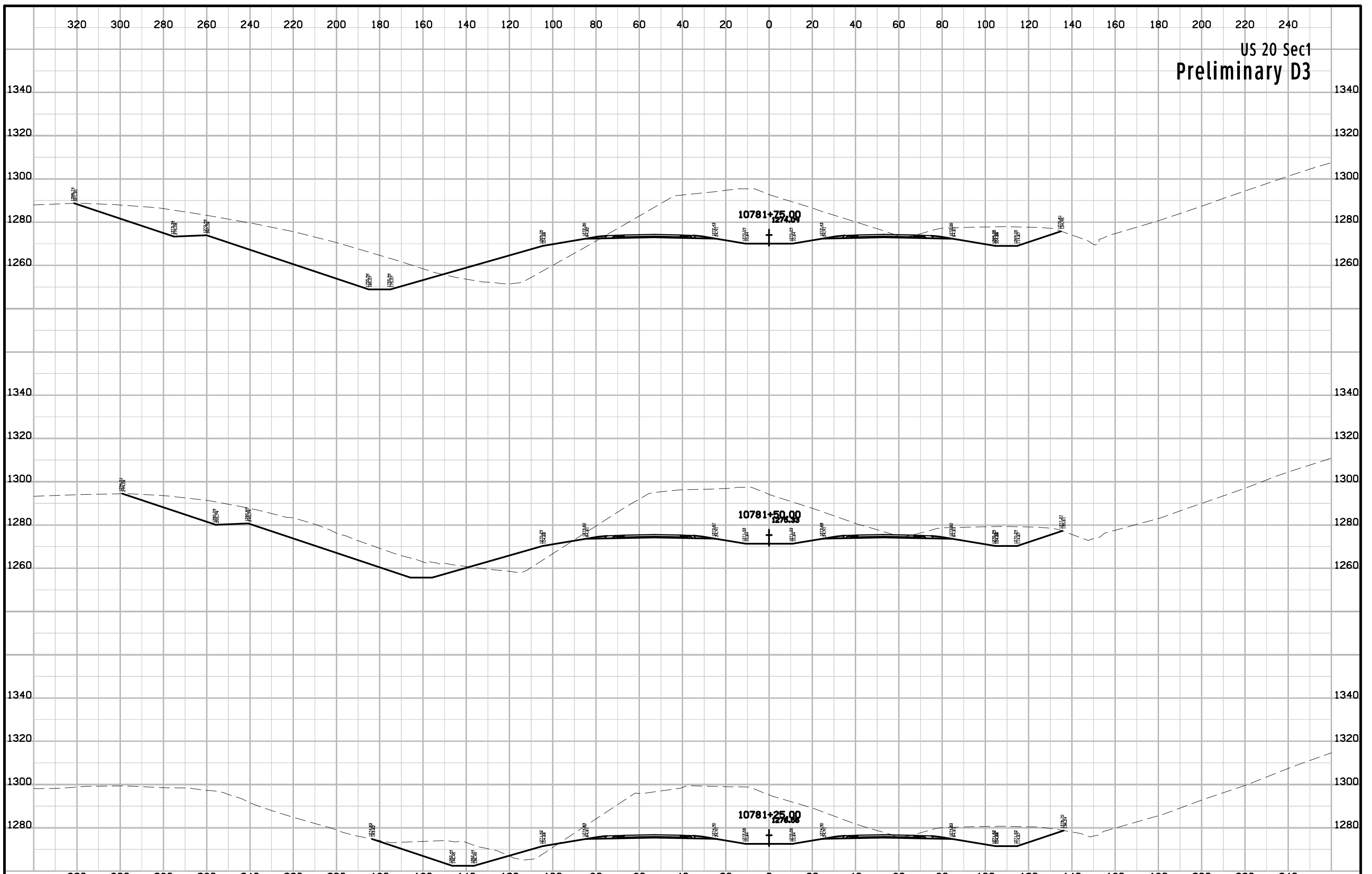
US 20 Sec1
Preliminary D3



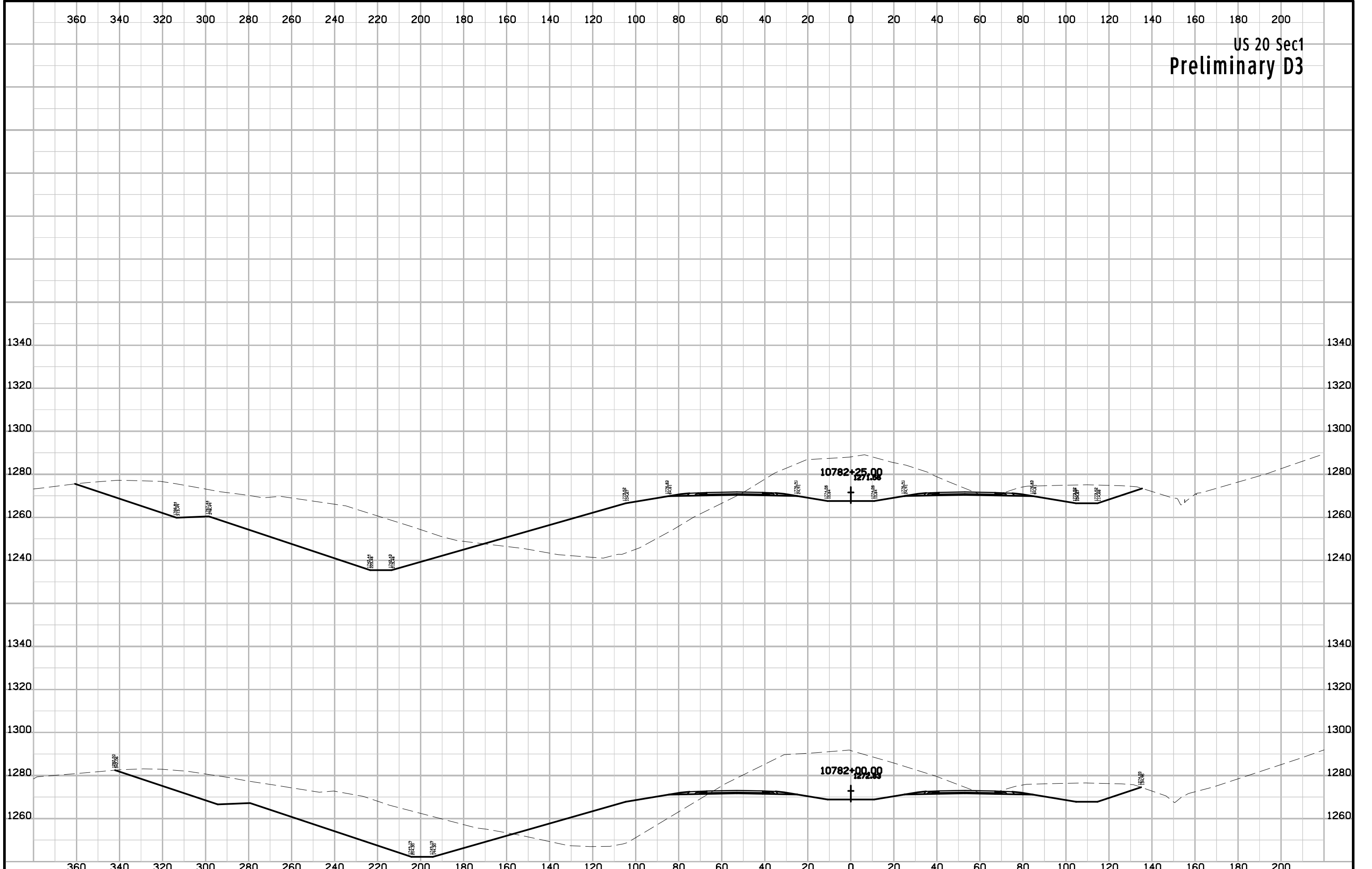
US 20 Sec1
Preliminary D3



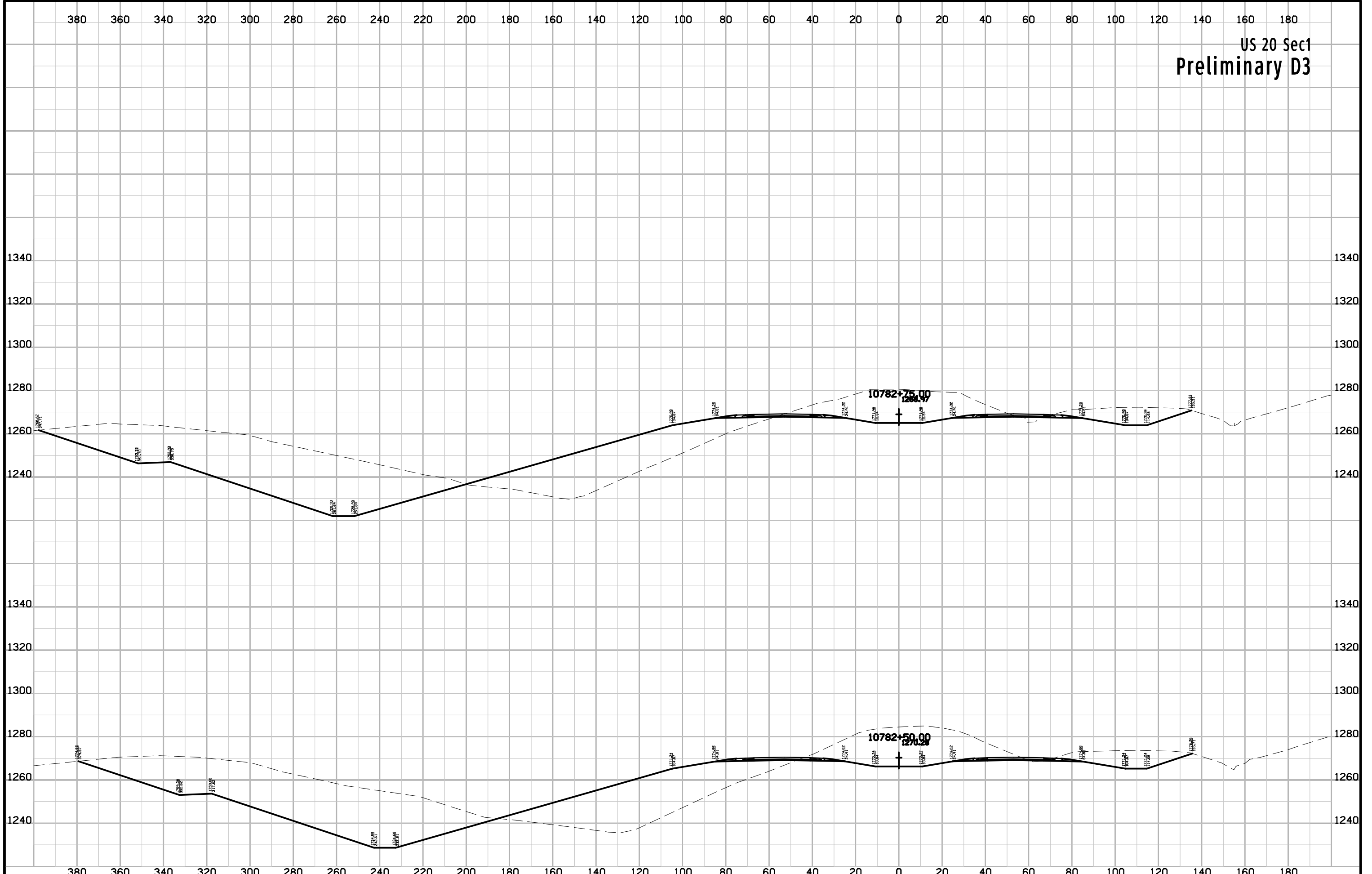
US 20 Sec1
Preliminary D3



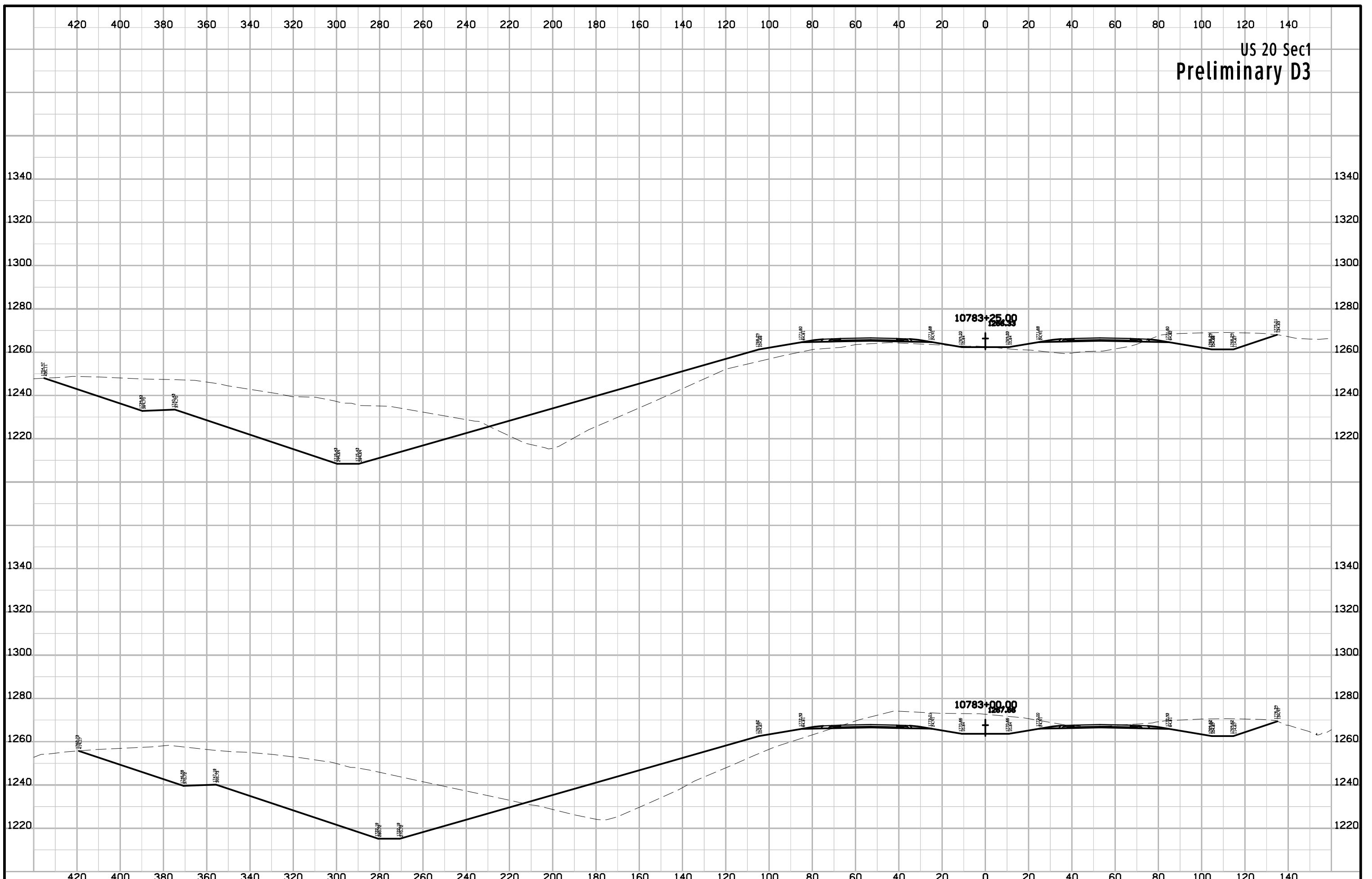
US 20 Sec1
Preliminary D3



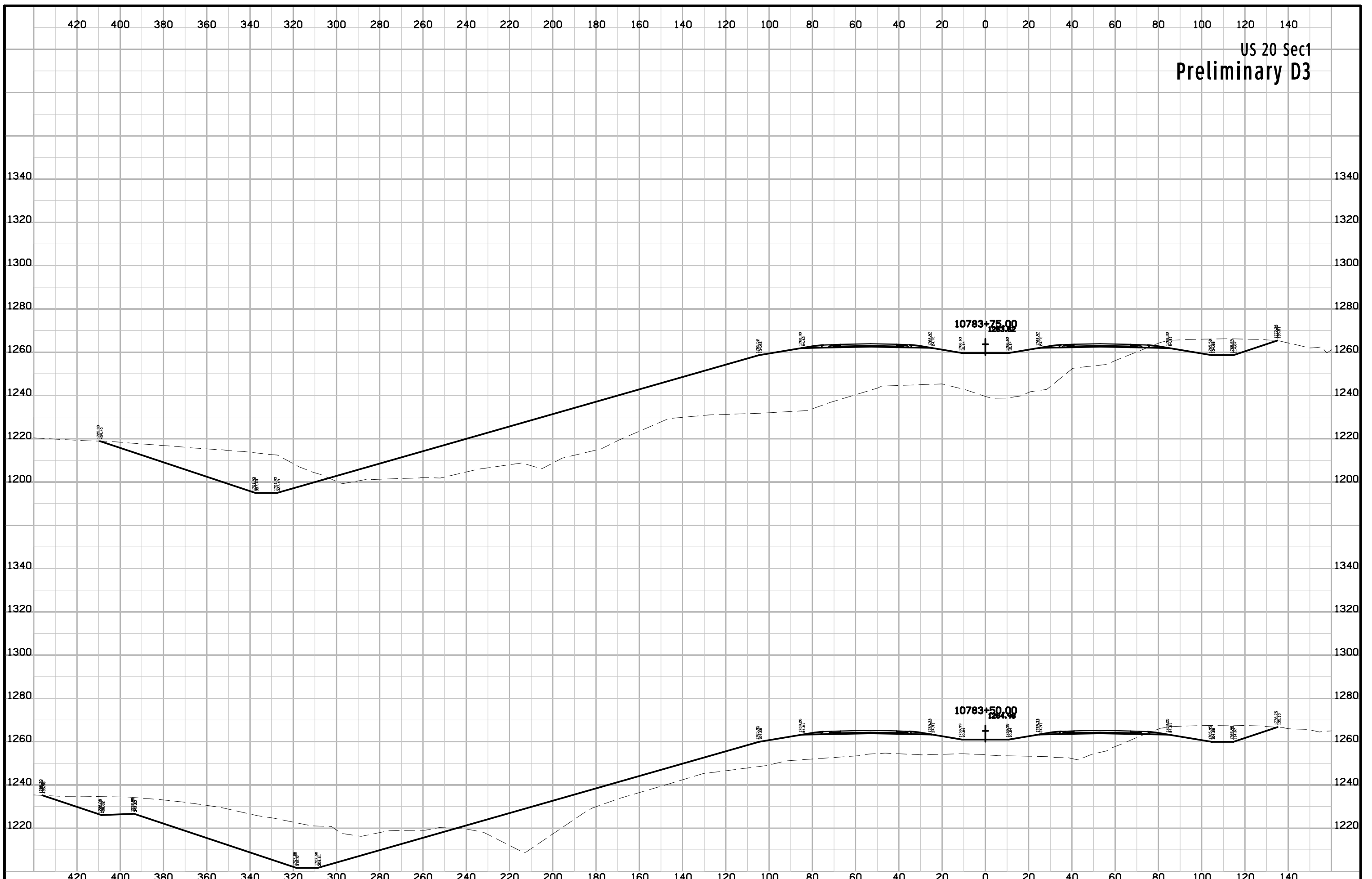
US 20 Sec1
Preliminary D3



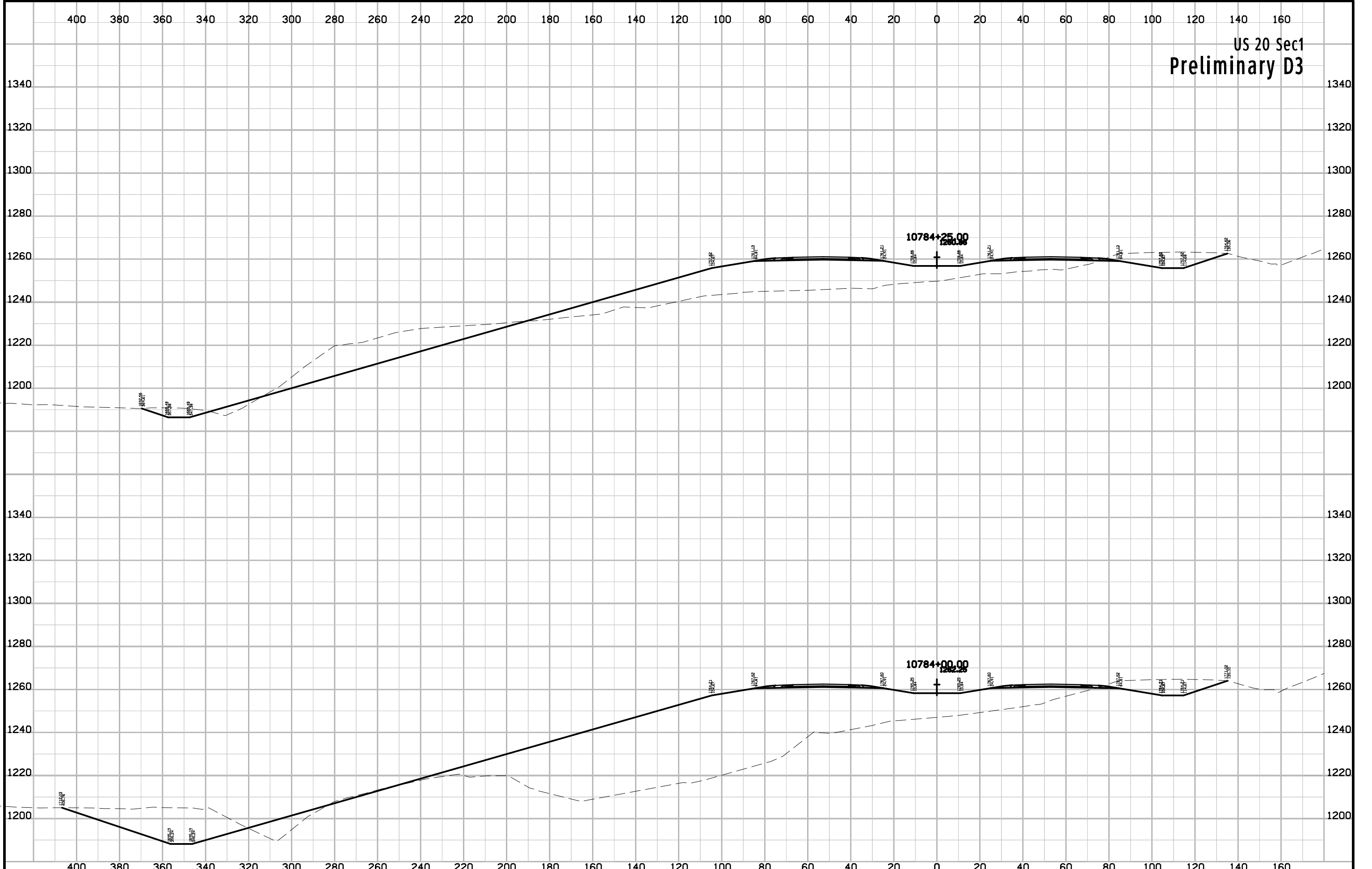
US 20 Sec1
Preliminary D3



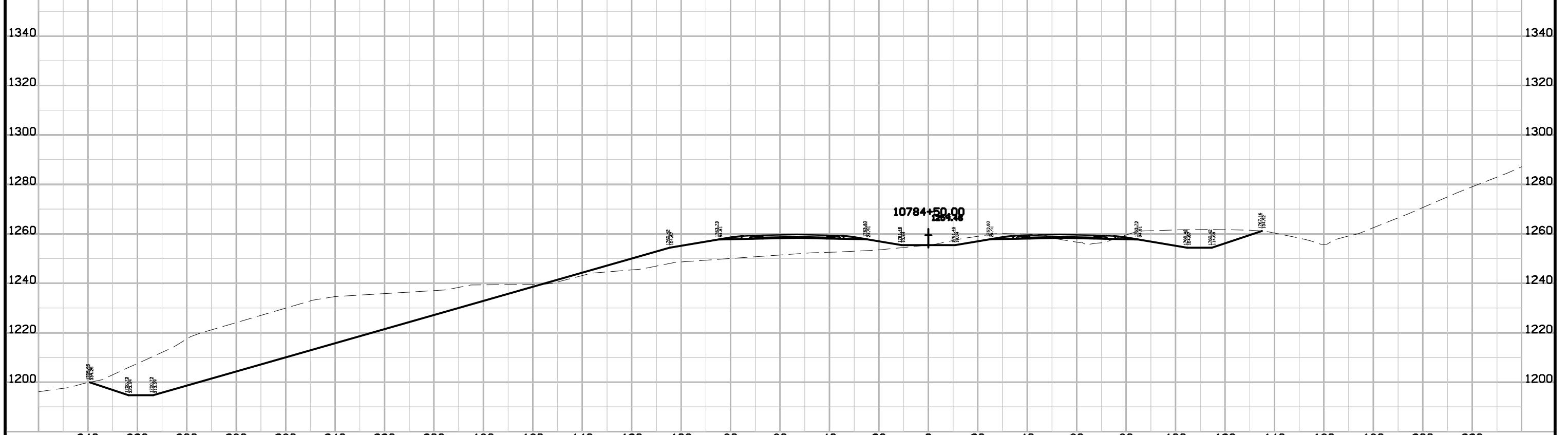
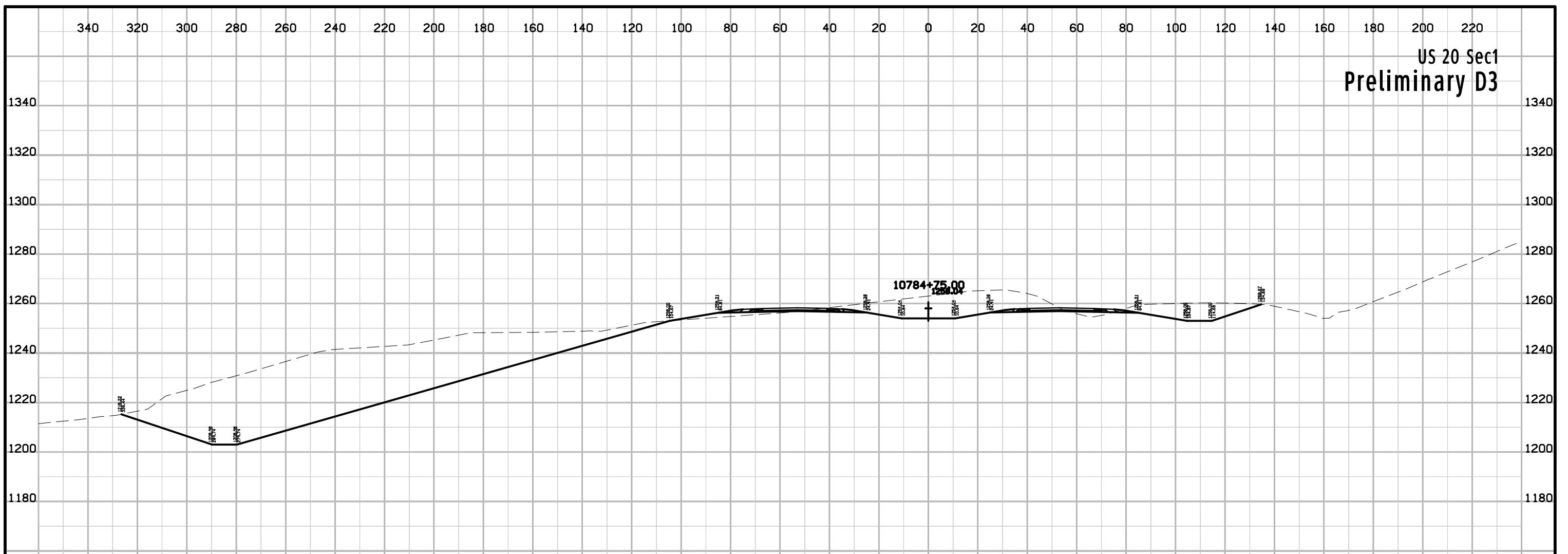
US 20 Sec1
Preliminary D3



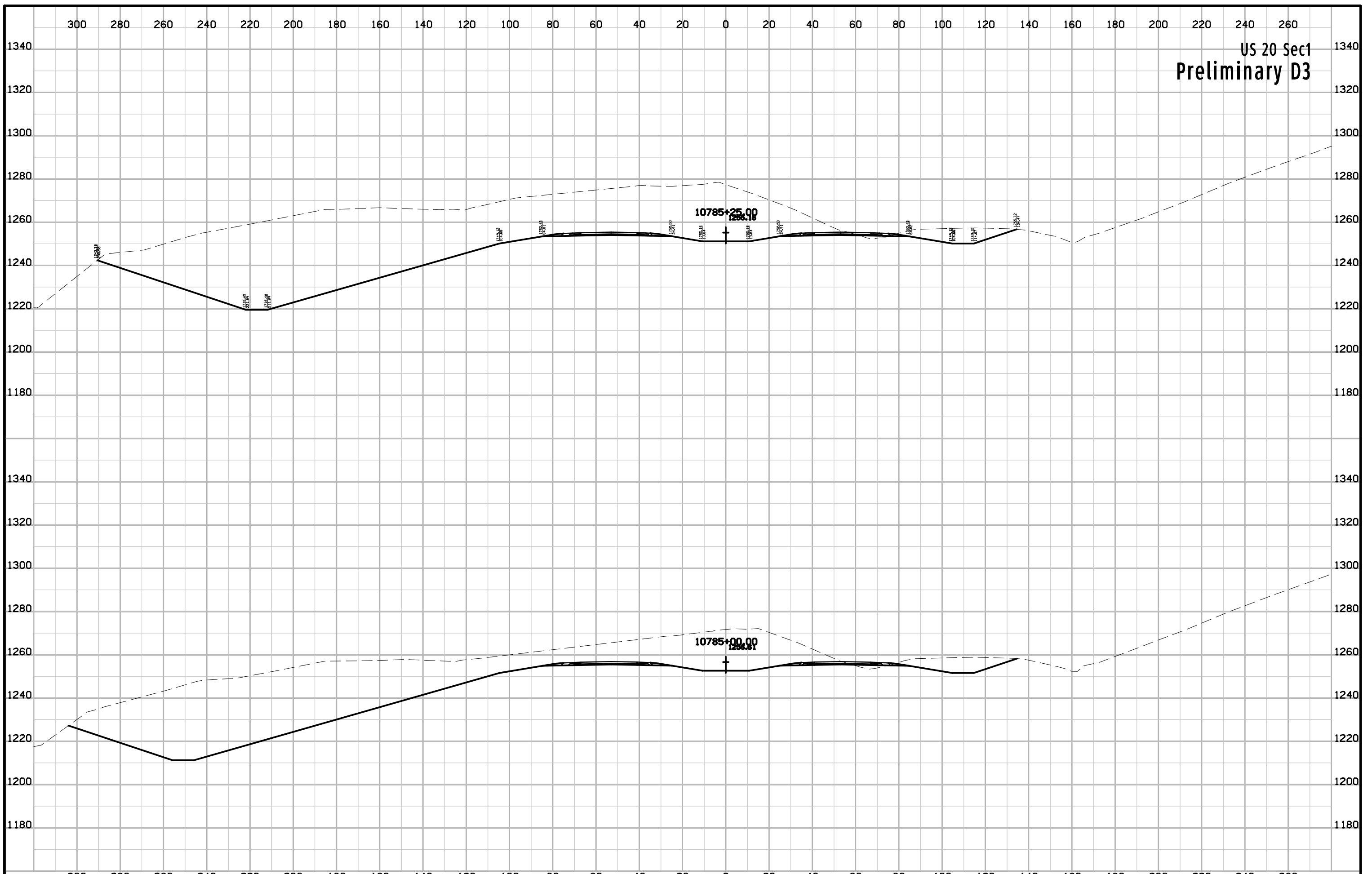
US 20 Sec1
Preliminary D3



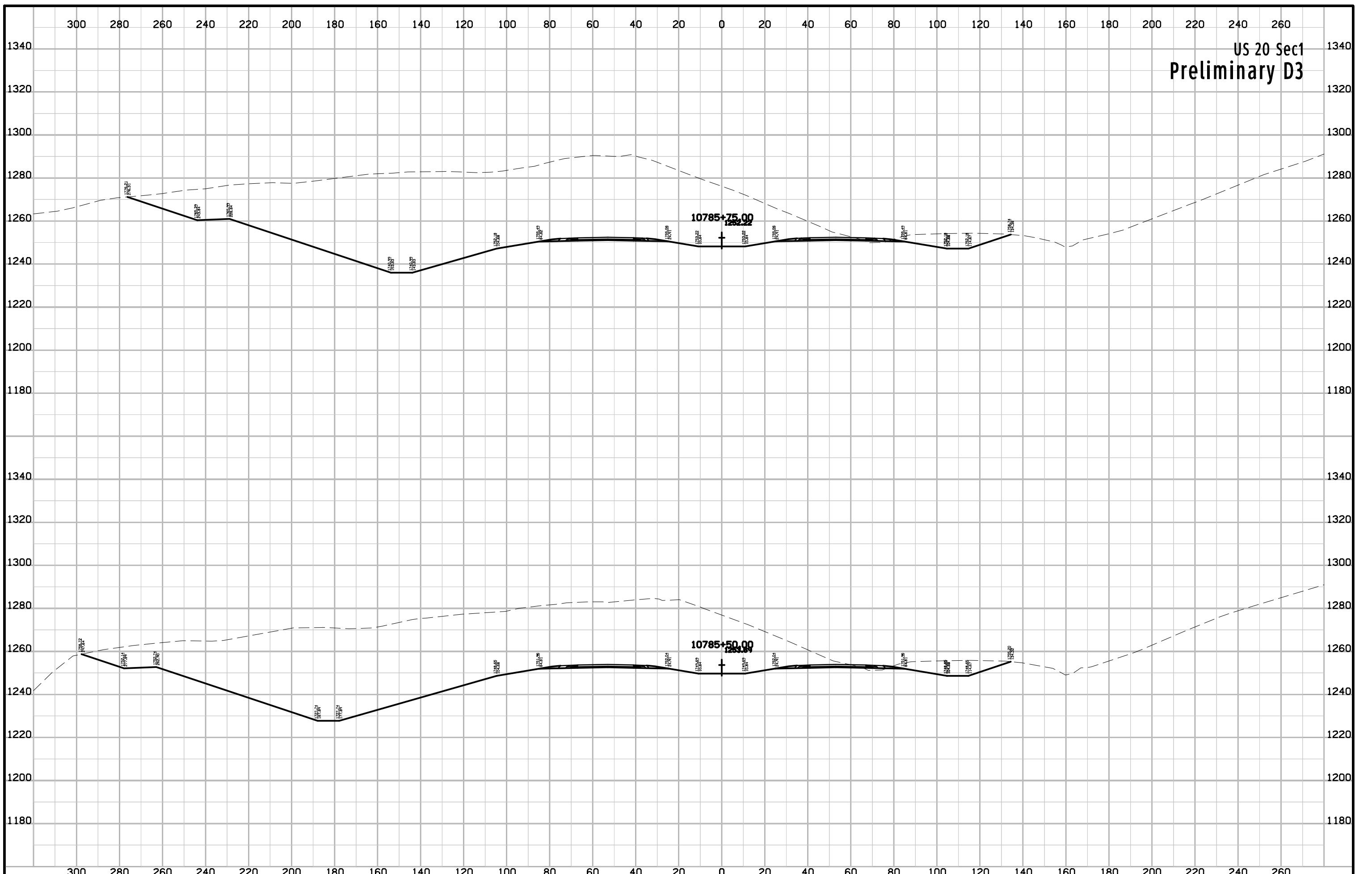
US 20 Sec1
Preliminary D3



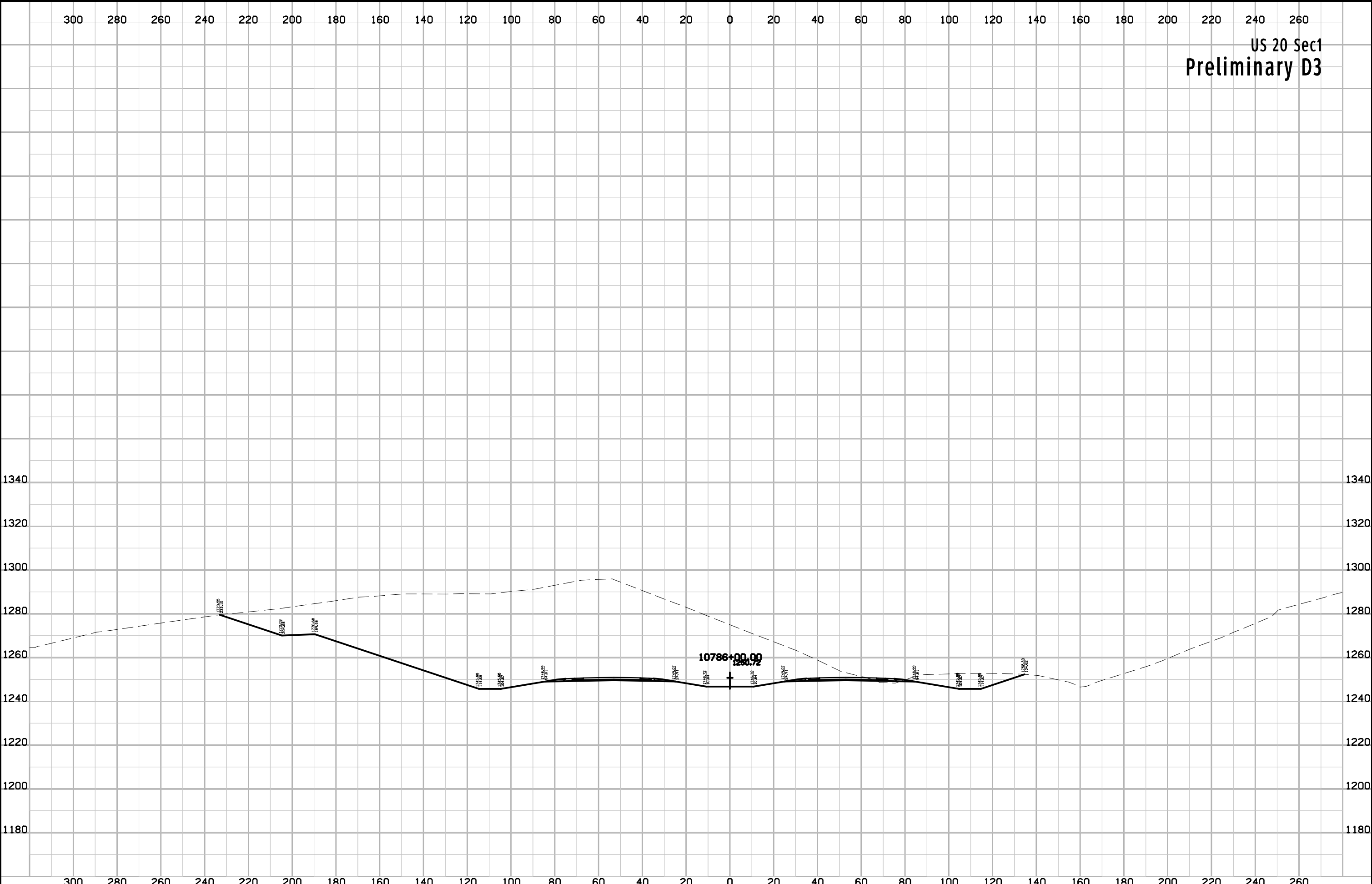
US 20 Sec1
Preliminary D3



US 20 Sec1
Preliminary D3



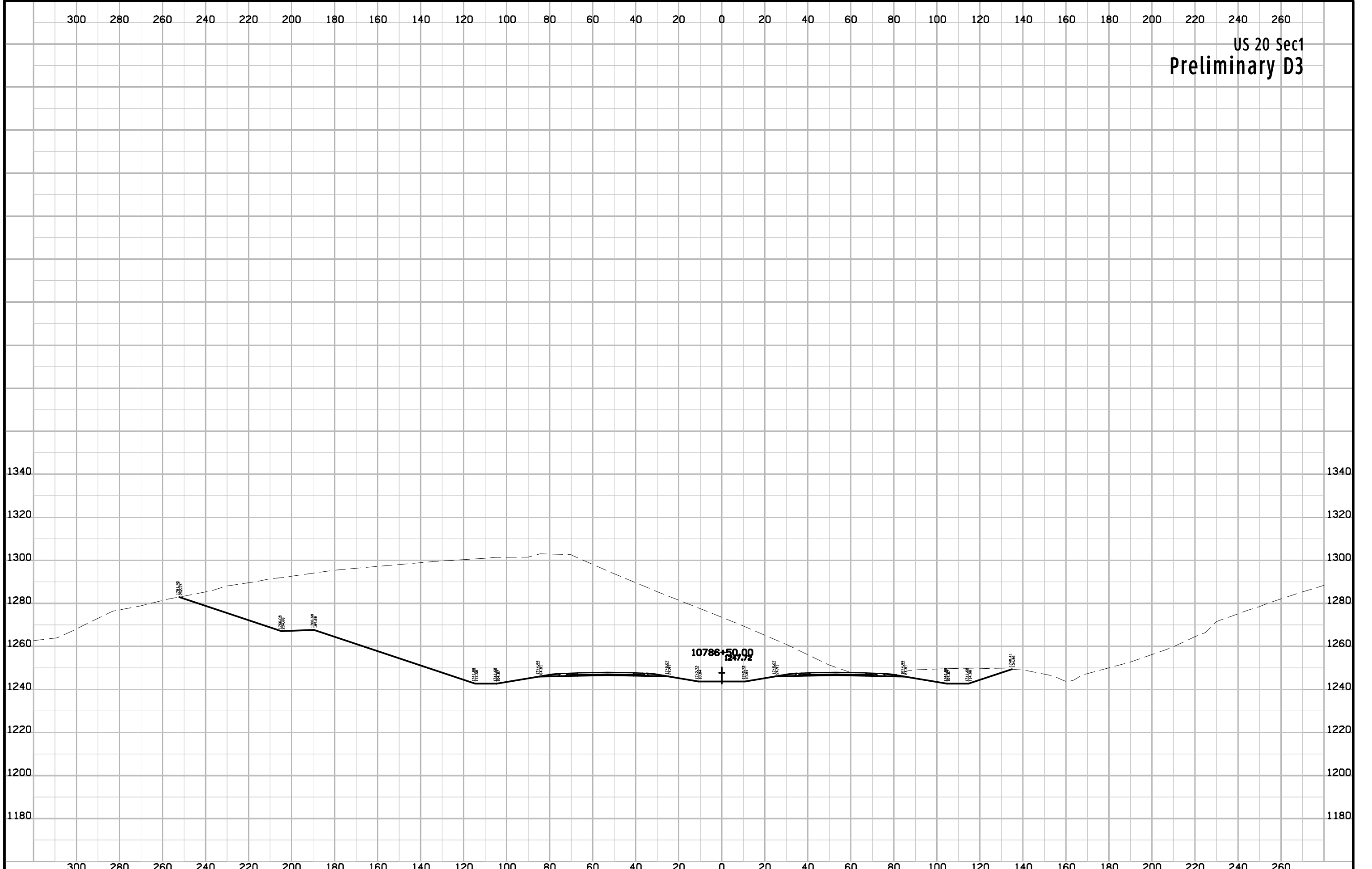
US 20 Sec1
Preliminary D3



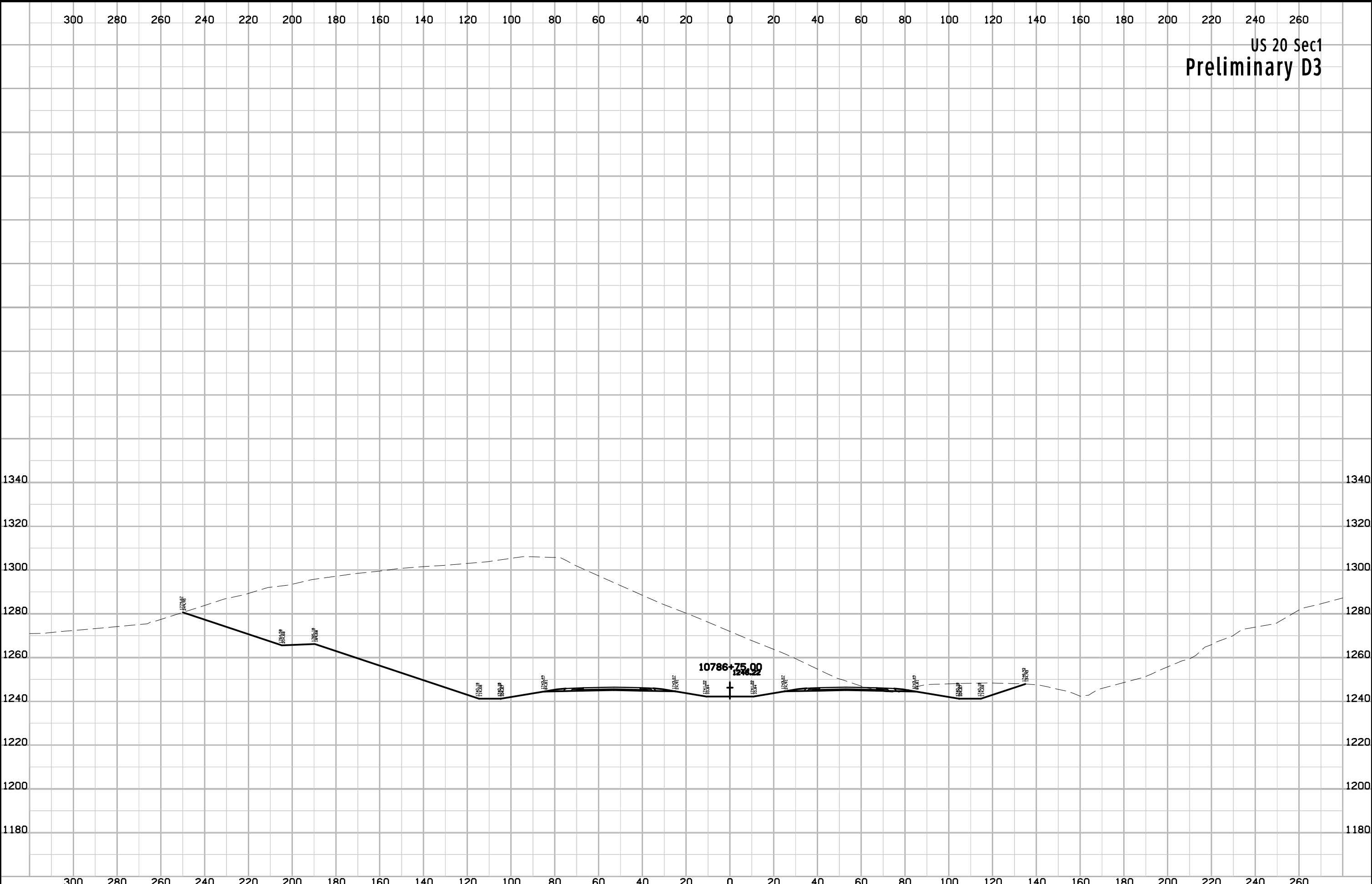
US 20 Sec1
Preliminary D3



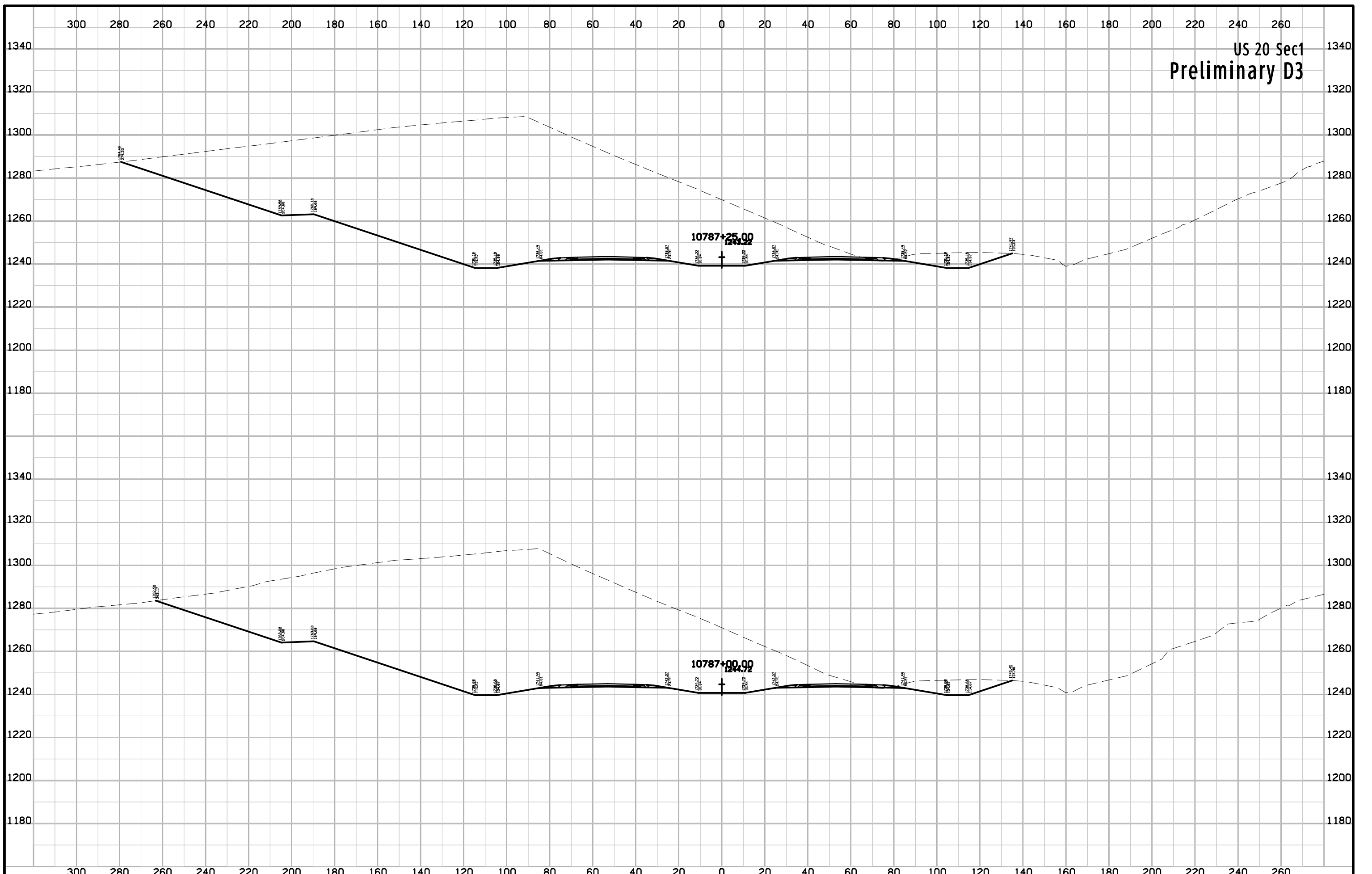
US 20 Sec1
Preliminary D3



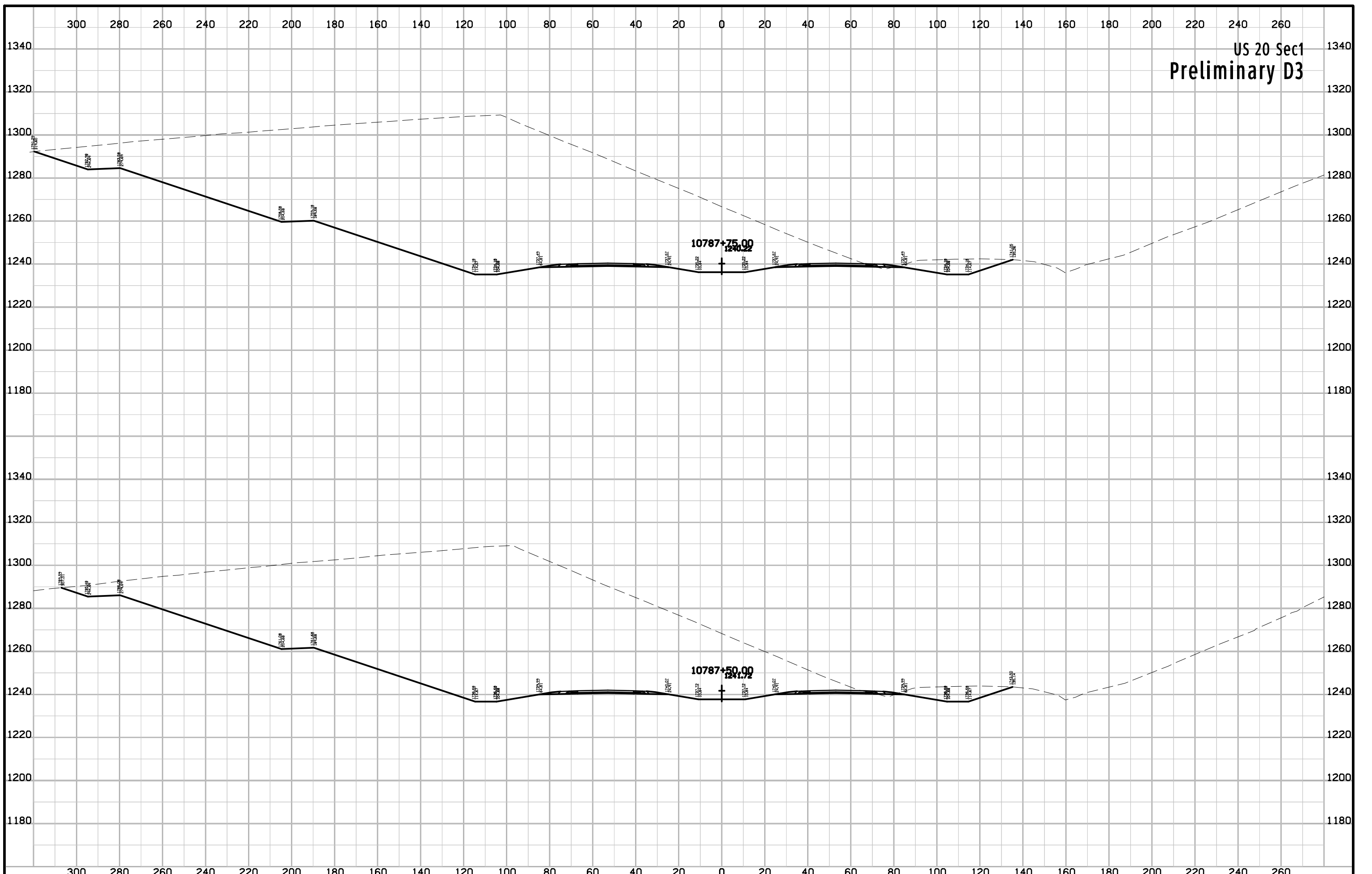
US 20 Sec1
Preliminary D3



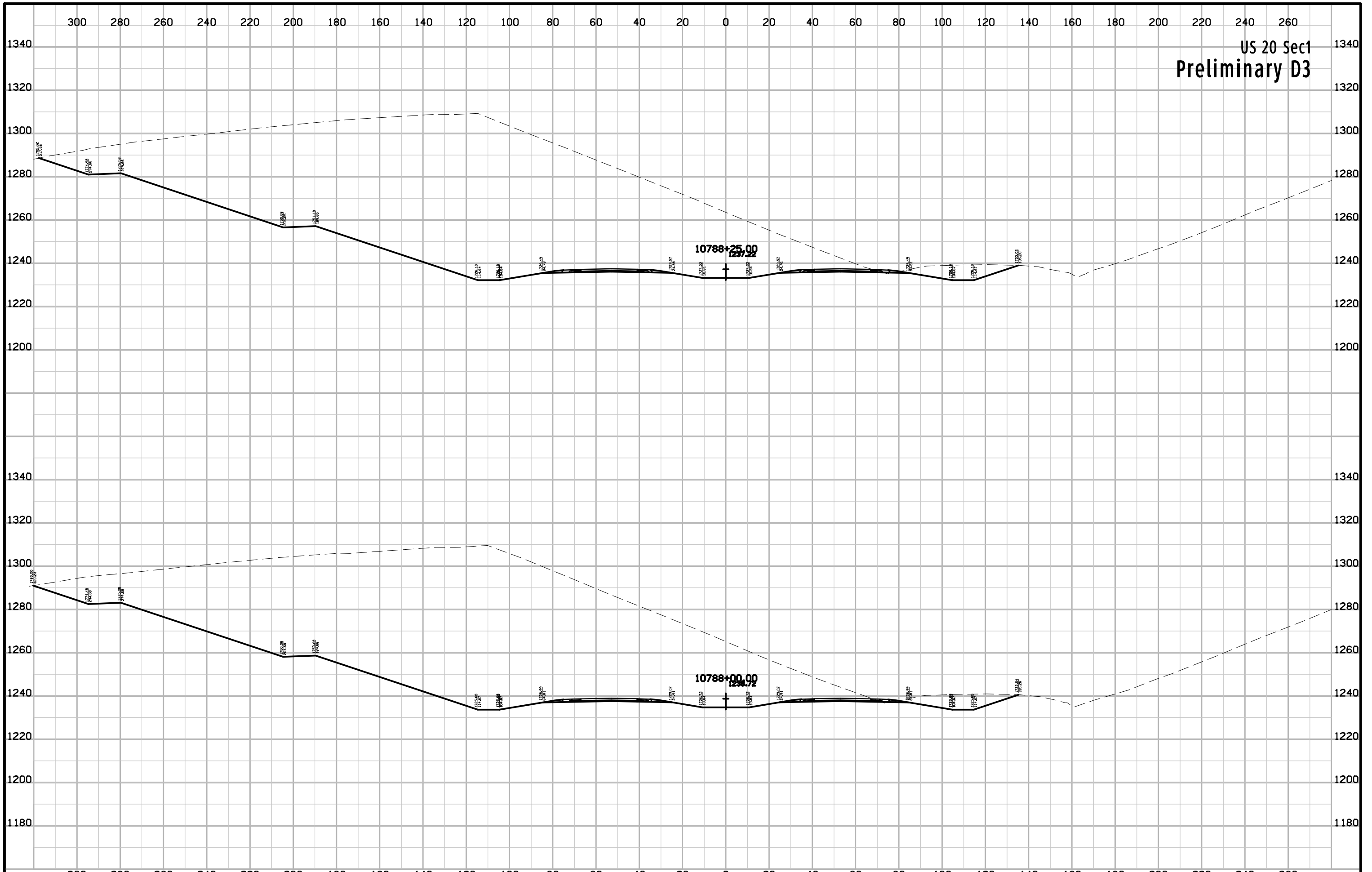
US 20 Sec1
Preliminary D3



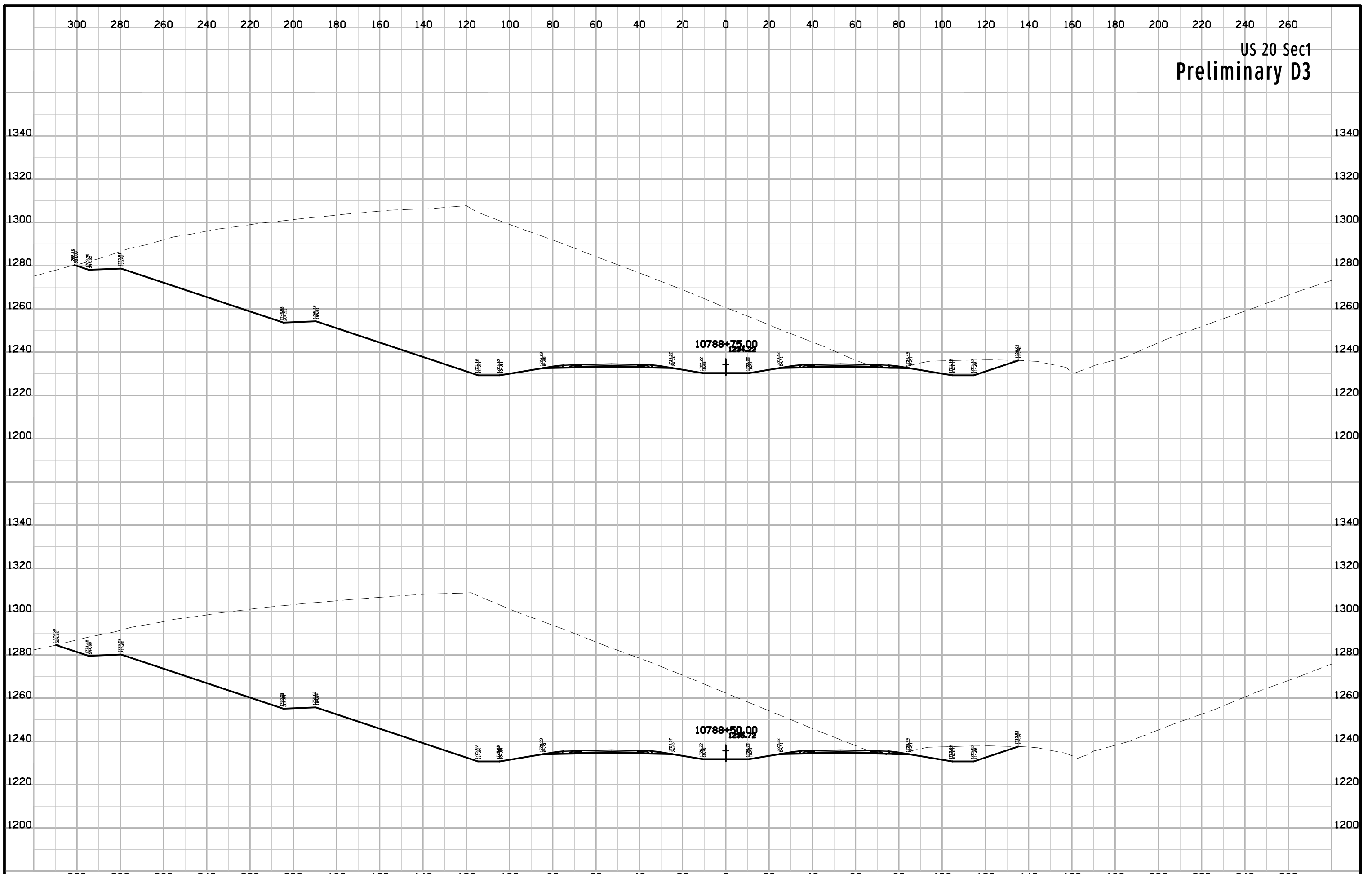
US 20 Sec1
Preliminary D3



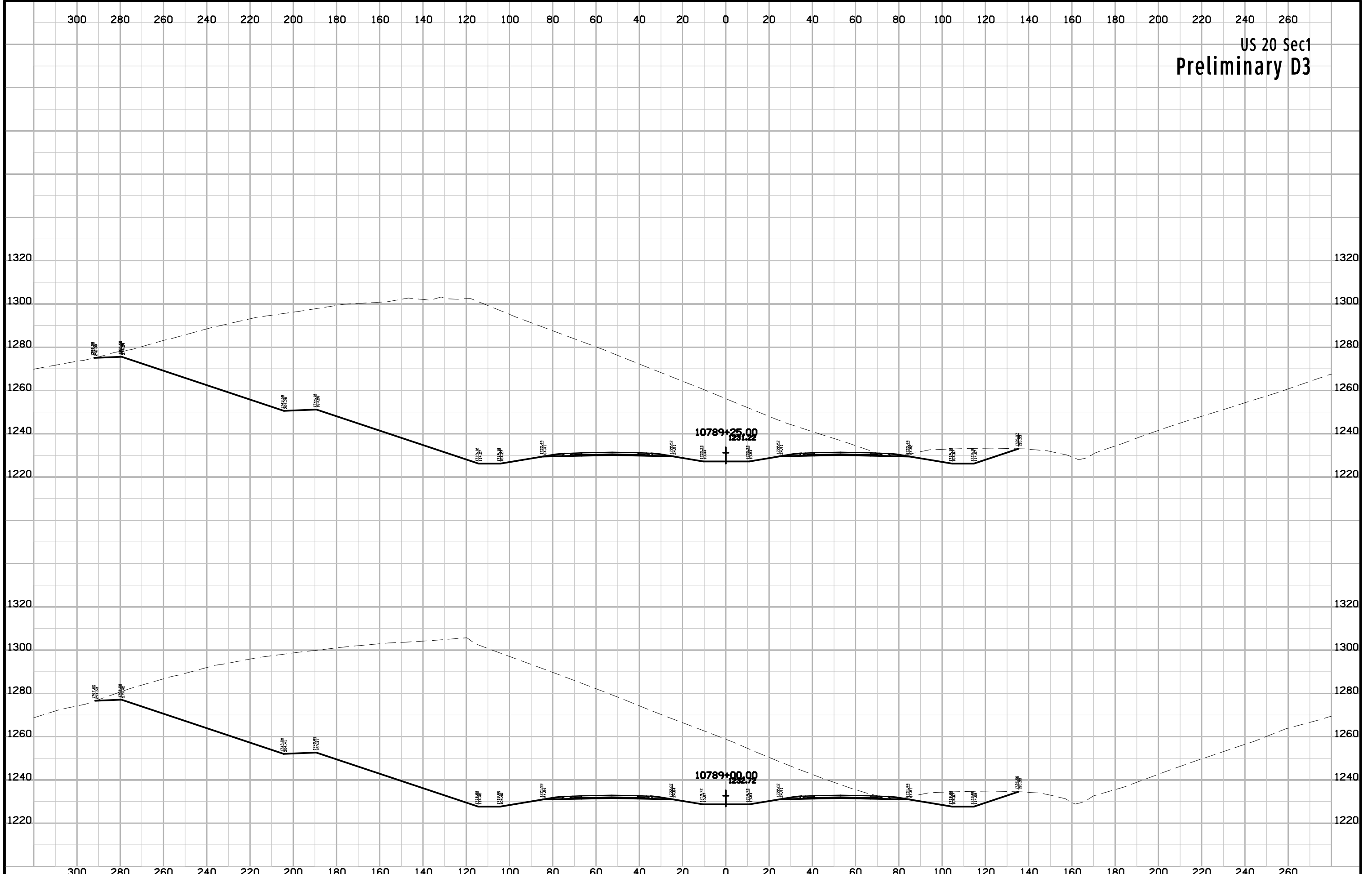
US 20 Sec1
Preliminary D3



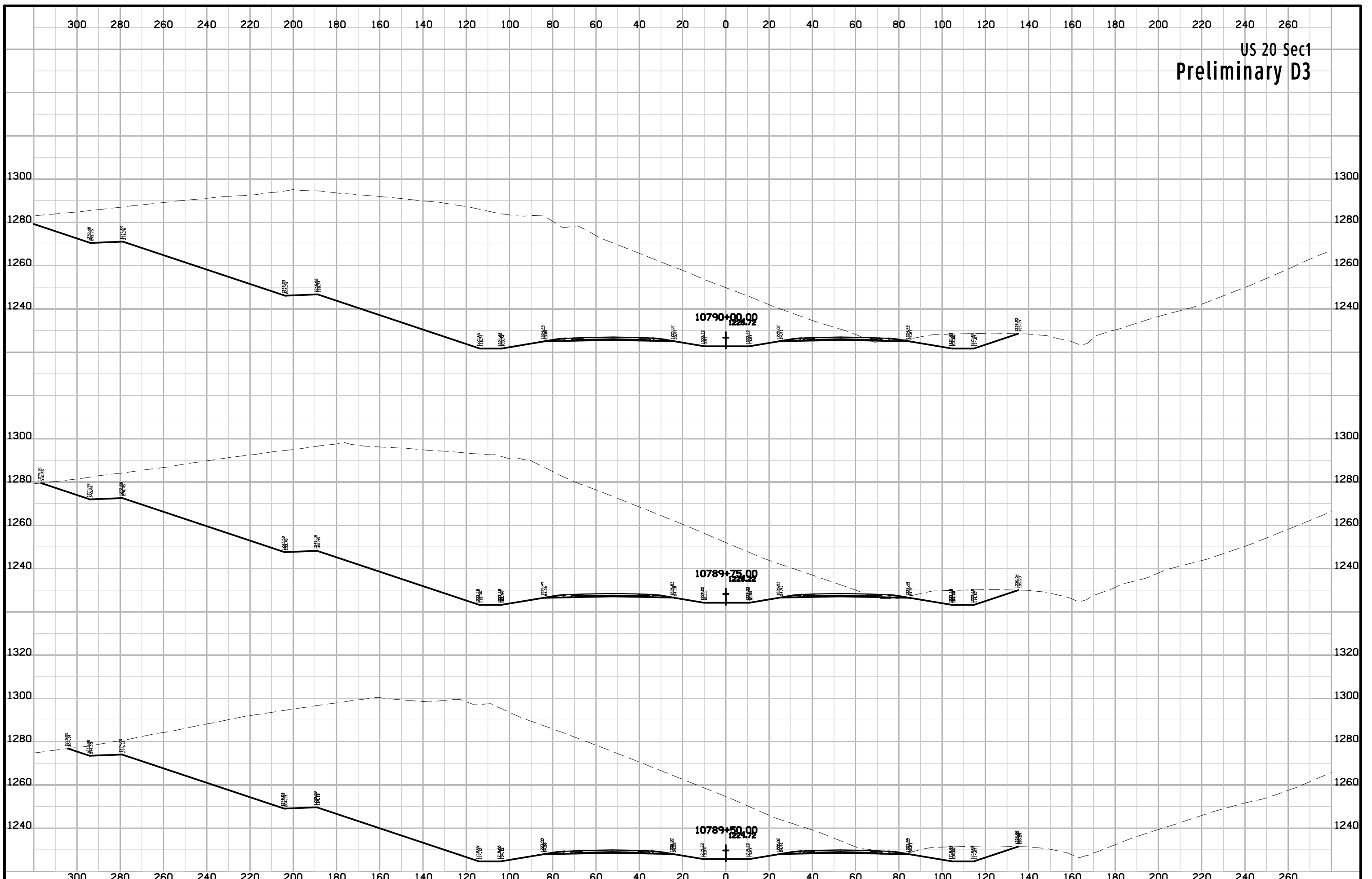
US 20 Sec1
Preliminary D3



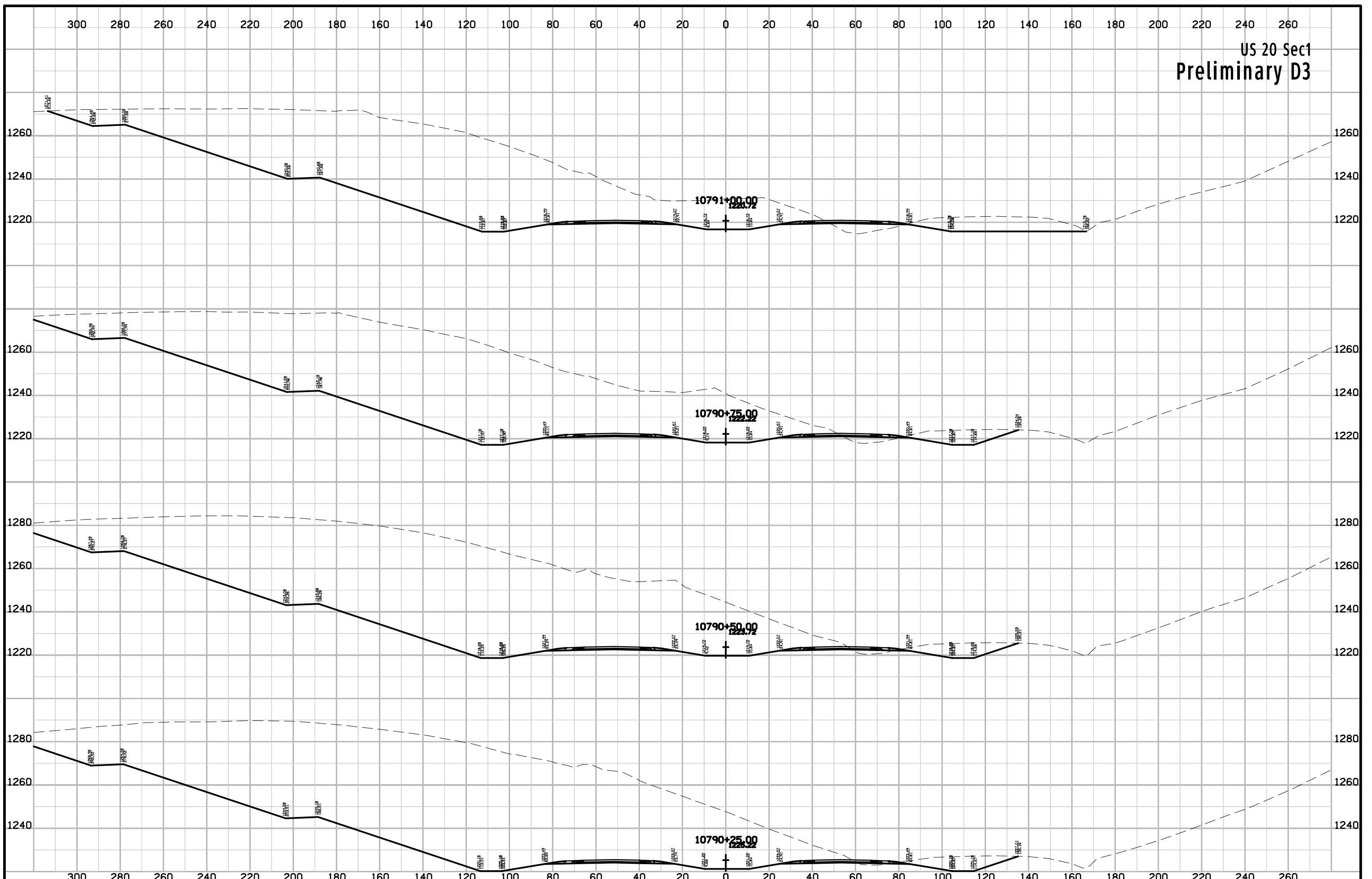
US 20 Sec1
Preliminary D3



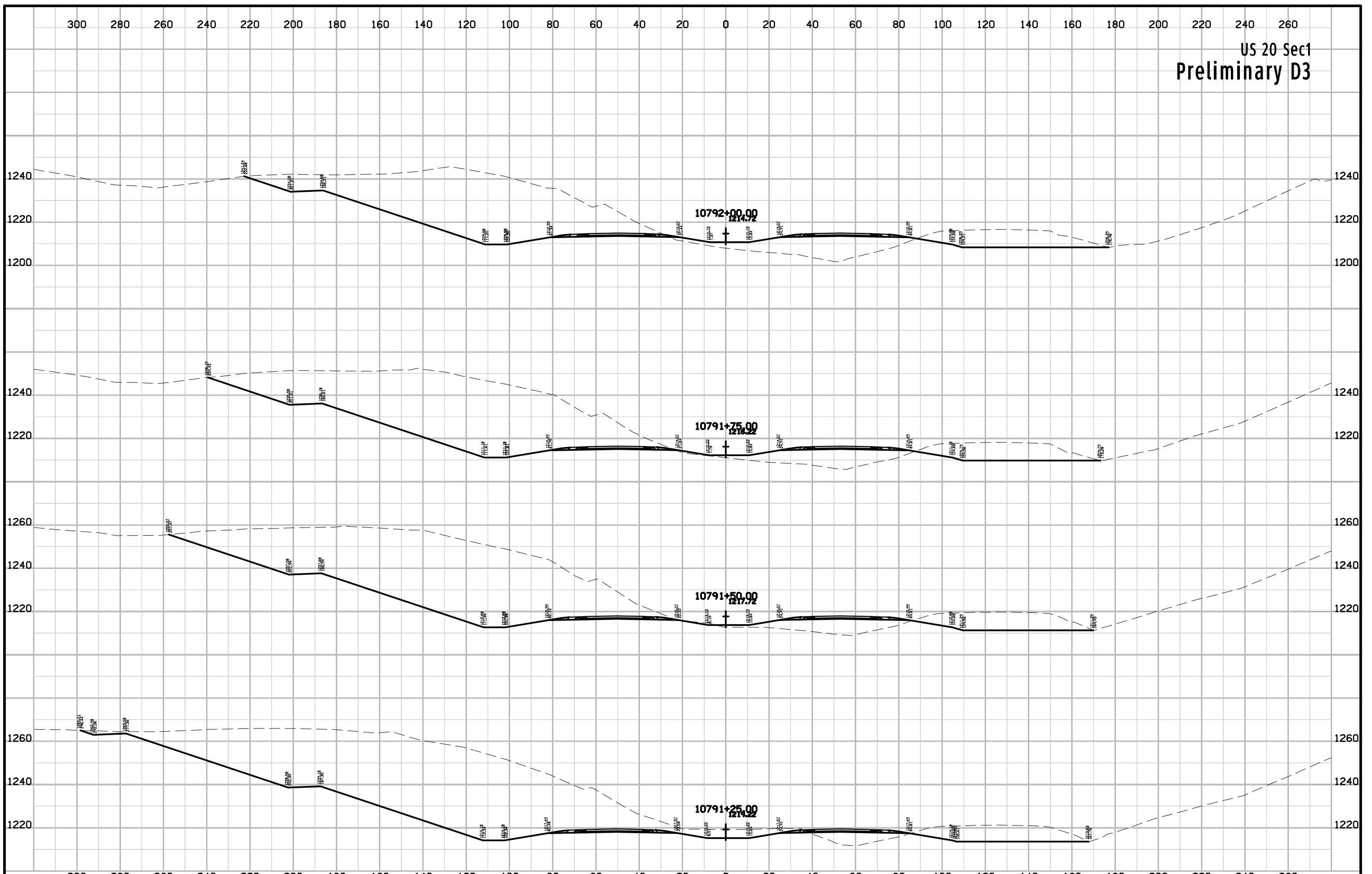
US 20 Sec1
Preliminary D3



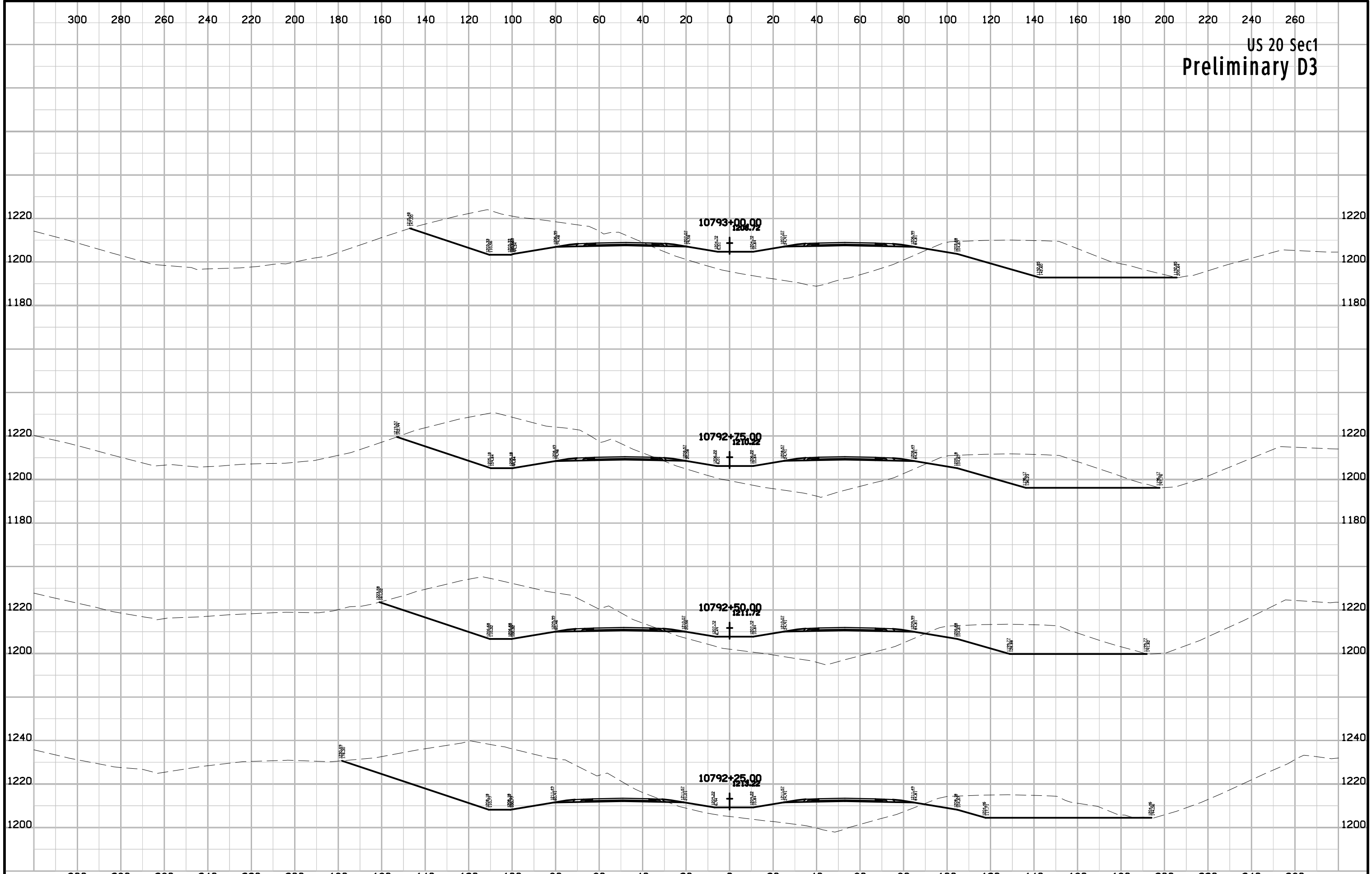
US 20 Sec1
Preliminary D3



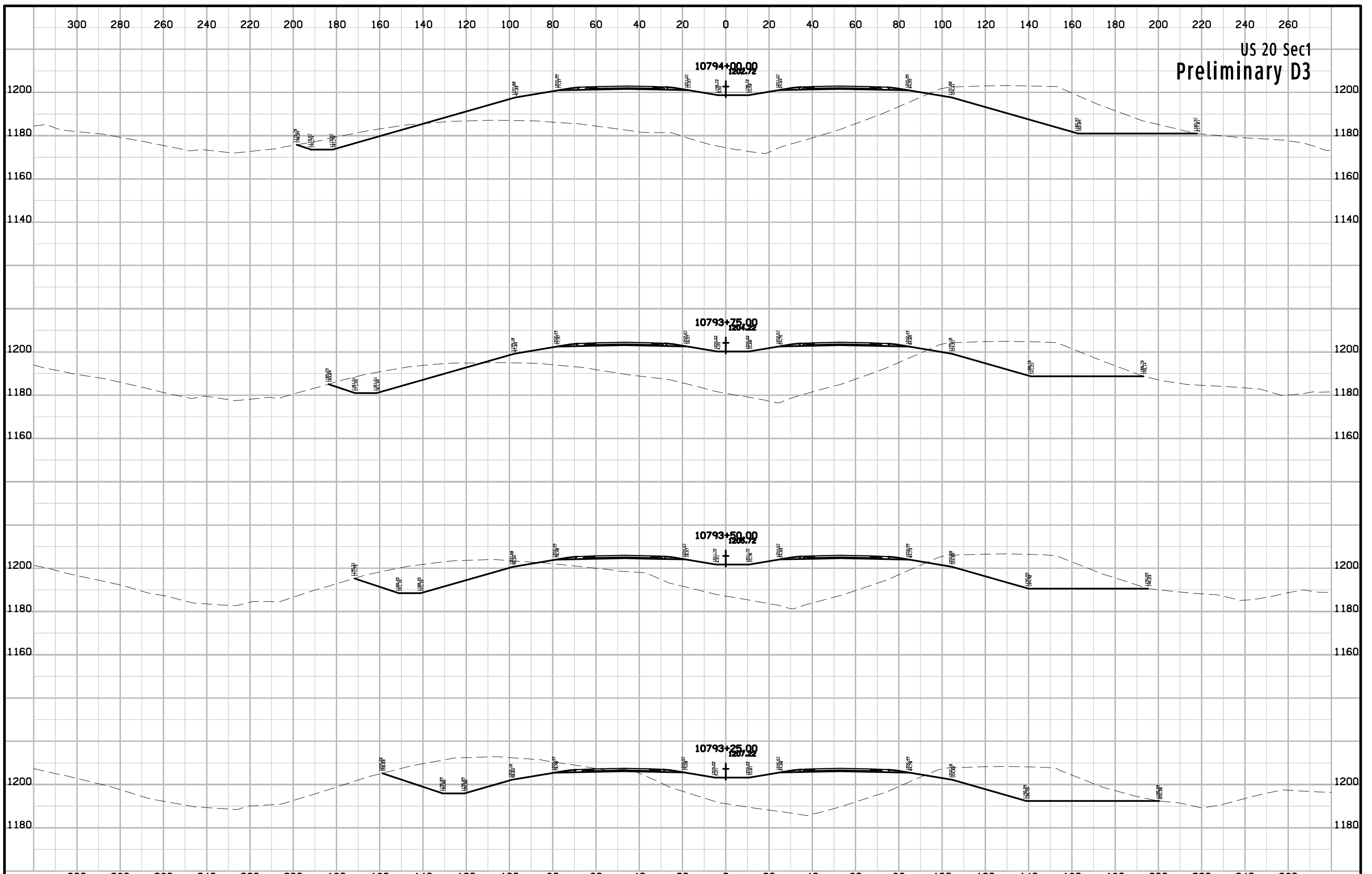
US 20 Sec1
Preliminary D3



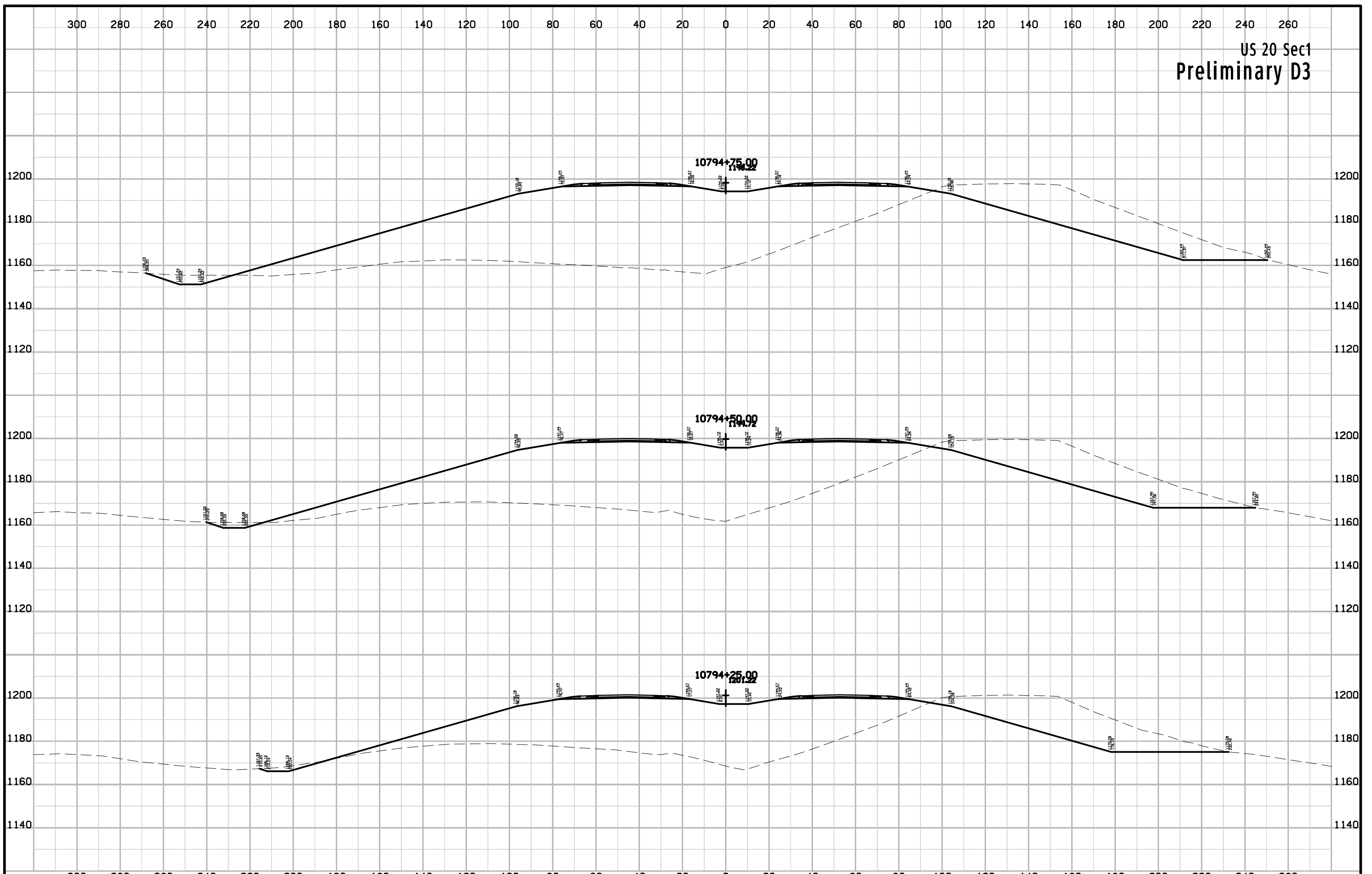
US 20 Sec1
Preliminary D3



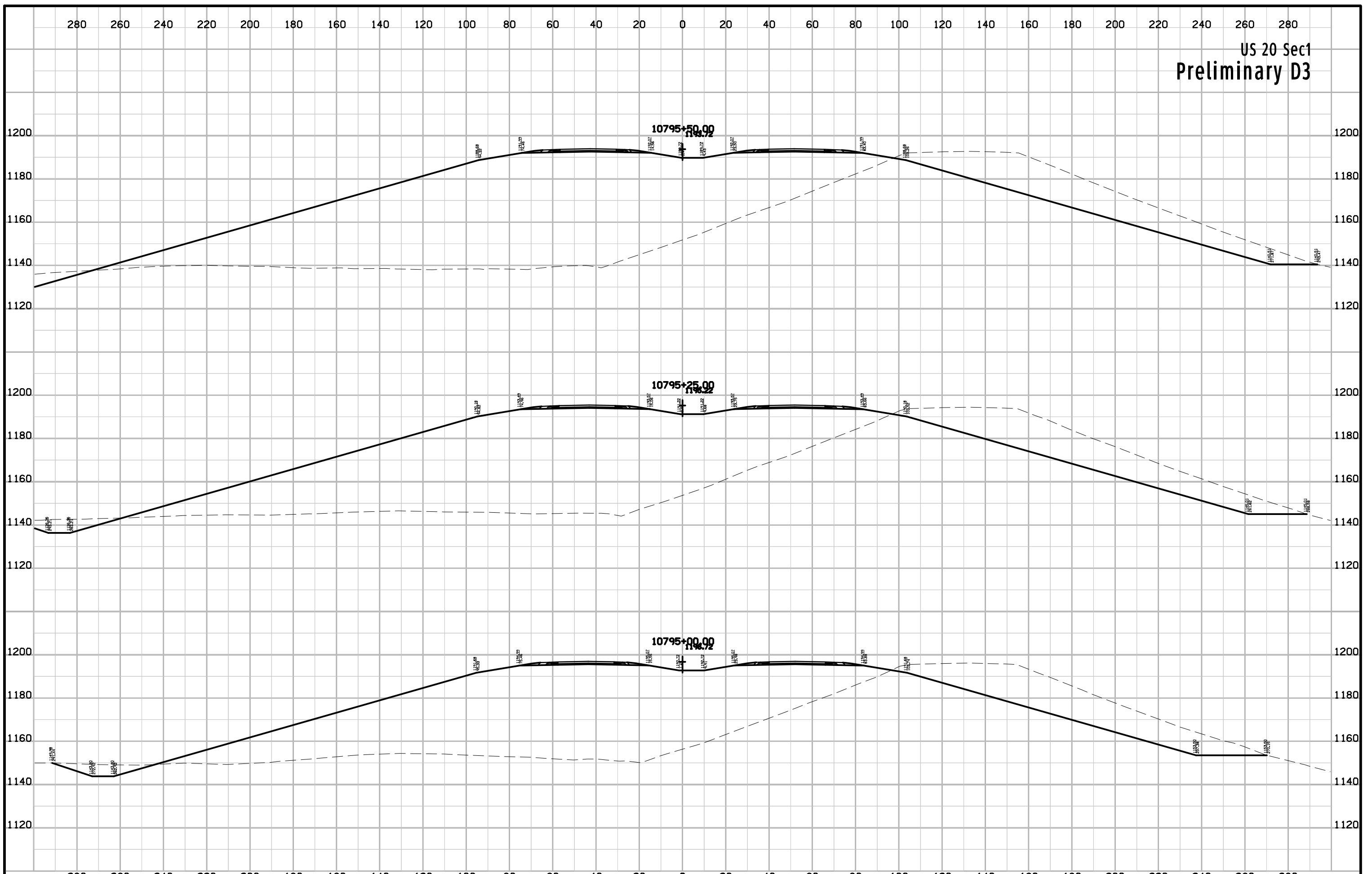
US 20 Sec1
Preliminary D3



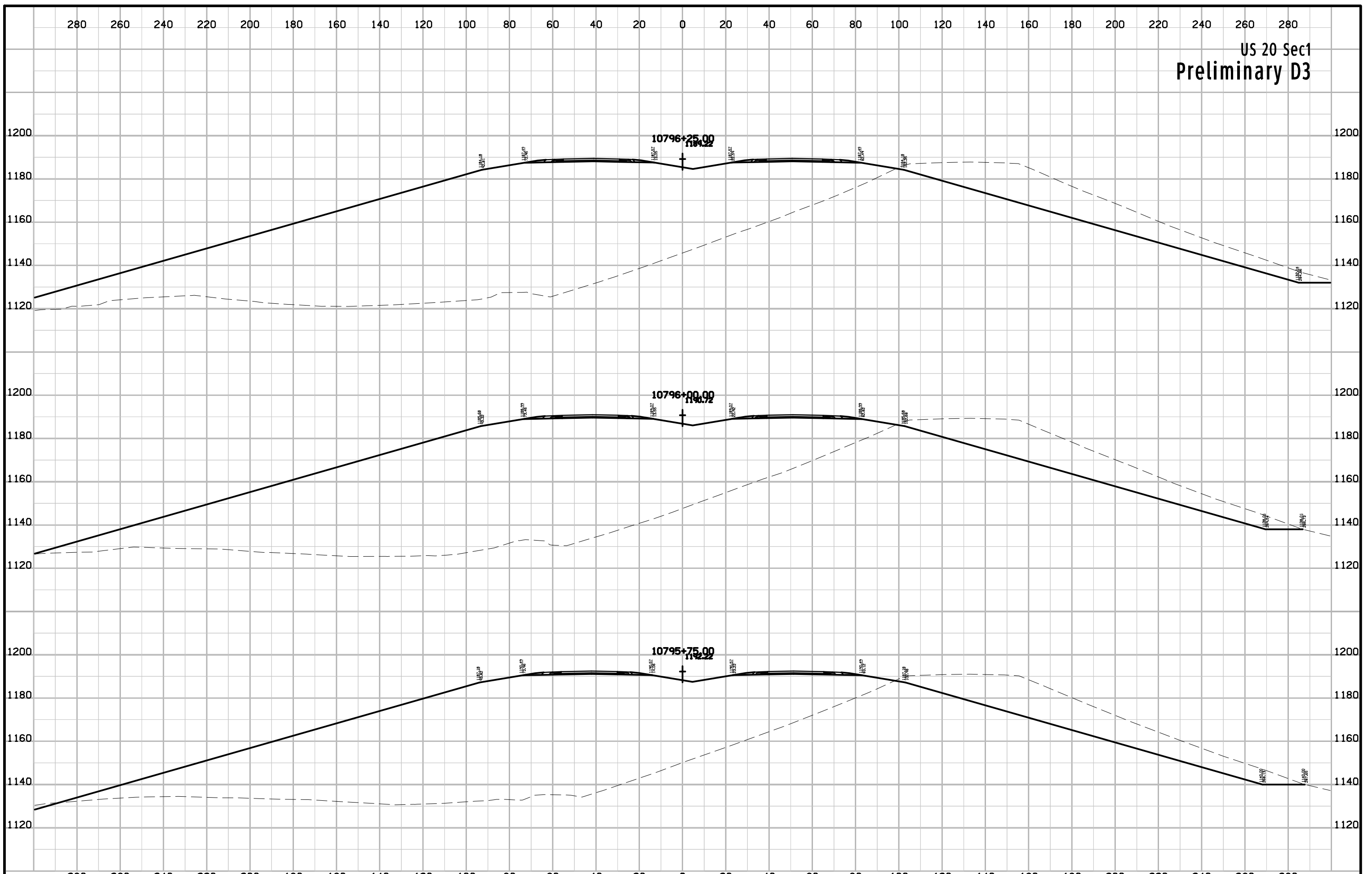
US 20 Sec1
Preliminary D3



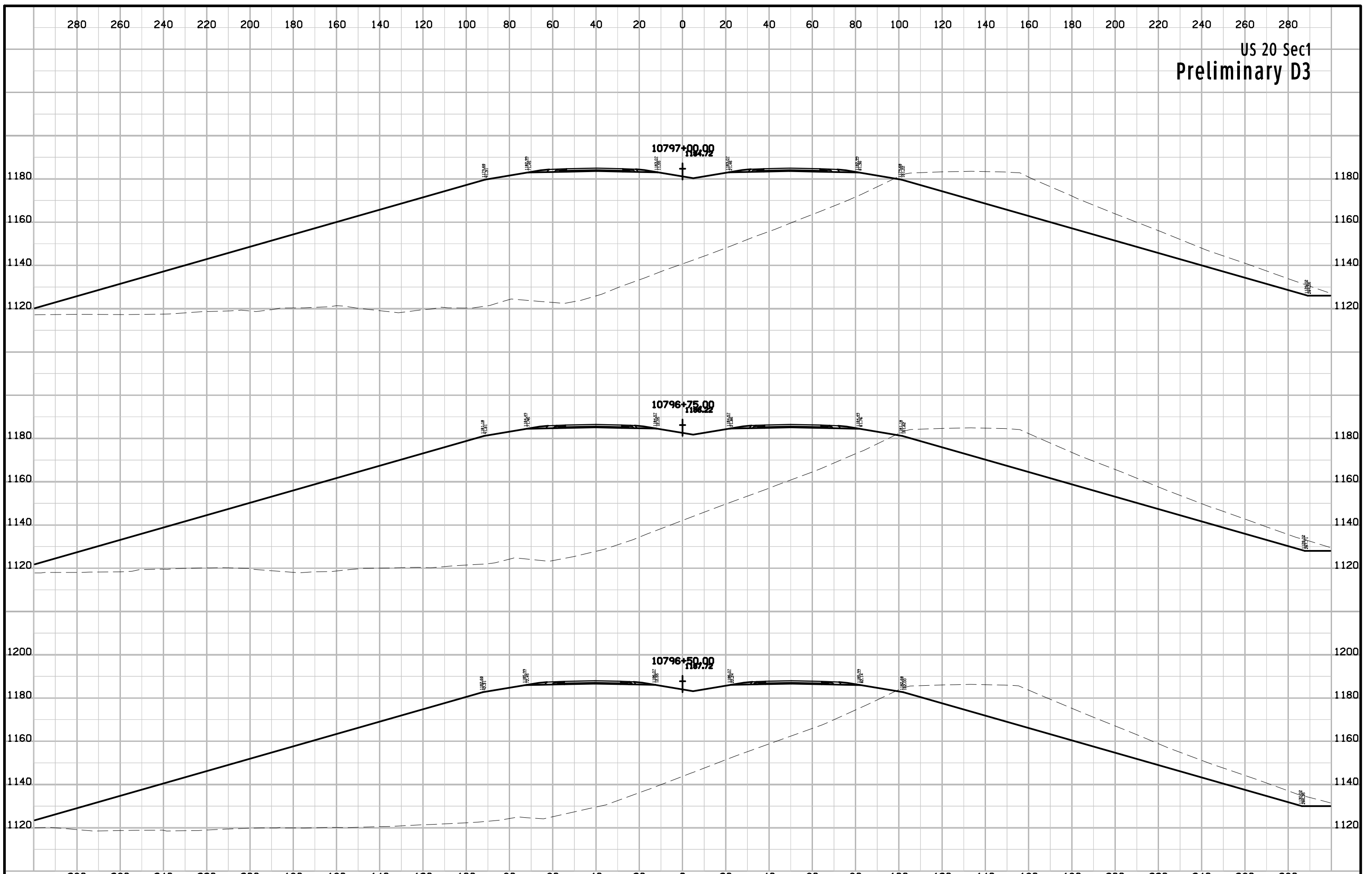
US 20 Sec1
Preliminary D3



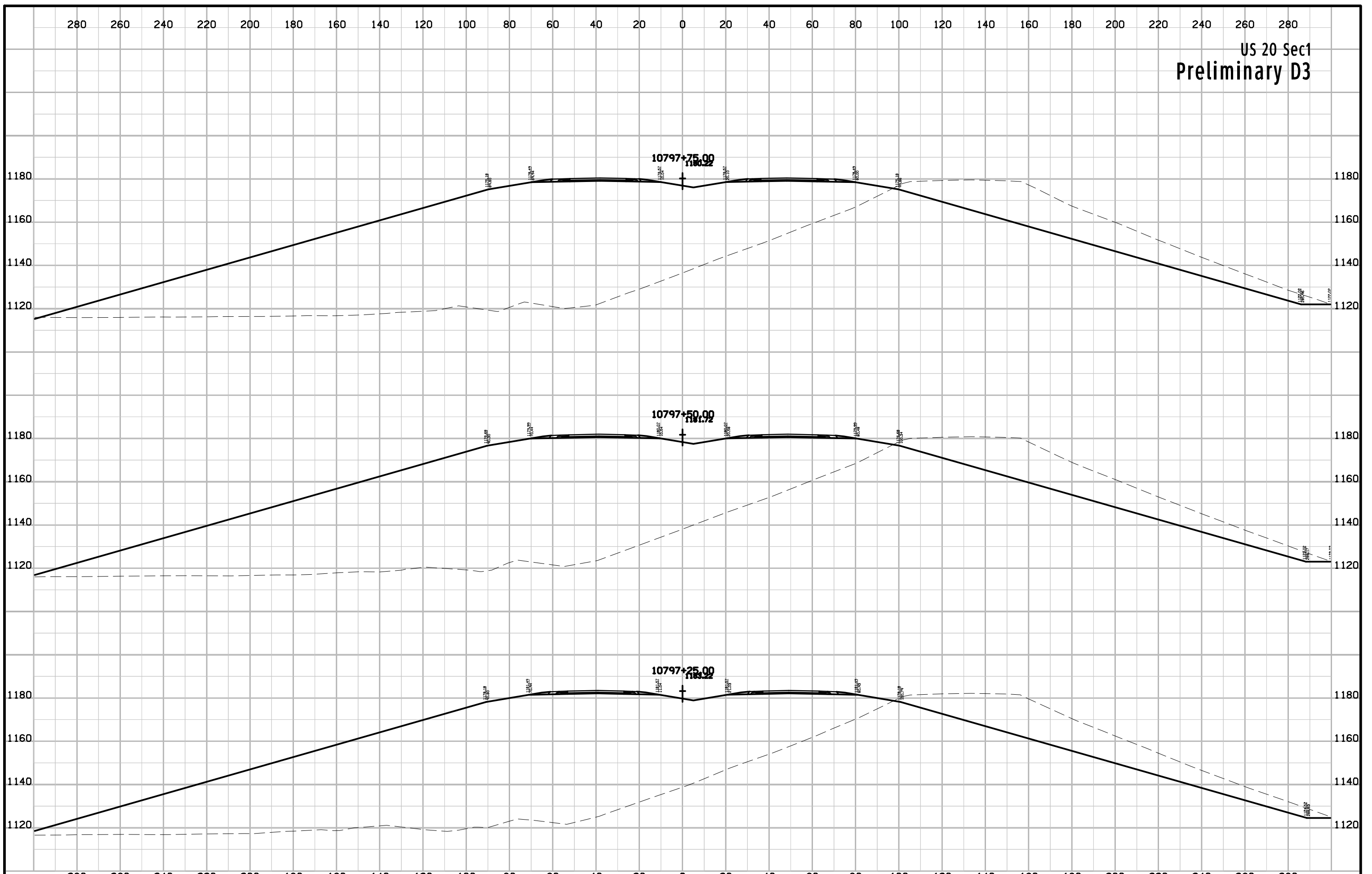
US 20 Sec1
Preliminary D3



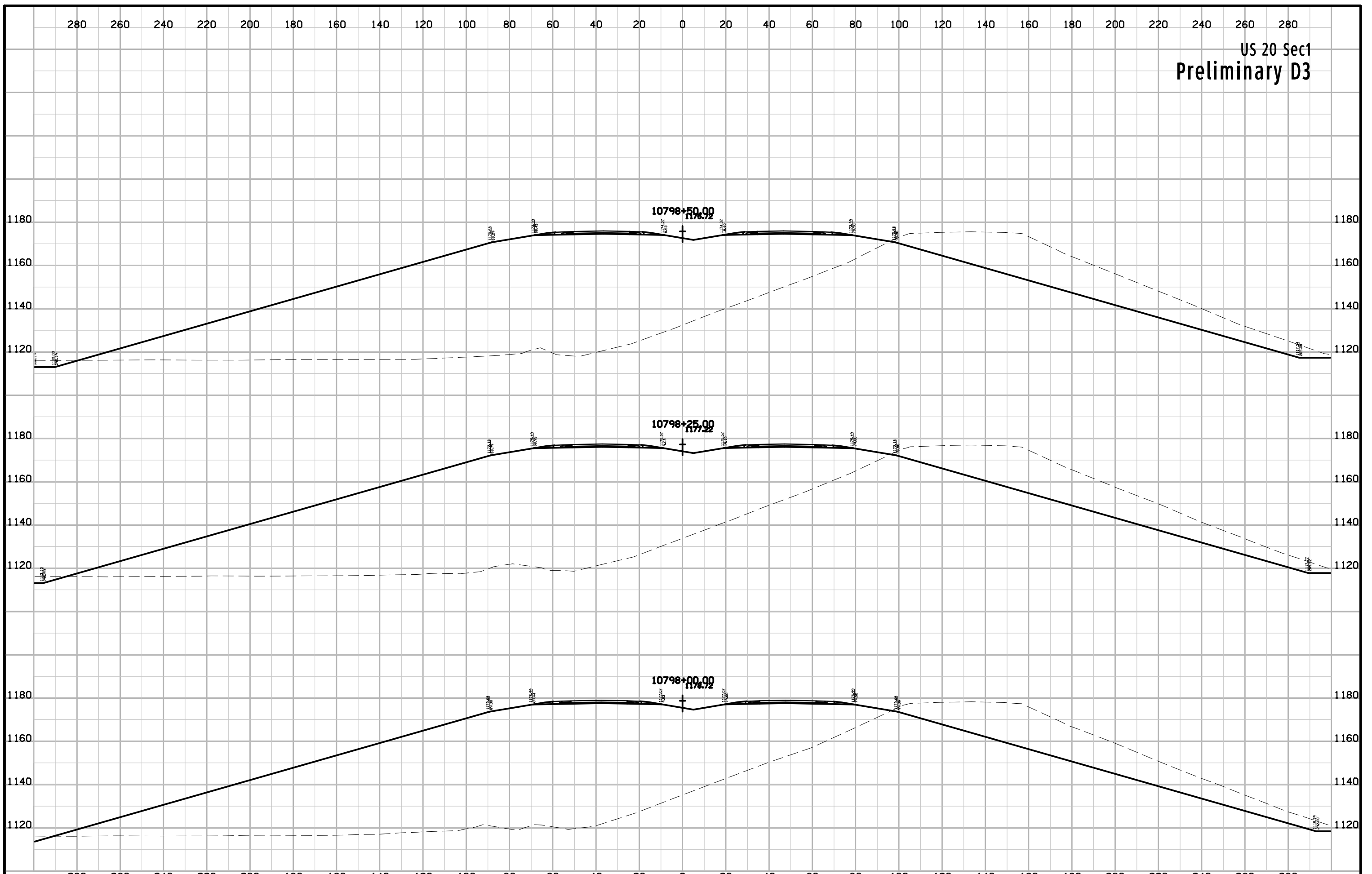
US 20 Sec1
Preliminary D3

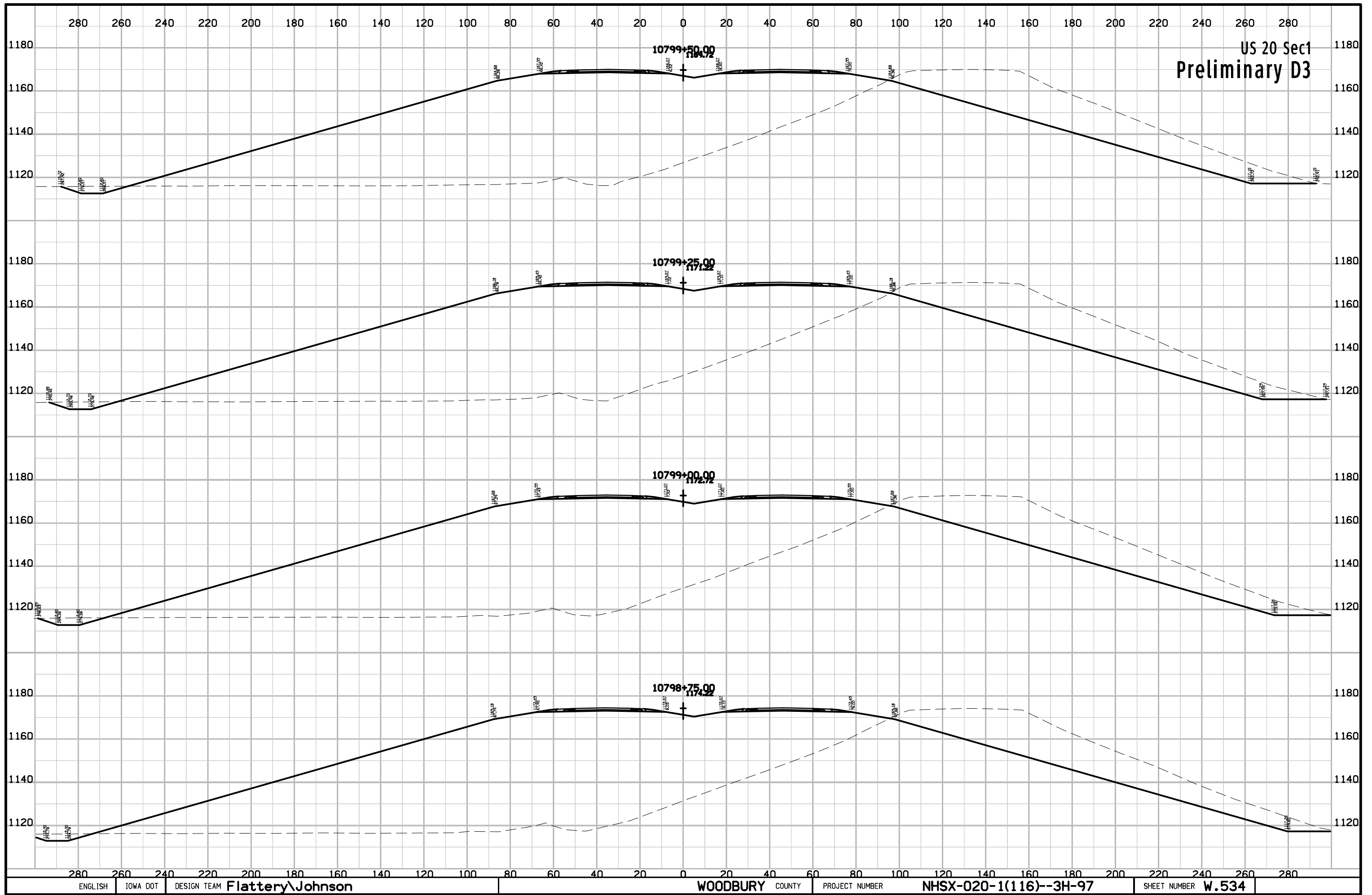


US 20 Sec1
Preliminary D3



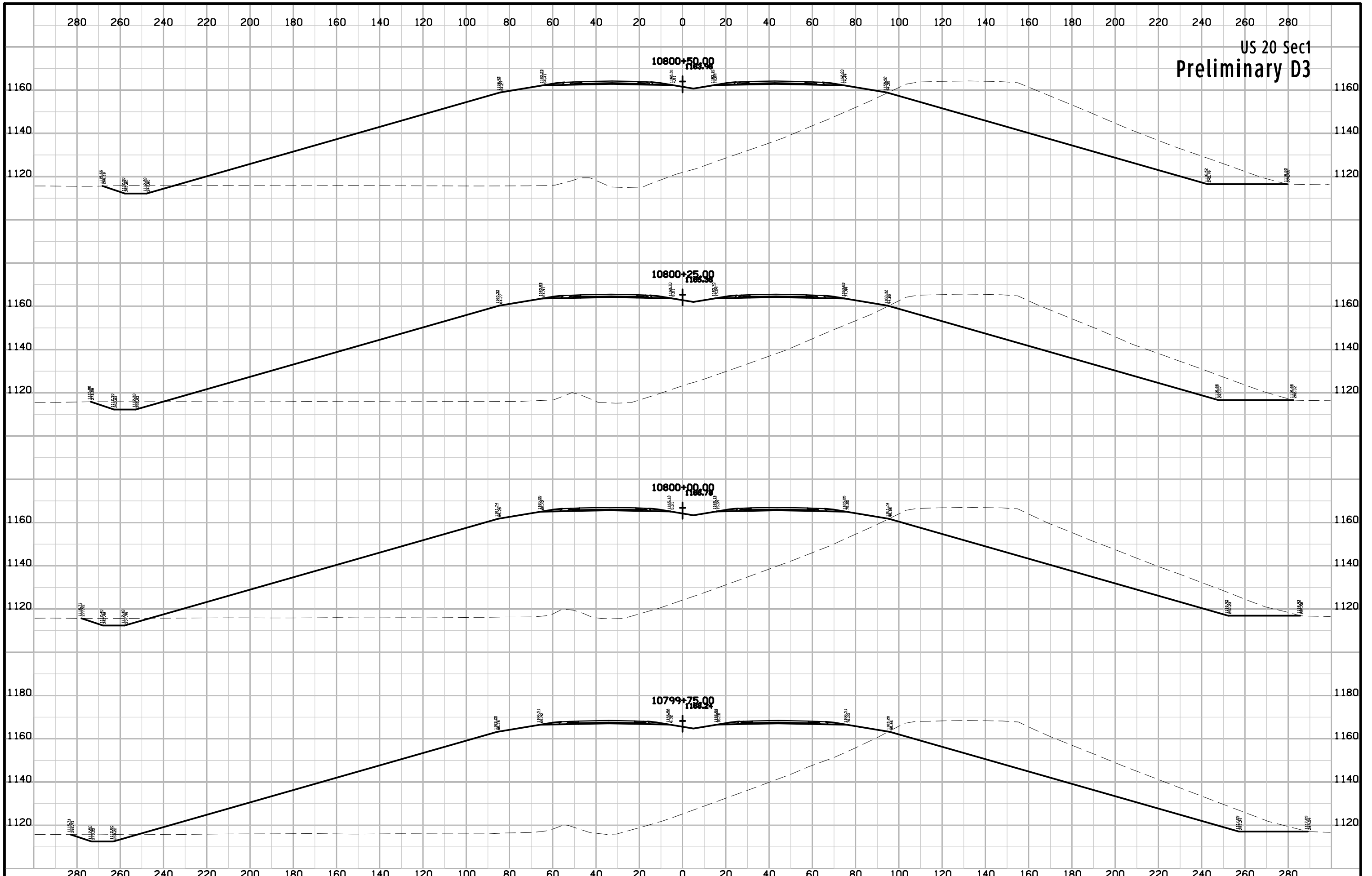
US 20 Sec1
Preliminary D3



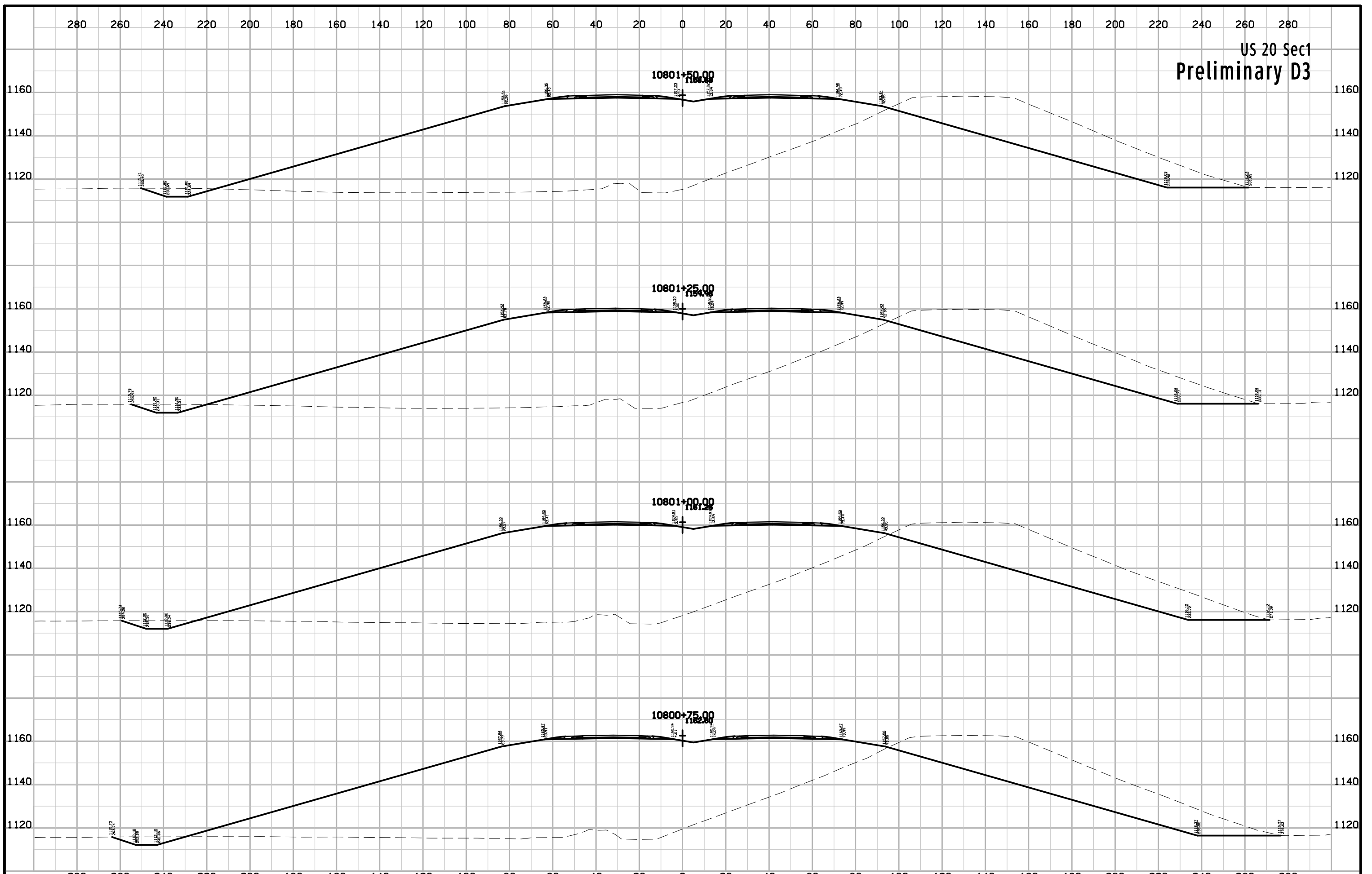


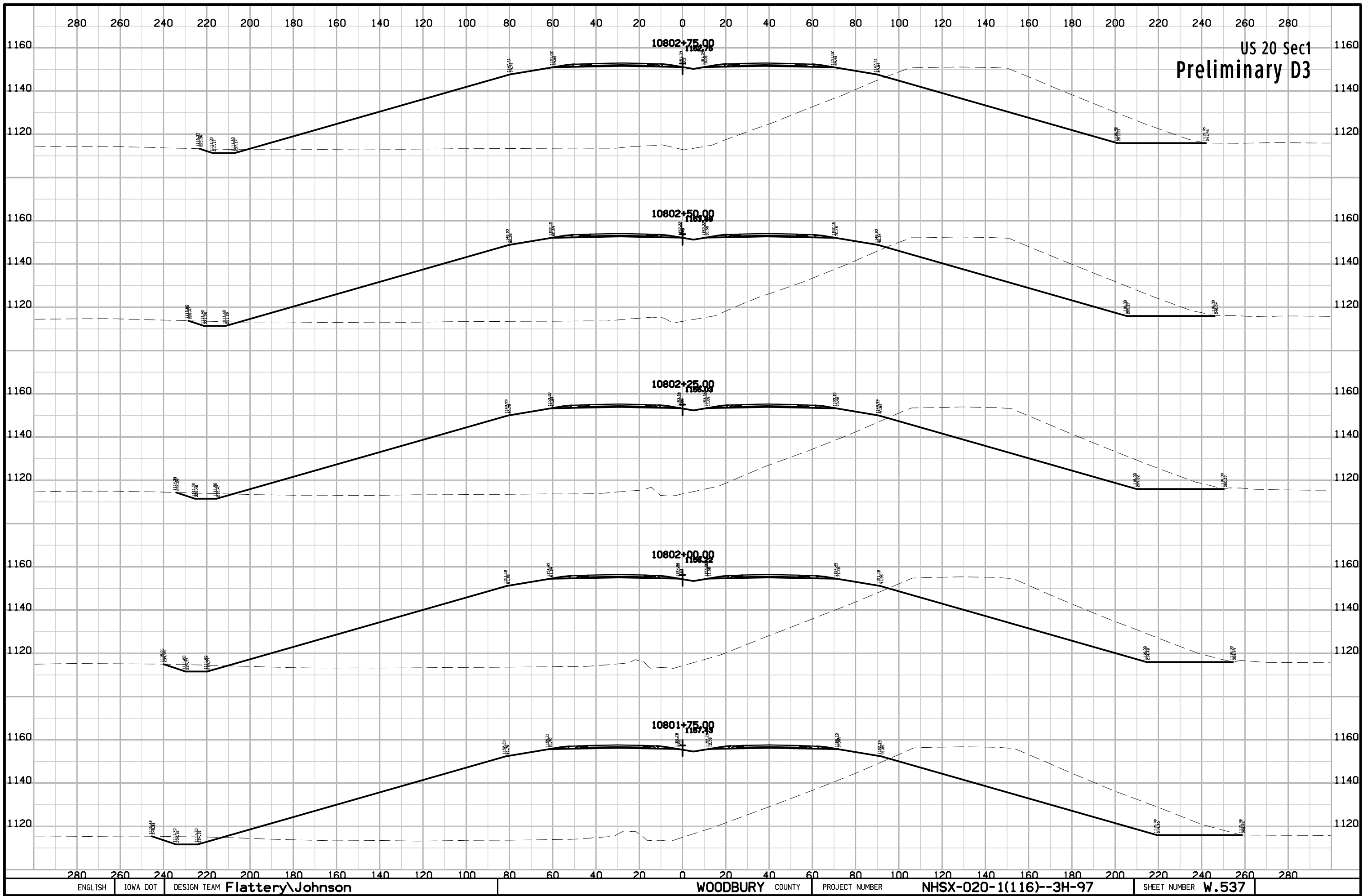
US 20 Sec1
Preliminary D3

US 20 Sec1
Preliminary D3

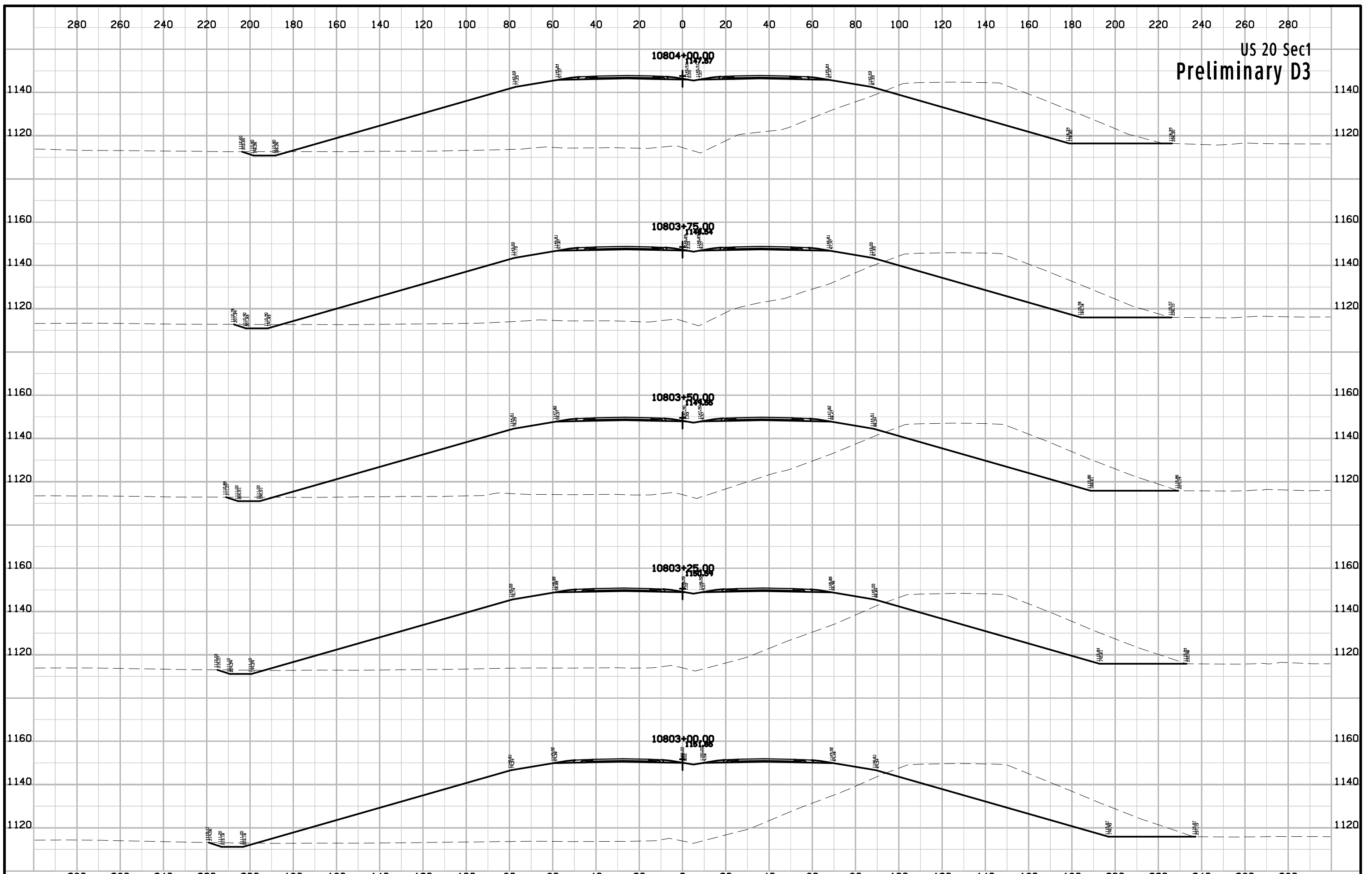


US 20 Sec1
Preliminary D3

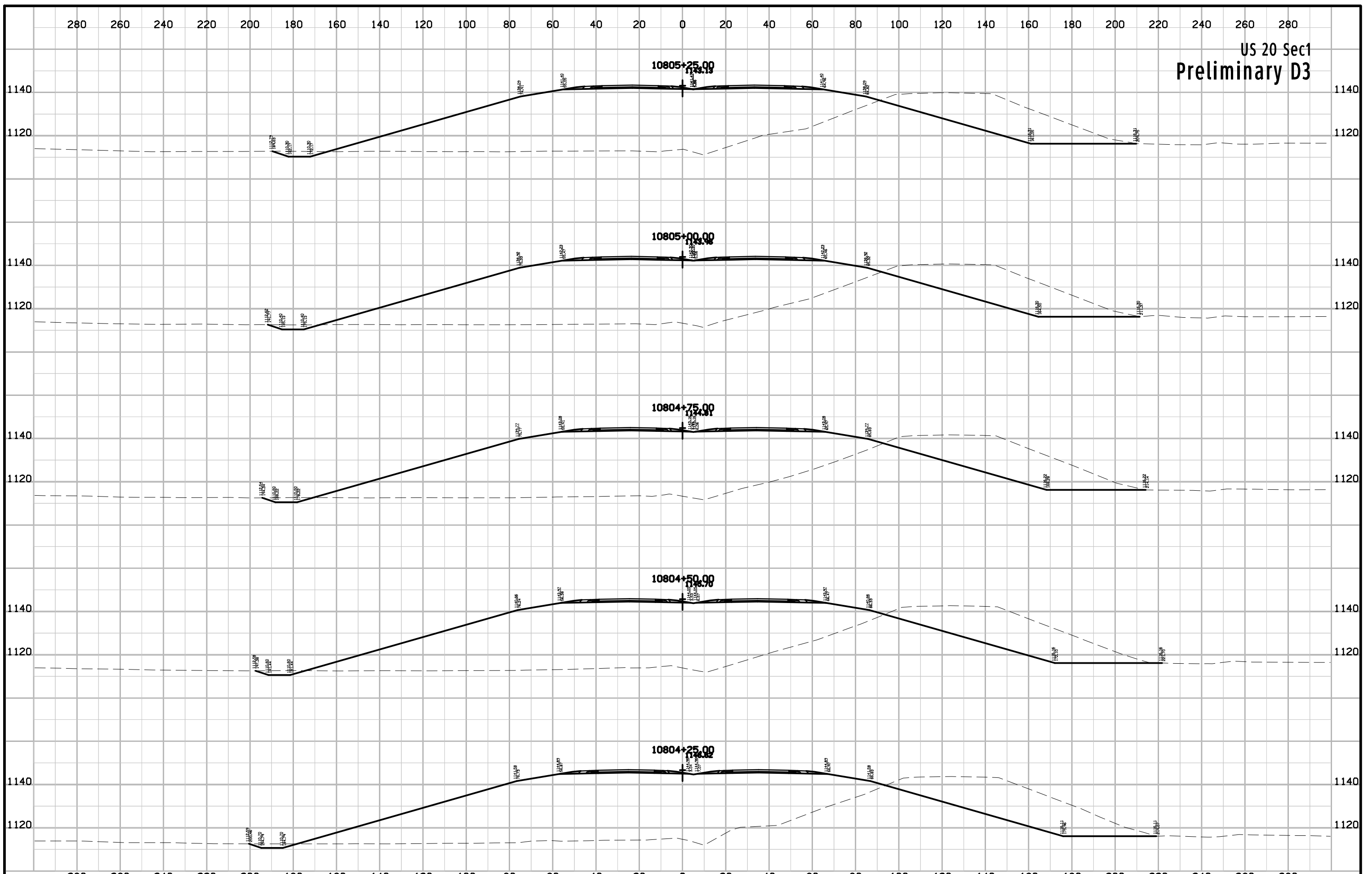




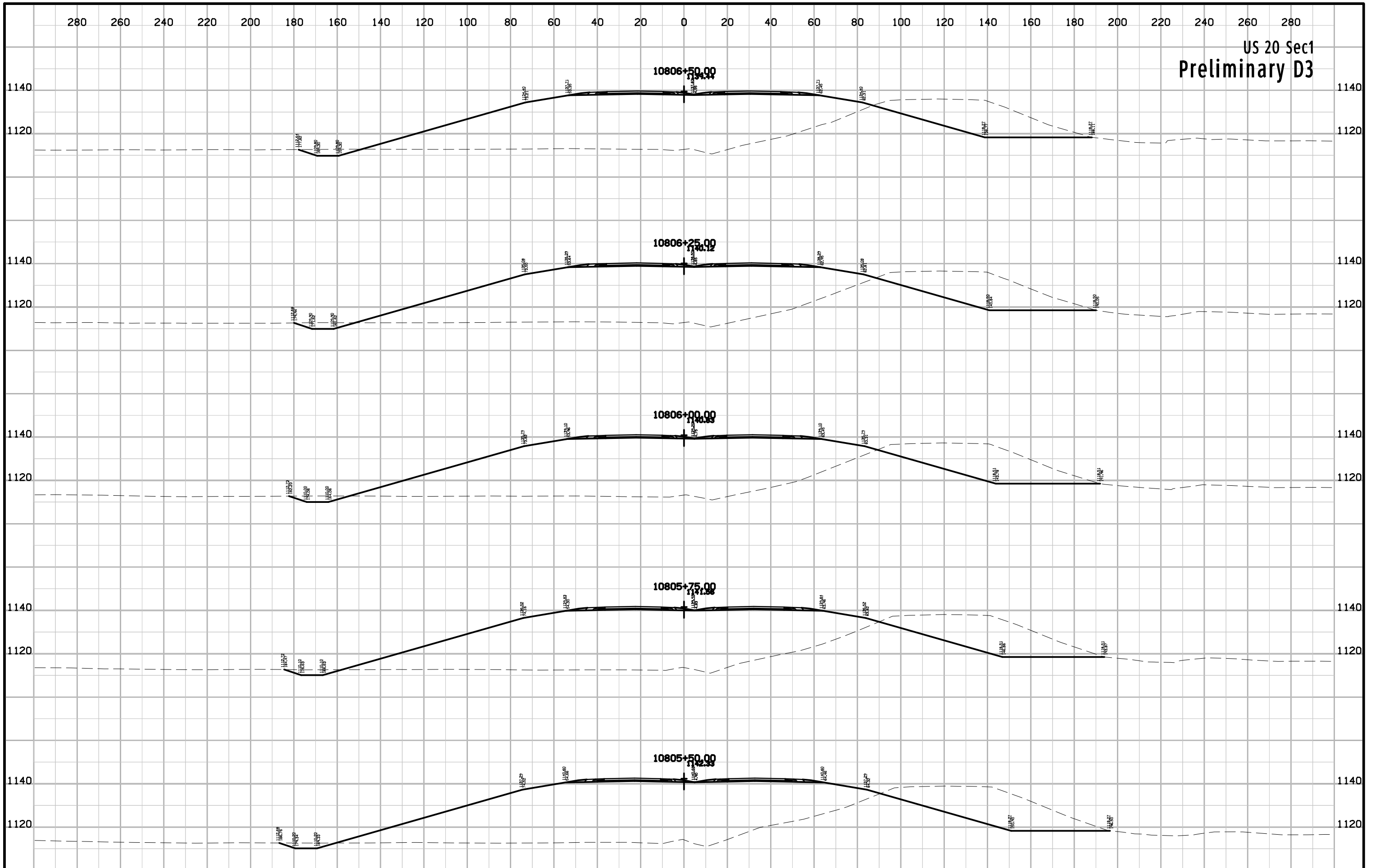
US 20 Sec1
Preliminary D3



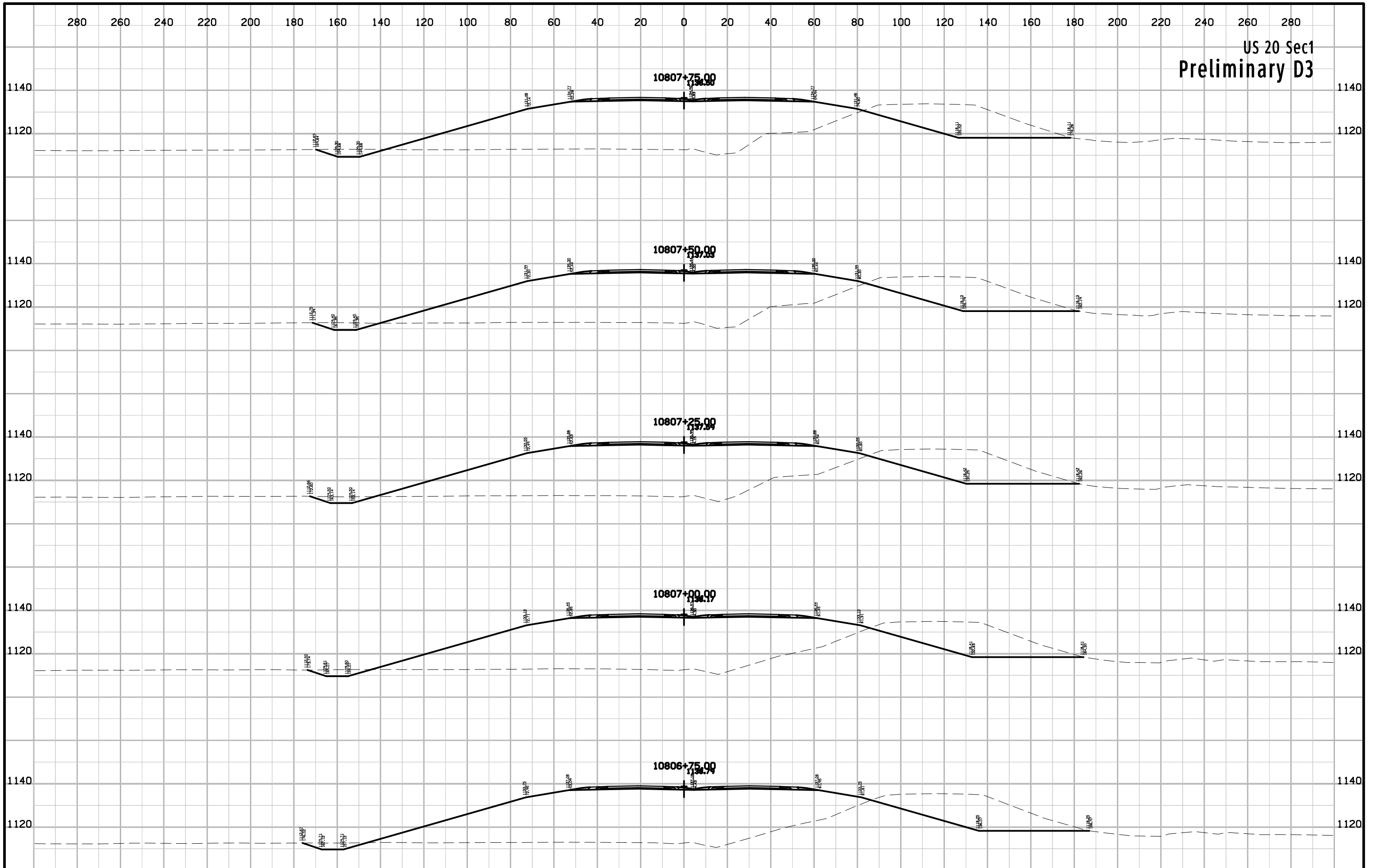
US 20 Sec1
Preliminary D3



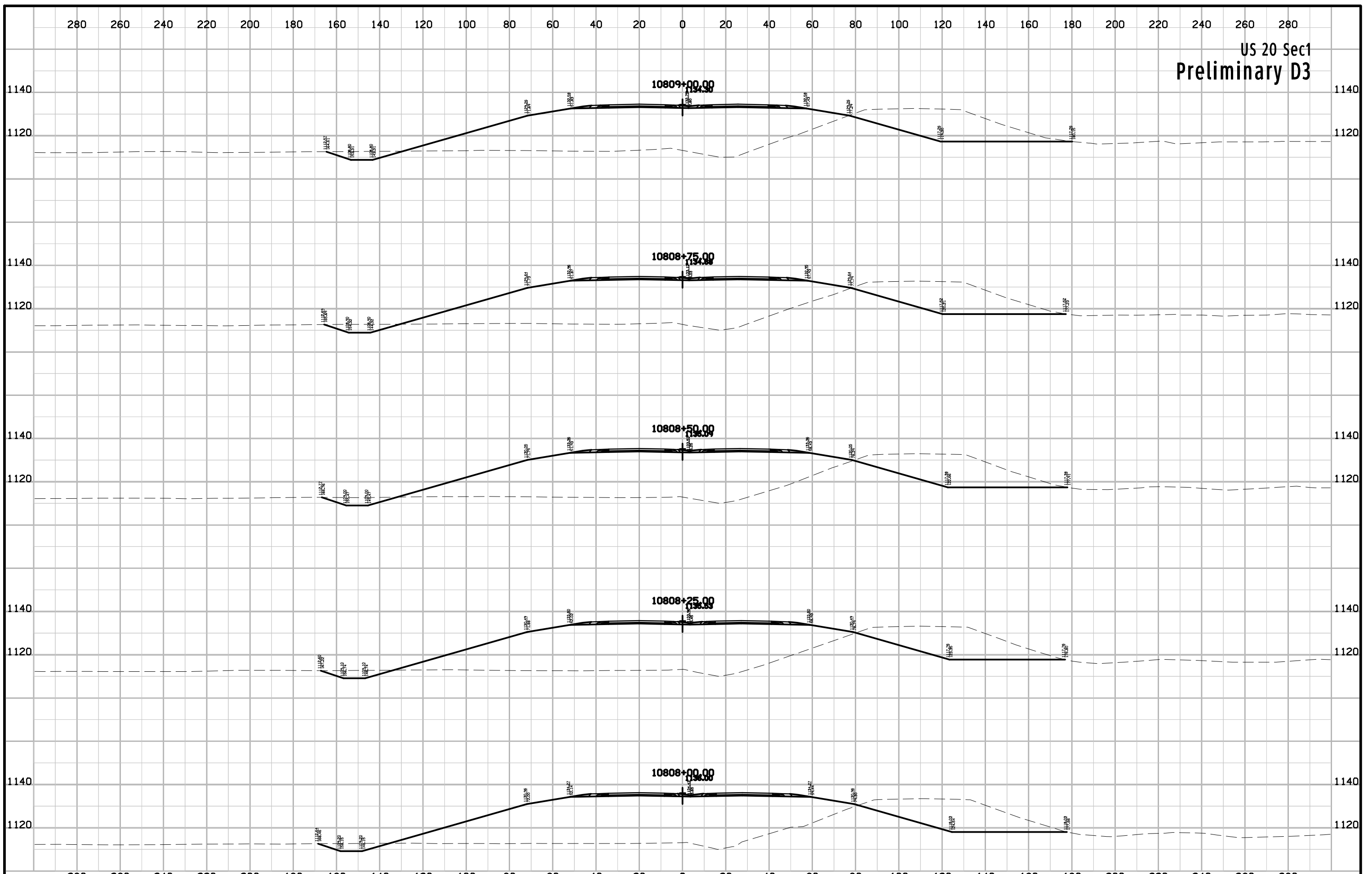
US 20 Sec1
Preliminary D3



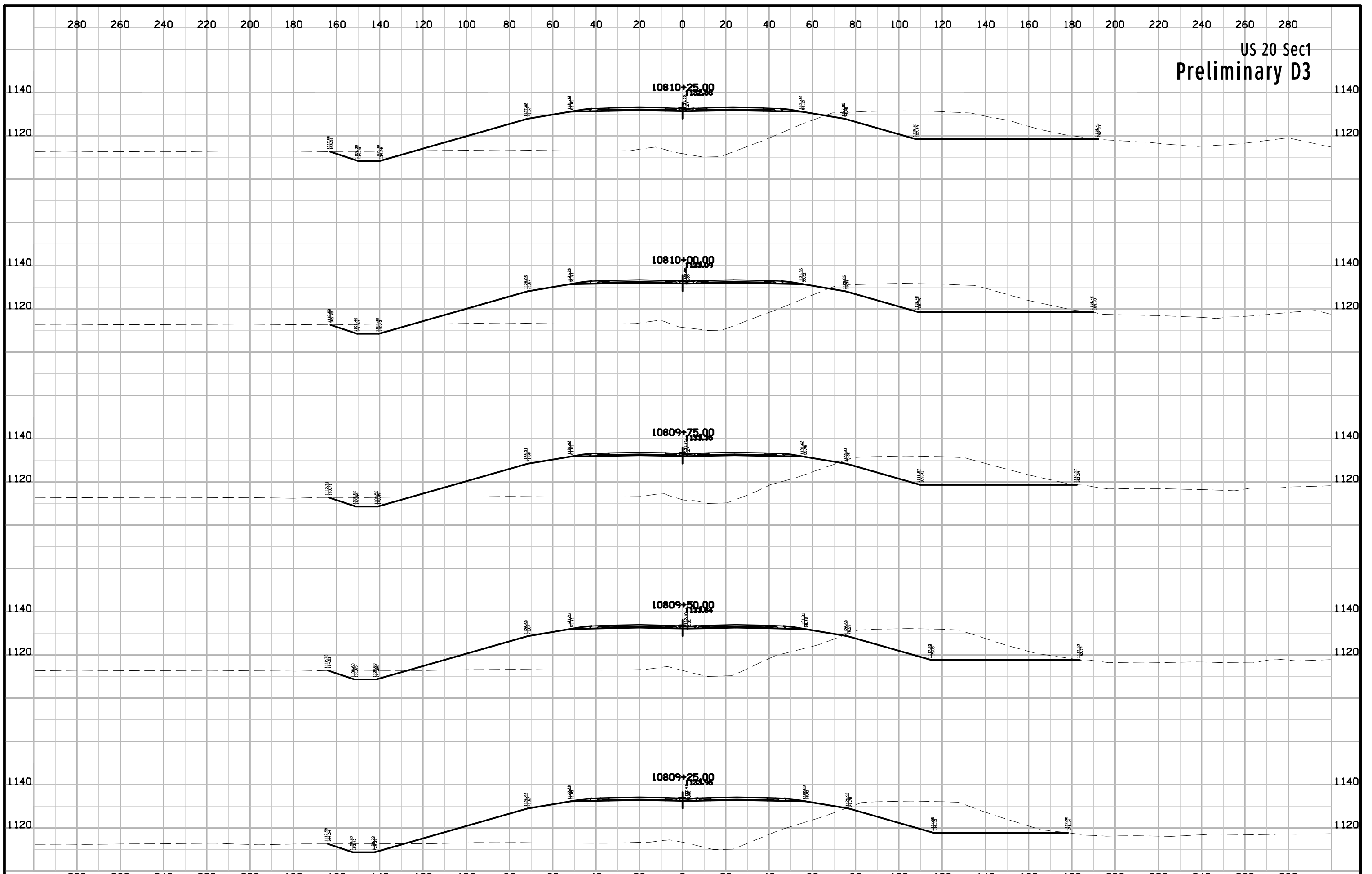
US 20 Sec1
Preliminary D3



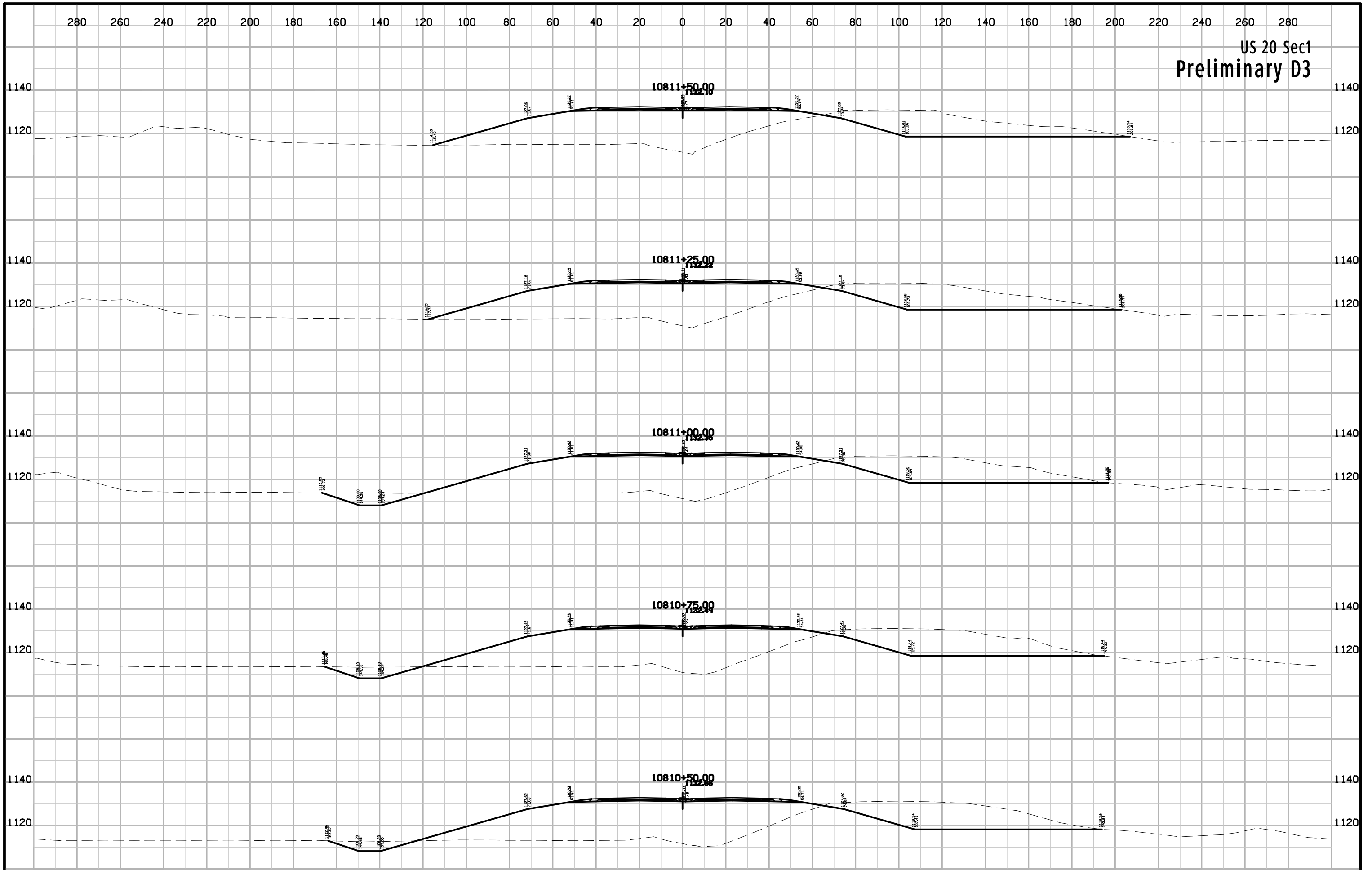
US 20 Sec1
Preliminary D3



US 20 Sec1
Preliminary D3

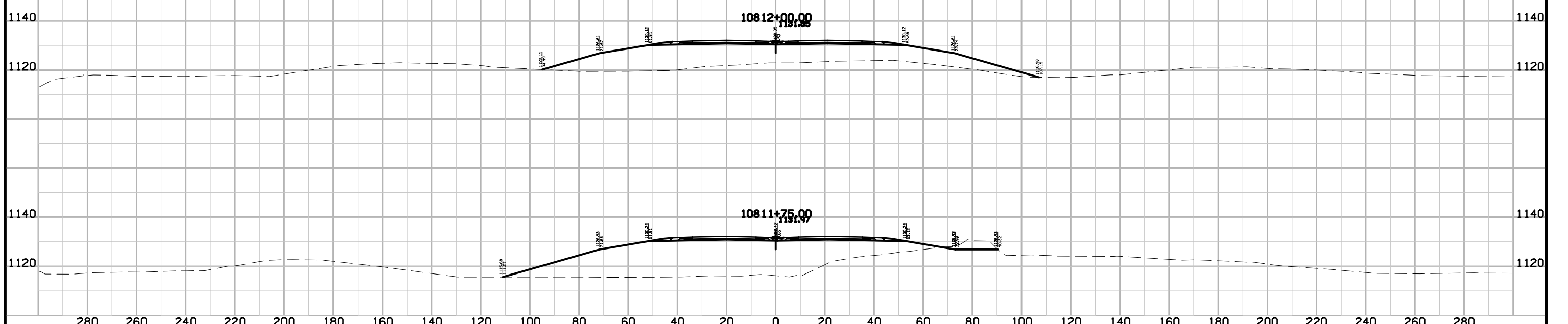


US 20 Sec1
Preliminary D3



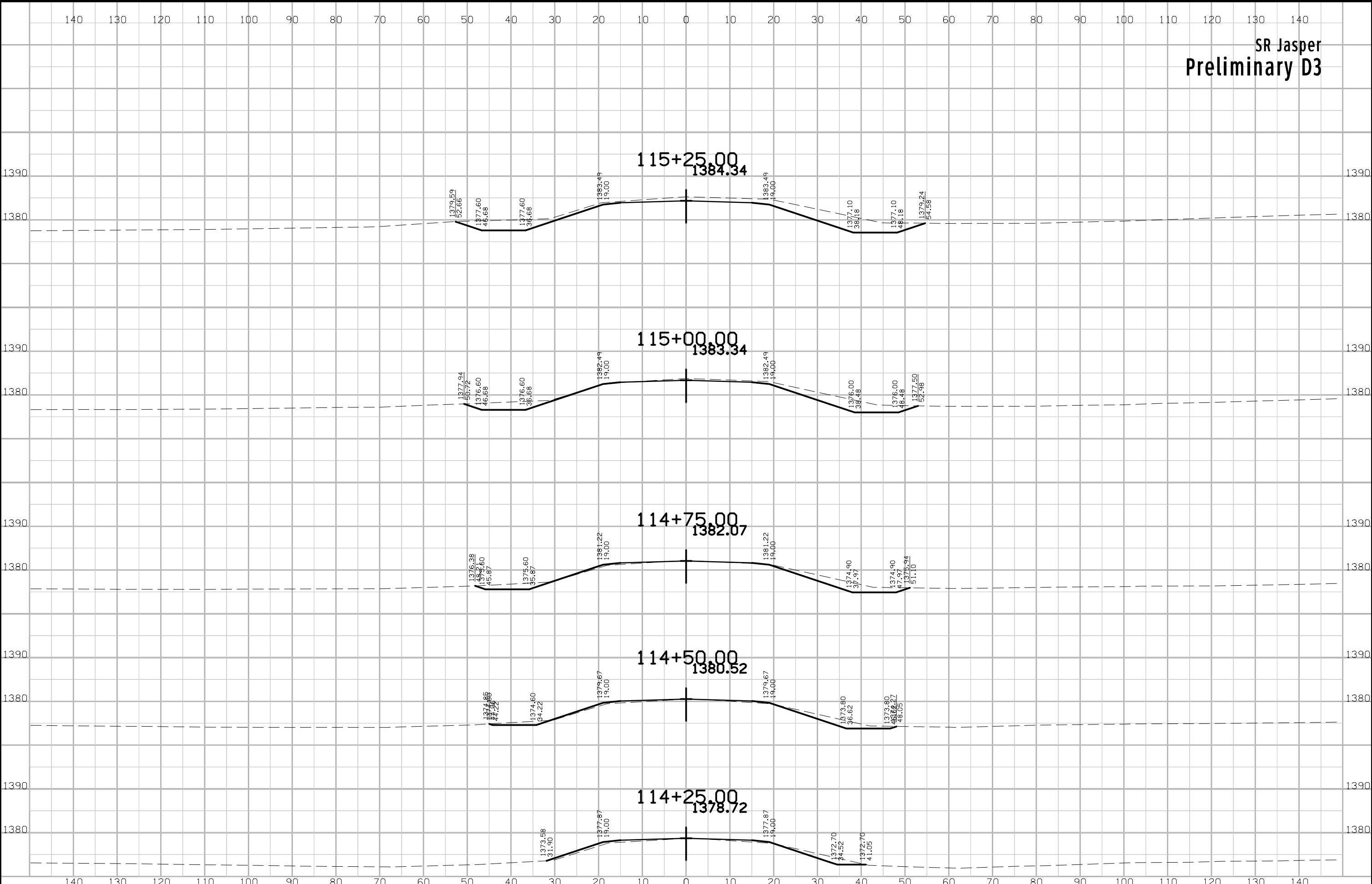
280 260 240 220 200 180 160 140 120 100 80 60 40 20 0 20 40 60 80 100 120 140 160 180 200 220 240 260 280

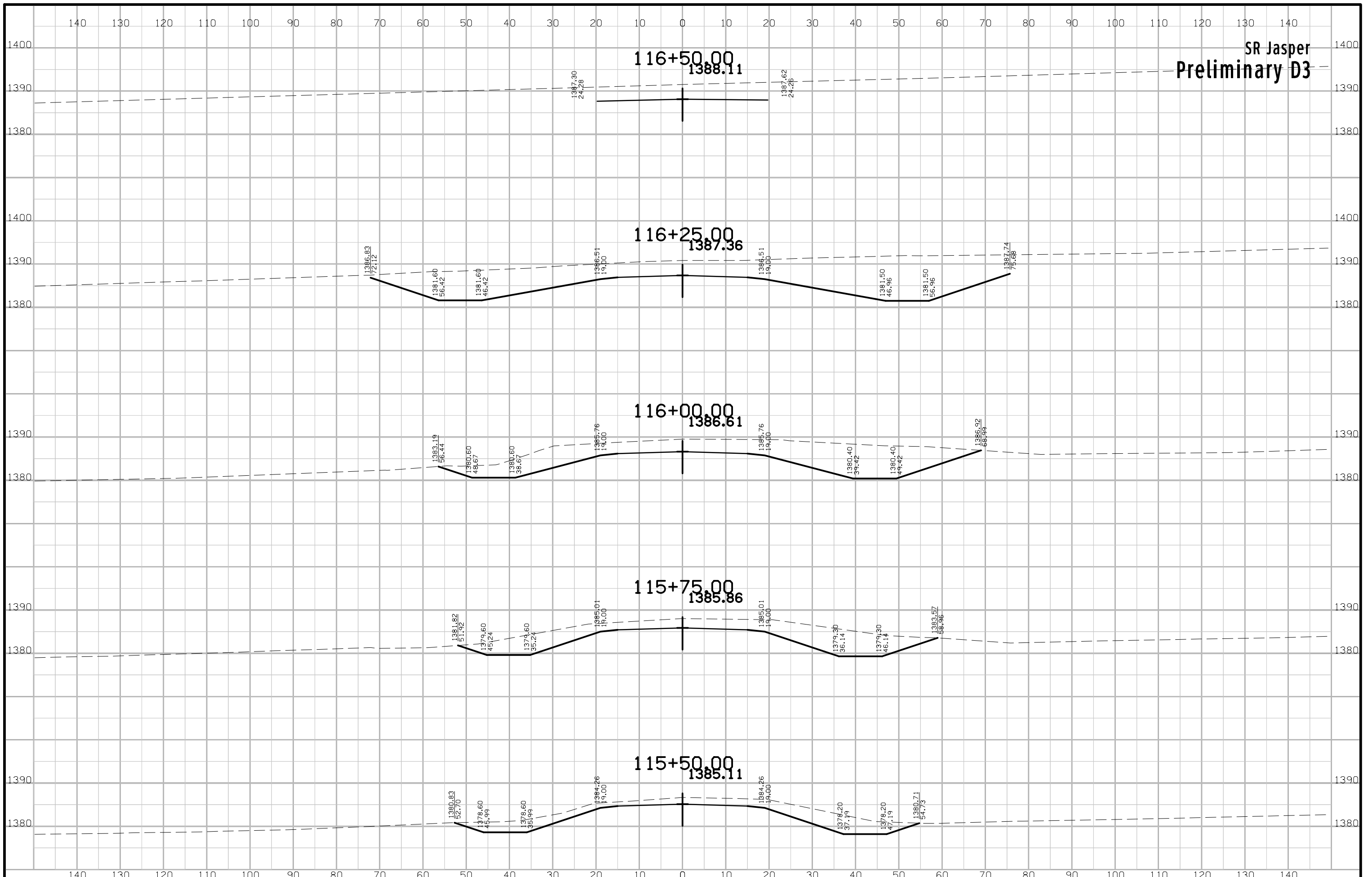
US 20 Sec1
Preliminary D3



280 260 240 220 200 180 160 140 120 100 80 60 40 20 0 20 40 60 80 100 120 140 160 180 200 220 240 260 280

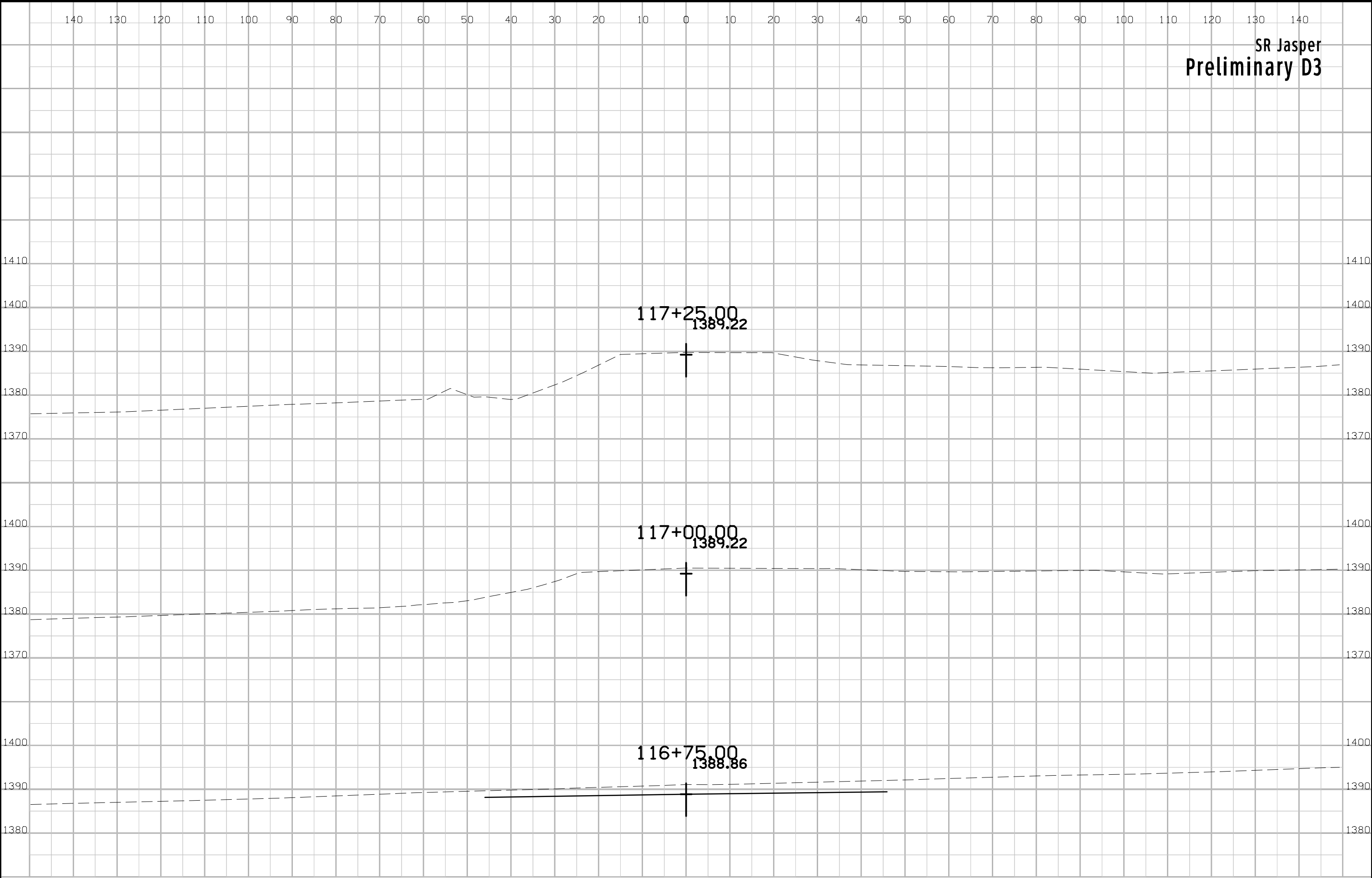
SR Jasper
Preliminary D3



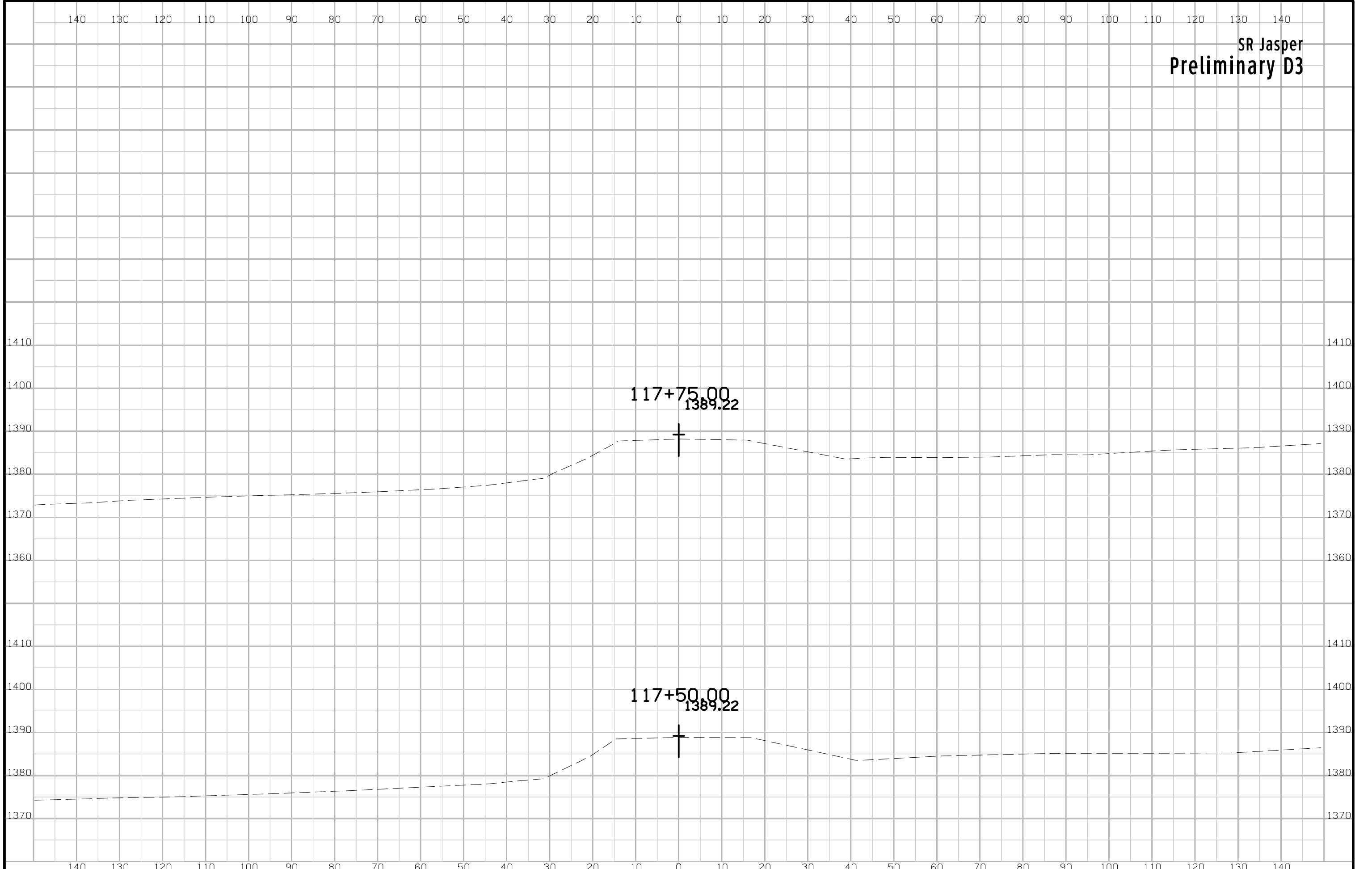


SR Jasper
Preliminary D3

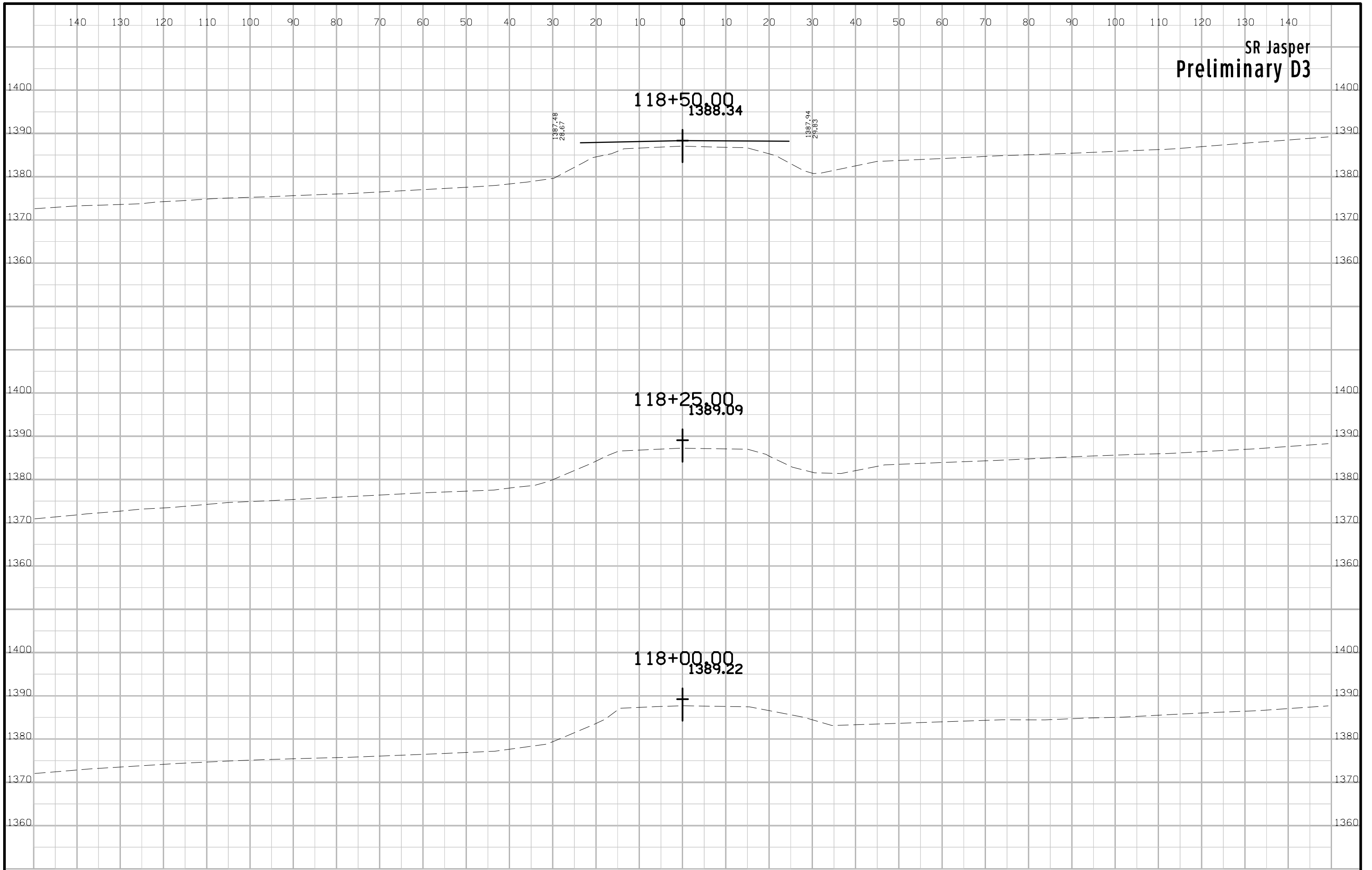
SR Jasper
Preliminary D3



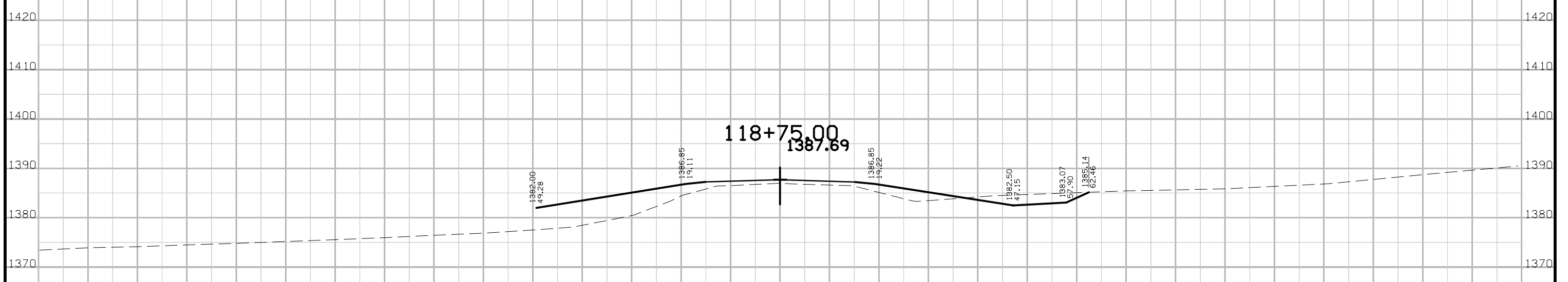
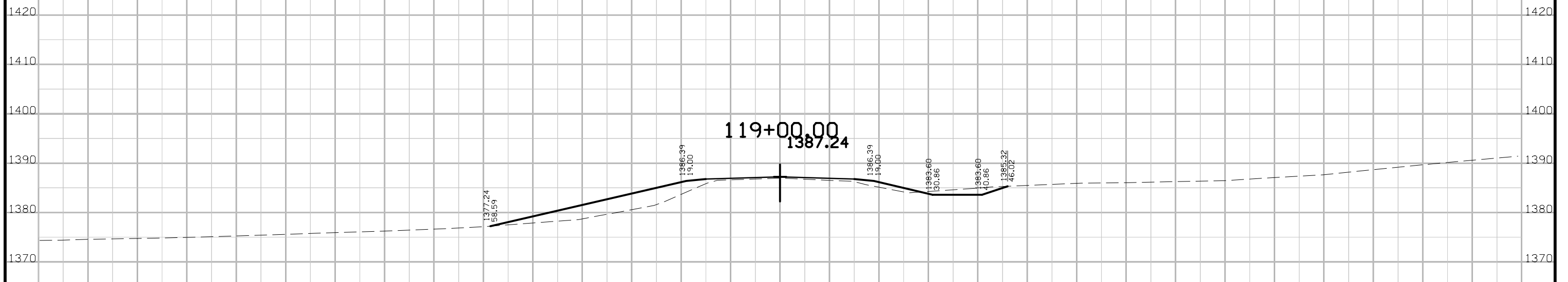
SR Jasper
Preliminary D3



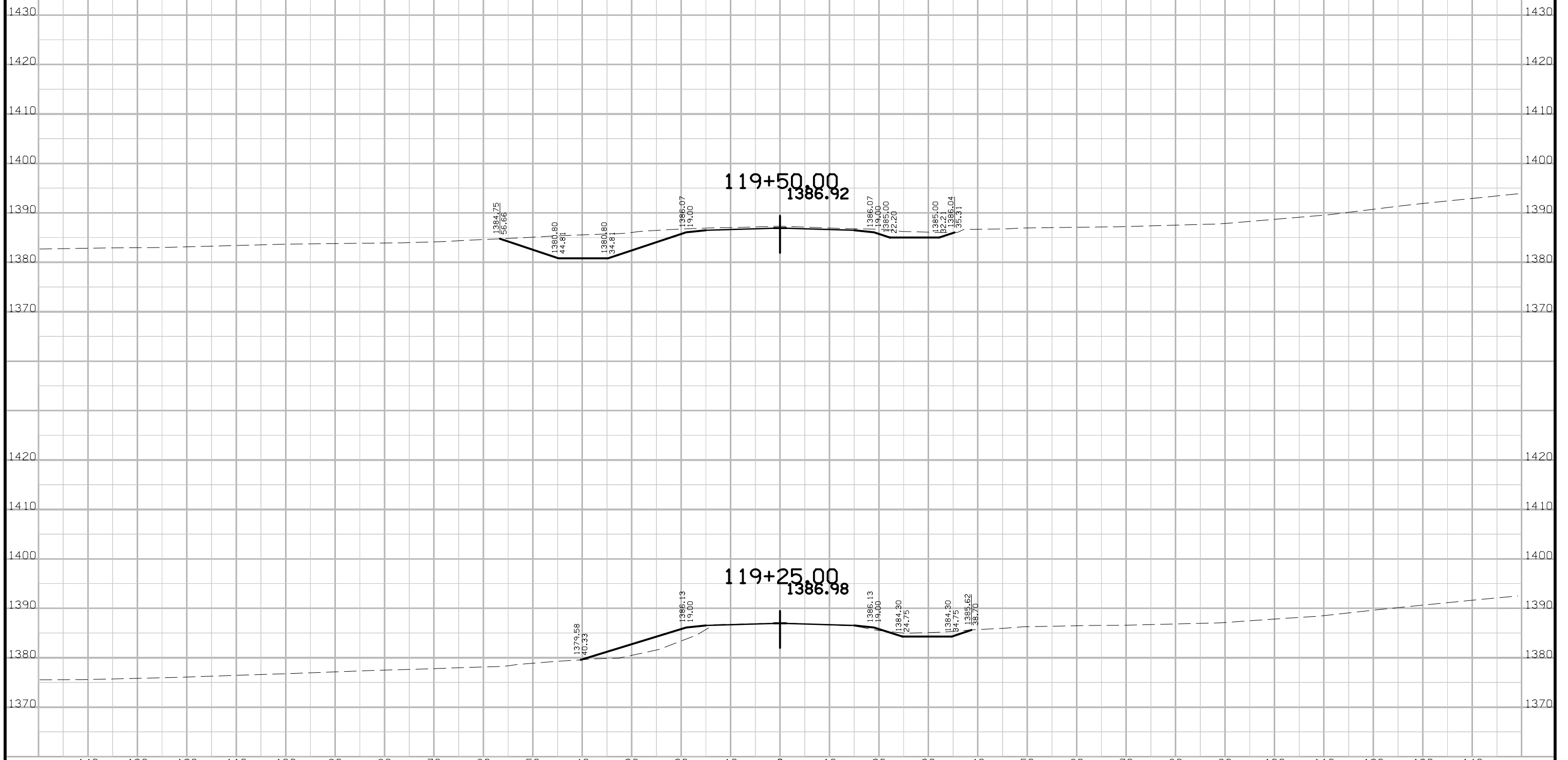
SR Jasper
Preliminary D3



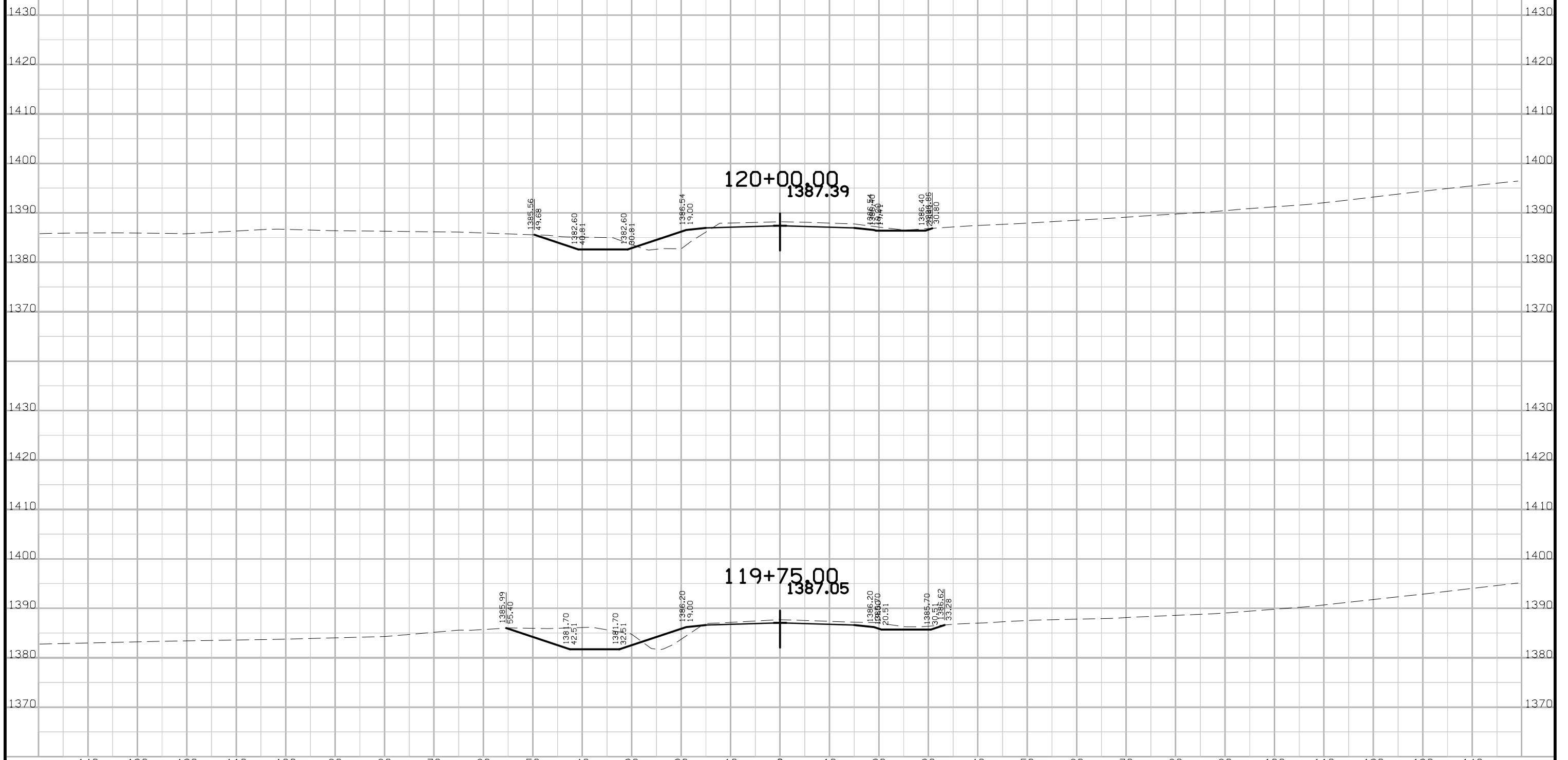
SR Jasper
Preliminary D3



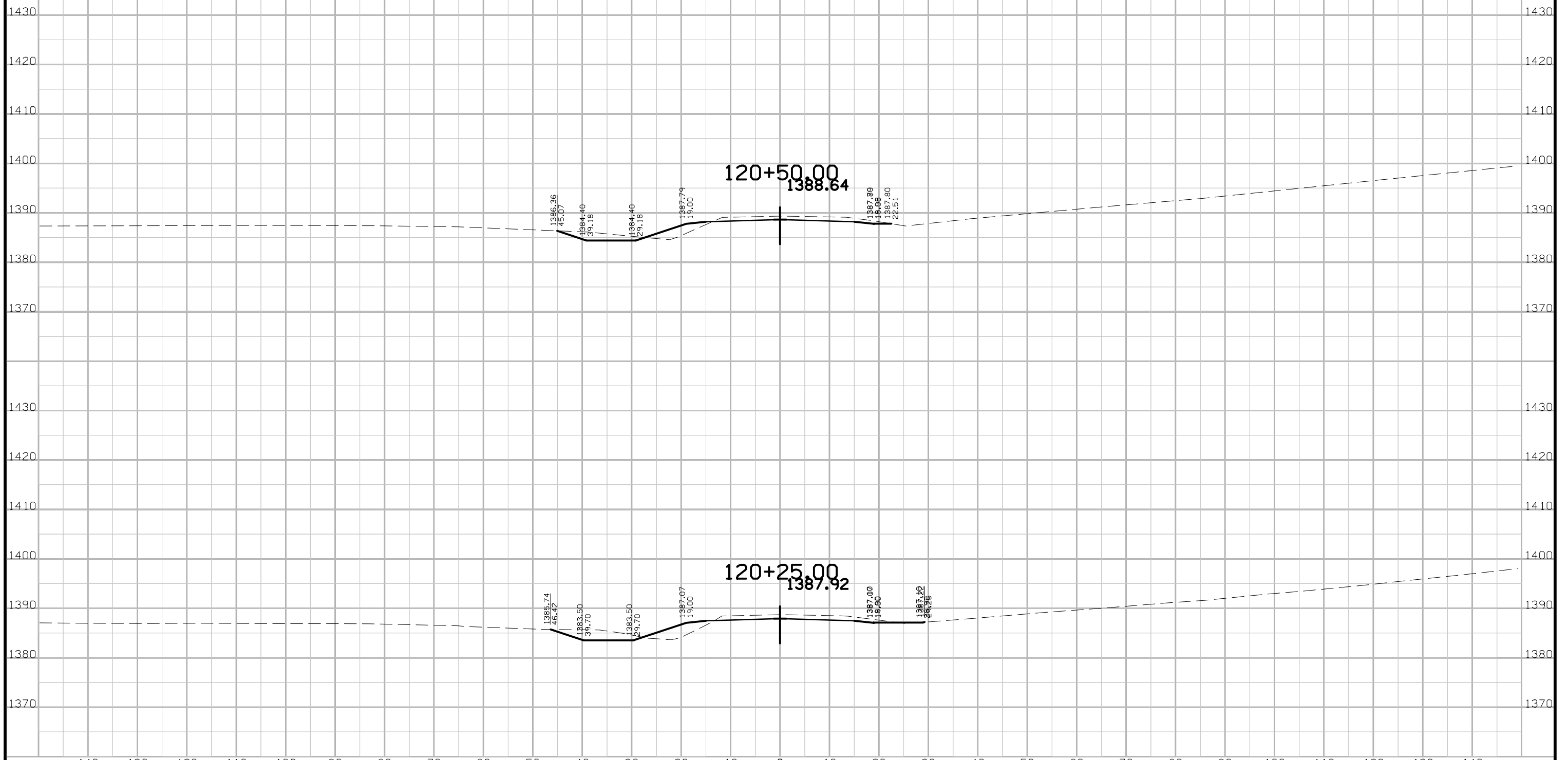
SR Jasper
Preliminary D3



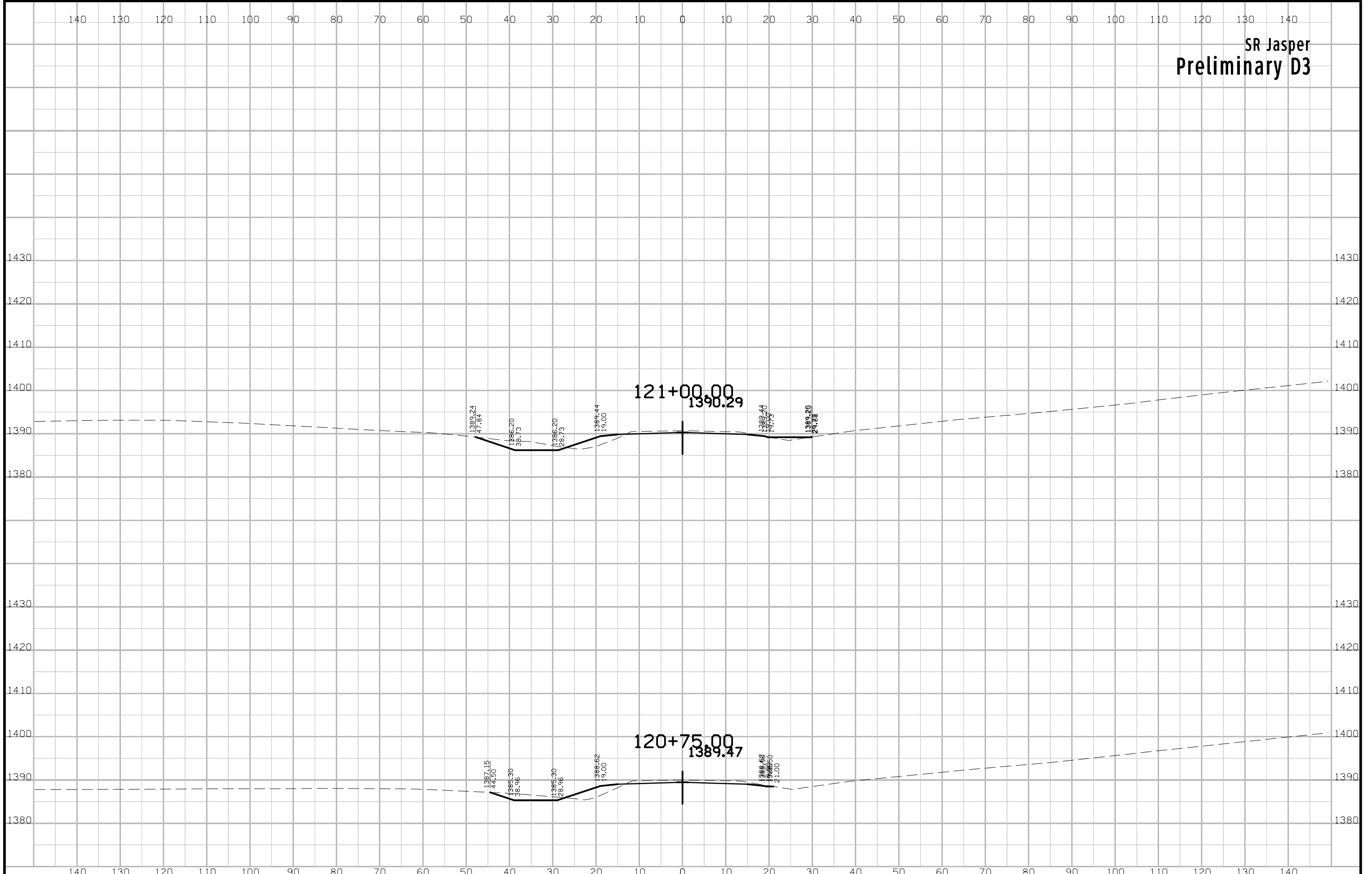
SR Jasper
Preliminary D3



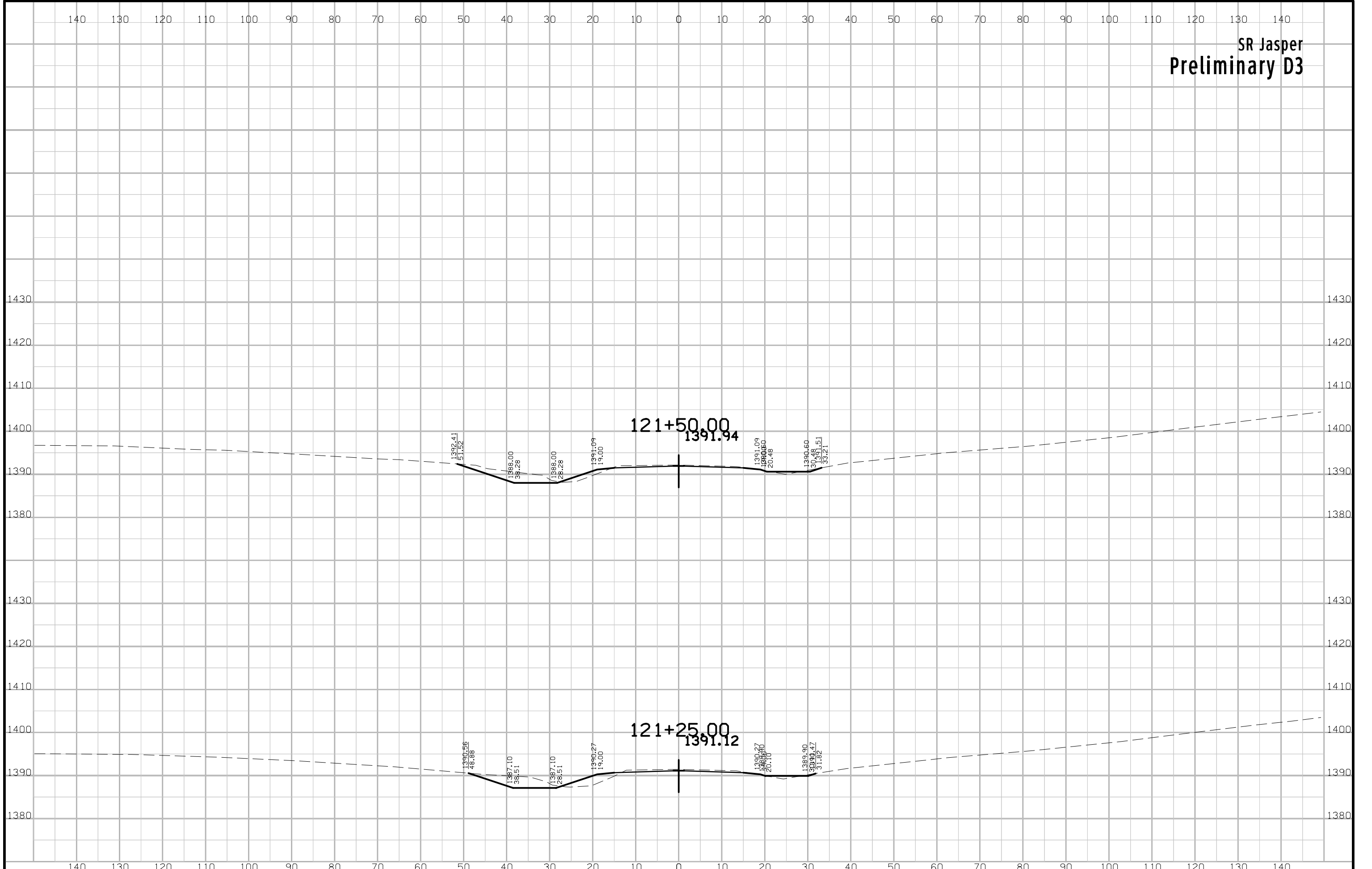
SR Jasper
Preliminary D3



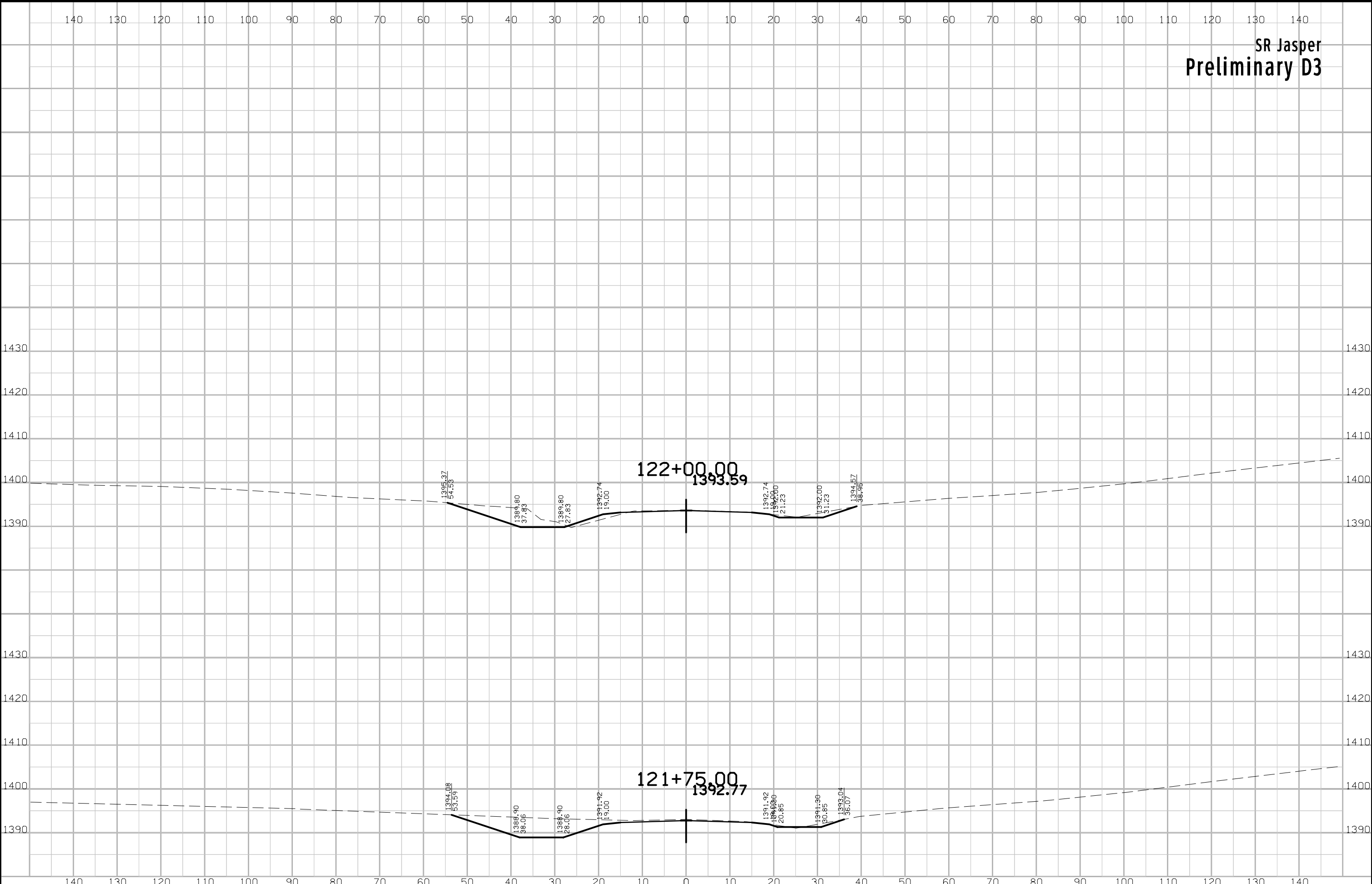
SR Jasper
Preliminary D3



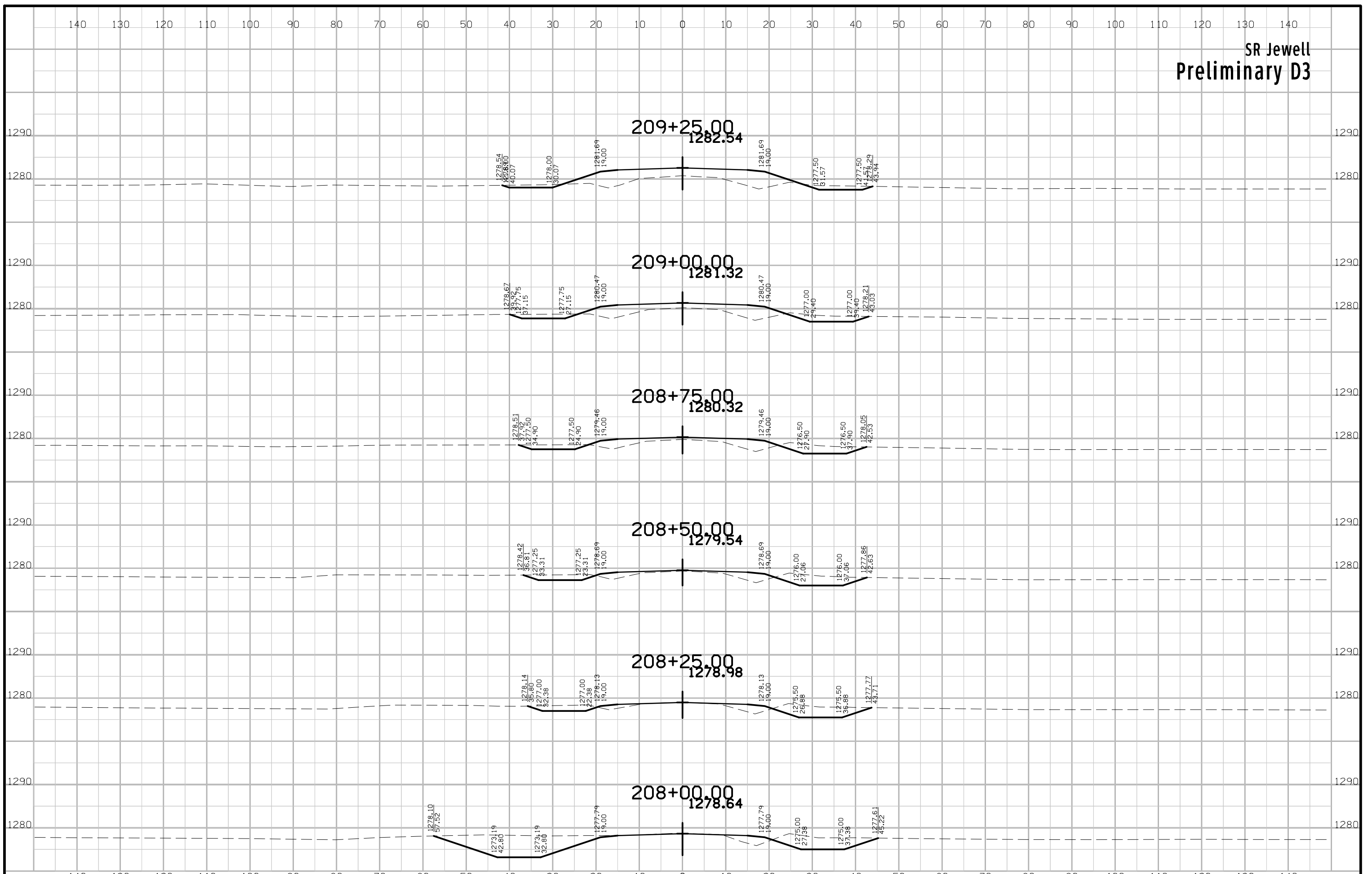
SR Jasper
Preliminary D3



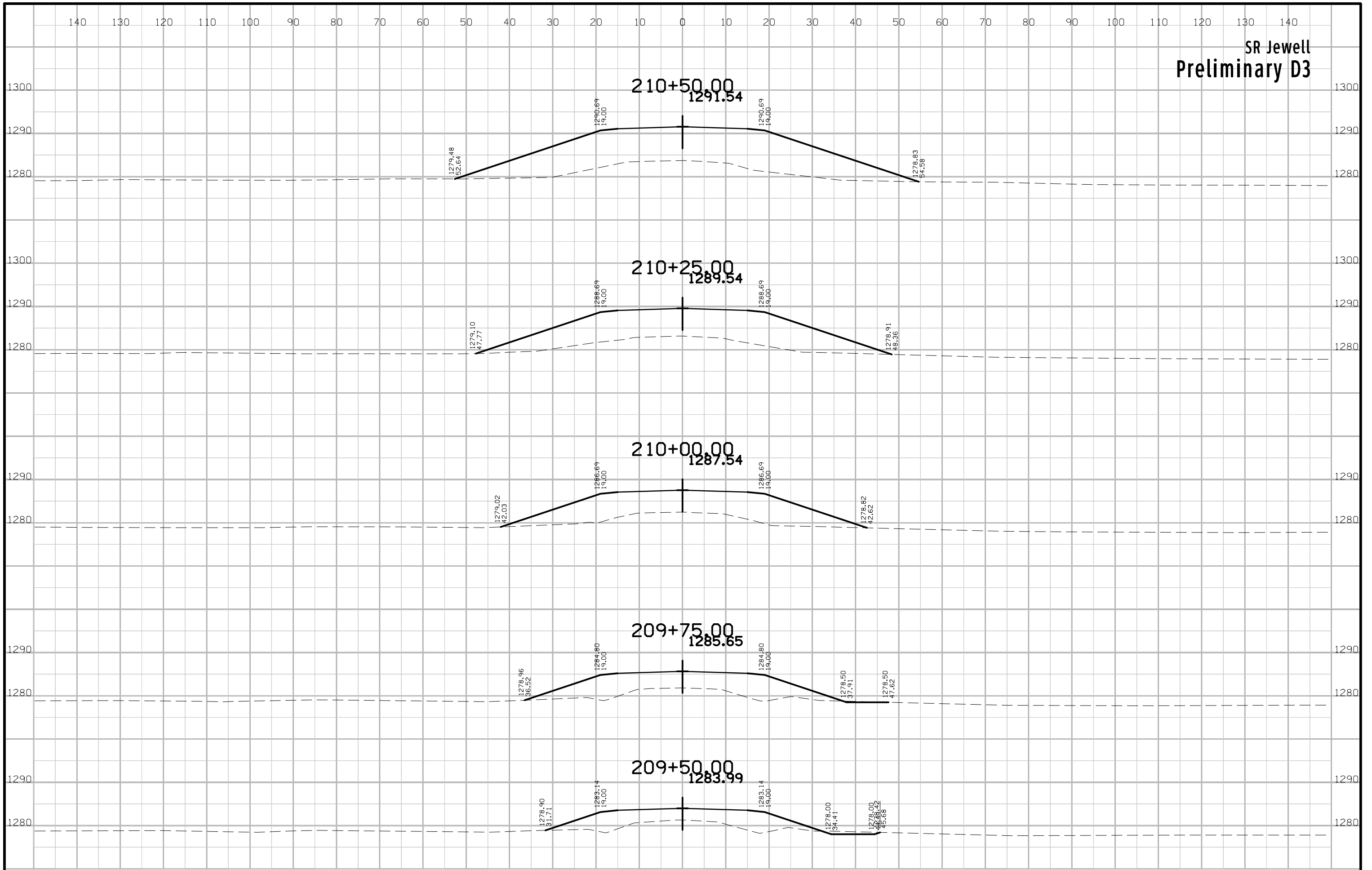
SR Jasper
Preliminary D3



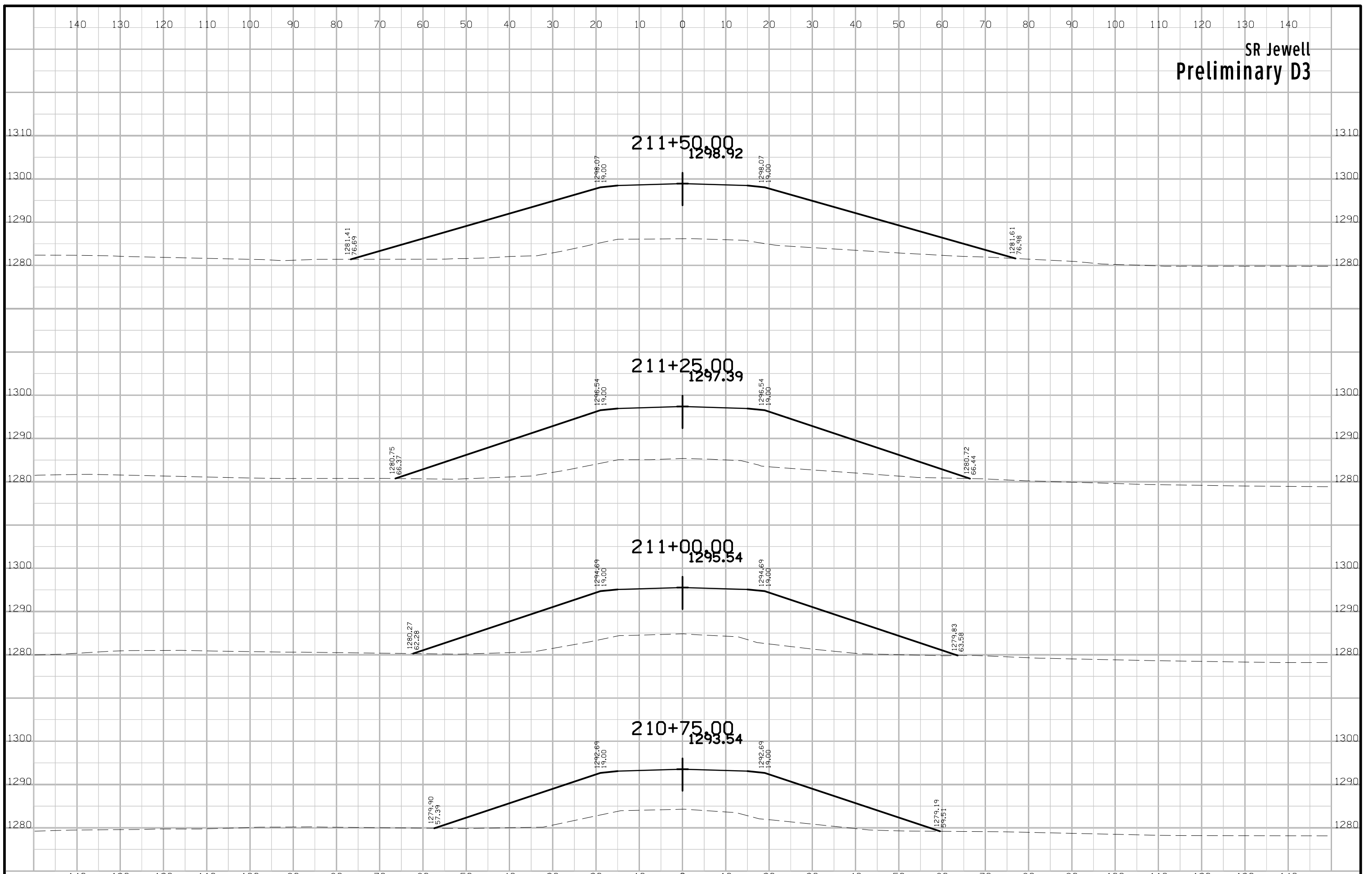
SR Jewell
Preliminary D3

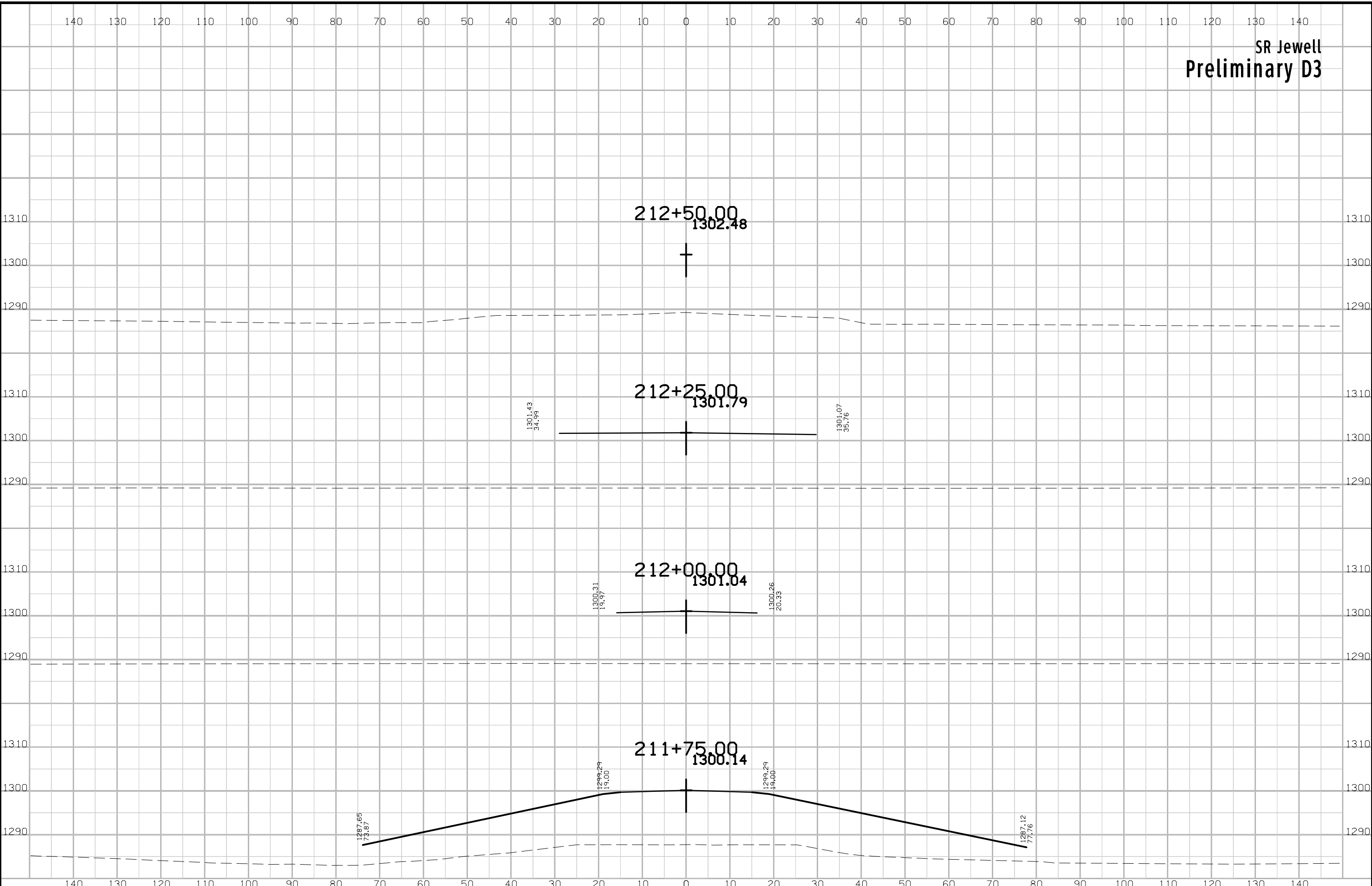


SR Jewell
Preliminary D3

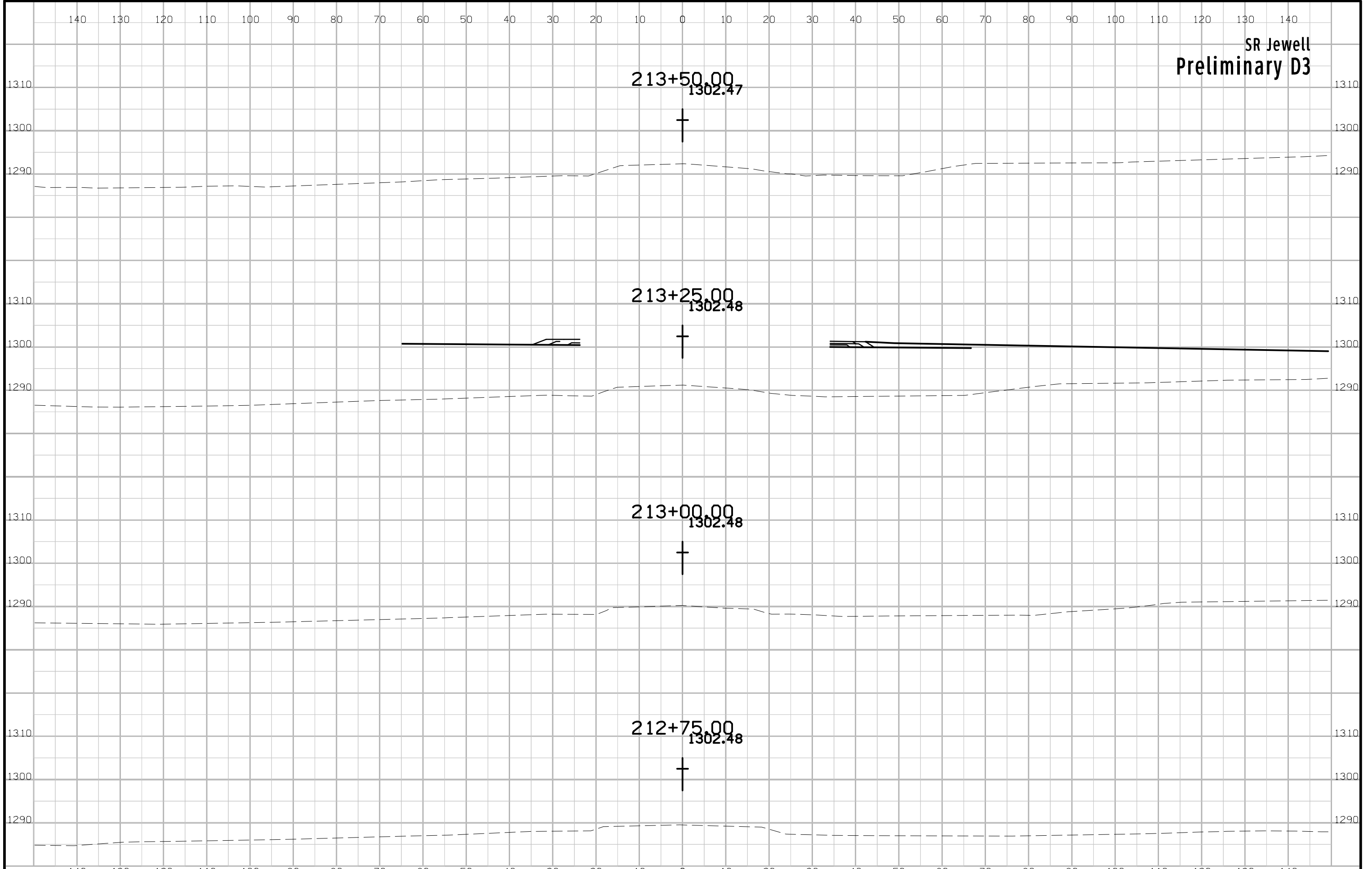


SR Jewell
Preliminary D3

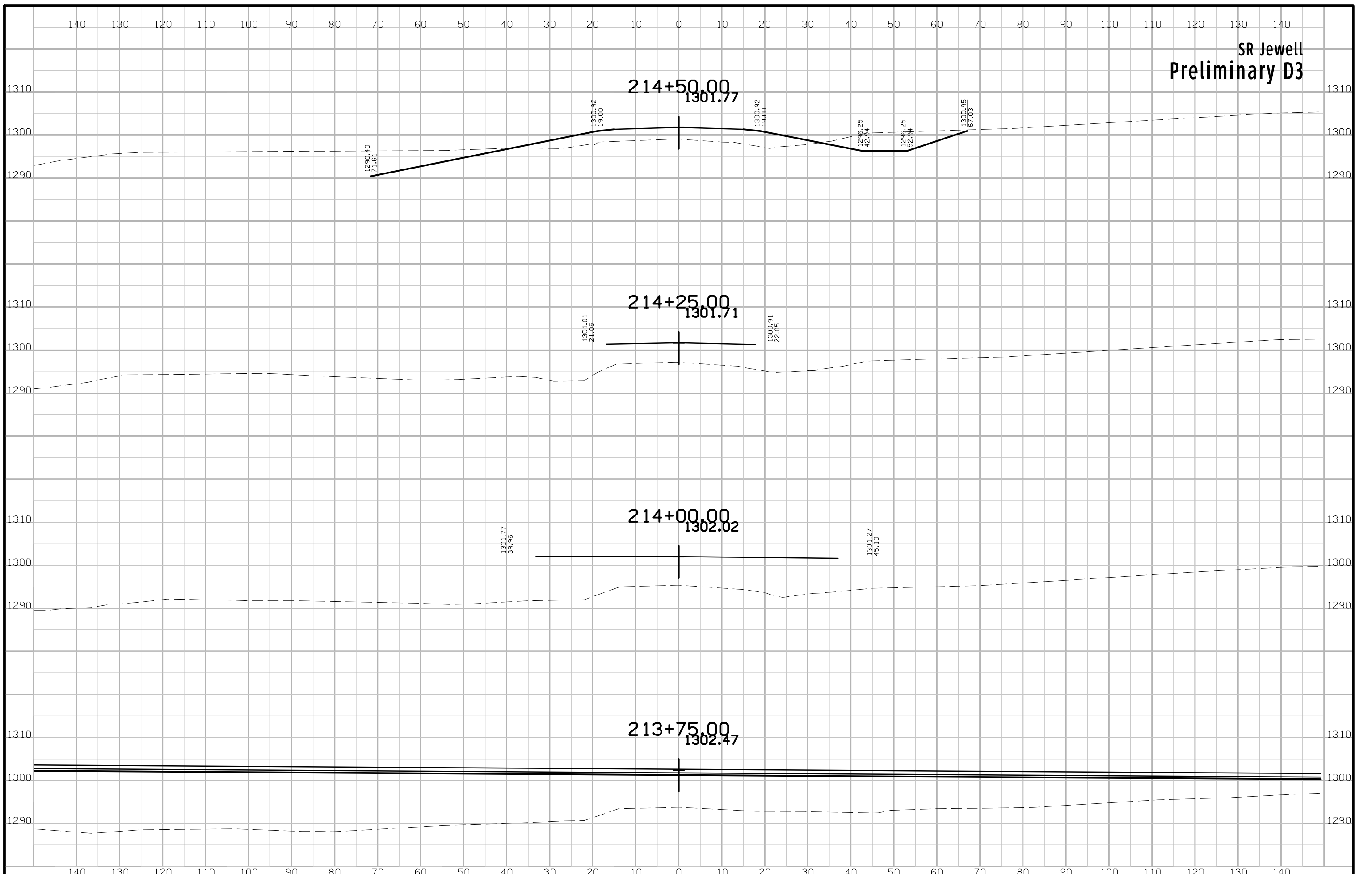




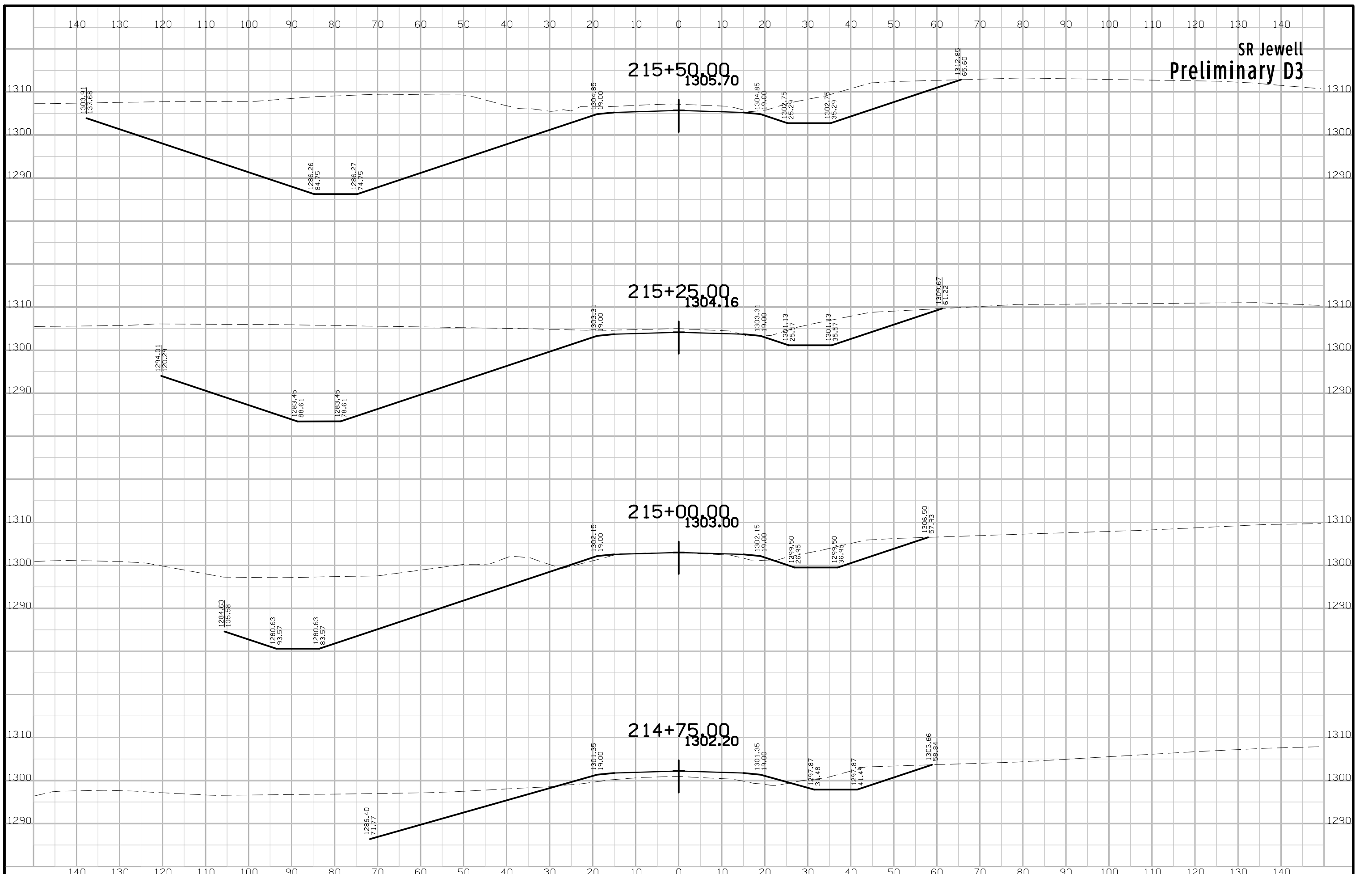
SR Jewell
Preliminary D3



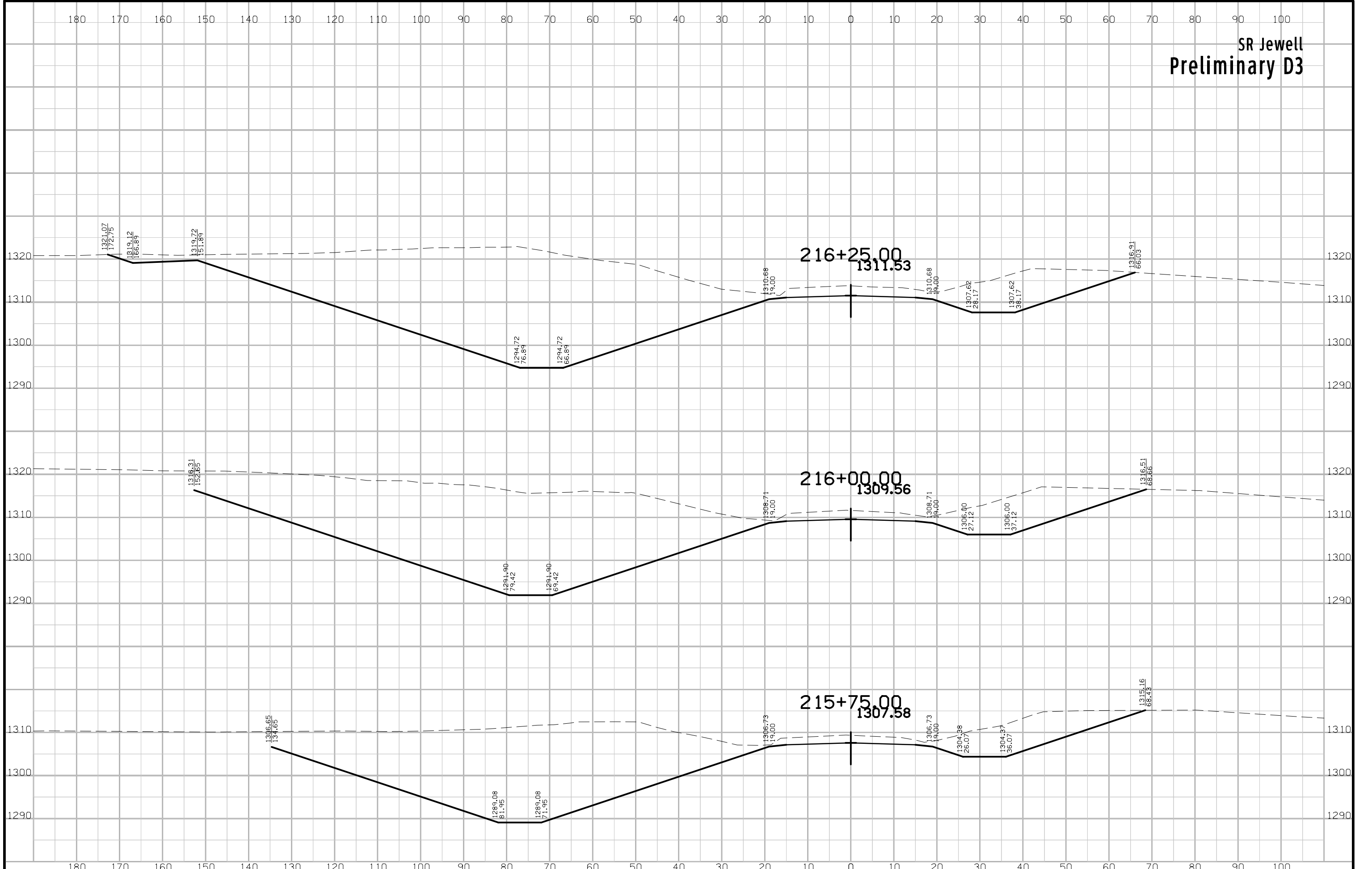
SR Jewell
Preliminary D3



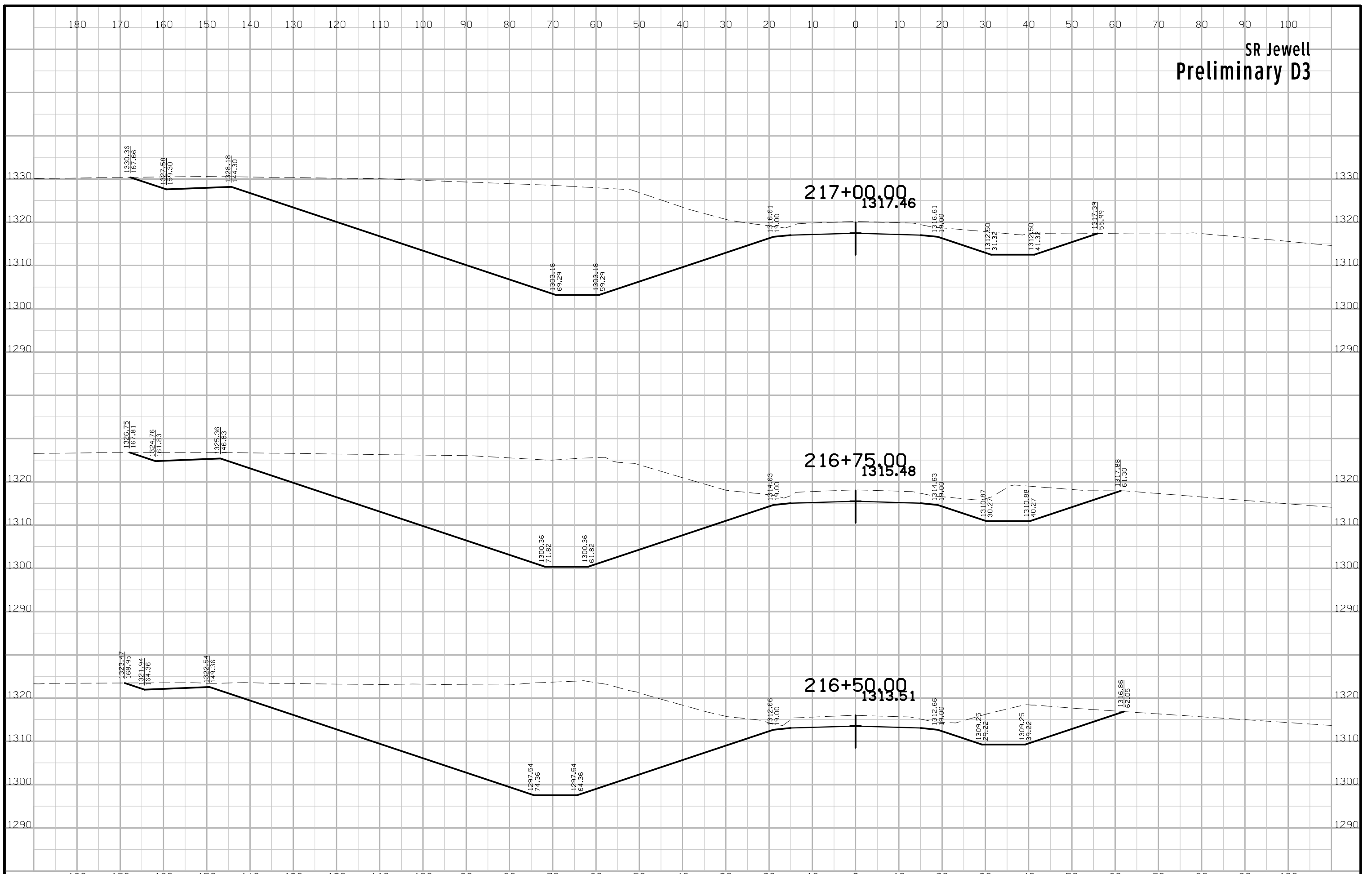
SR Jewell
Preliminary D3



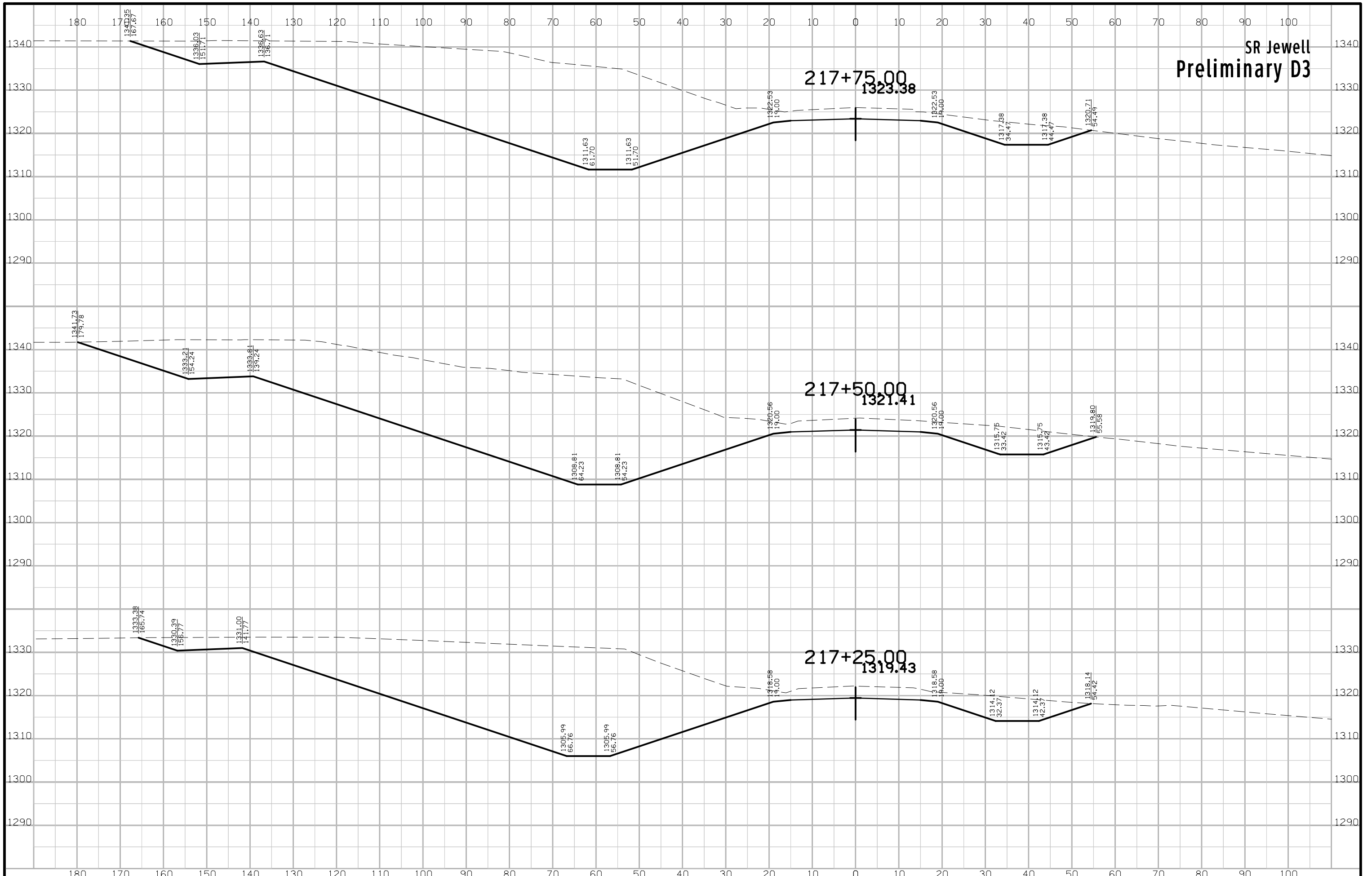
SR Jewell
Preliminary D3



SR Jewell
Preliminary D3



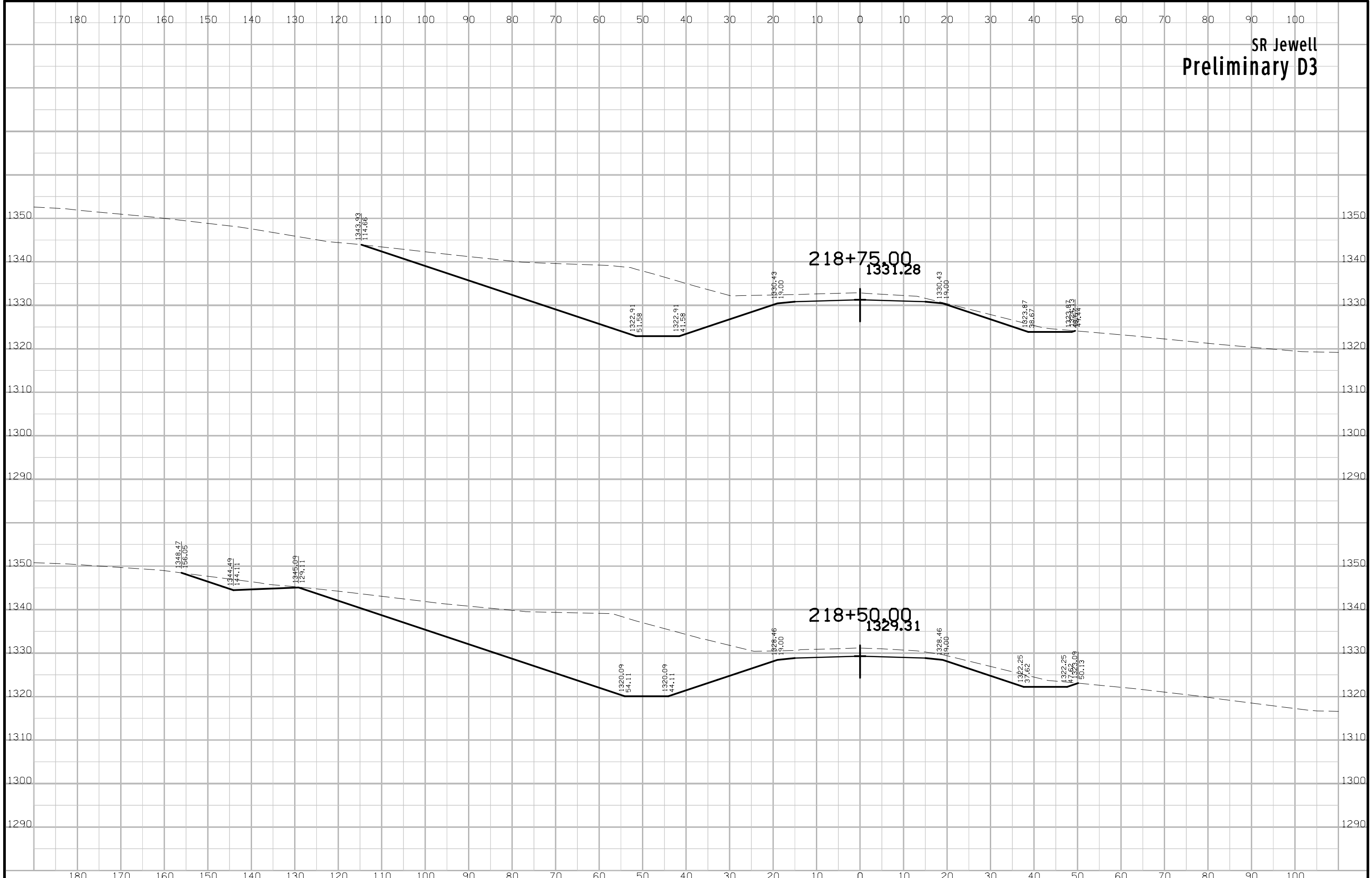
SR Jewell
Preliminary D3



SR Jewell
Preliminary D3



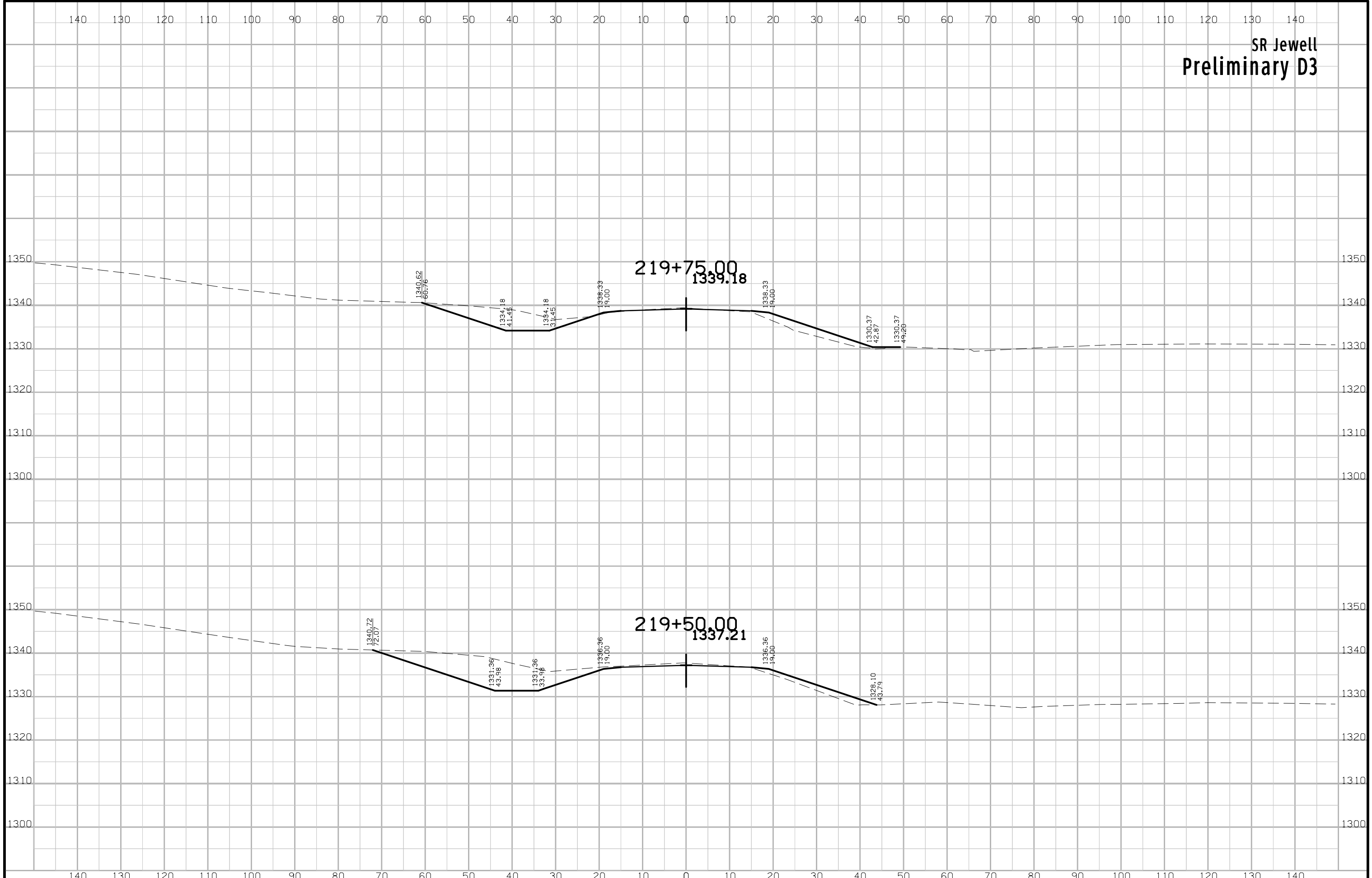
SR Jewell
Preliminary D3

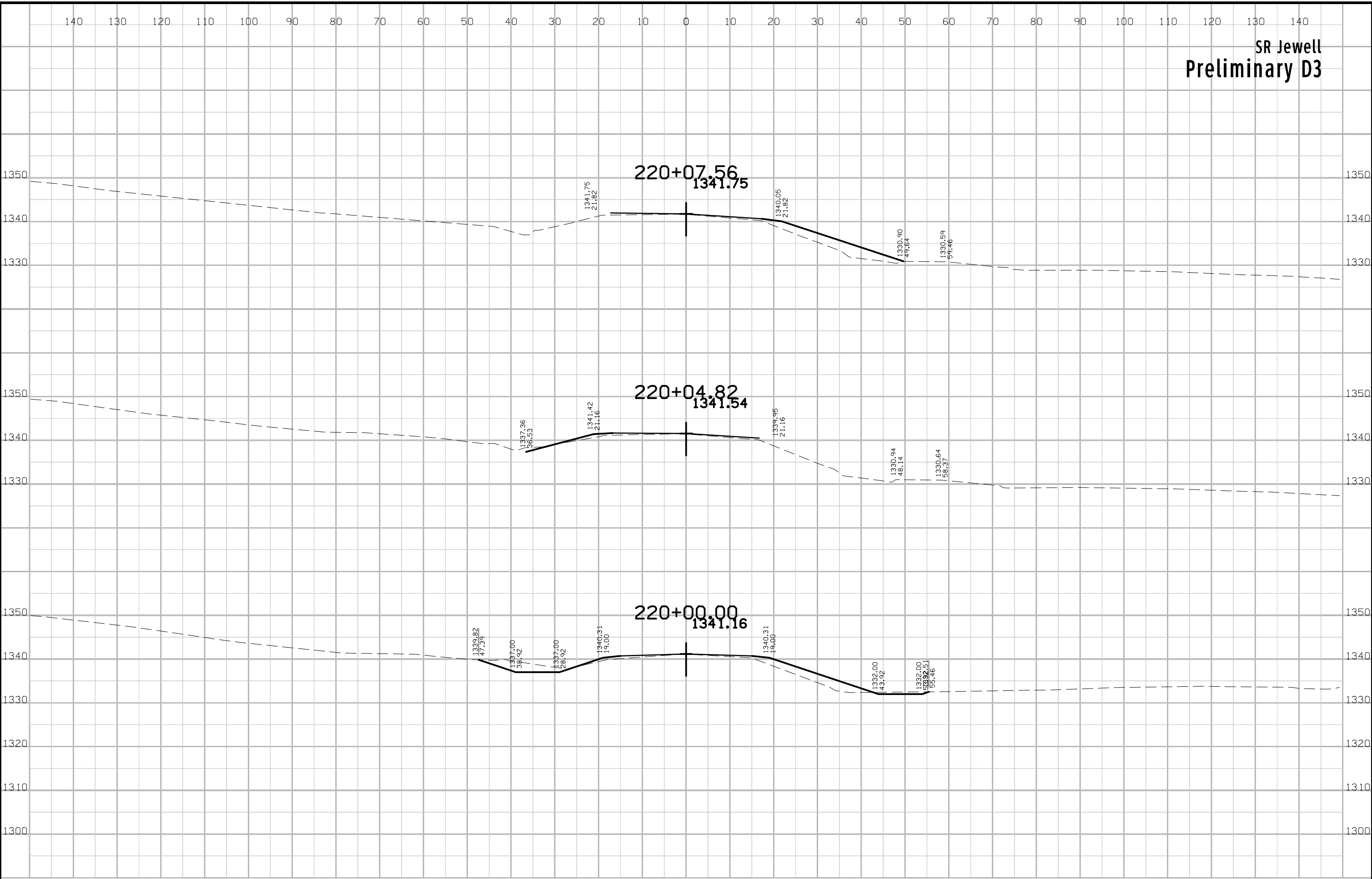


SR Jewell
Preliminary D3

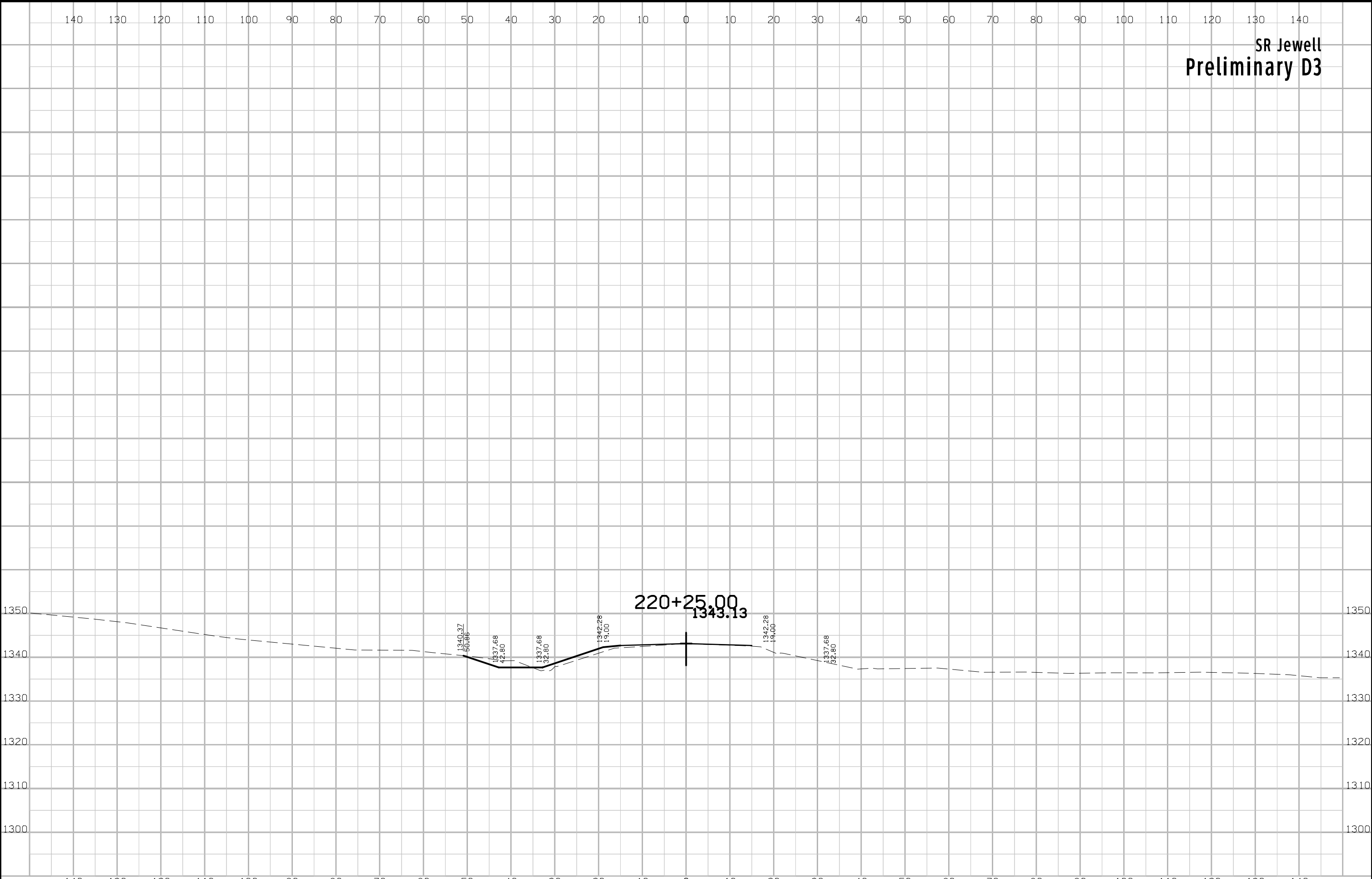


SR Jewell
Preliminary D3

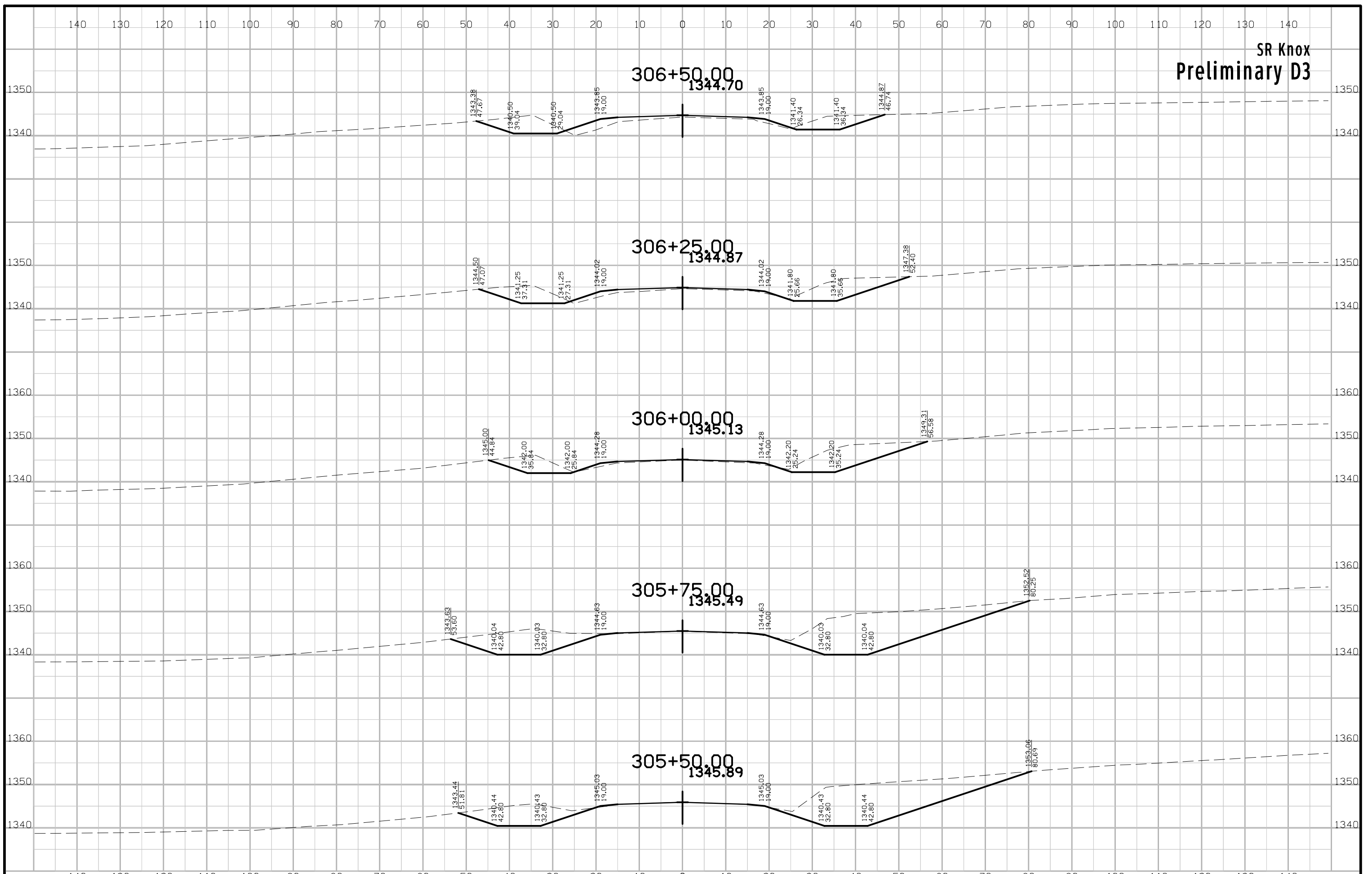




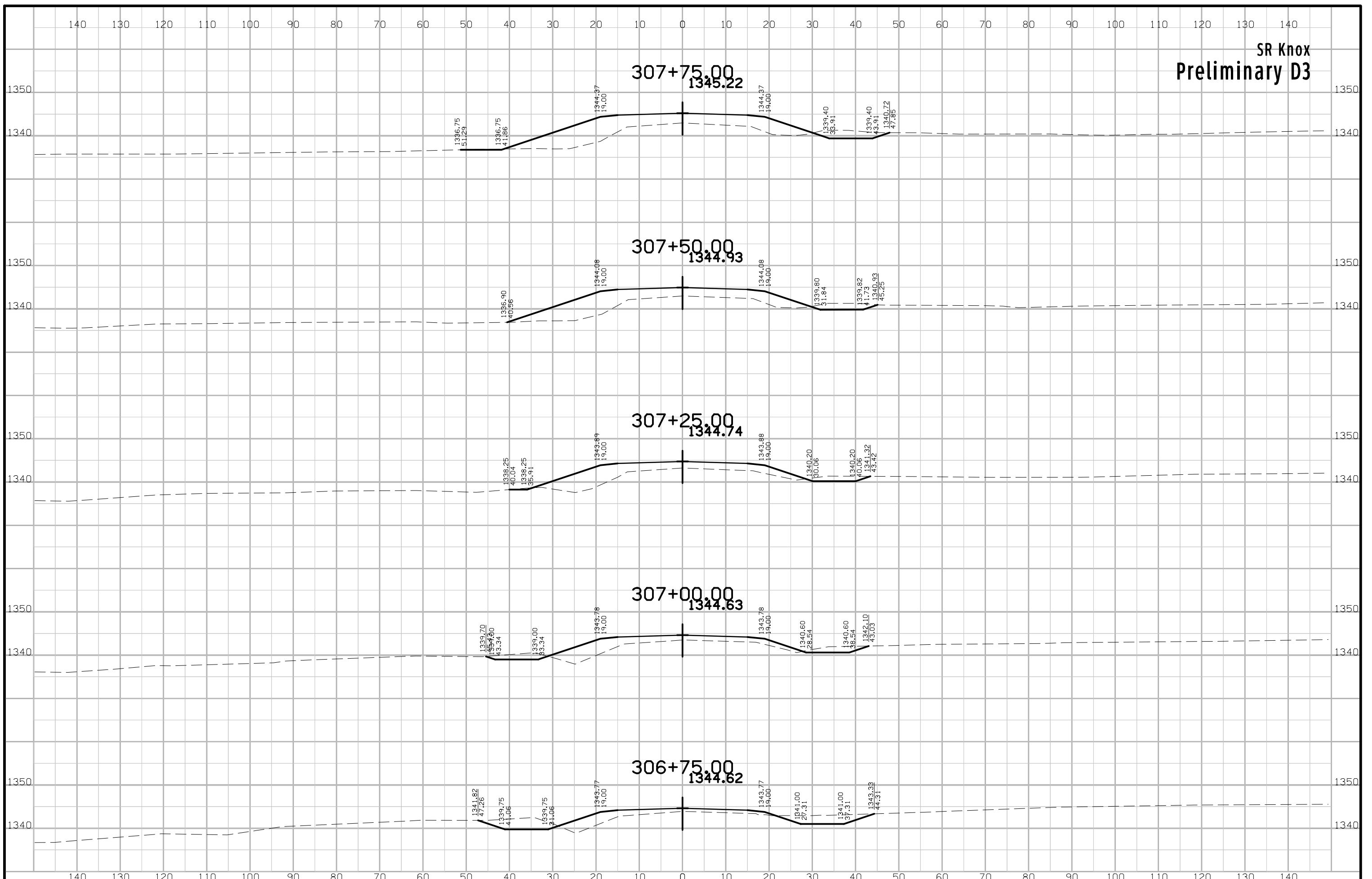
SR Jewell
Preliminary D3



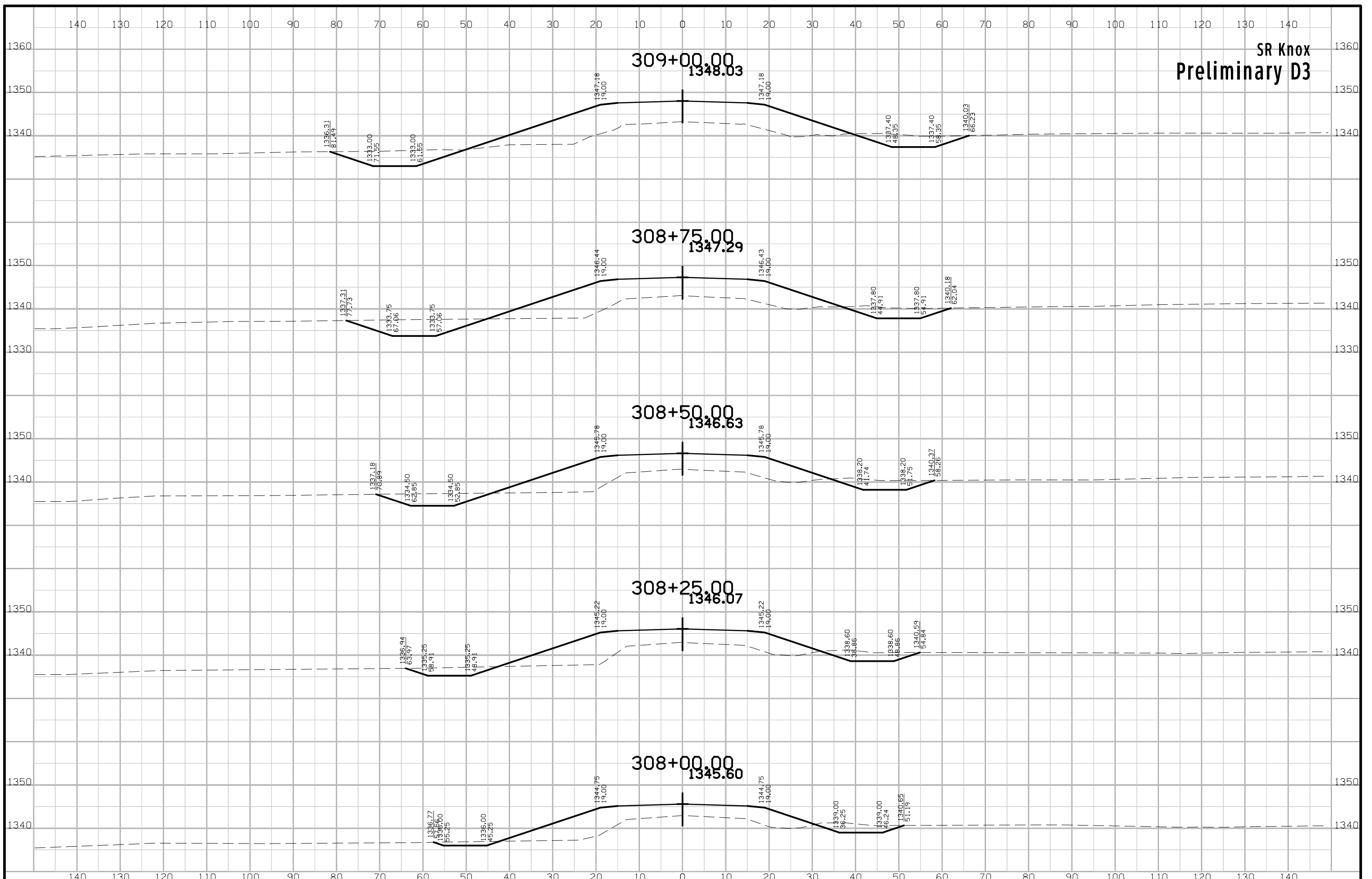
SR Knox
Preliminary D3



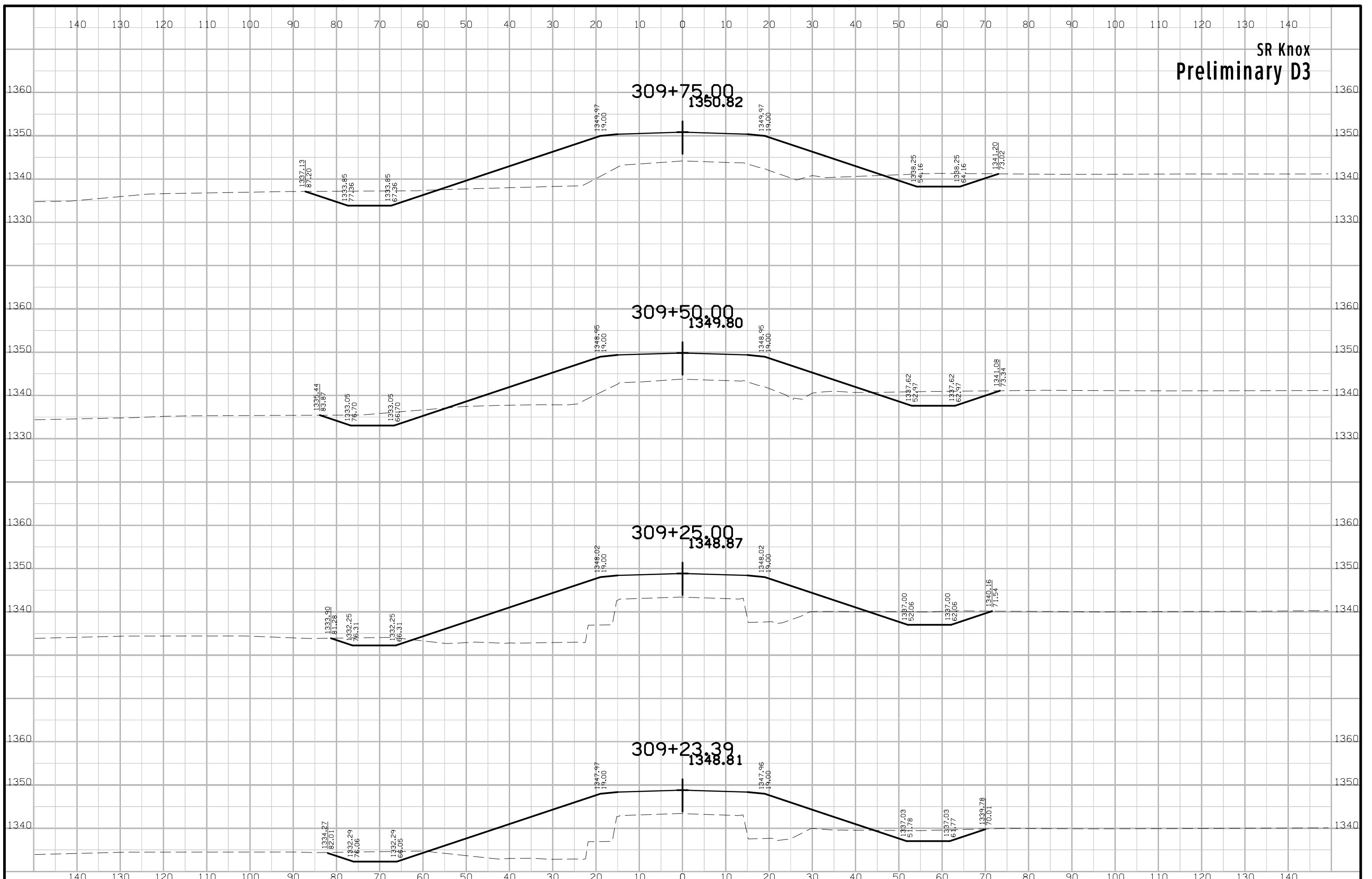
SR Knox
Preliminary D3



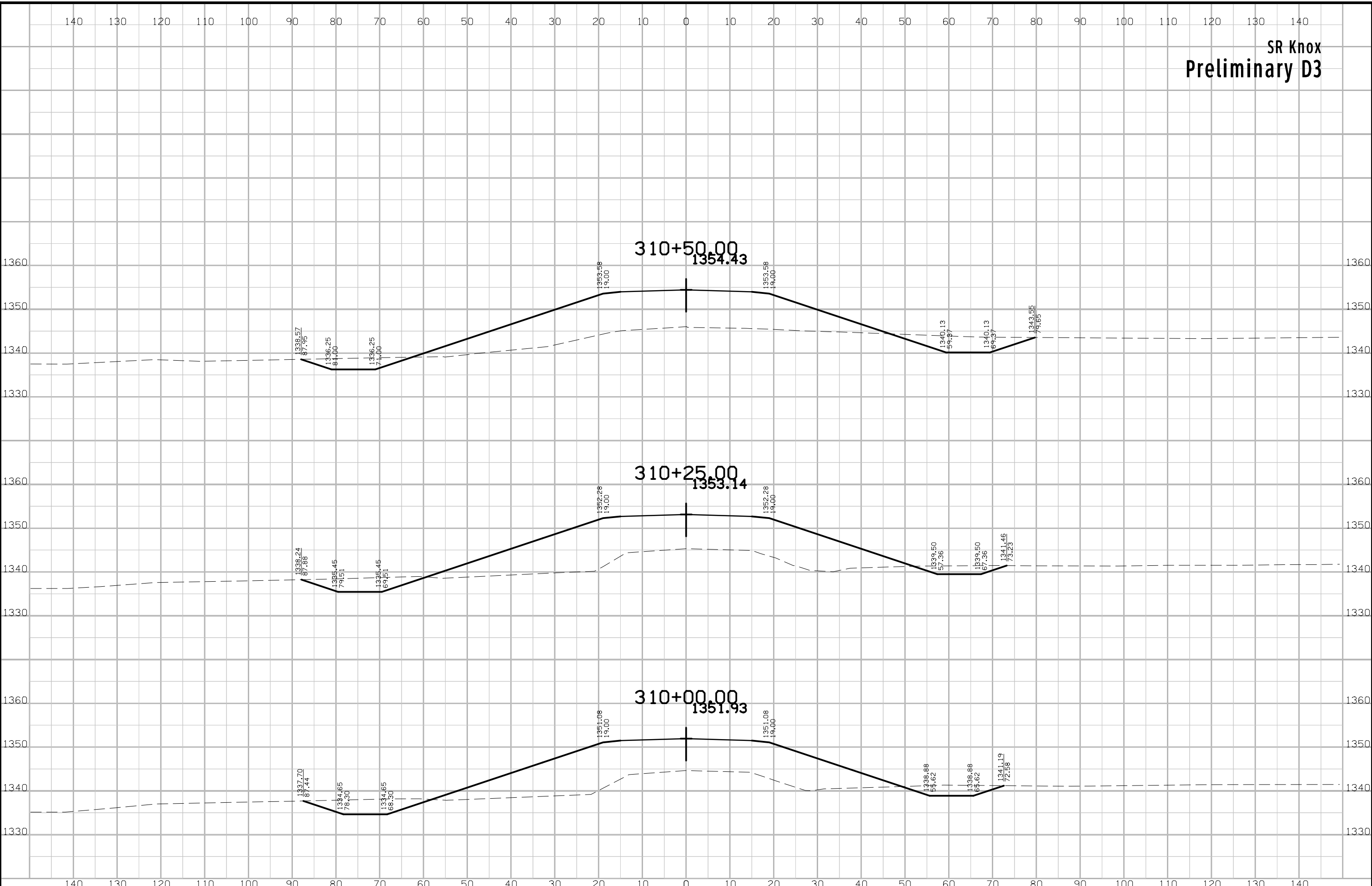
SR Knox
Preliminary D3



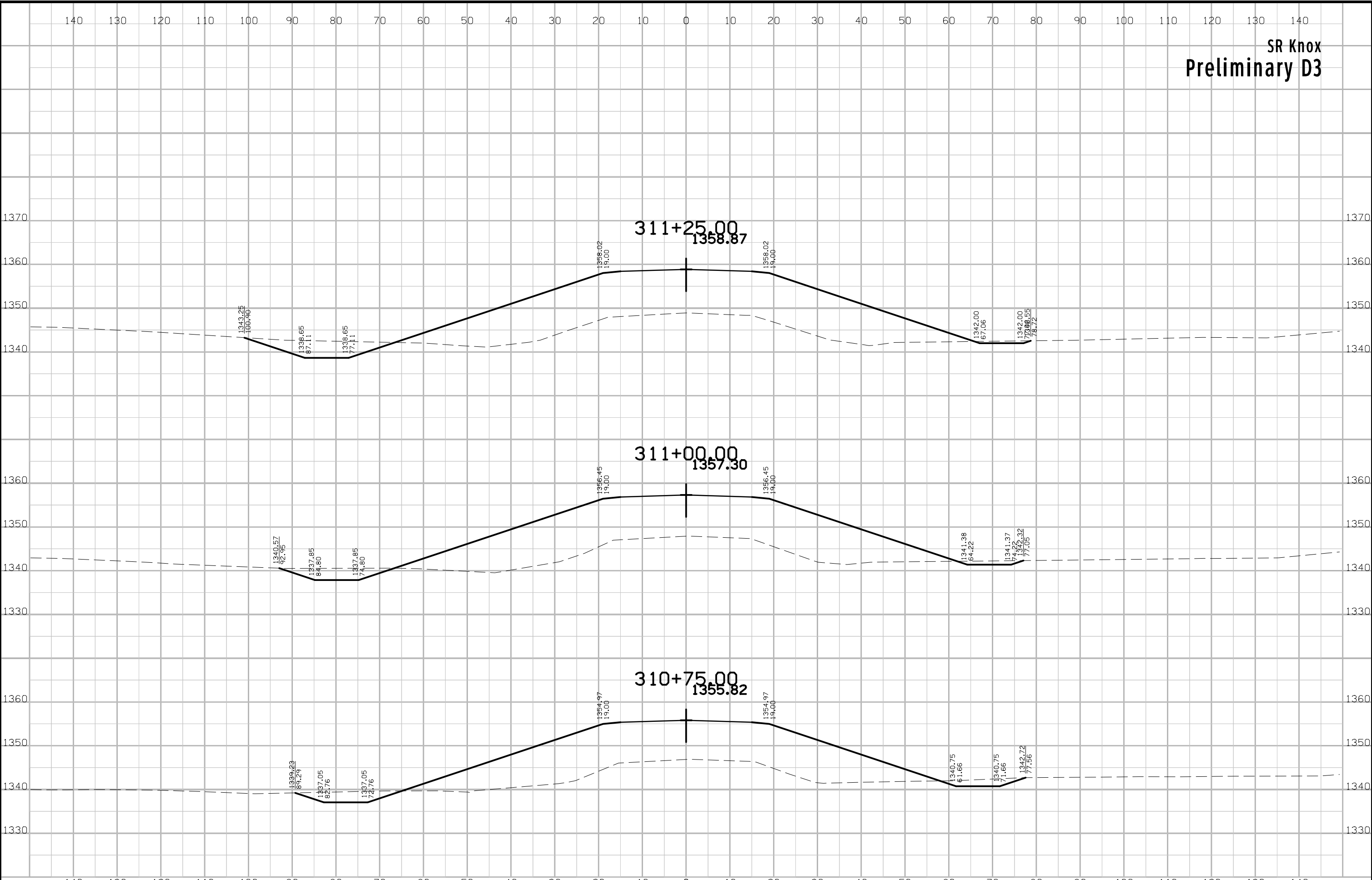
SR Knox
Preliminary D3



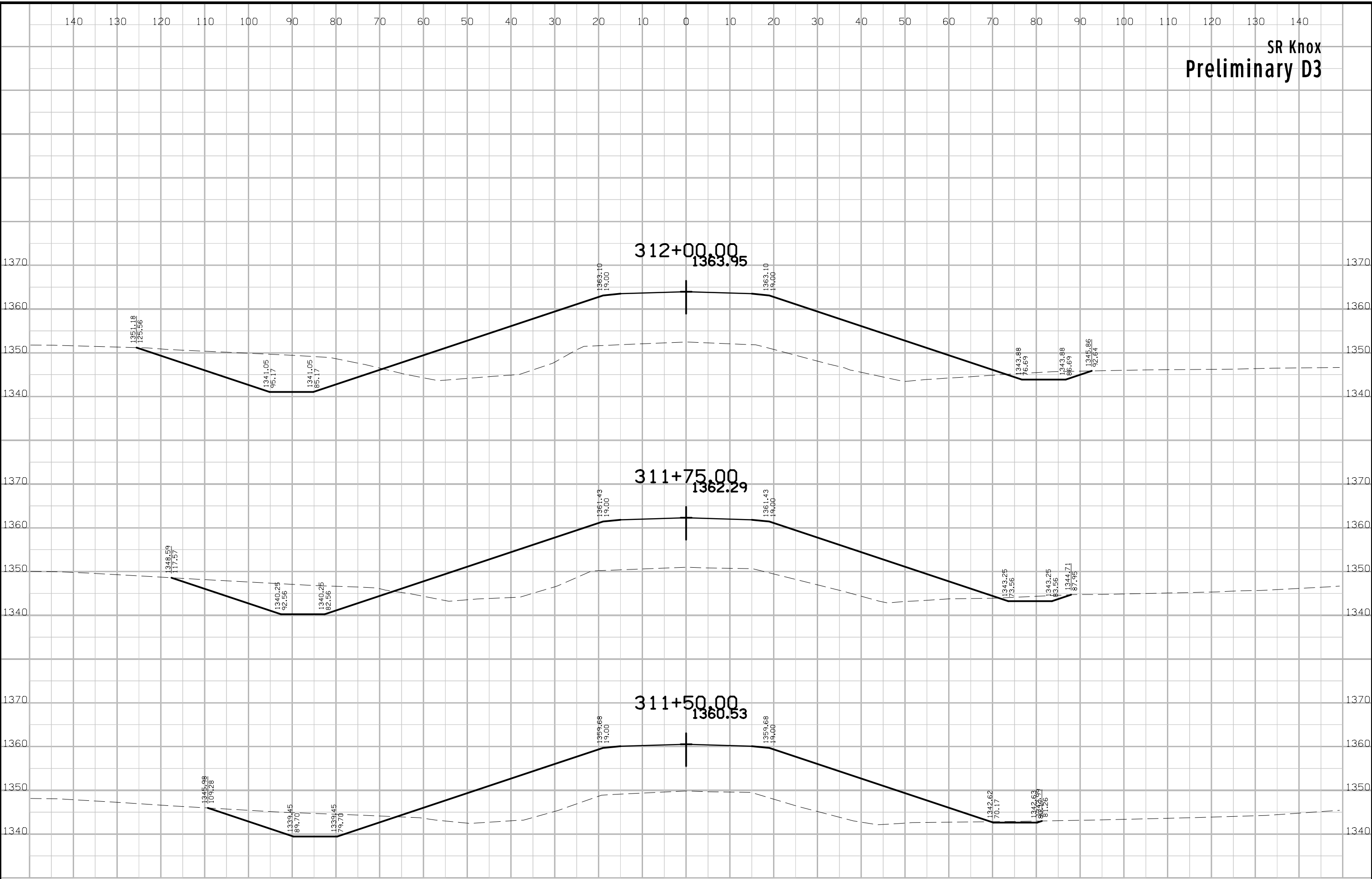
SR Knox
Preliminary D3



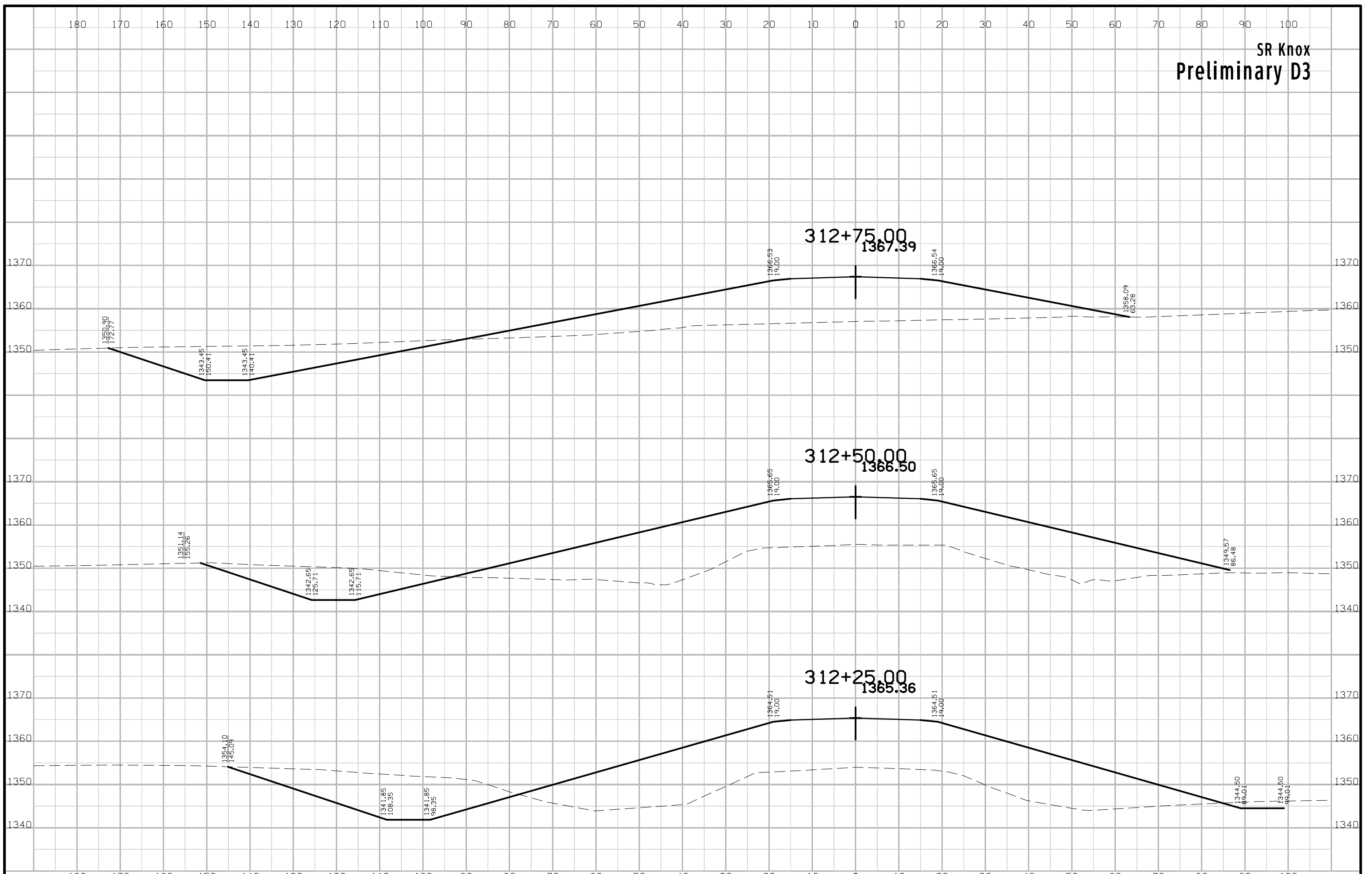
SR Knox
Preliminary D3



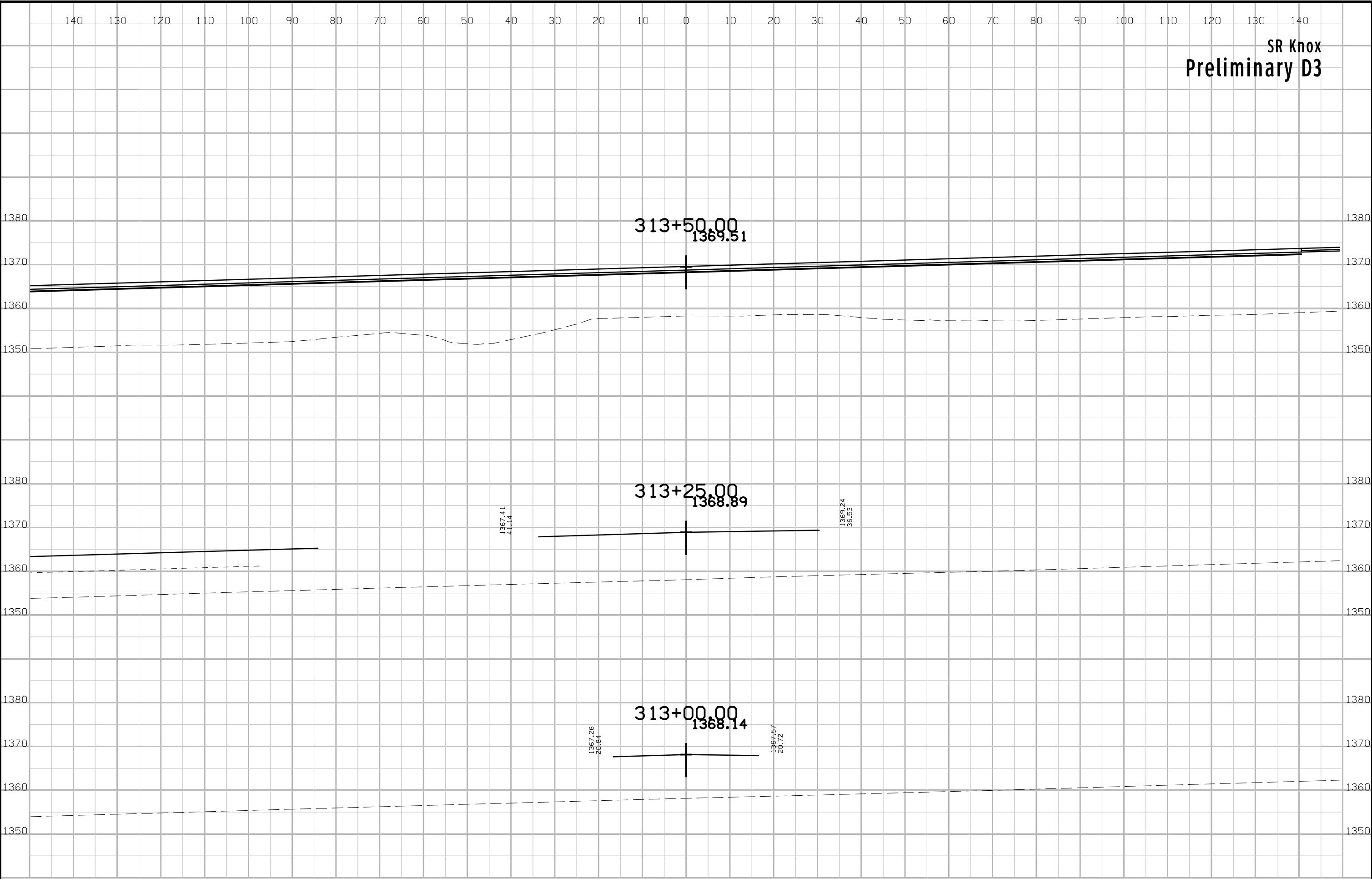
SR Knox
Preliminary D3

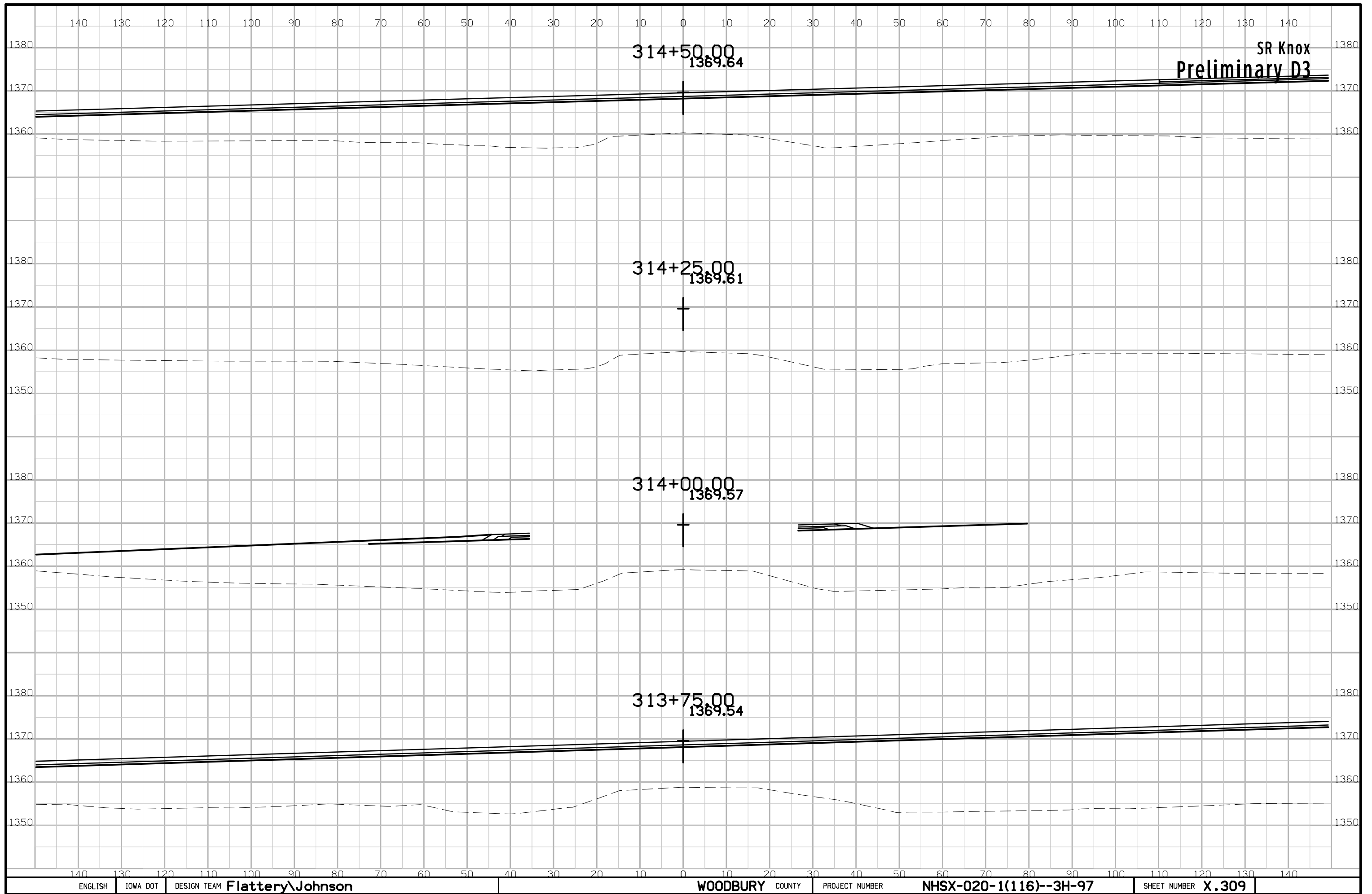


SR Knox
Preliminary D3



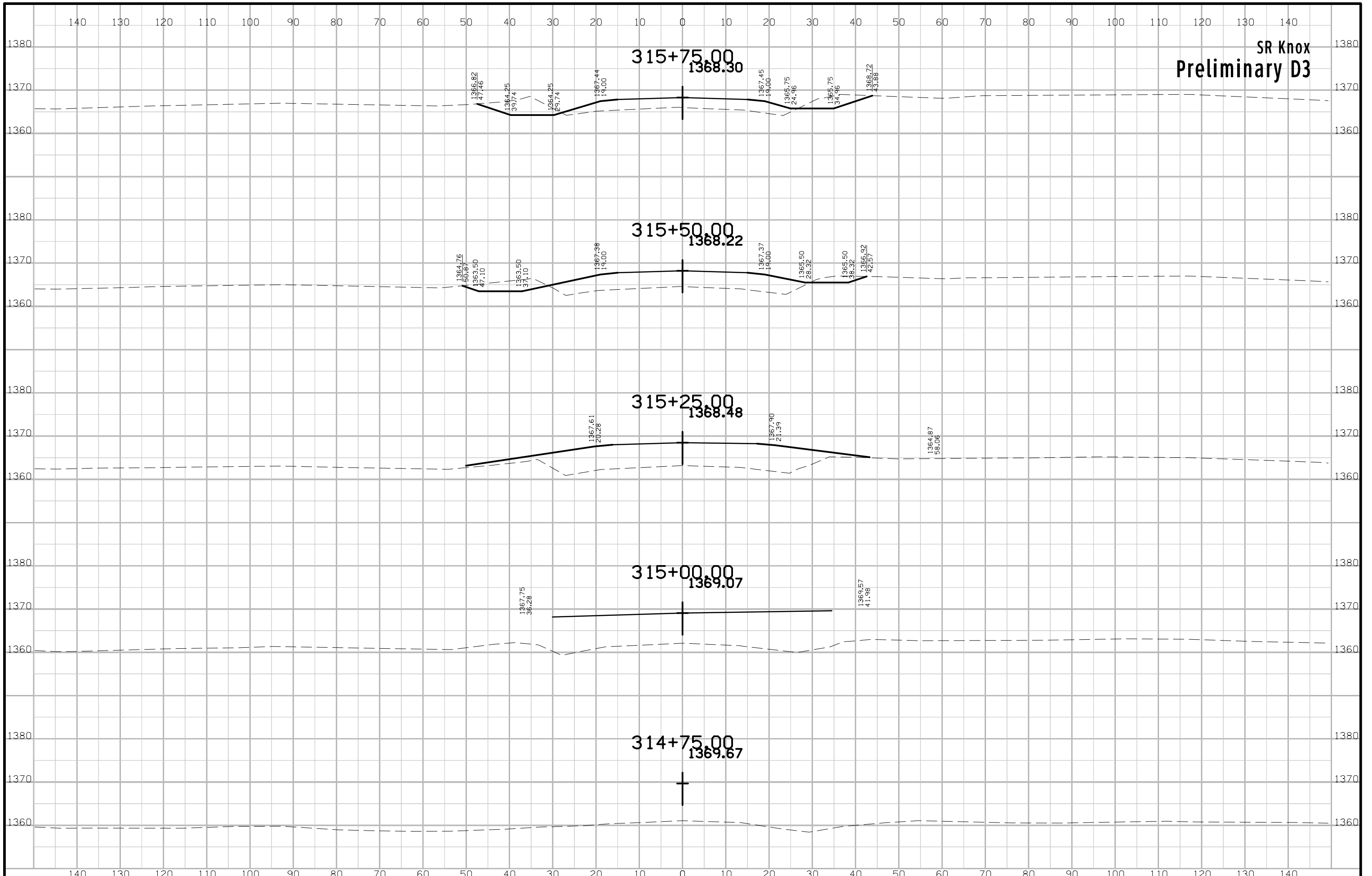
SR Knox
Preliminary D3



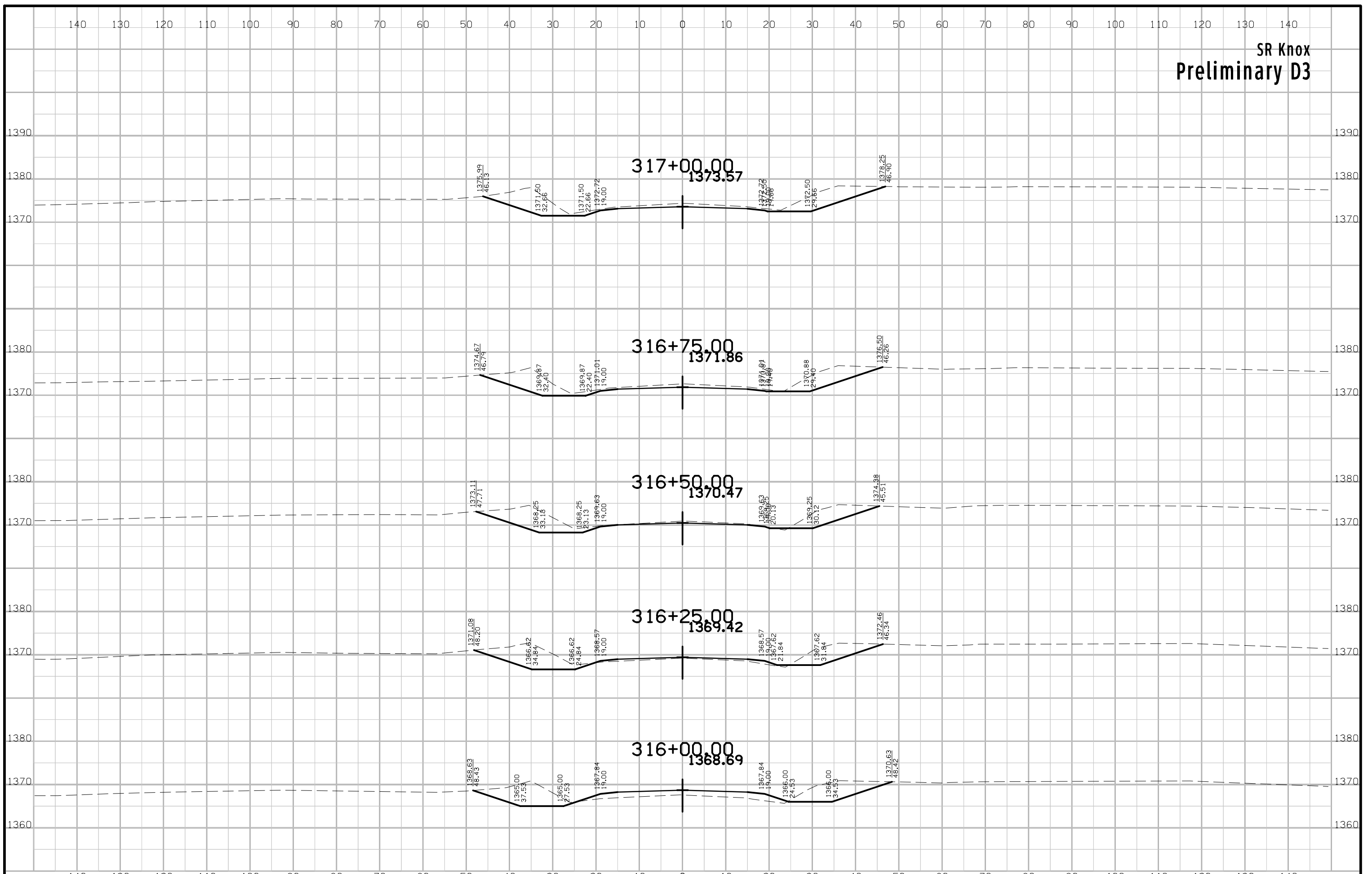


SR Knox
Preliminary D3

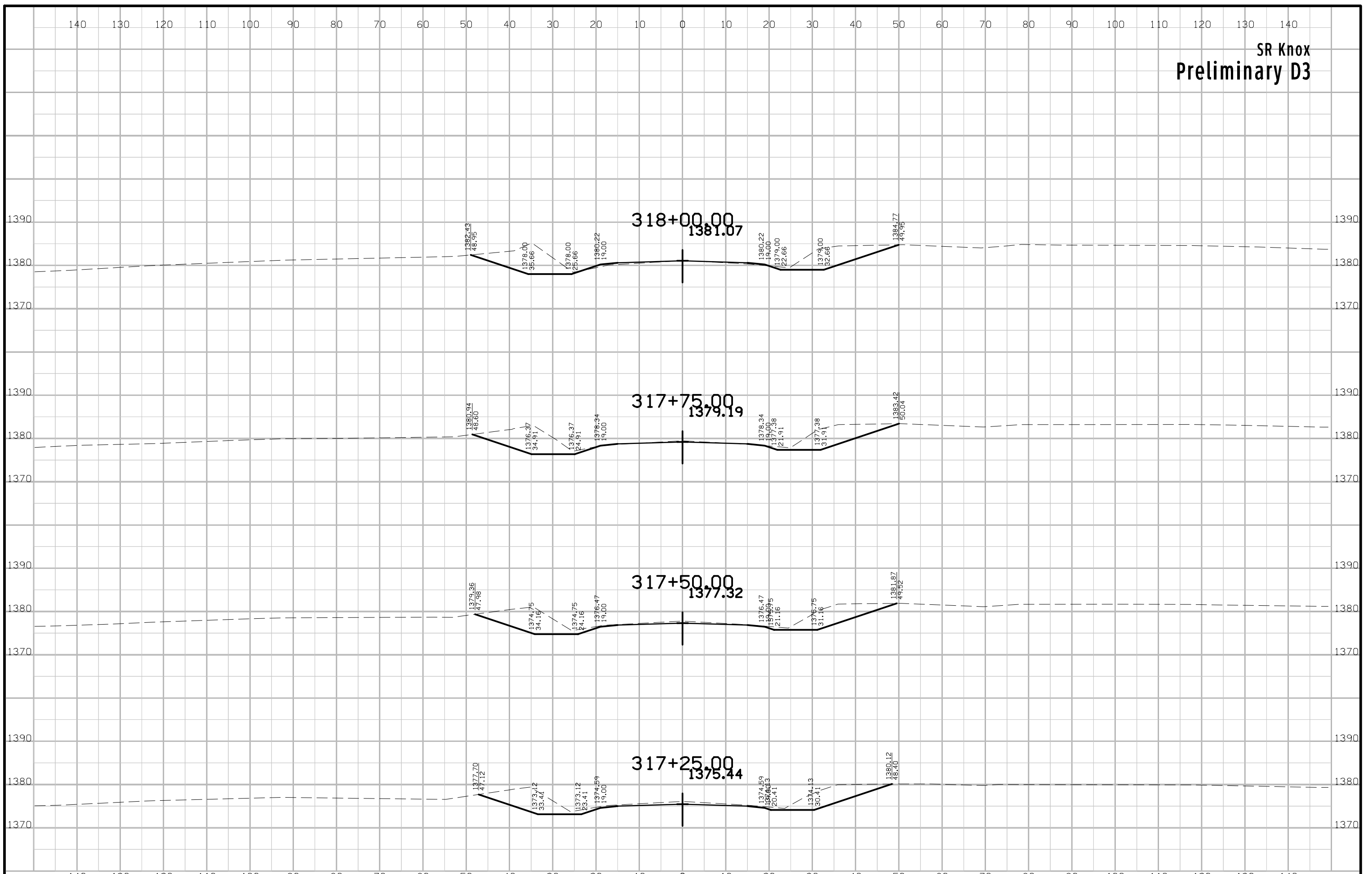
SR Knox
Preliminary D3



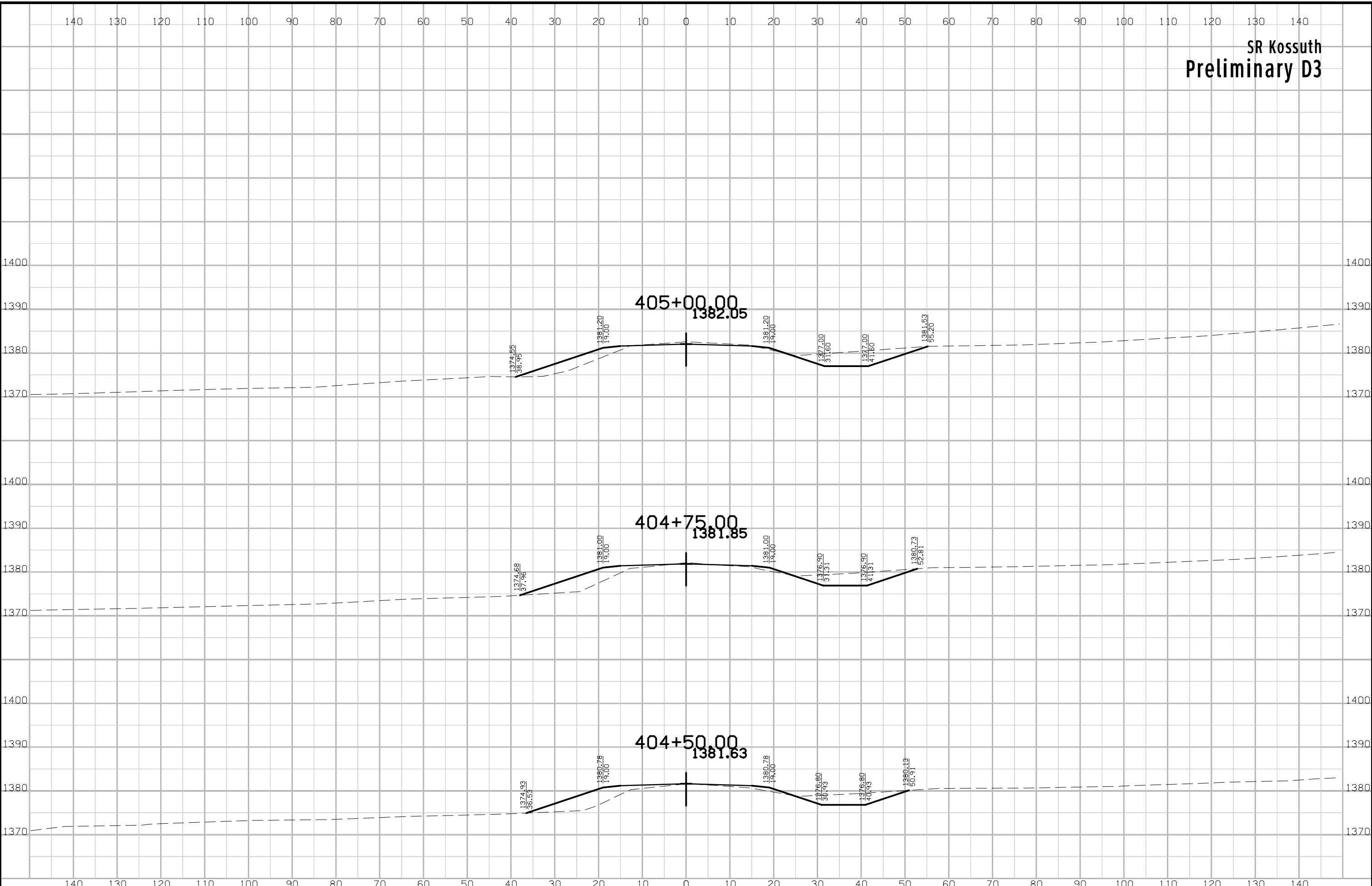
SR Knox
Preliminary D3



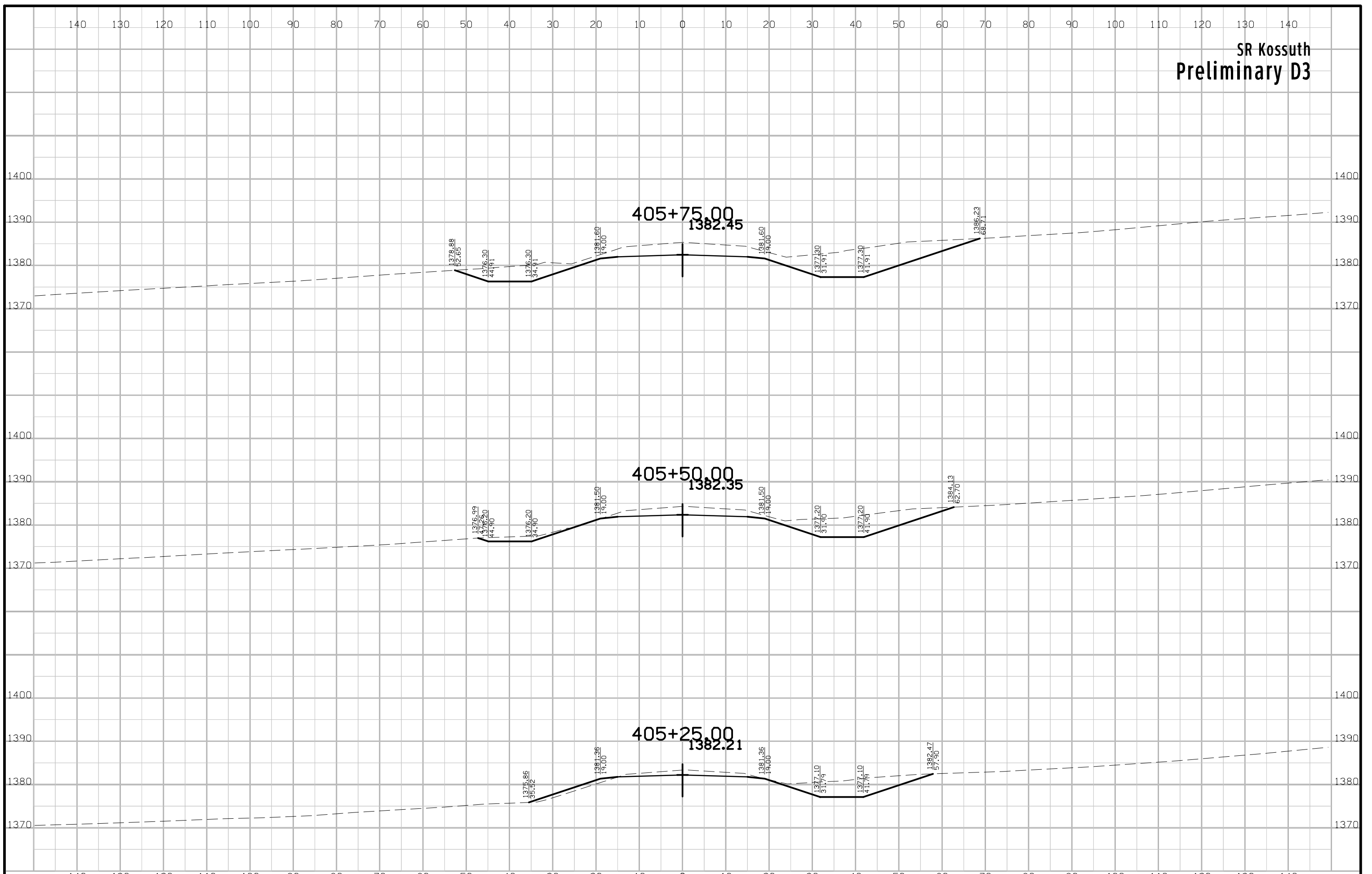
SR Knox
Preliminary D3



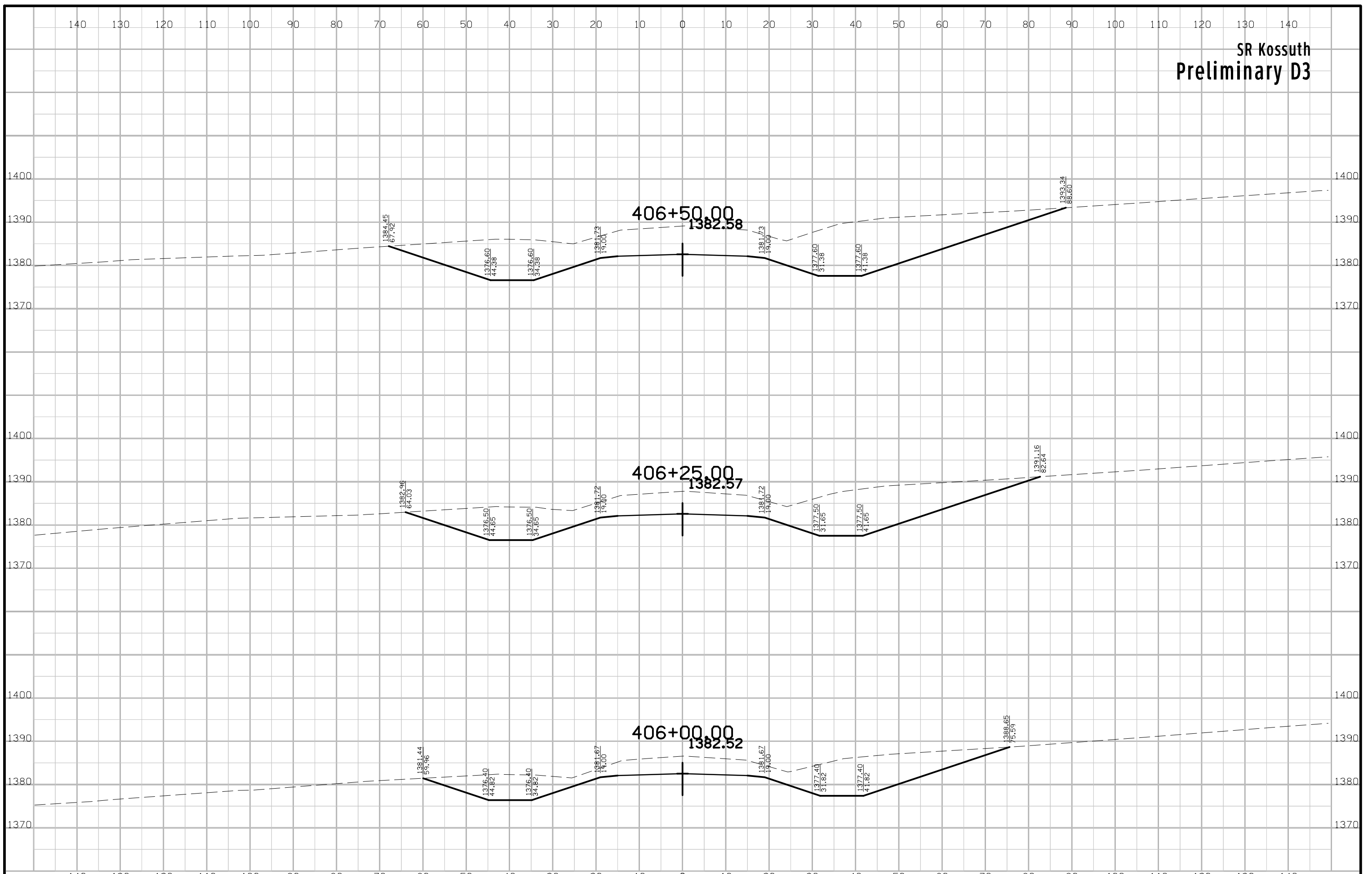
SR Kossuth
Preliminary D3



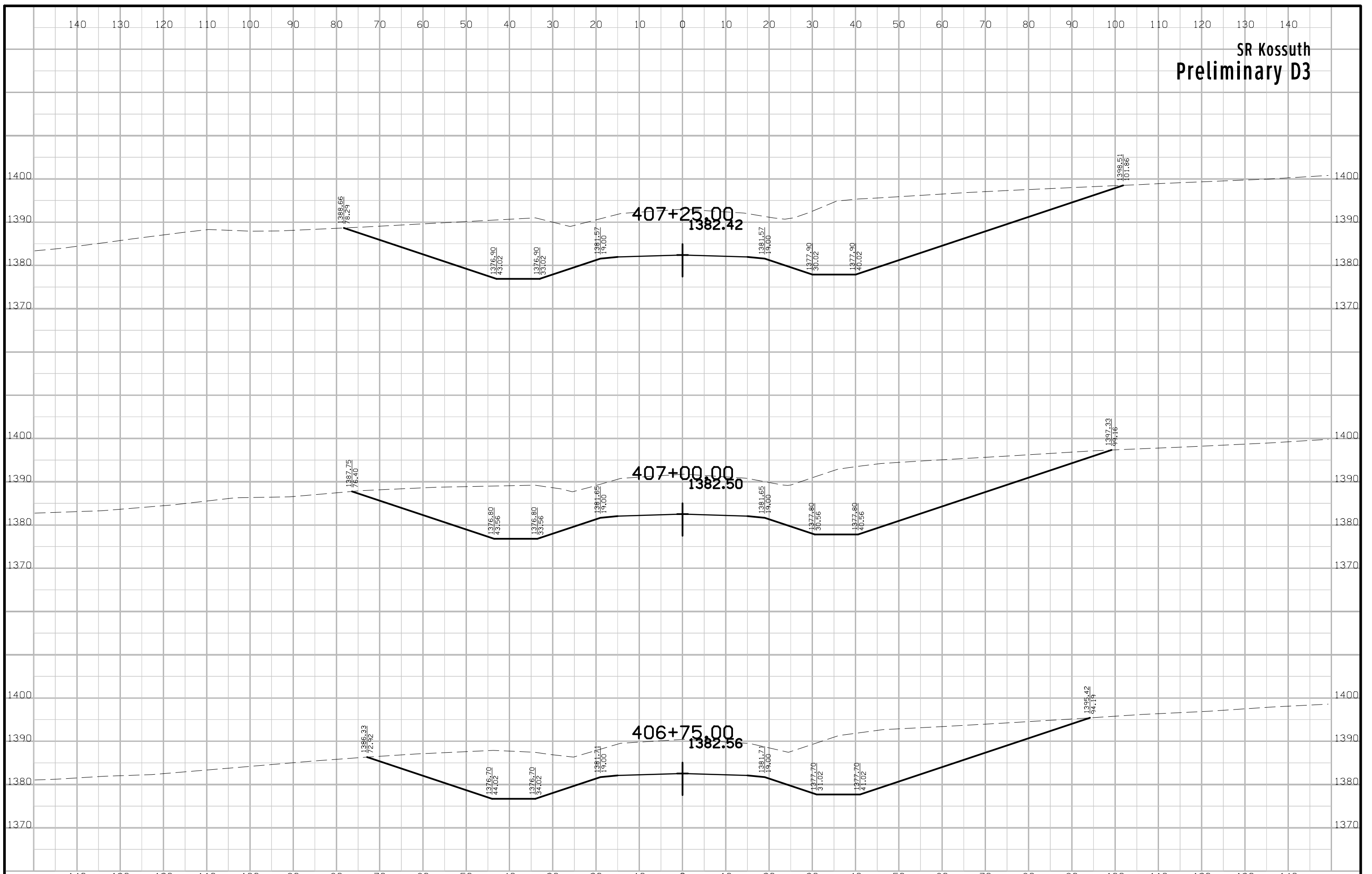
SR Kossuth
Preliminary D3



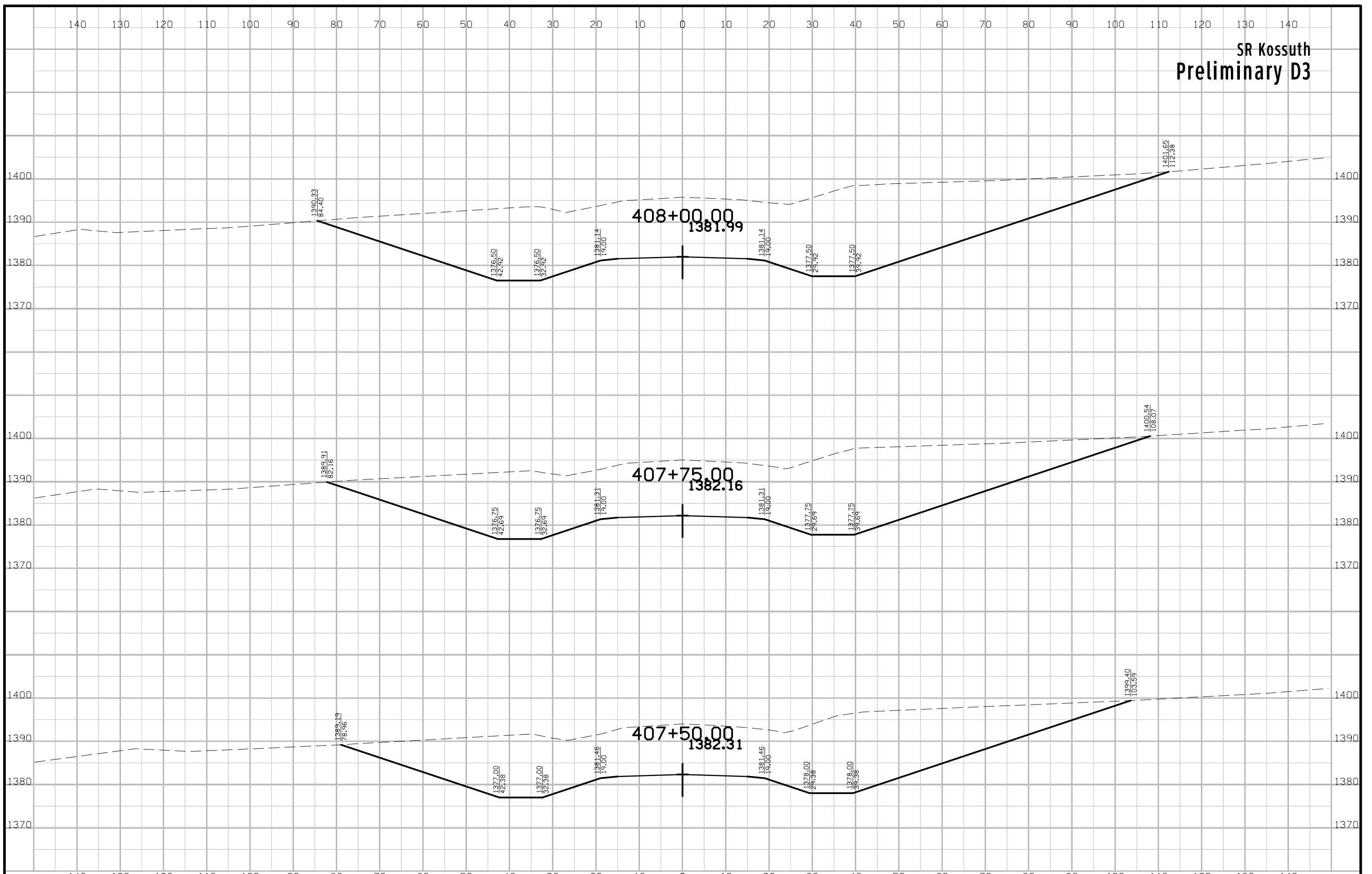
SR Kossuth
Preliminary D3



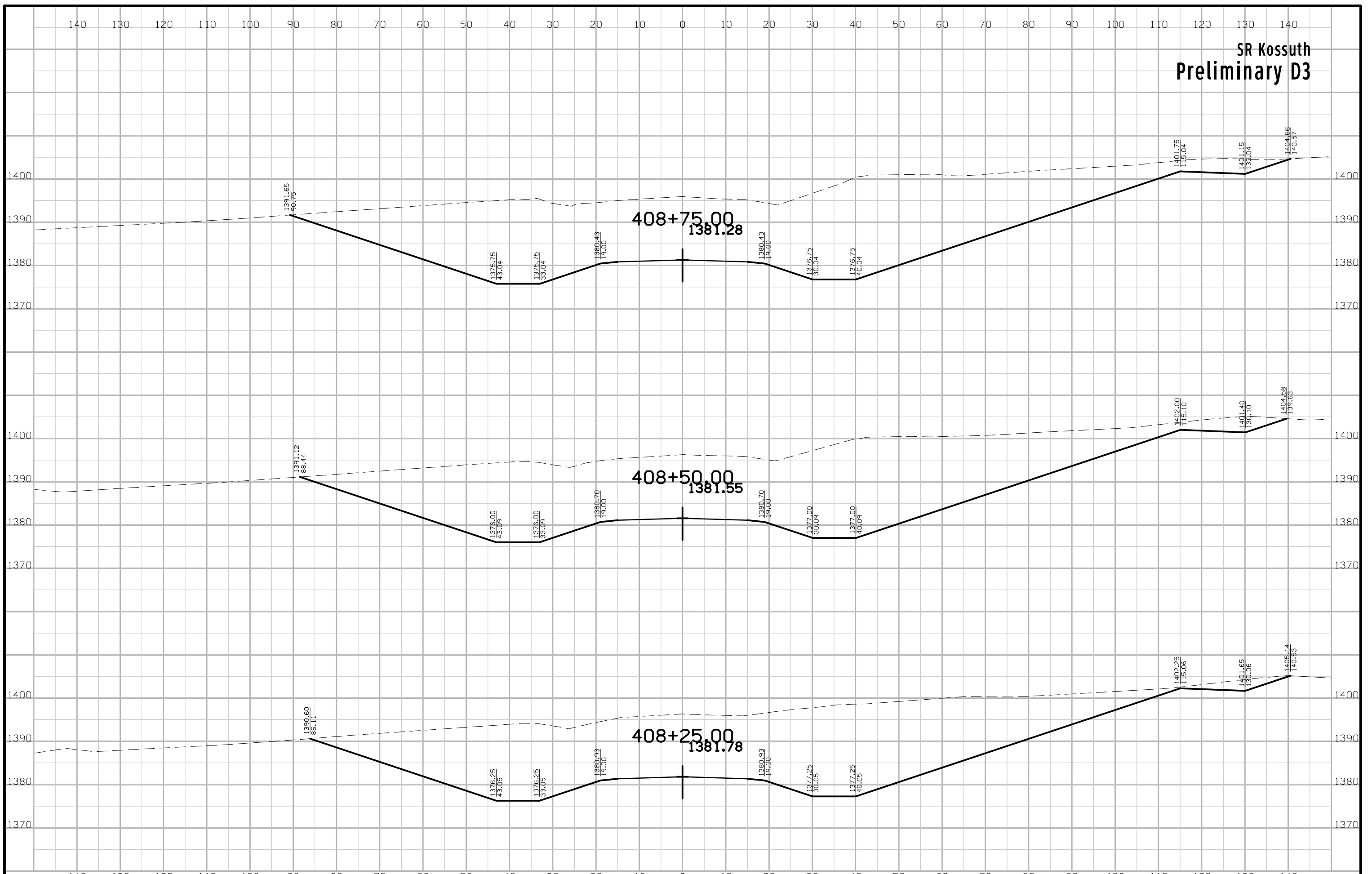
SR Kossuth
Preliminary D3



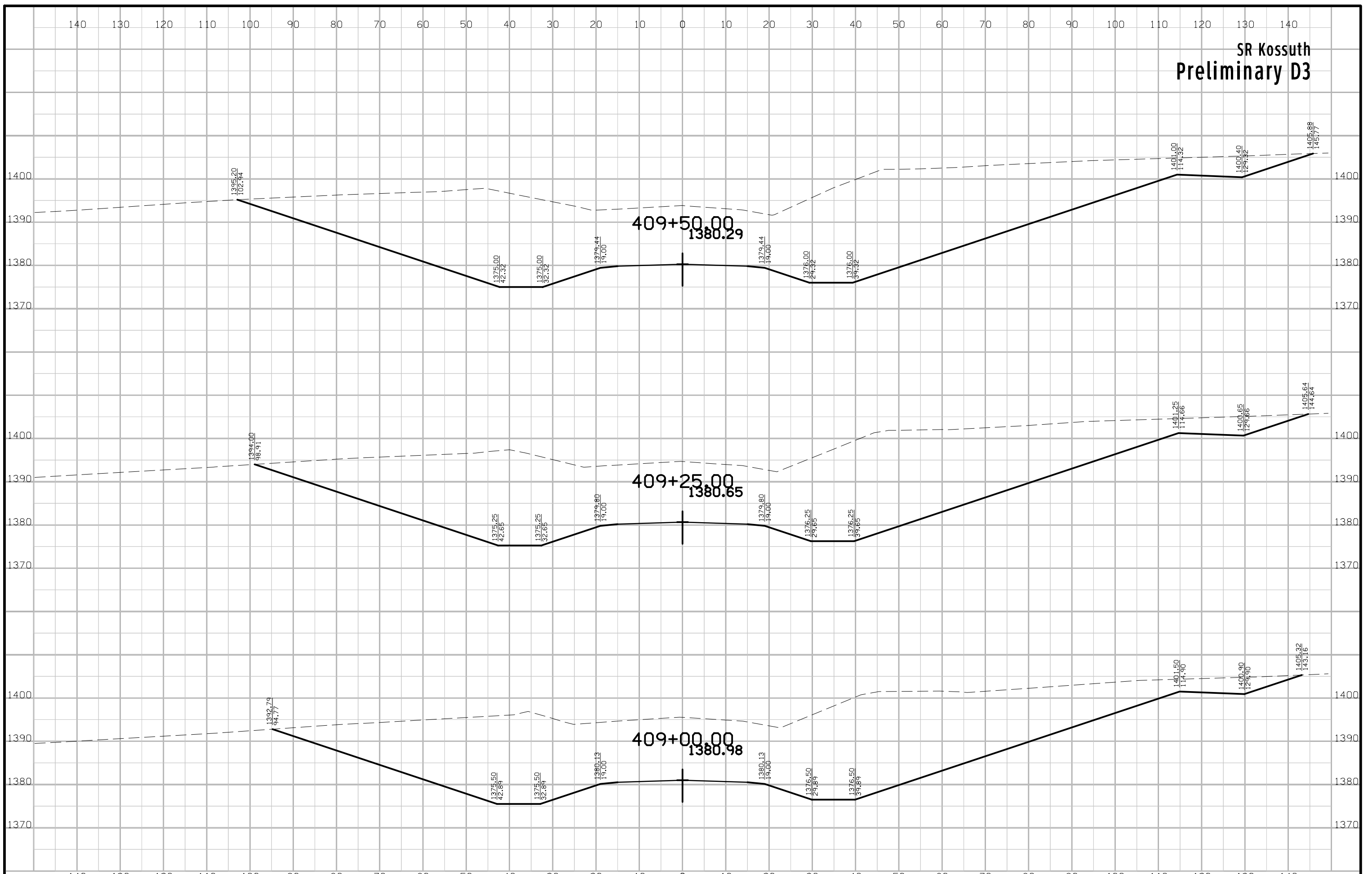
SR Kossuth
Preliminary D3



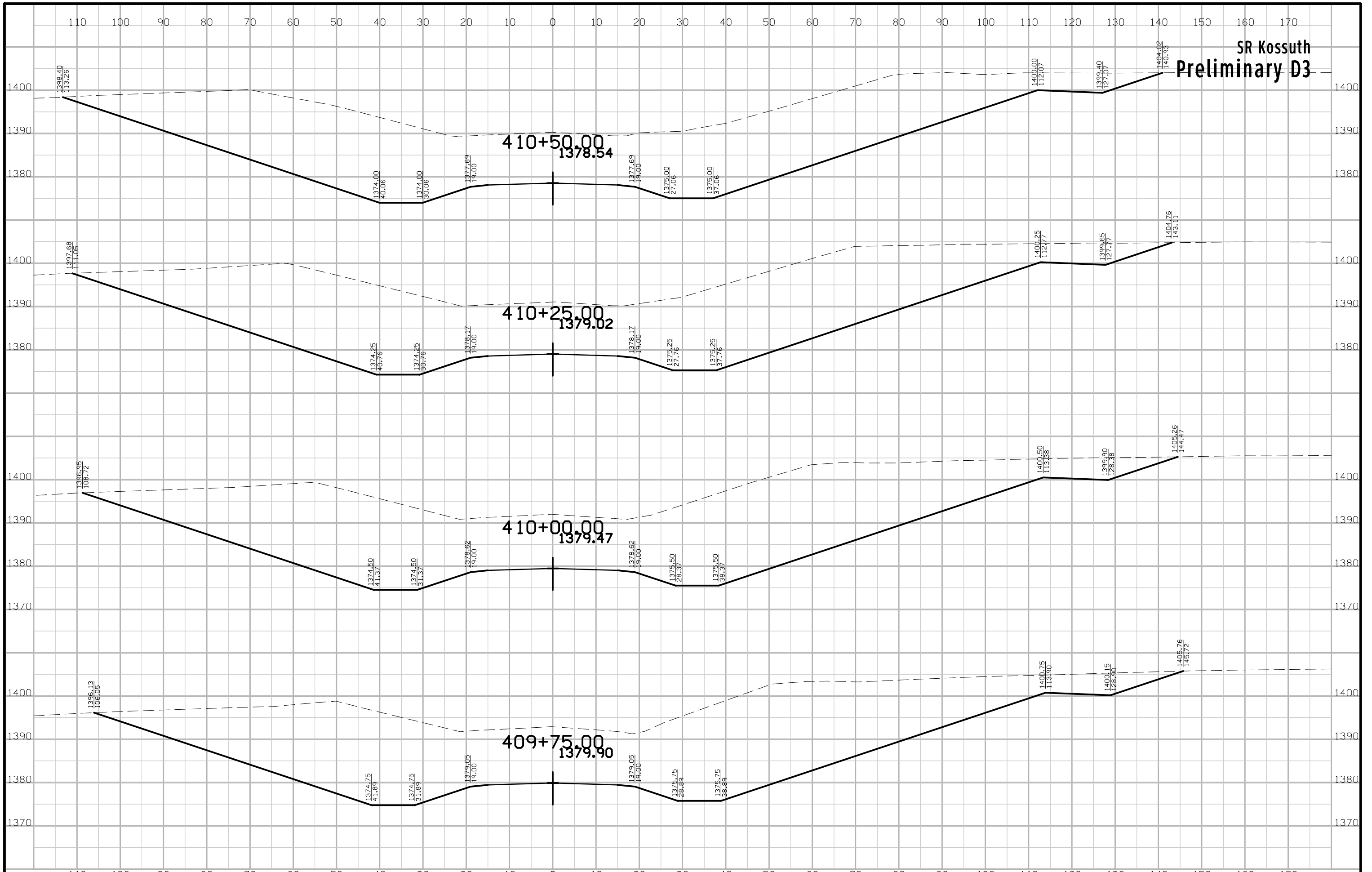
SR Kossuth
Preliminary D3



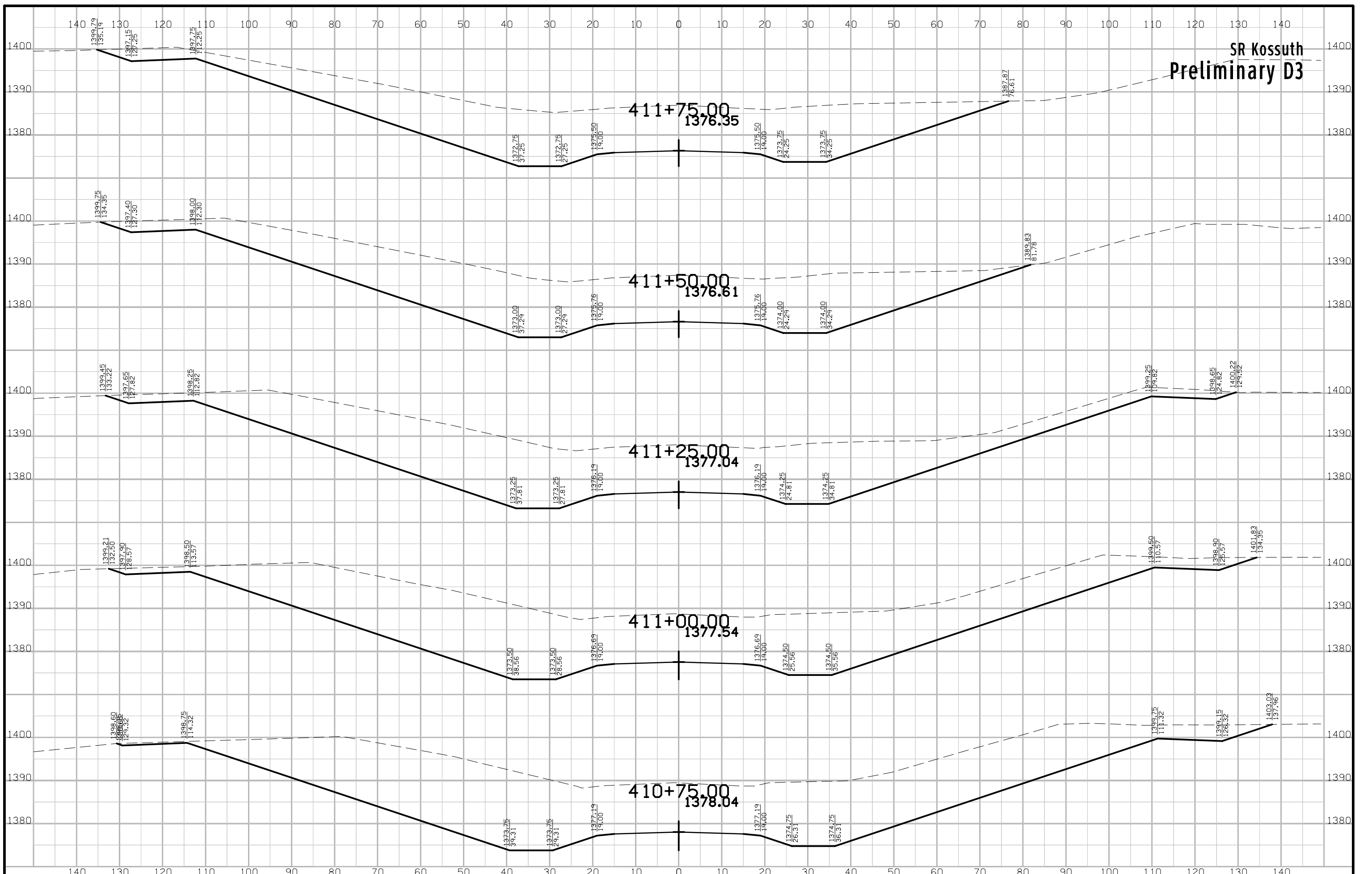
SR Kossuth
Preliminary D3



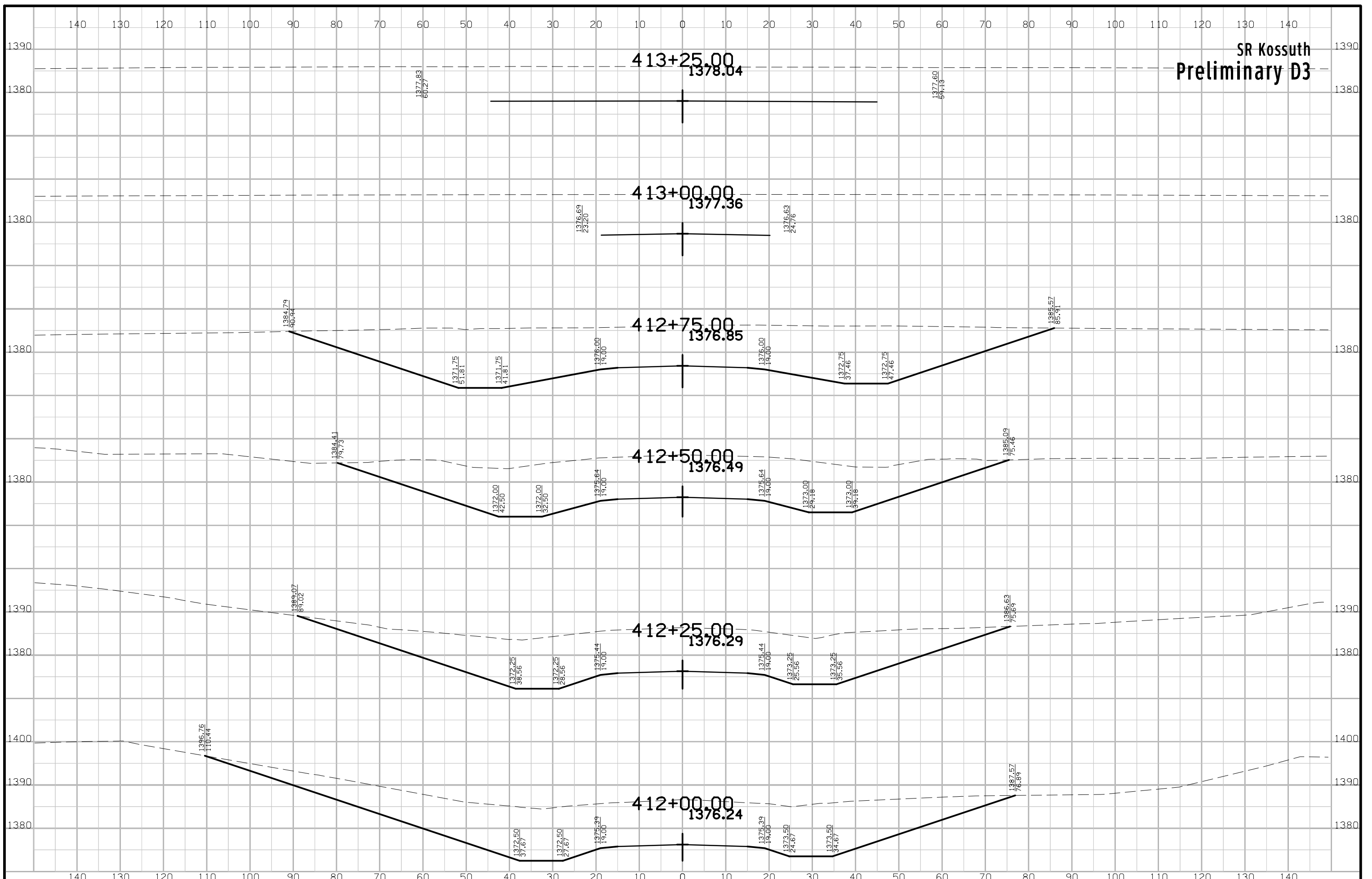
SR Kossuth
Preliminary D3



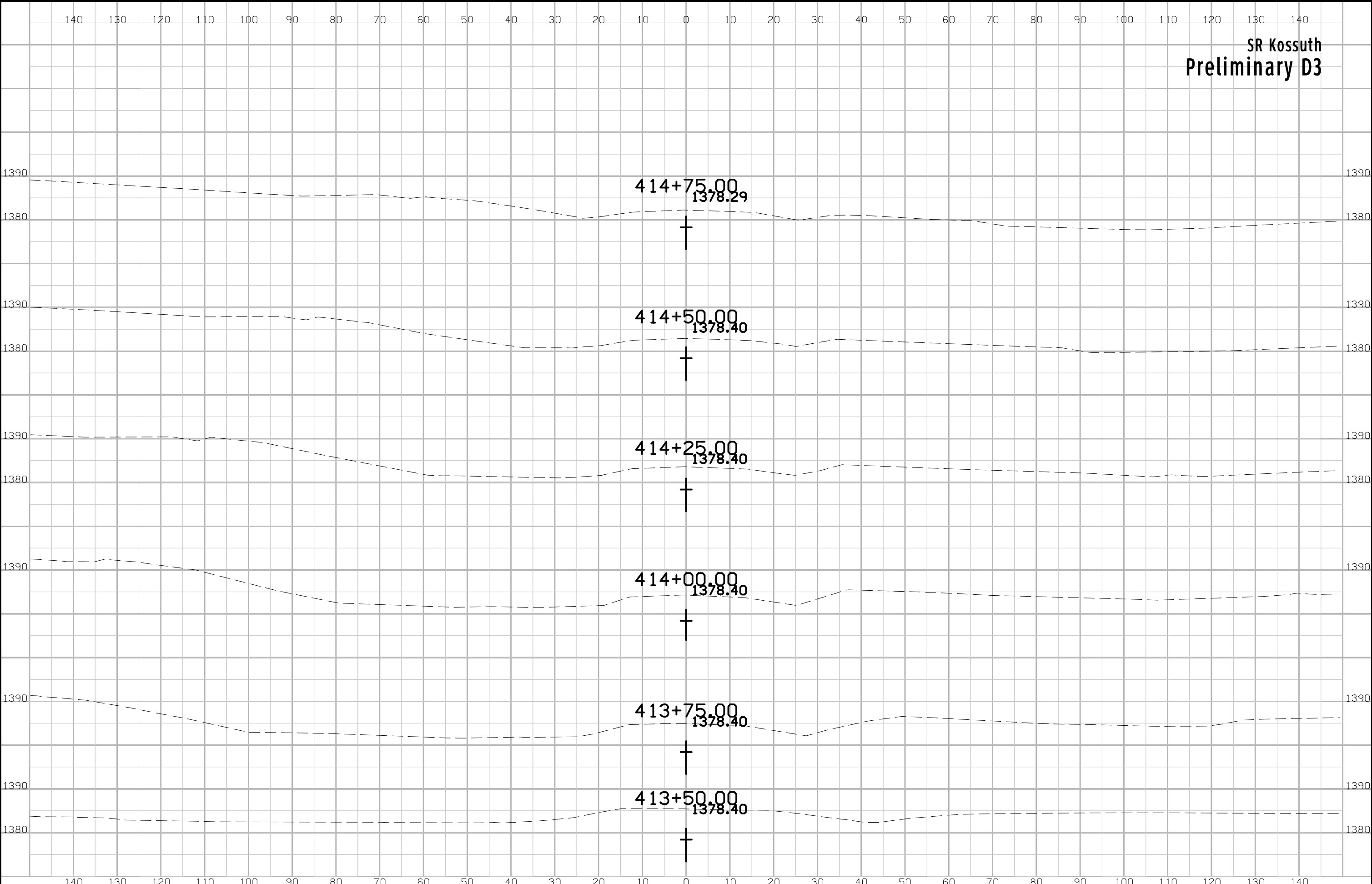
SR Kossuth
Preliminary D3



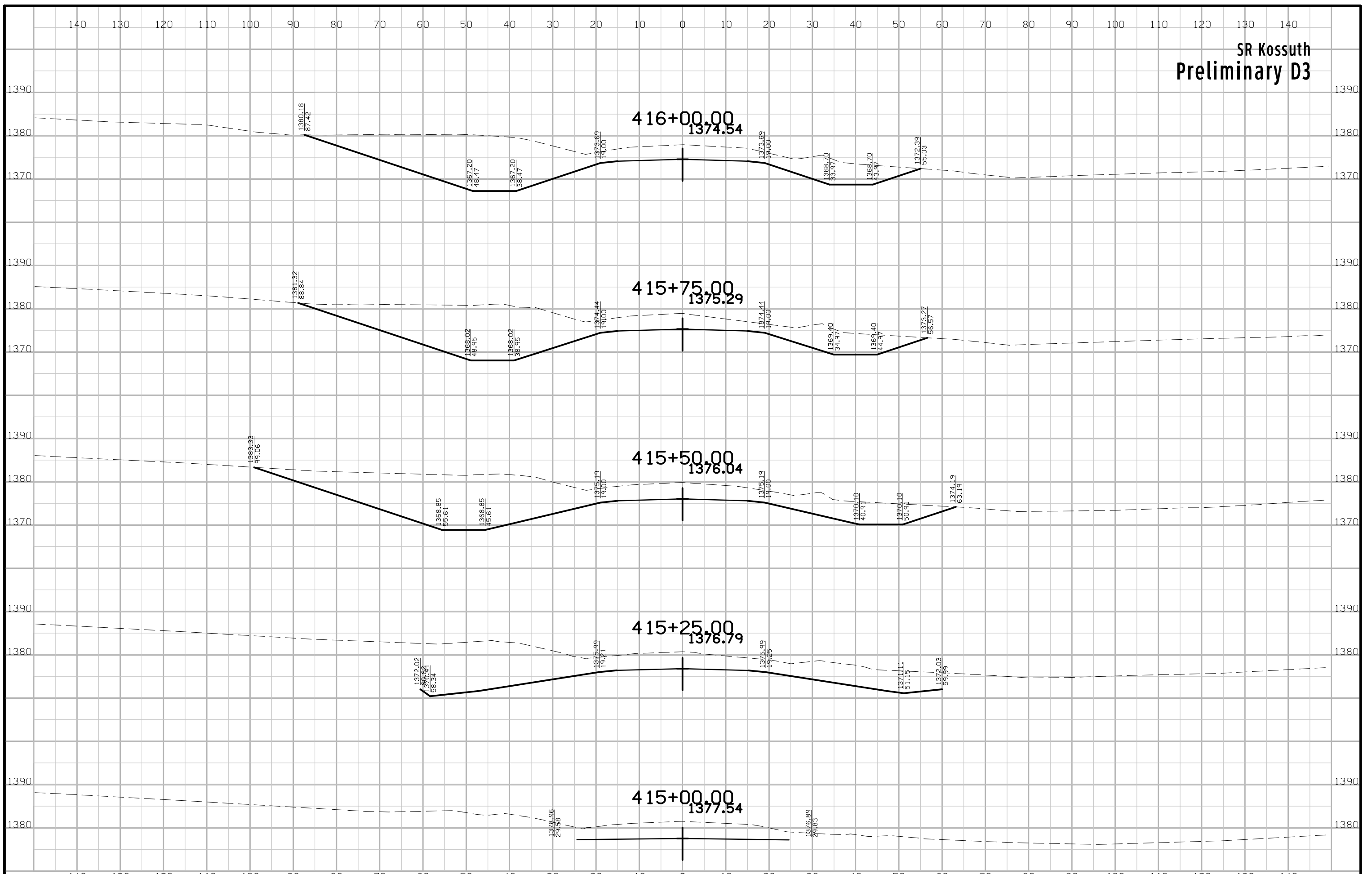
SR Kossuth
Preliminary D3



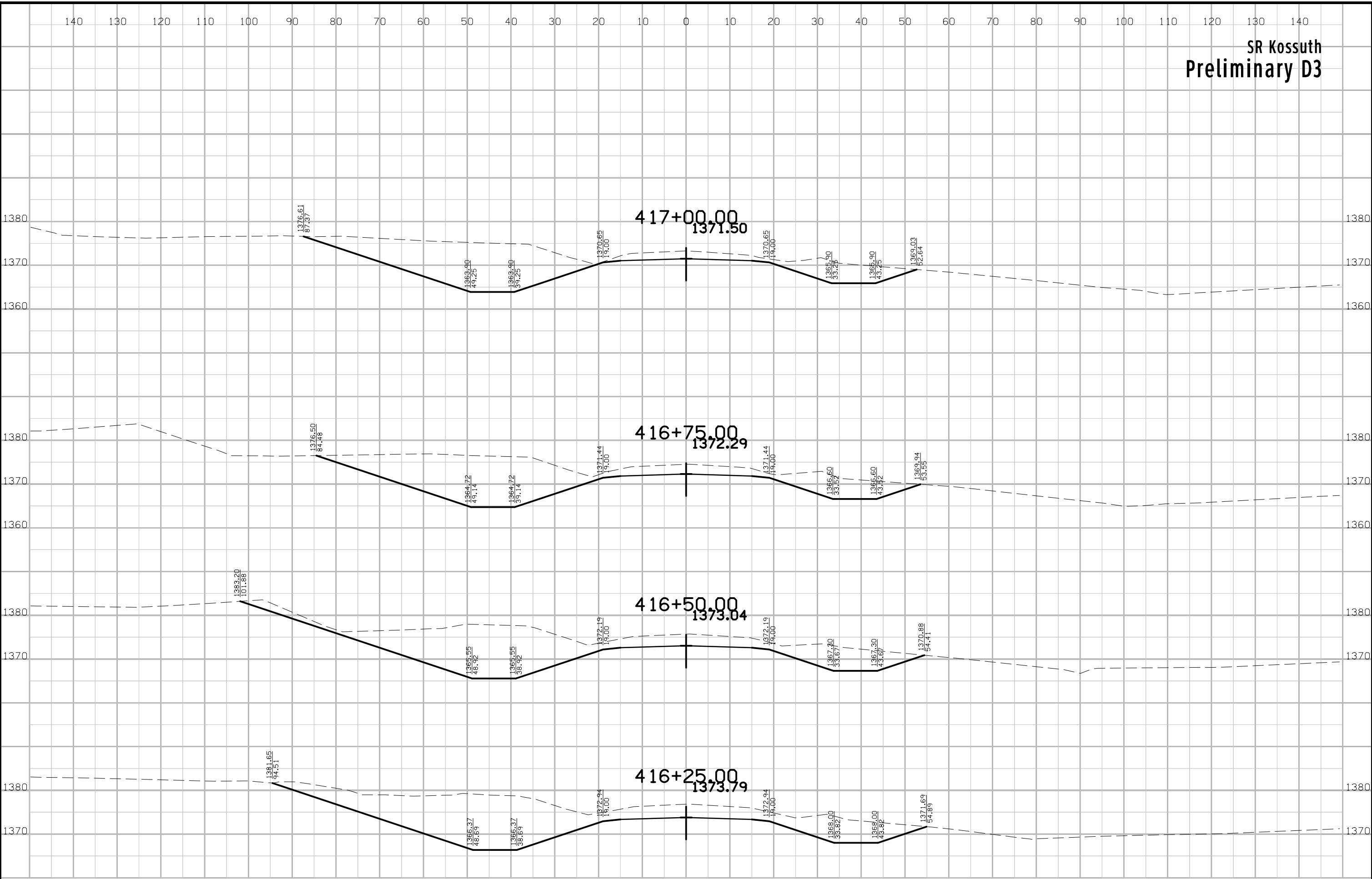
SR Kossuth
Preliminary D3



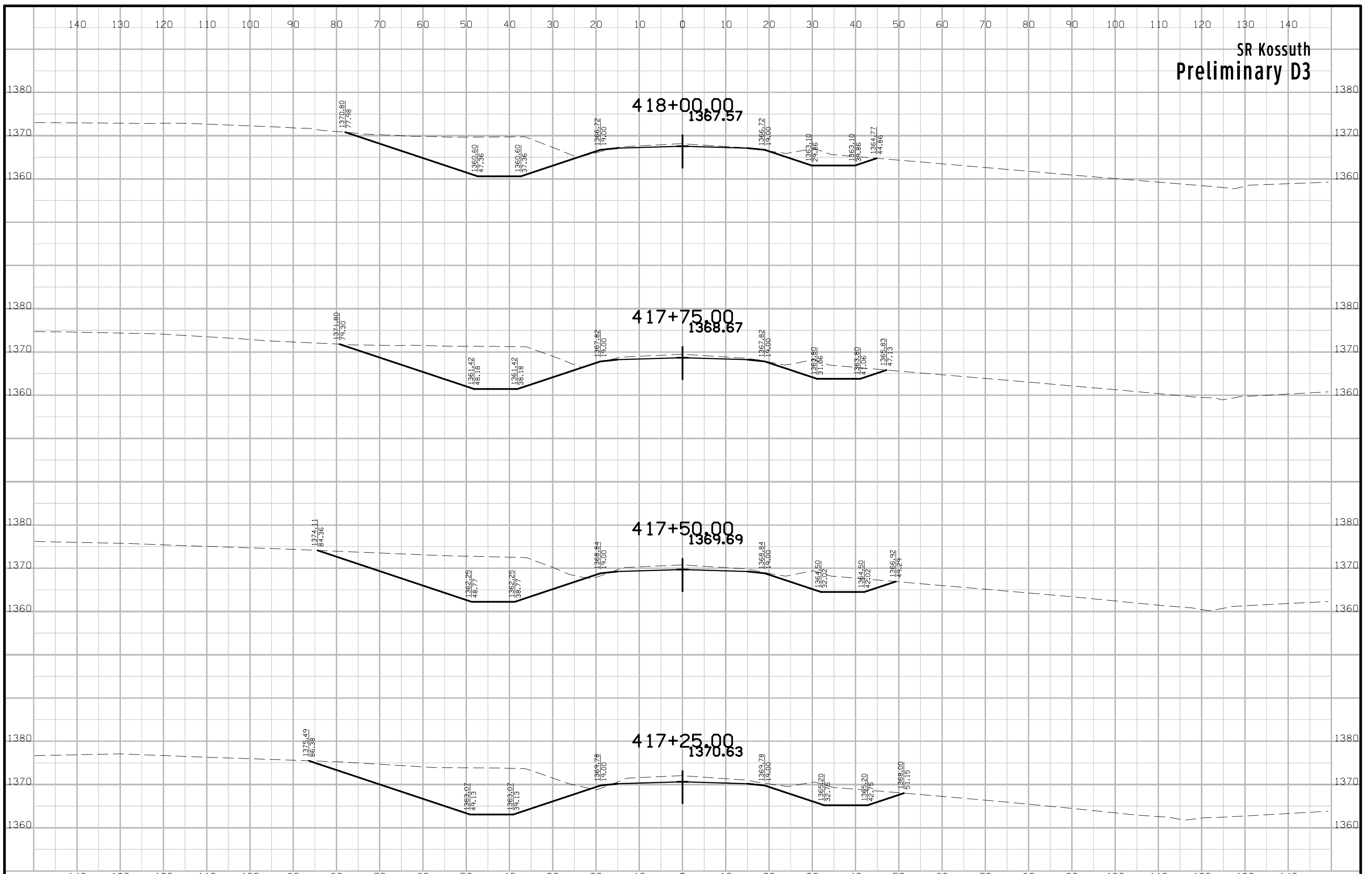
SR Kossuth
Preliminary D3



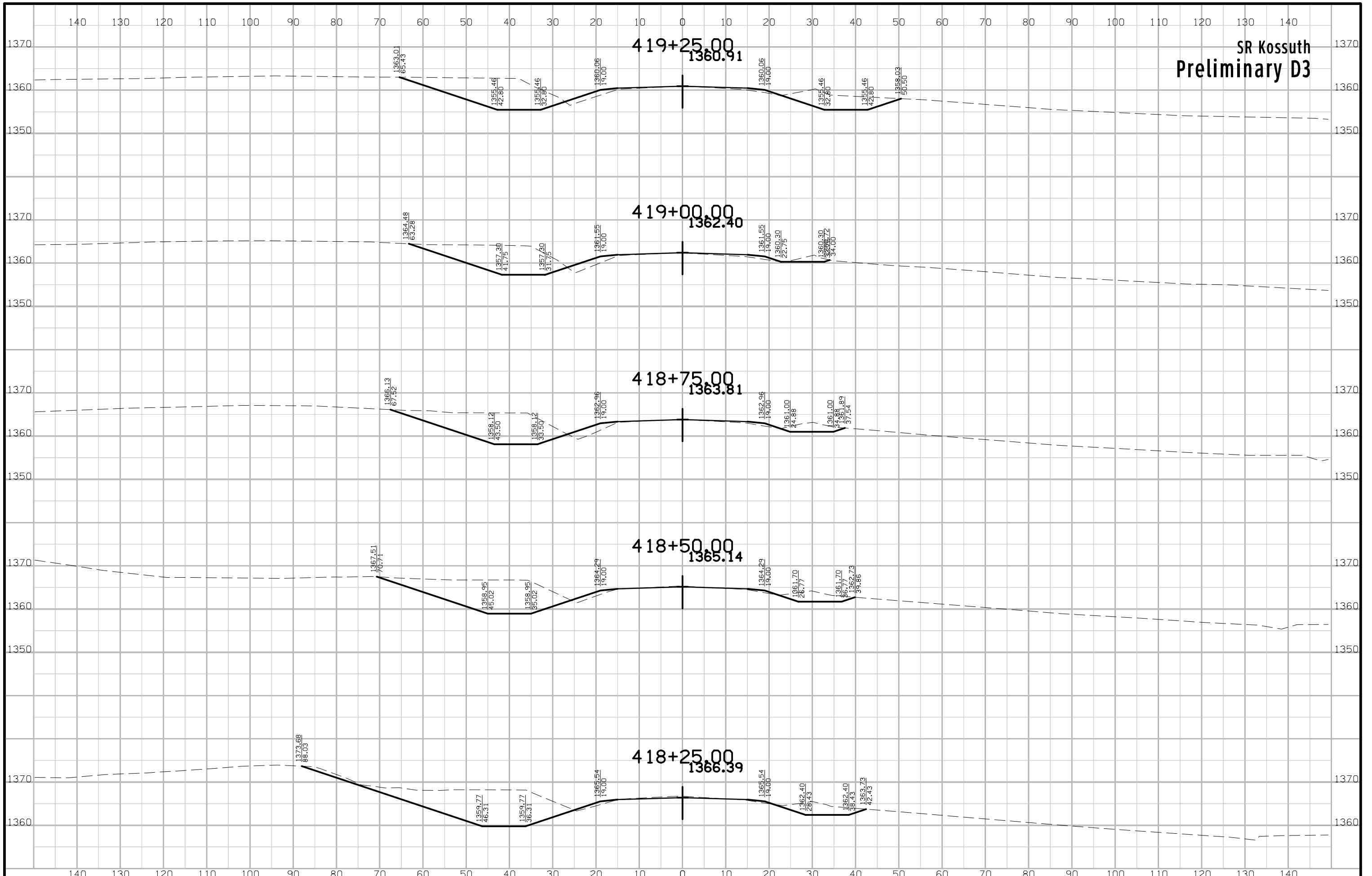
SR Kossuth
Preliminary D3



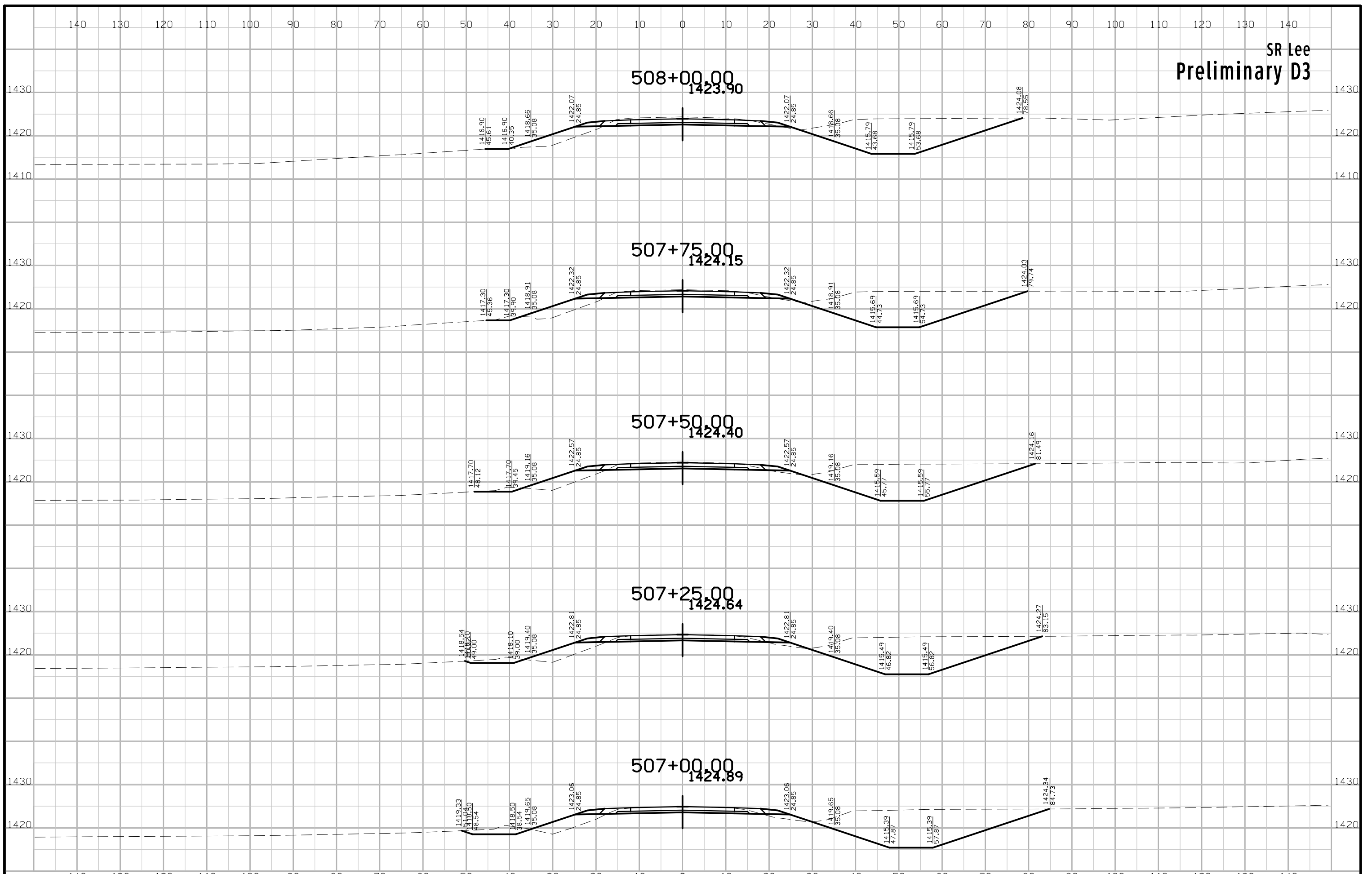
SR Kossuth
Preliminary D3

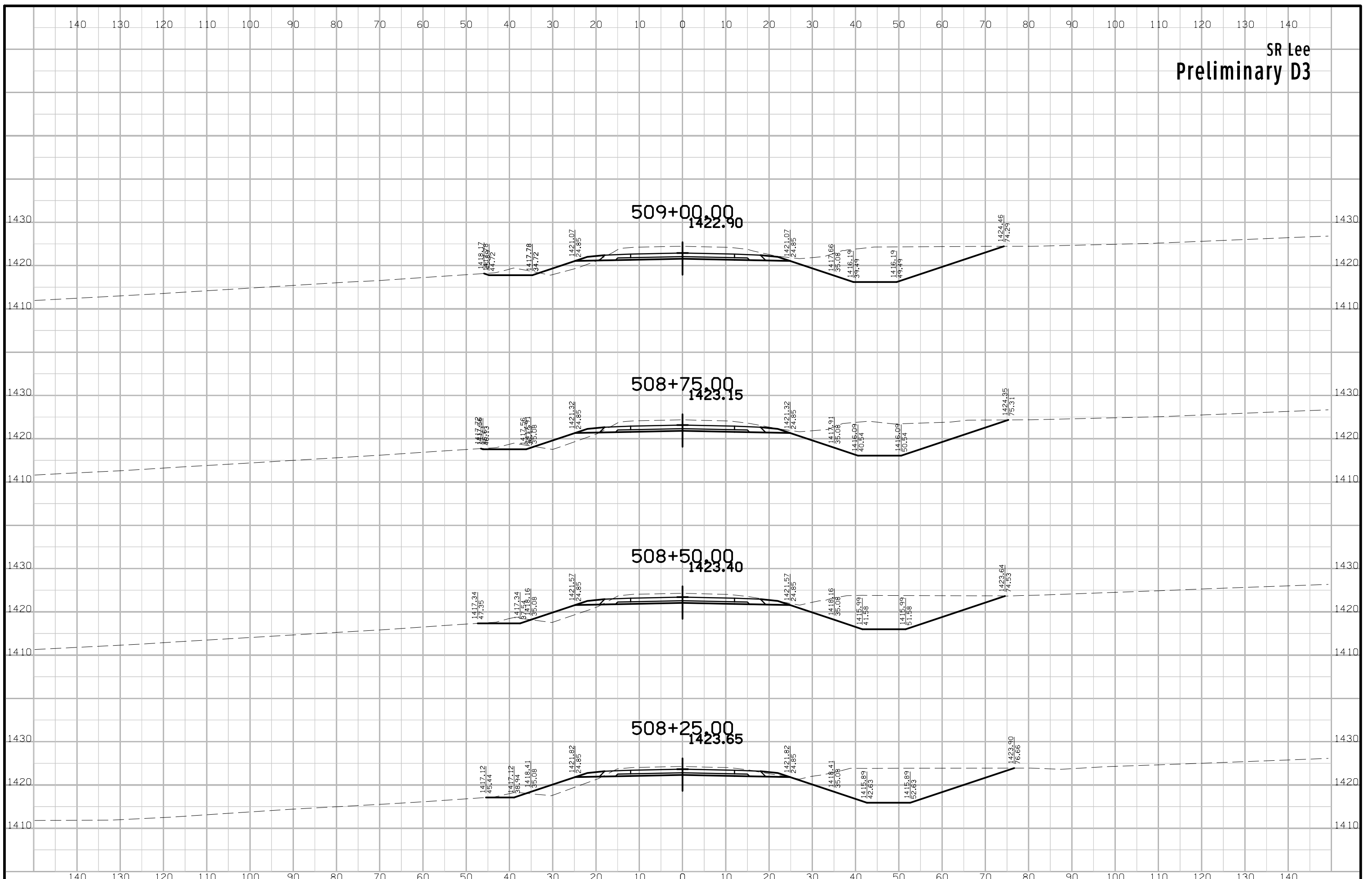


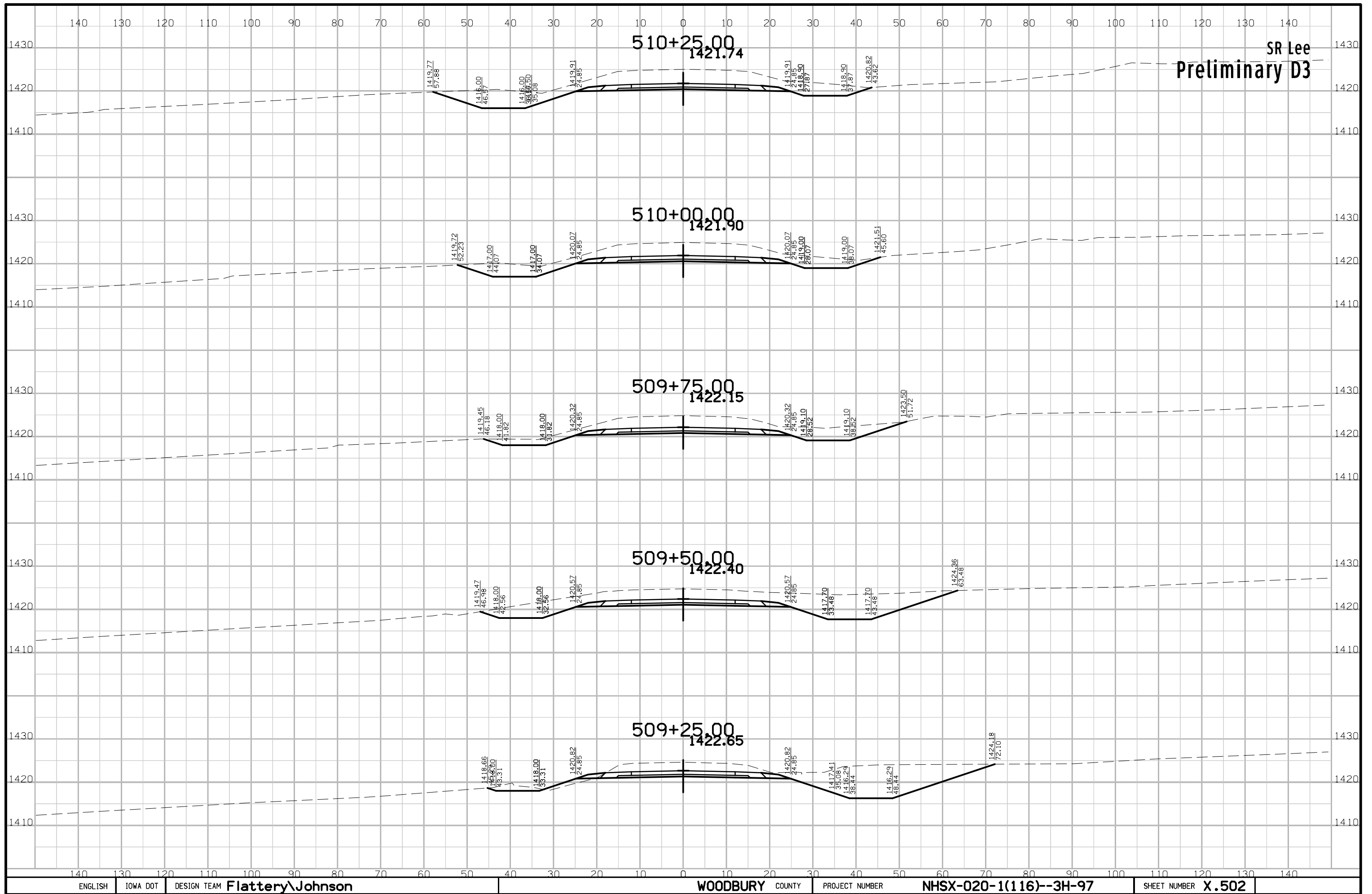
SR Kossuth
Preliminary D3

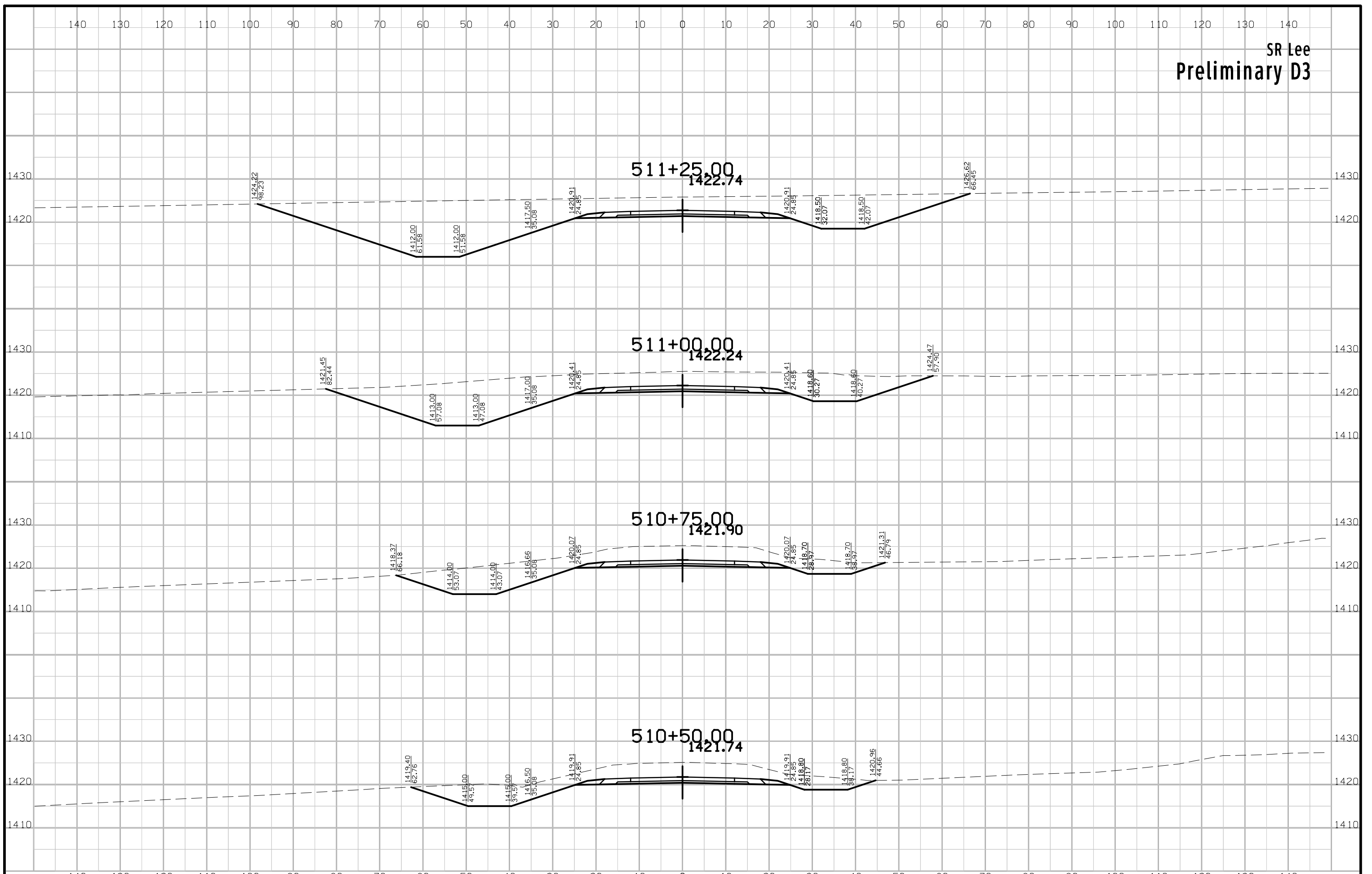


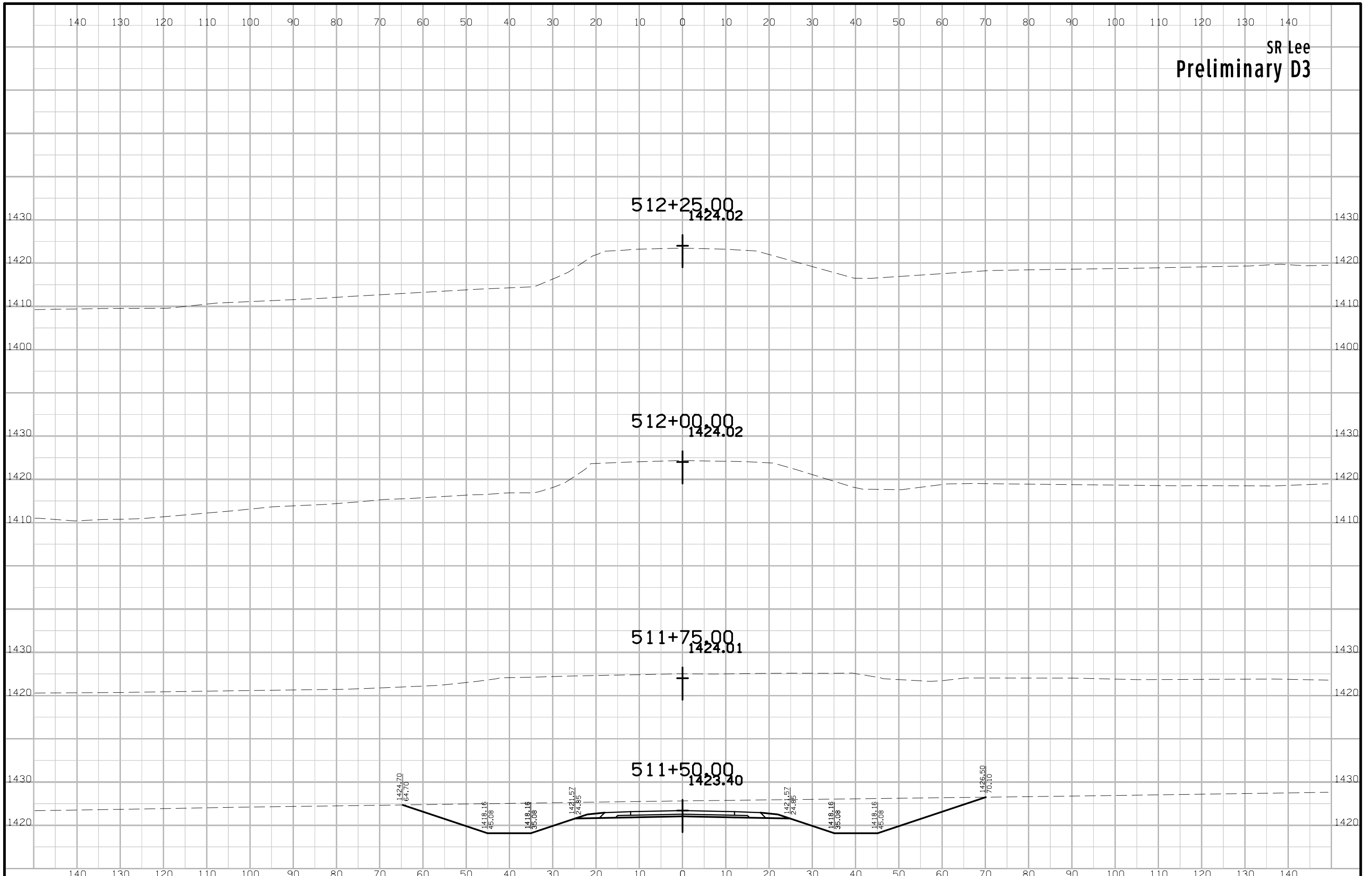
SR Lee
Preliminary D3

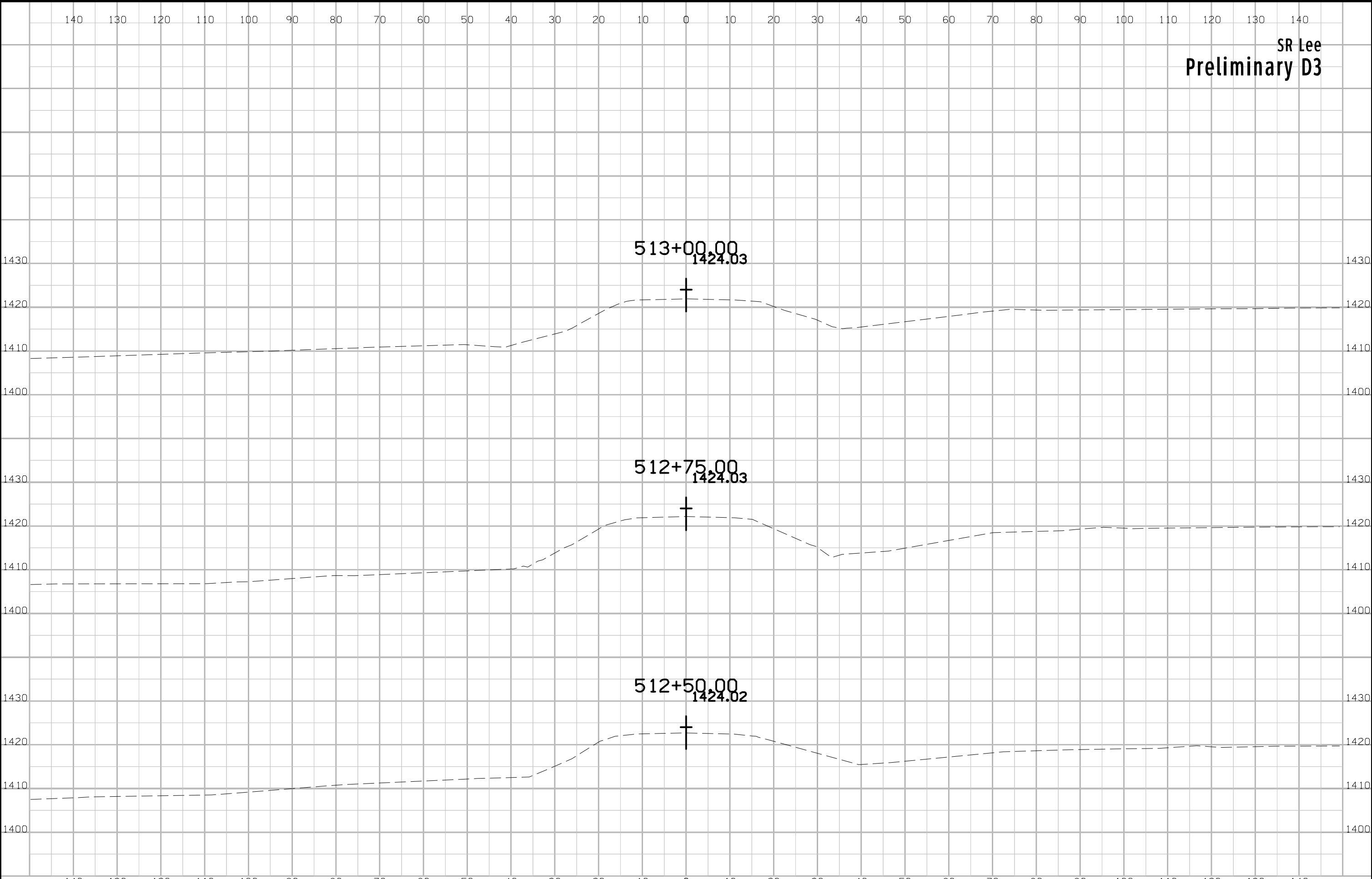


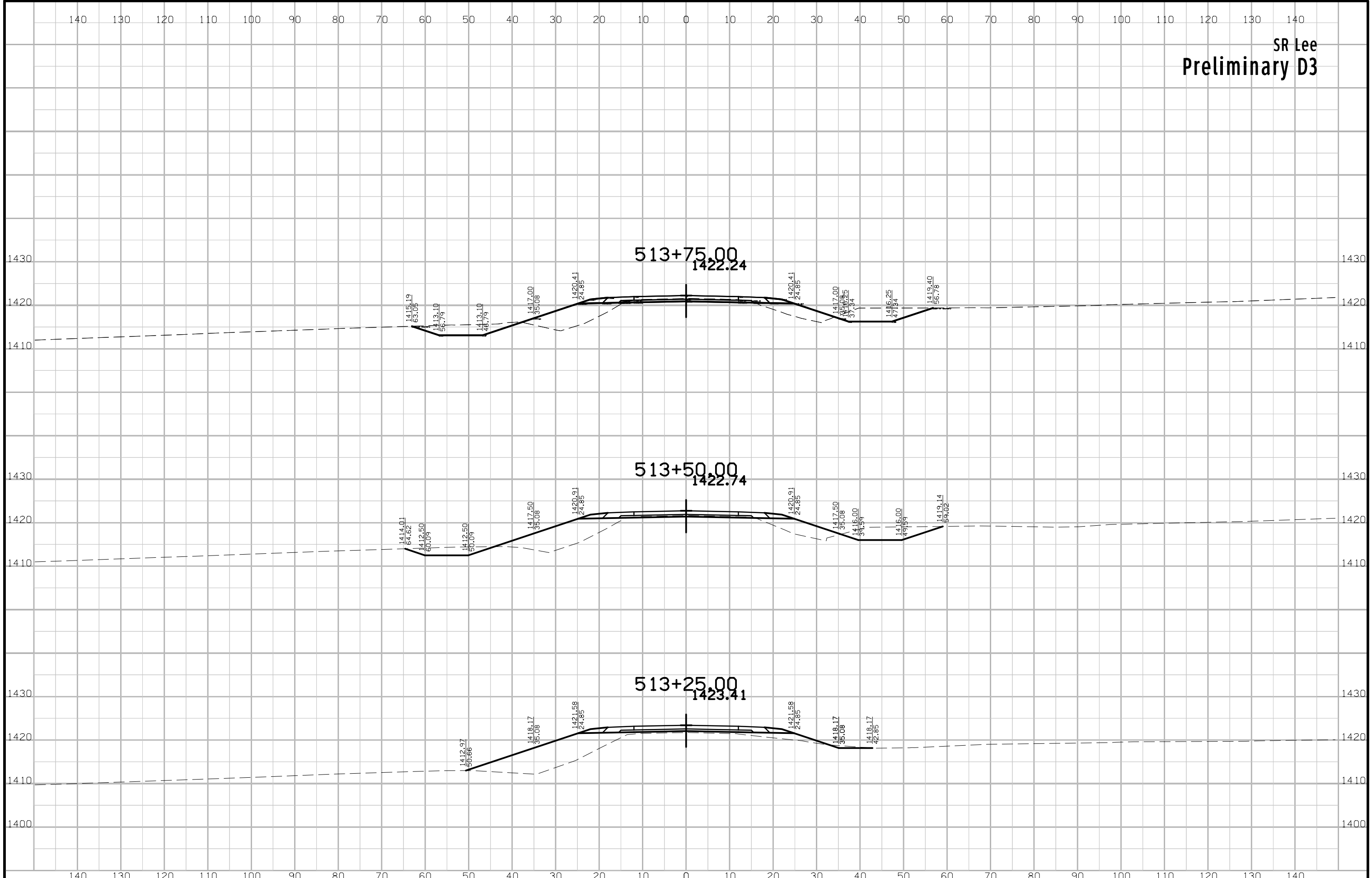




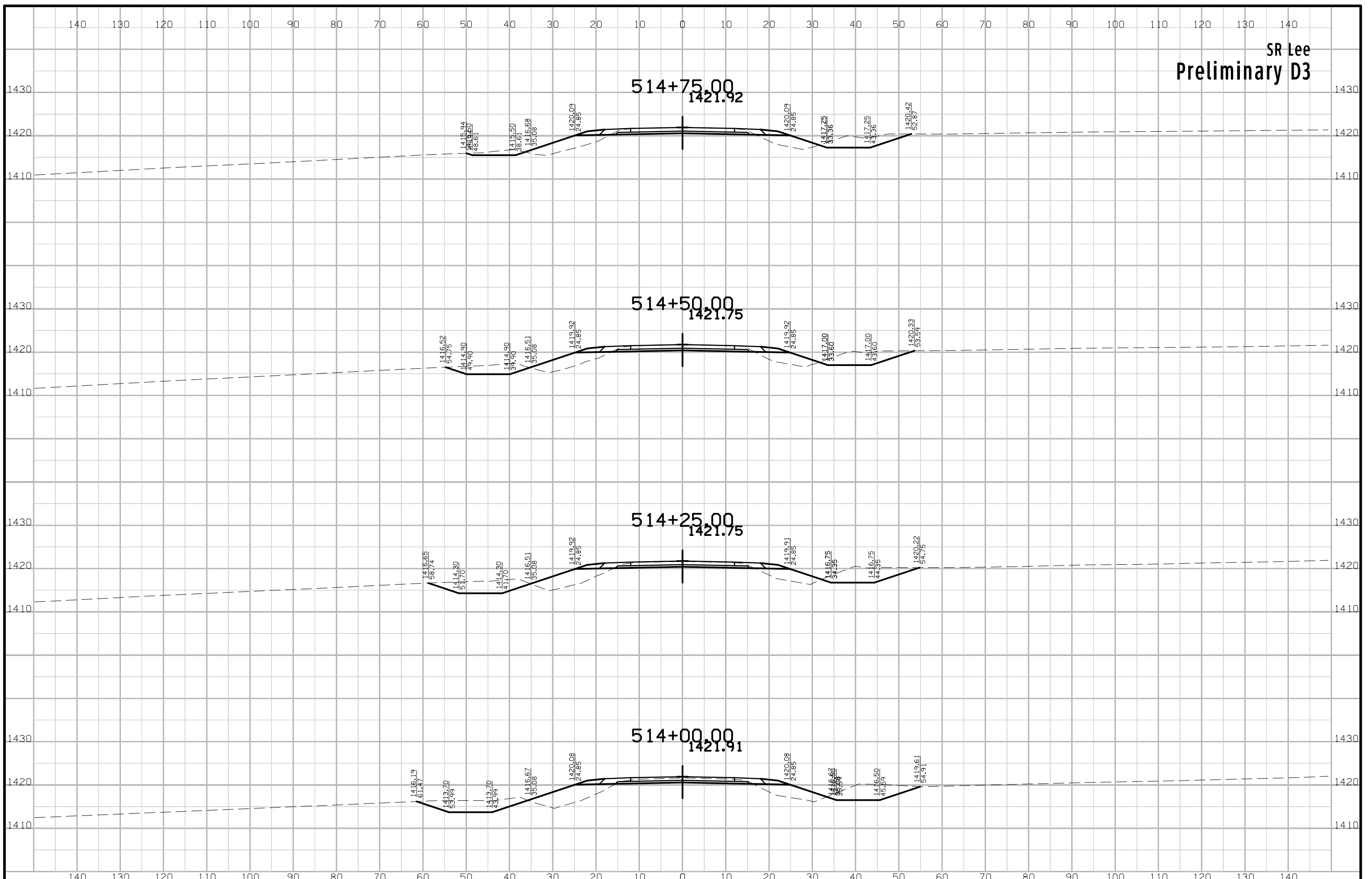


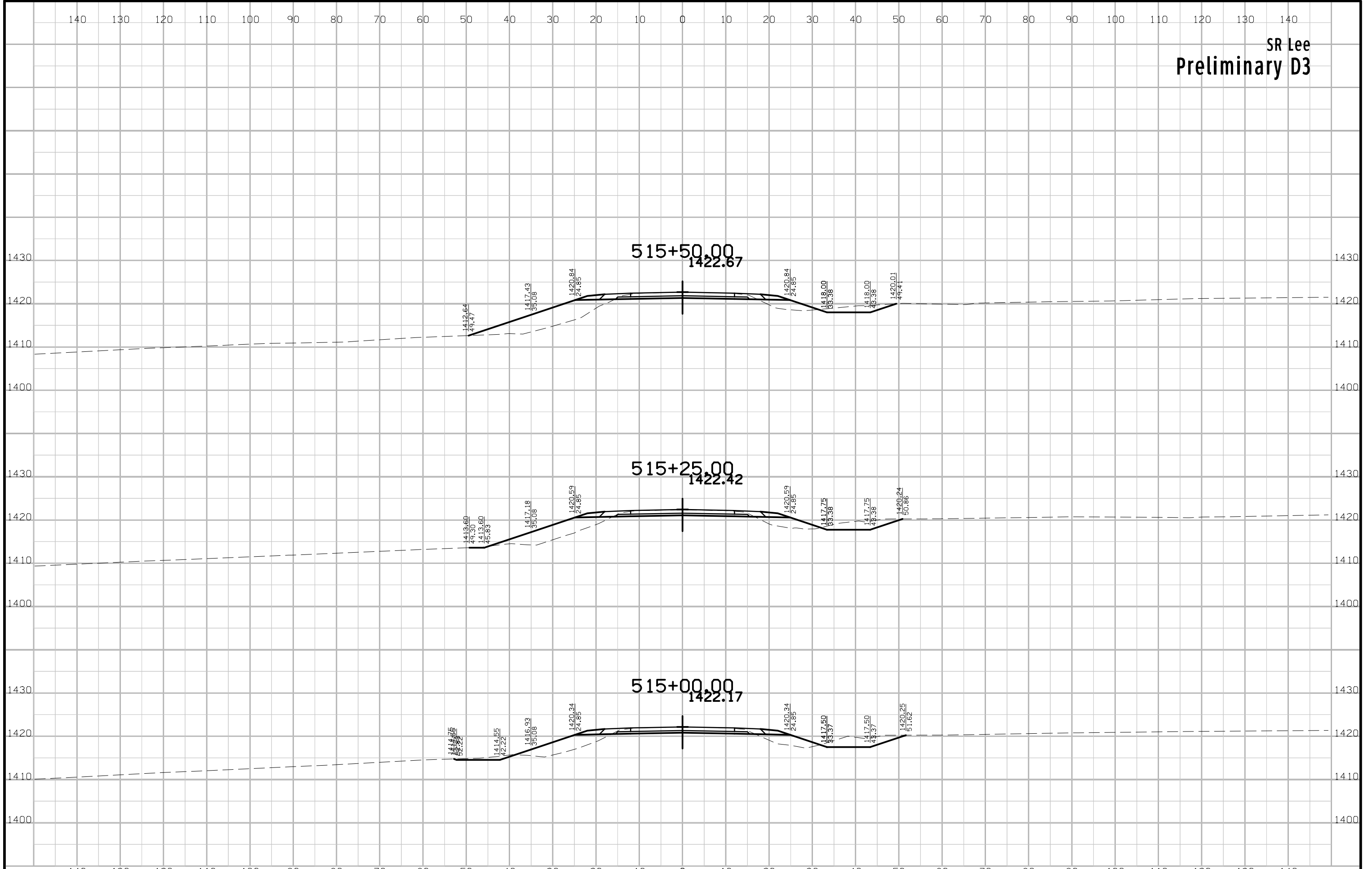




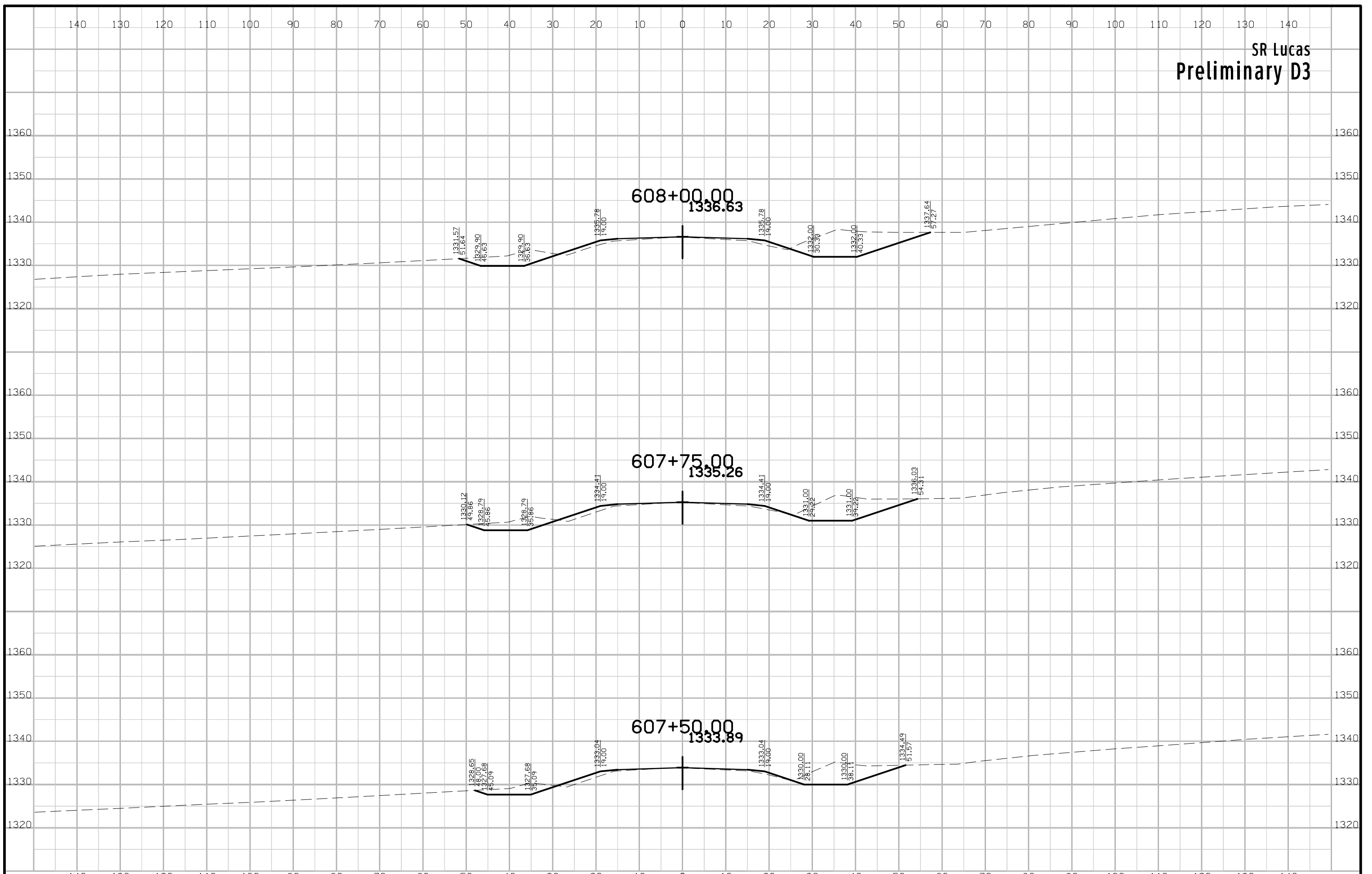


SR Lee
Preliminary D3

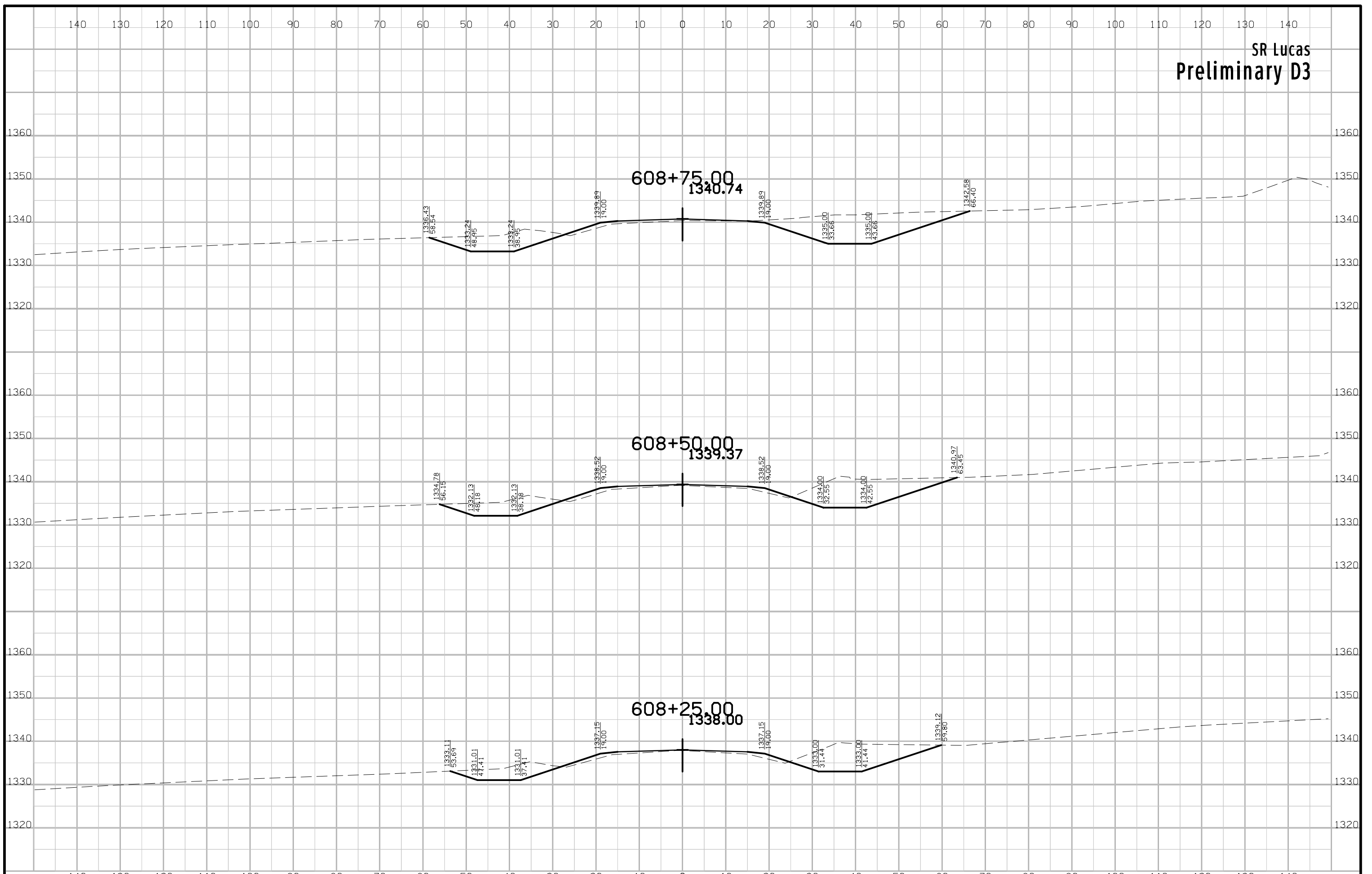




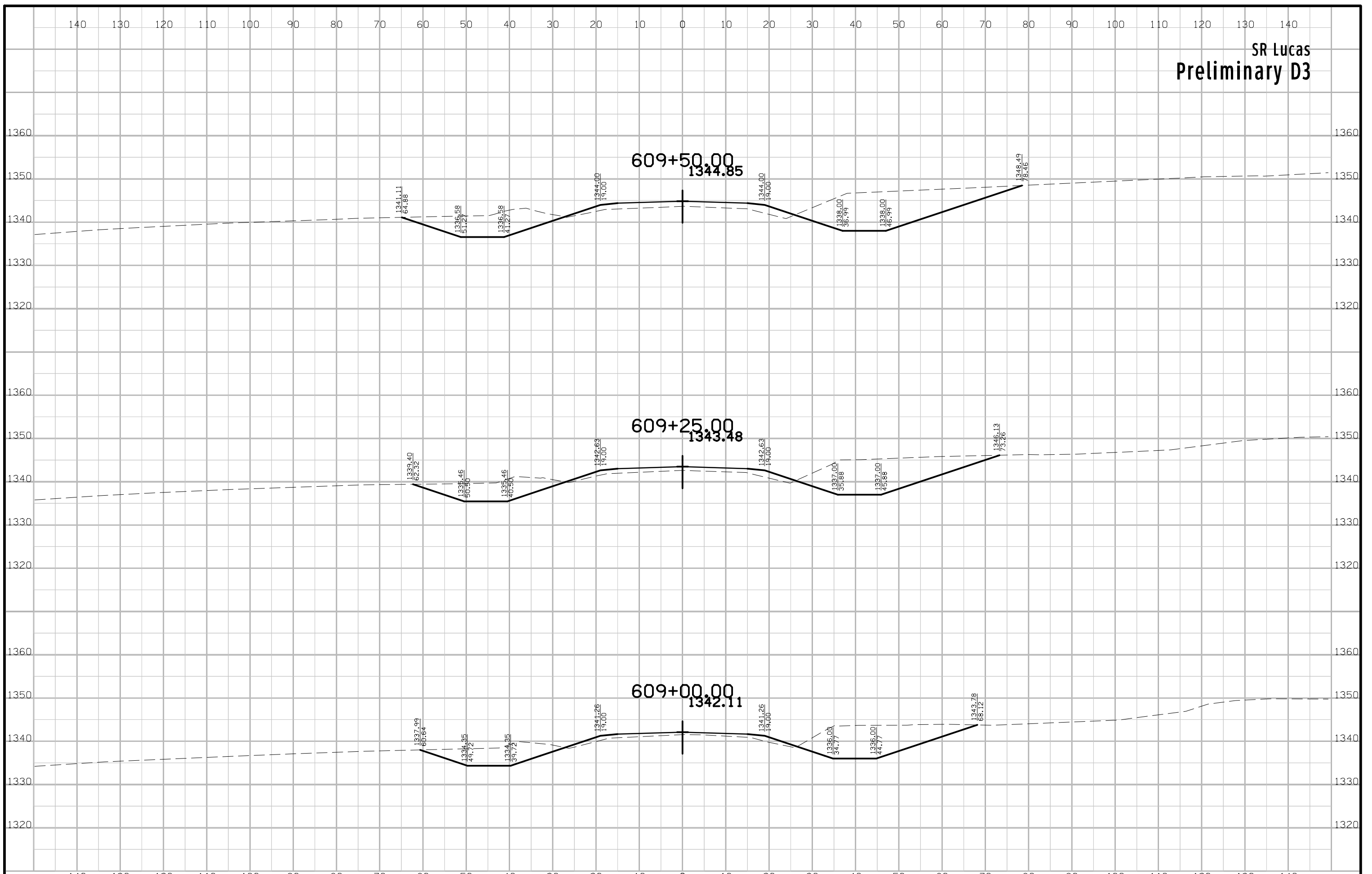
SR Lucas
Preliminary D3



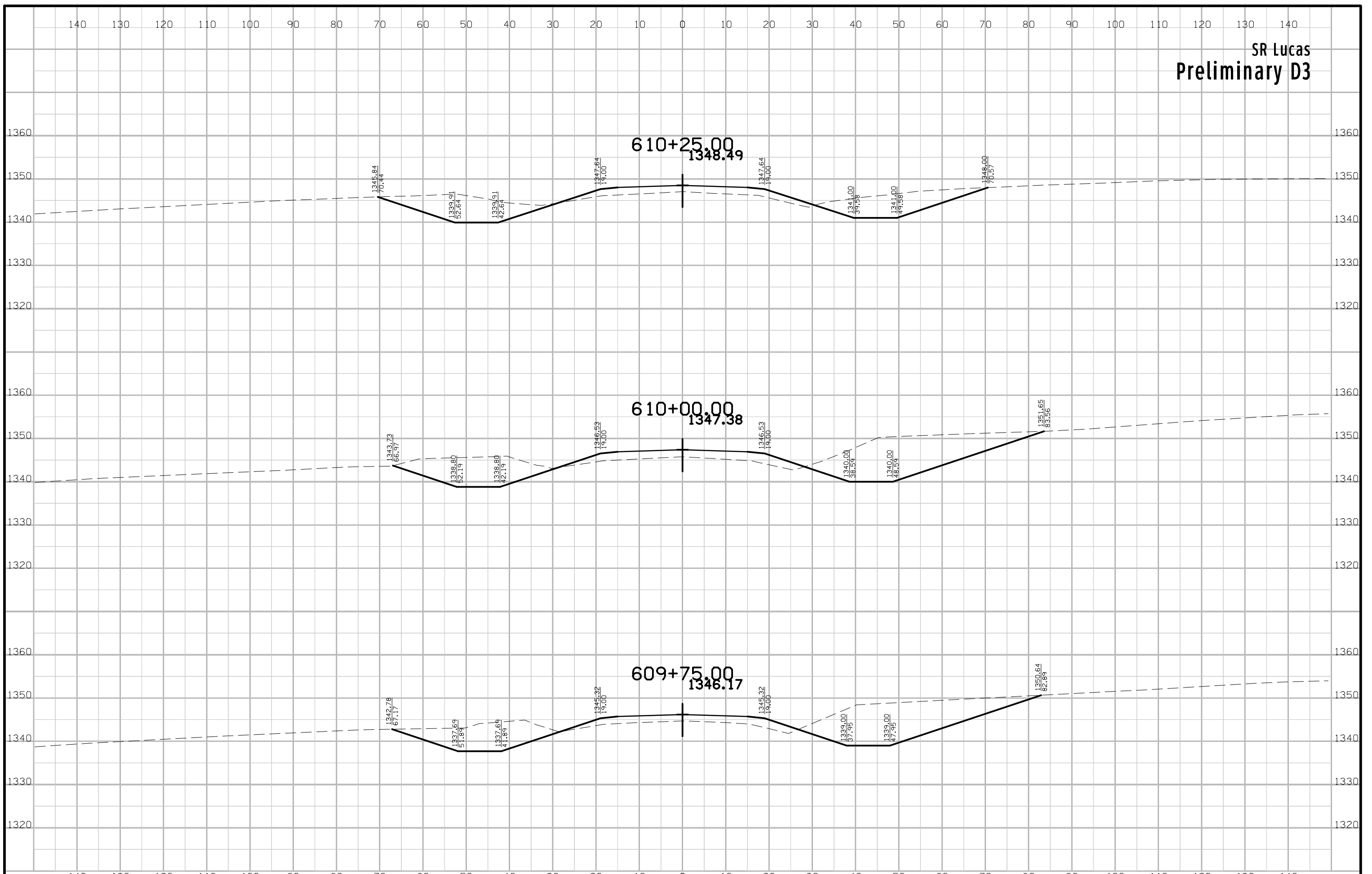
SR Lucas
Preliminary D3

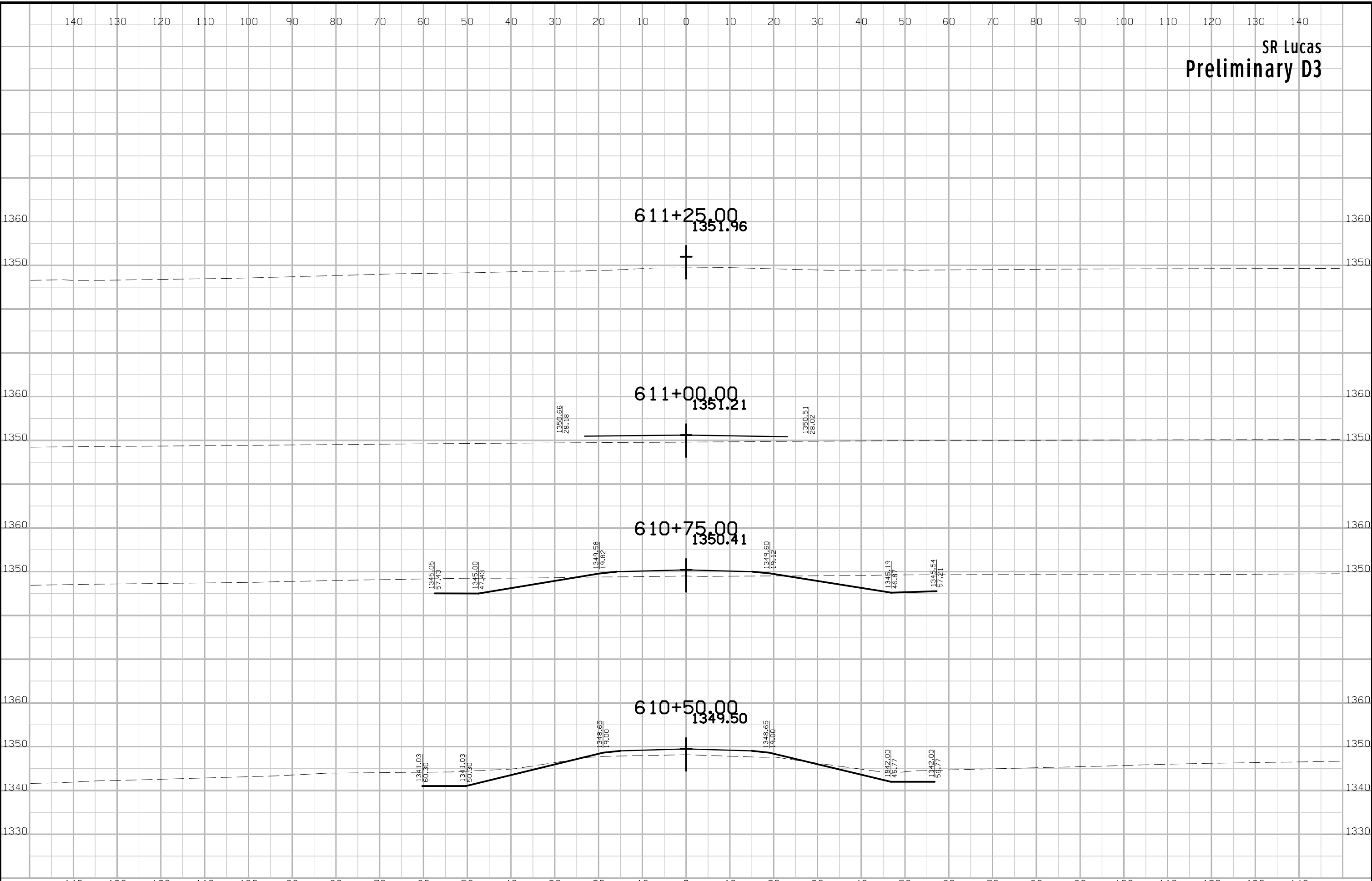


SR Lucas
Preliminary D3

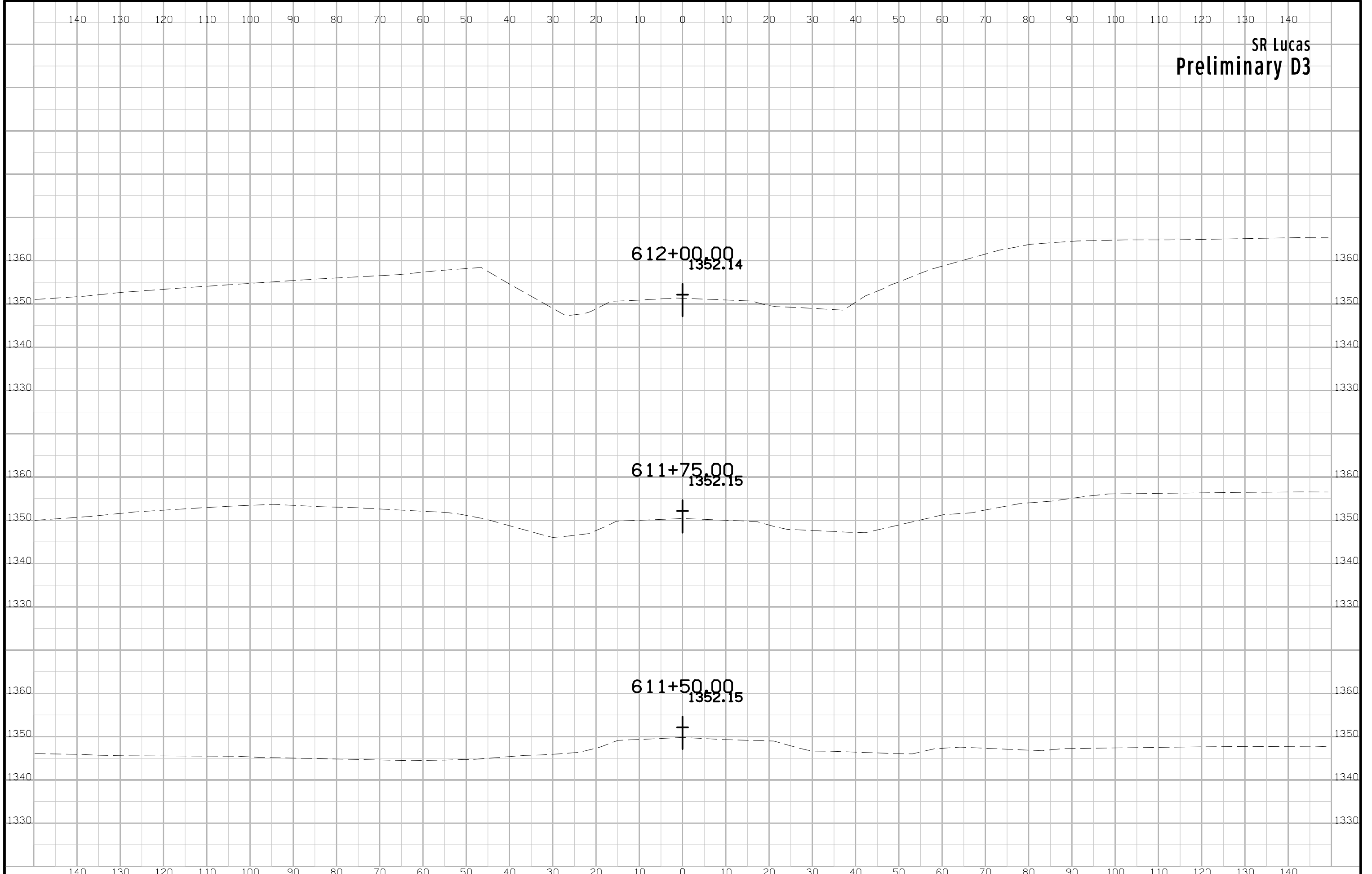


SR Lucas
Preliminary D3

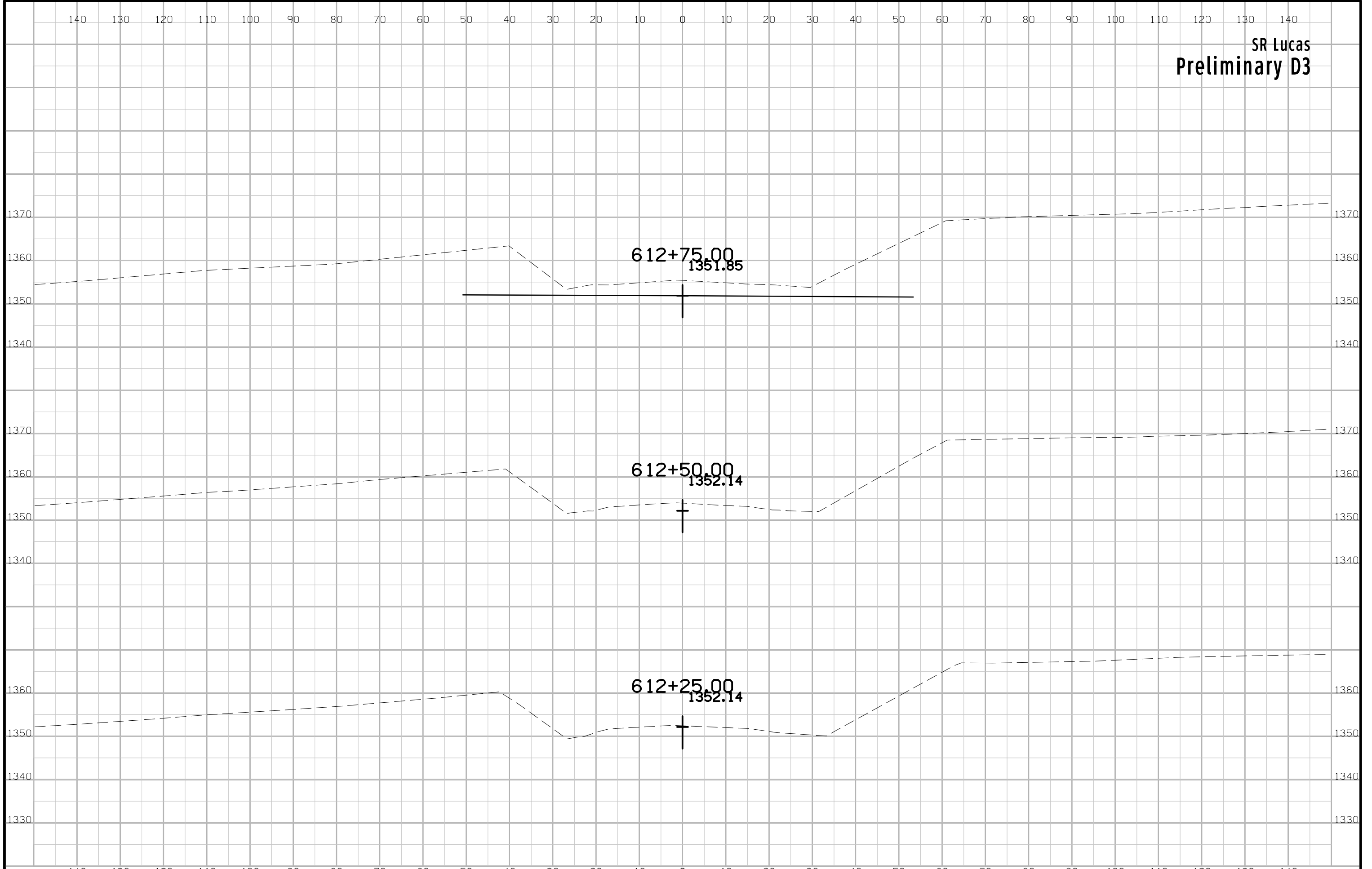




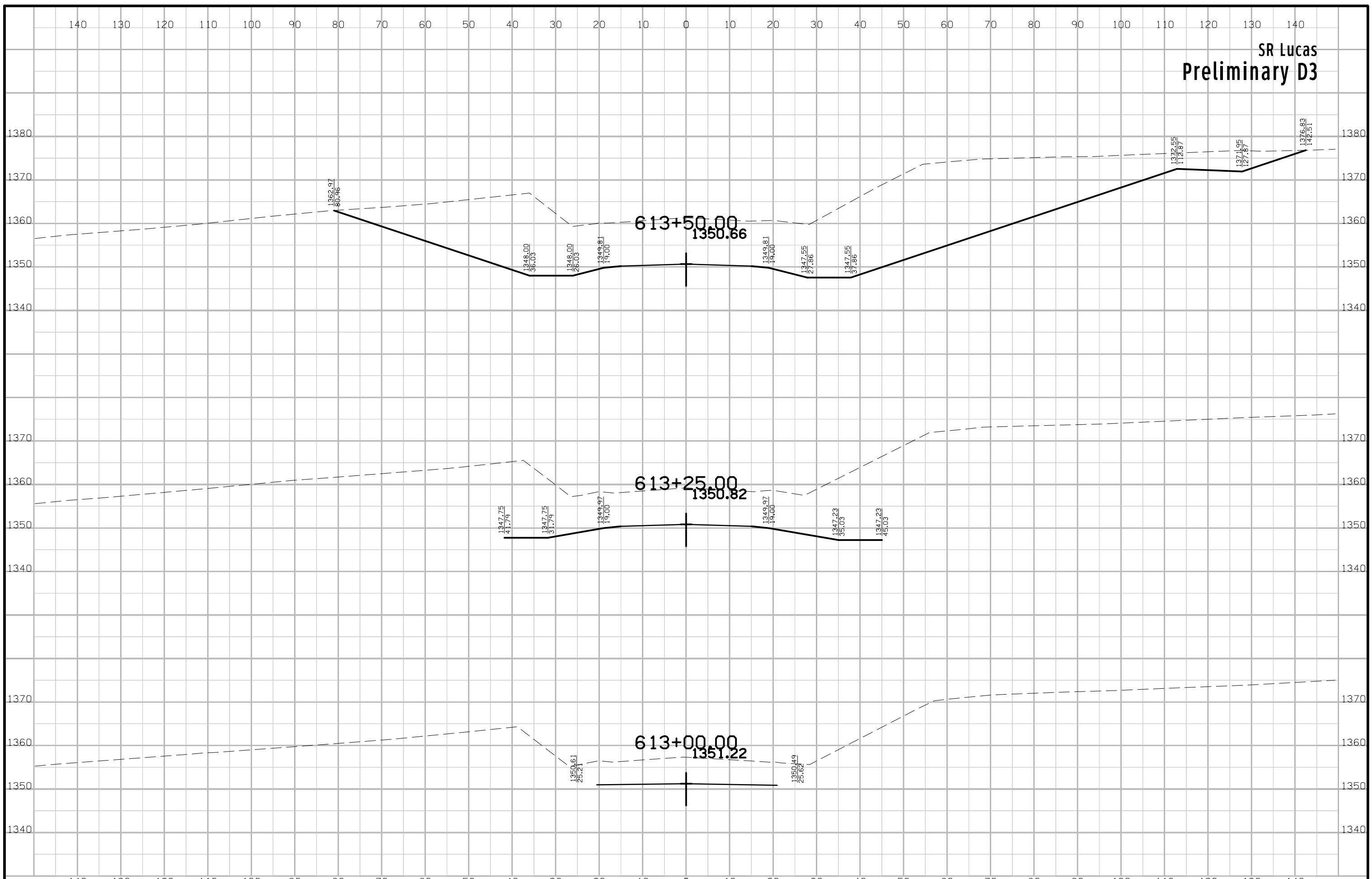
SR Lucas
Preliminary D3



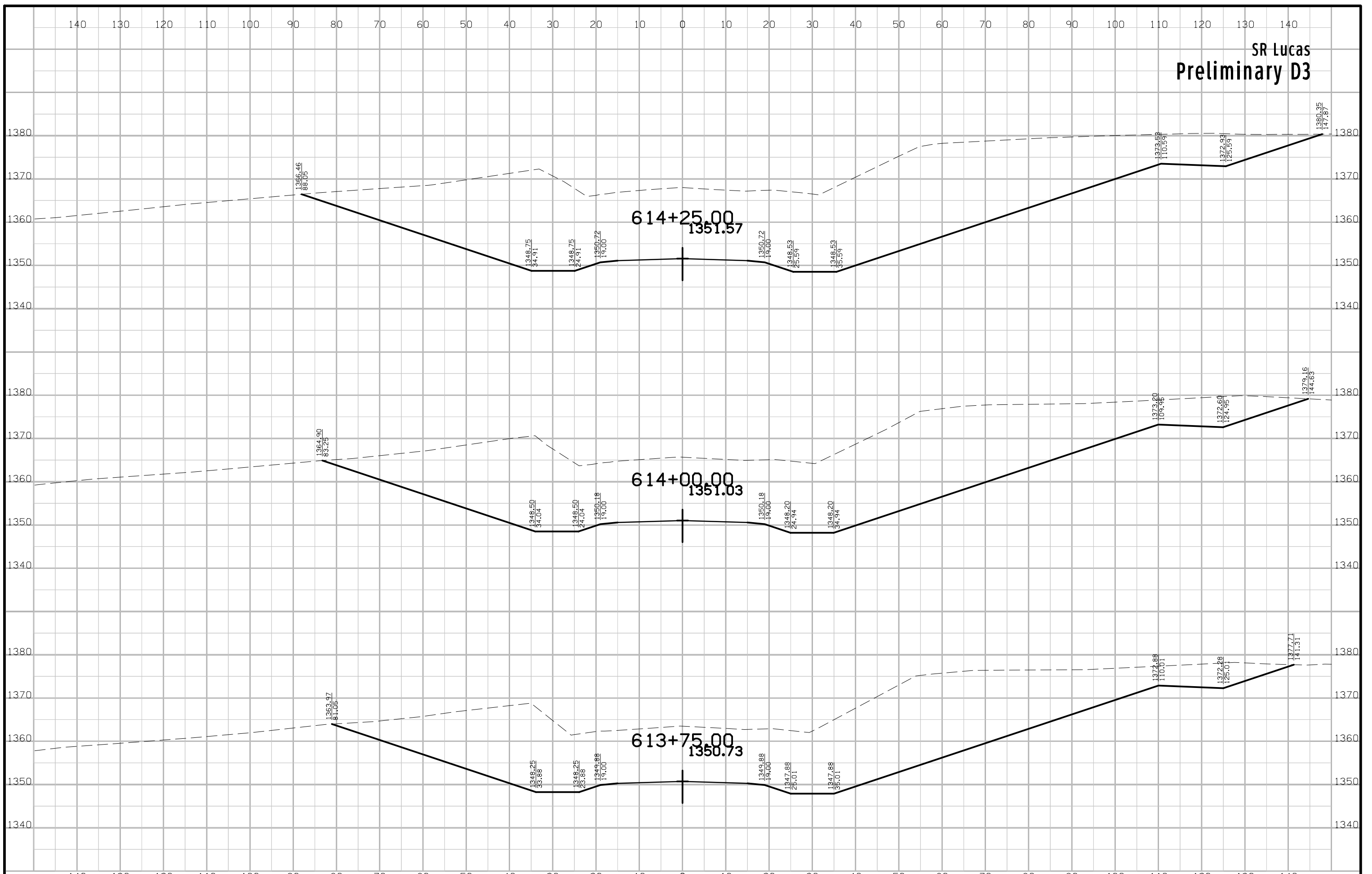
SR Lucas
Preliminary D3



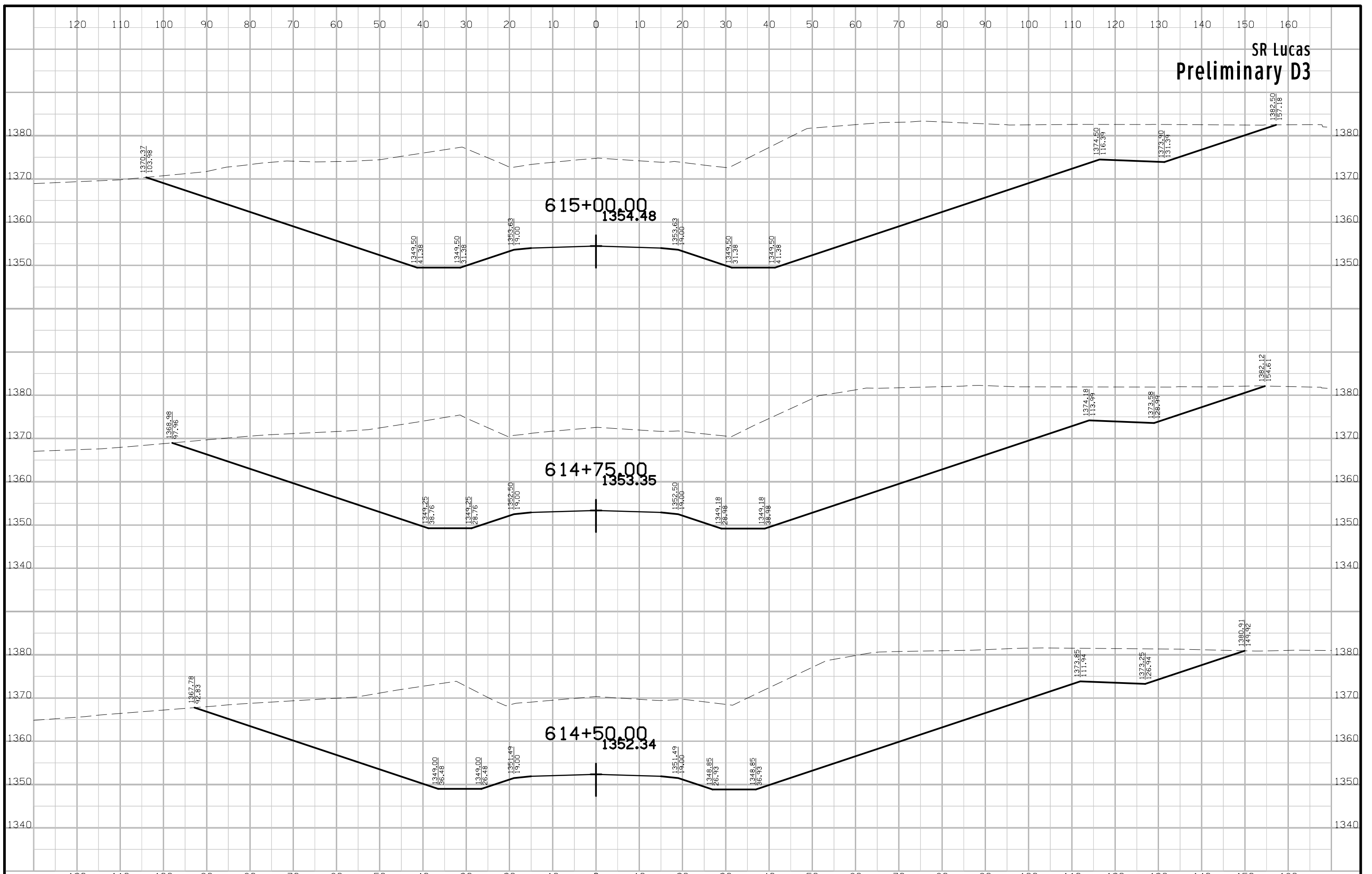
SR Lucas
Preliminary D3



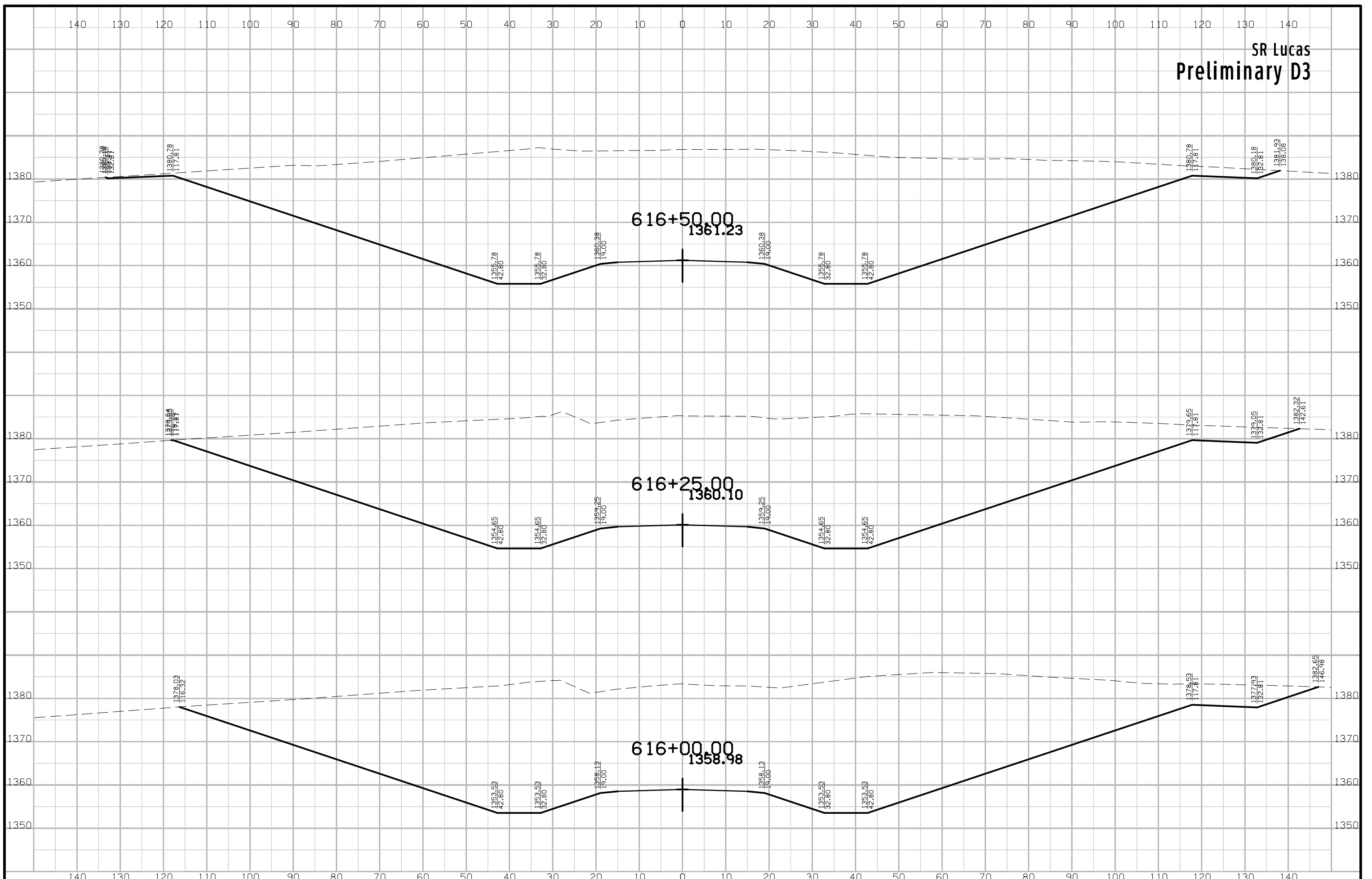
SR Lucas
Preliminary D3



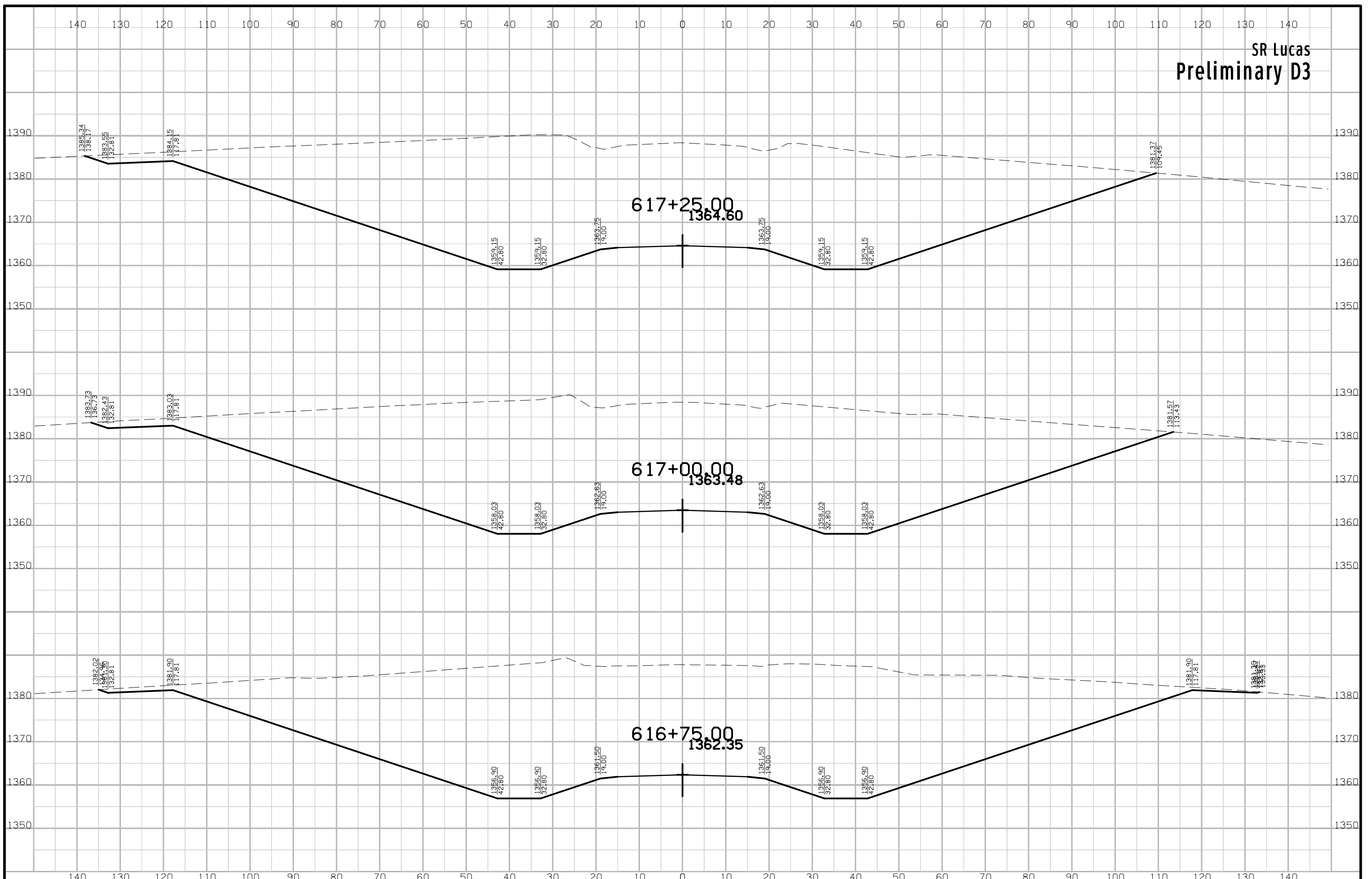
SR Lucas
Preliminary D3



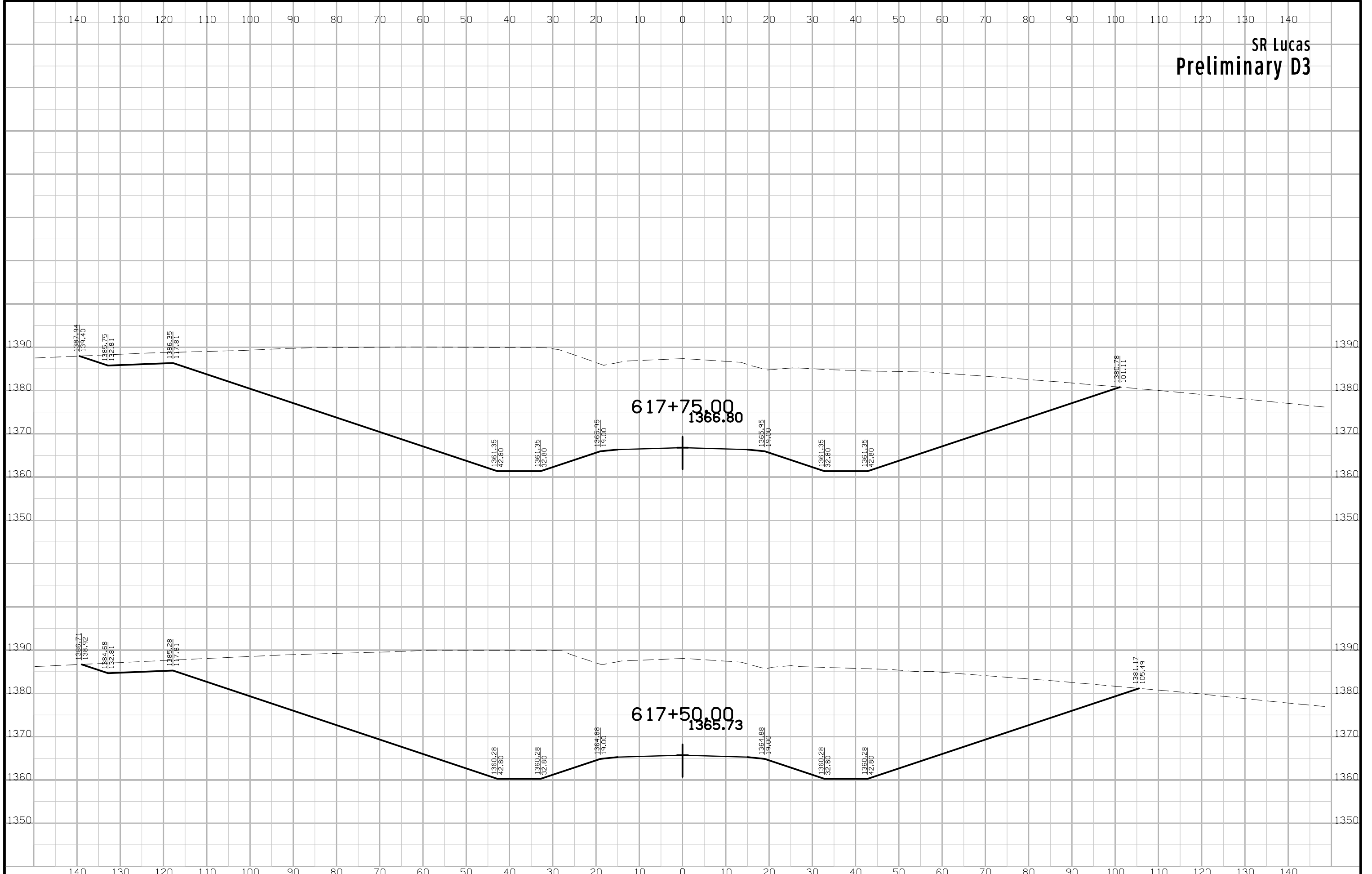
SR Lucas
Preliminary D3



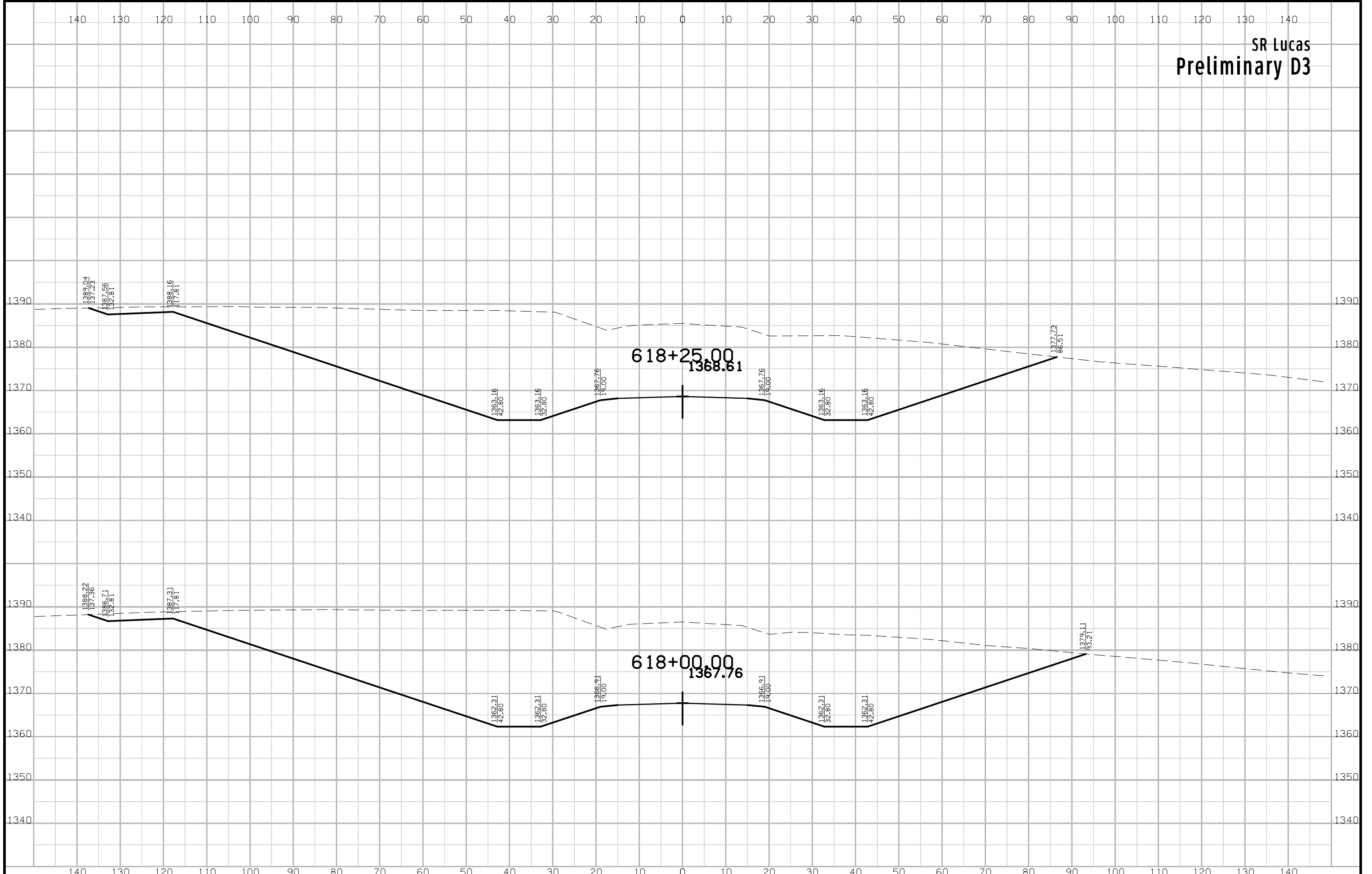
SR Lucas
Preliminary D3



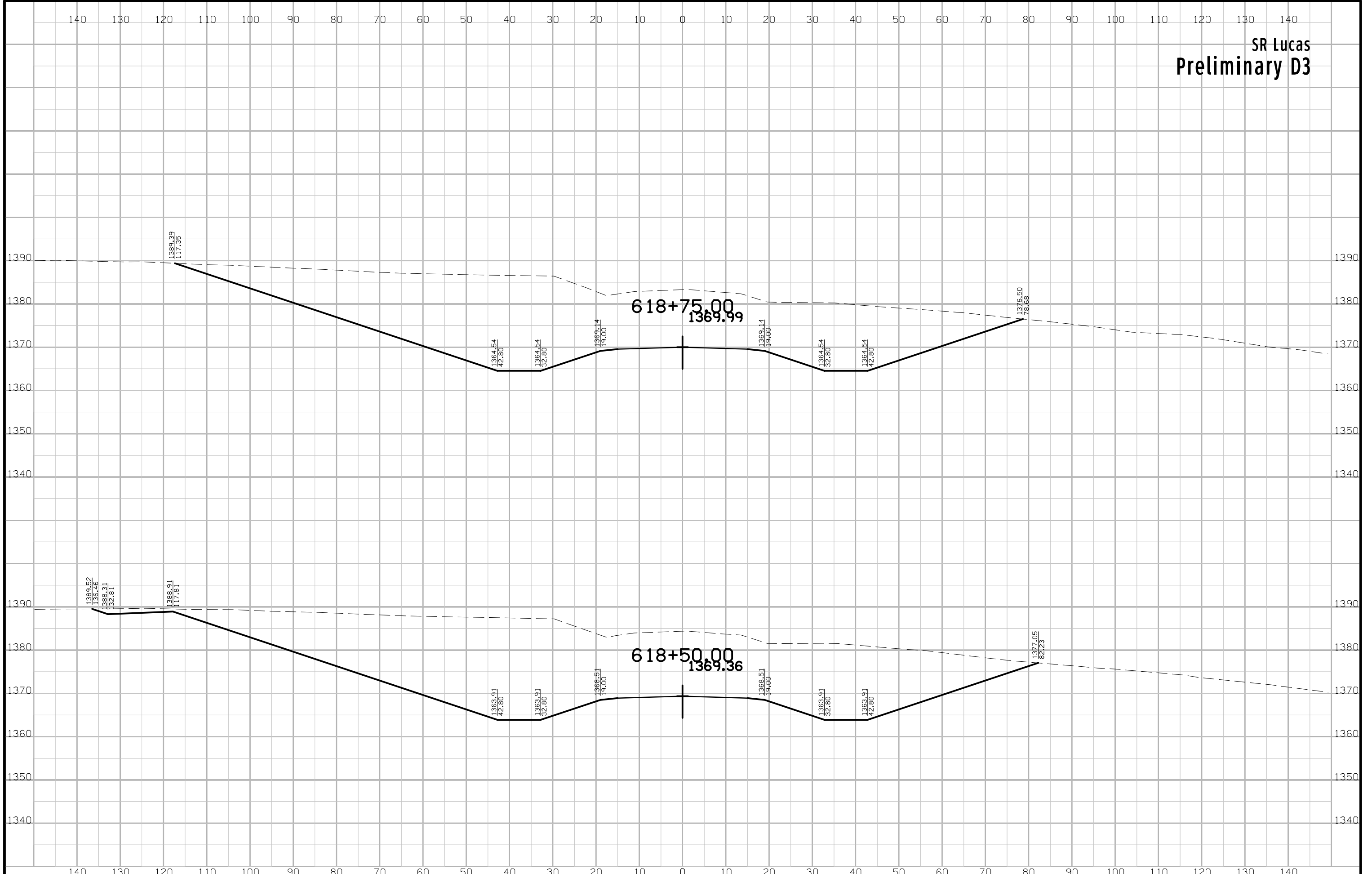
SR Lucas
Preliminary D3



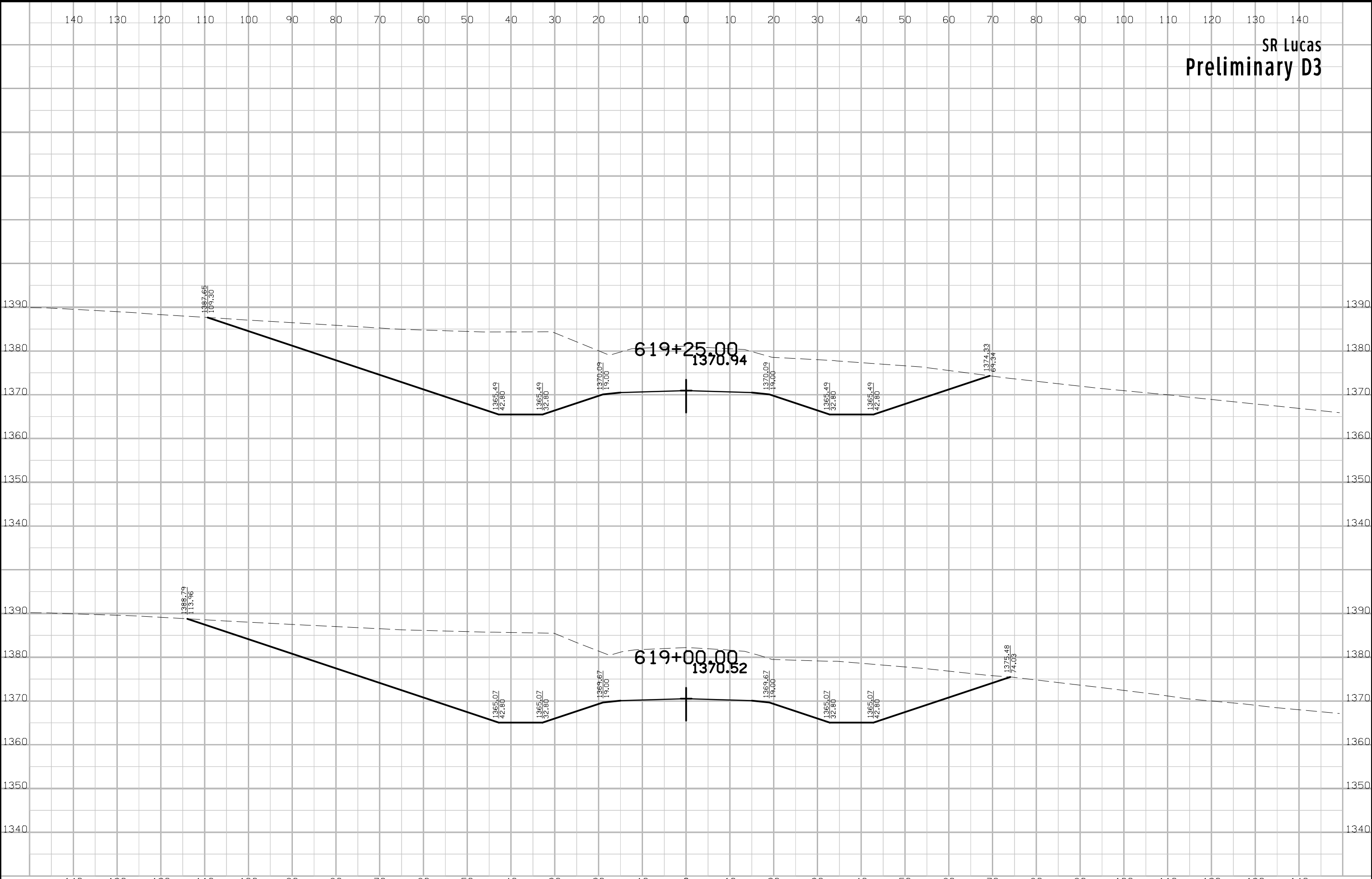
SR Lucas
Preliminary D3



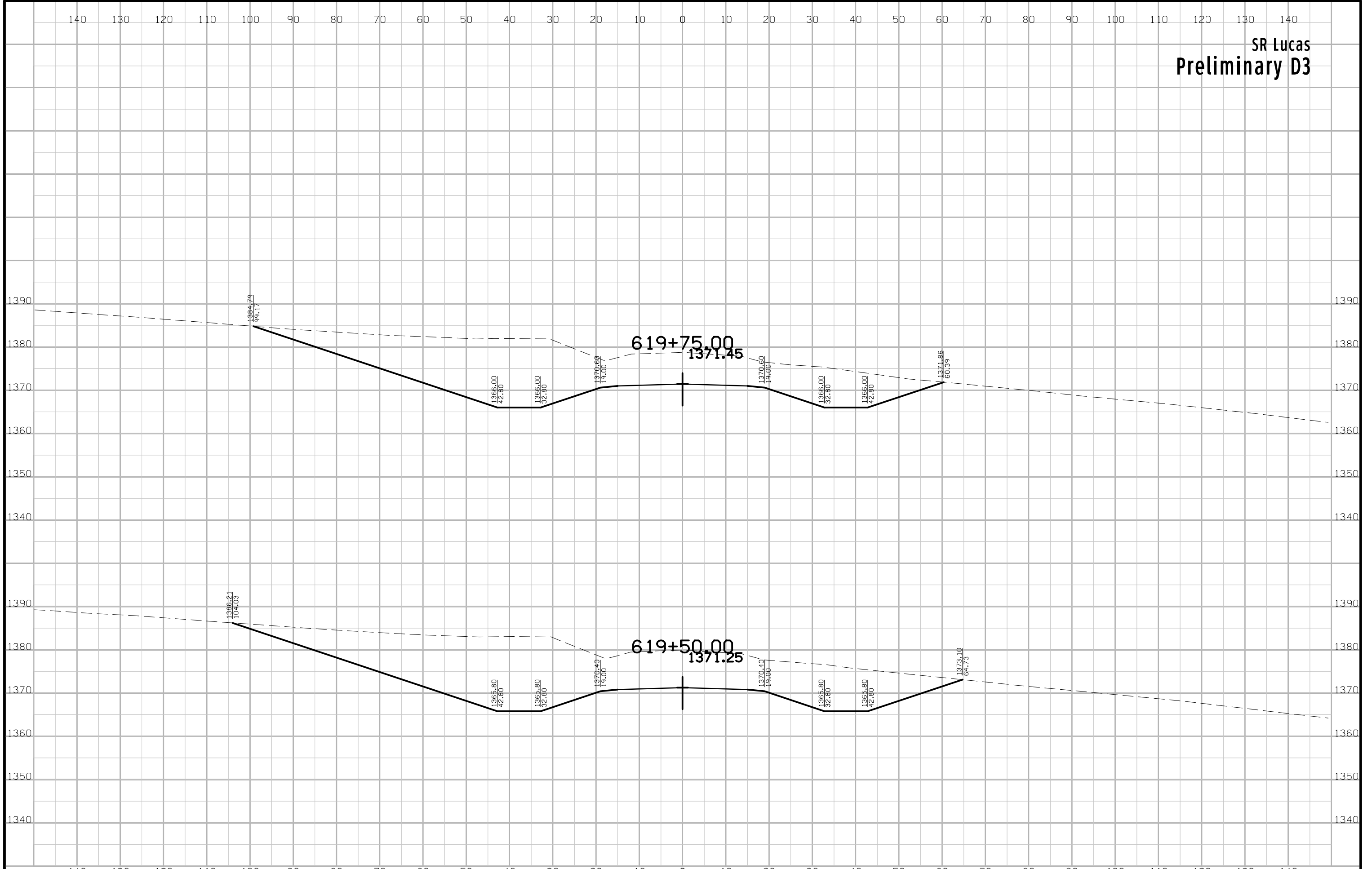
SR Lucas
Preliminary D3



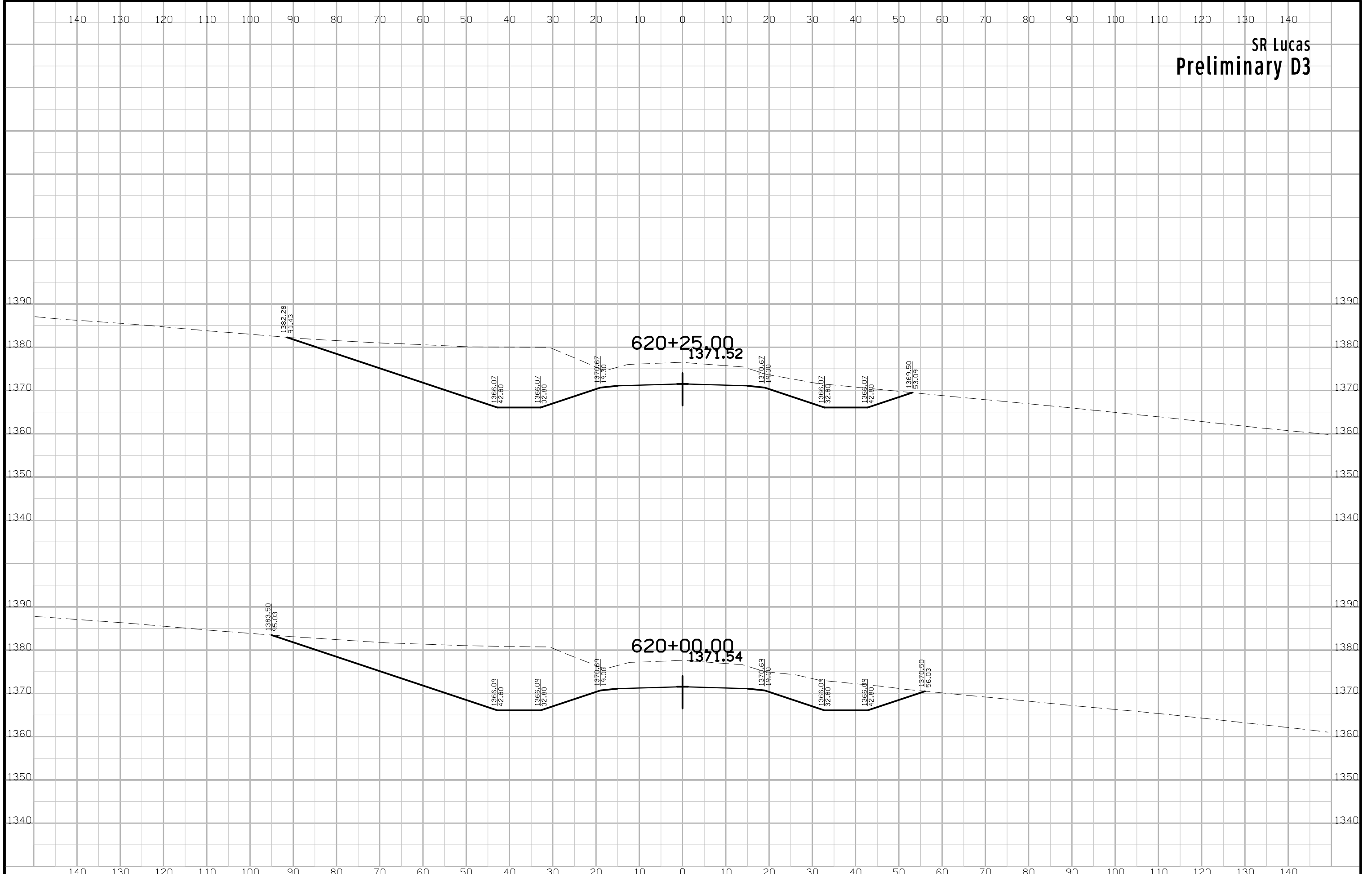
SR Lucas
Preliminary D3



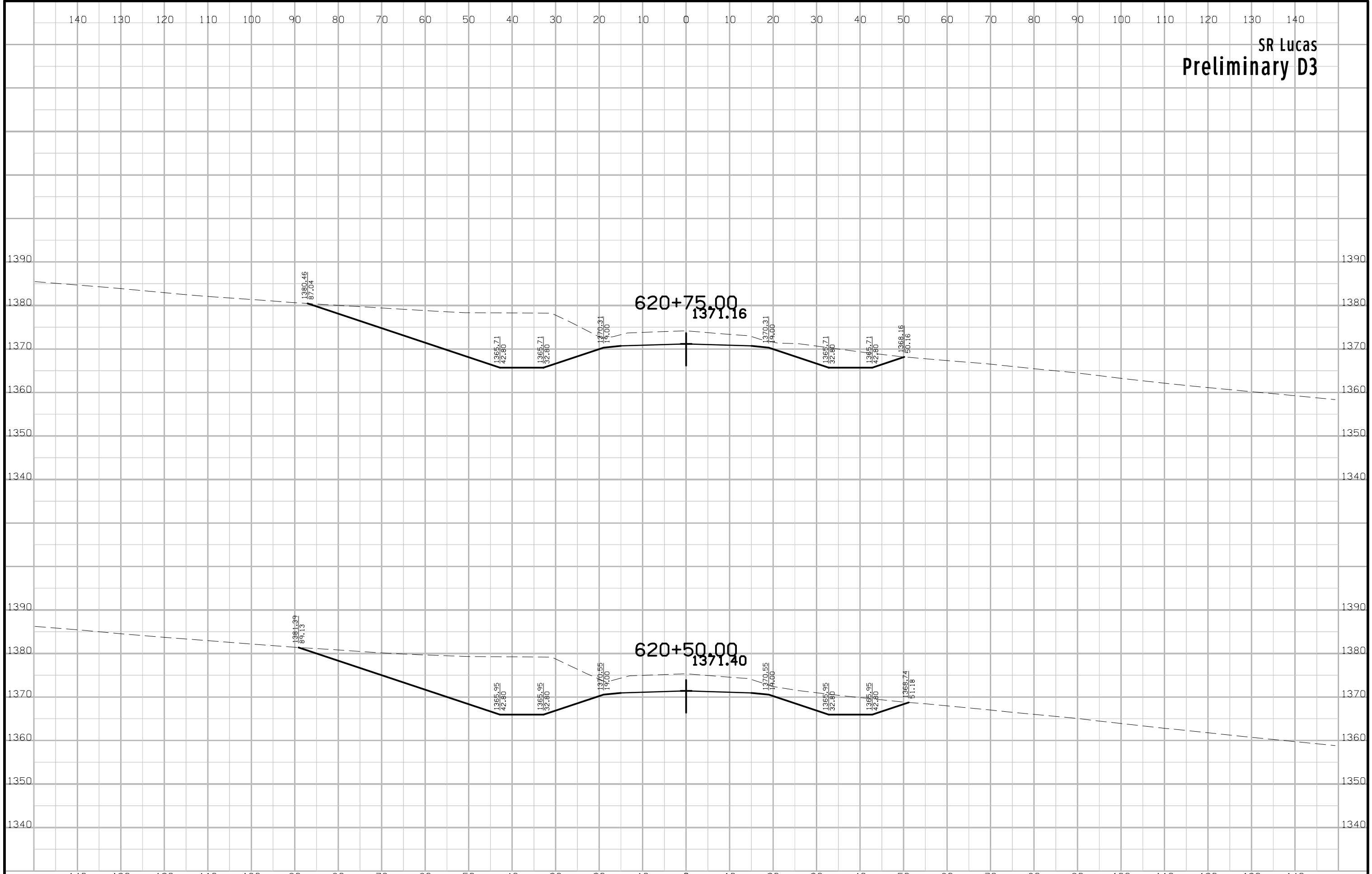
SR Lucas
Preliminary D3



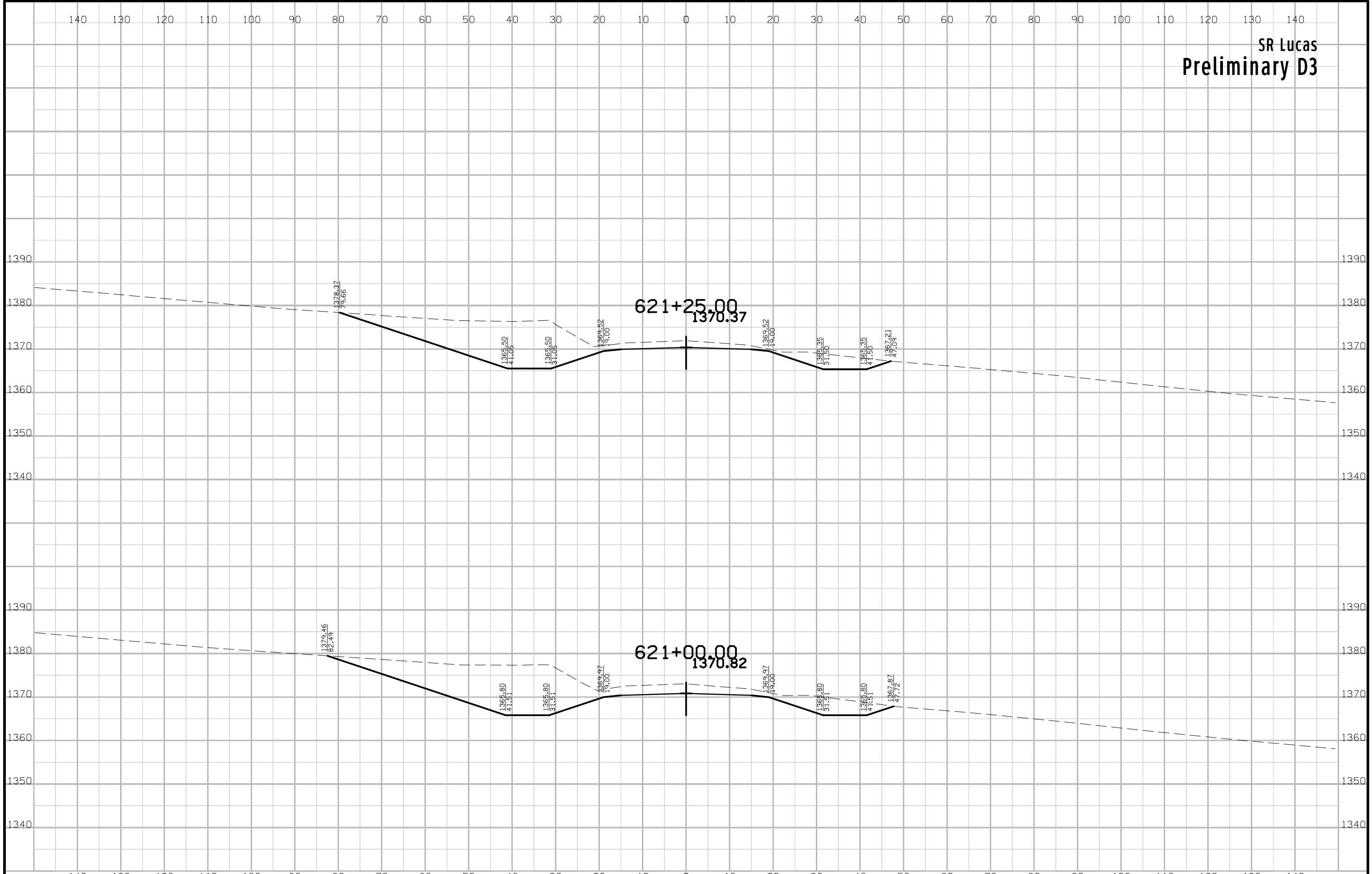
SR Lucas
Preliminary D3

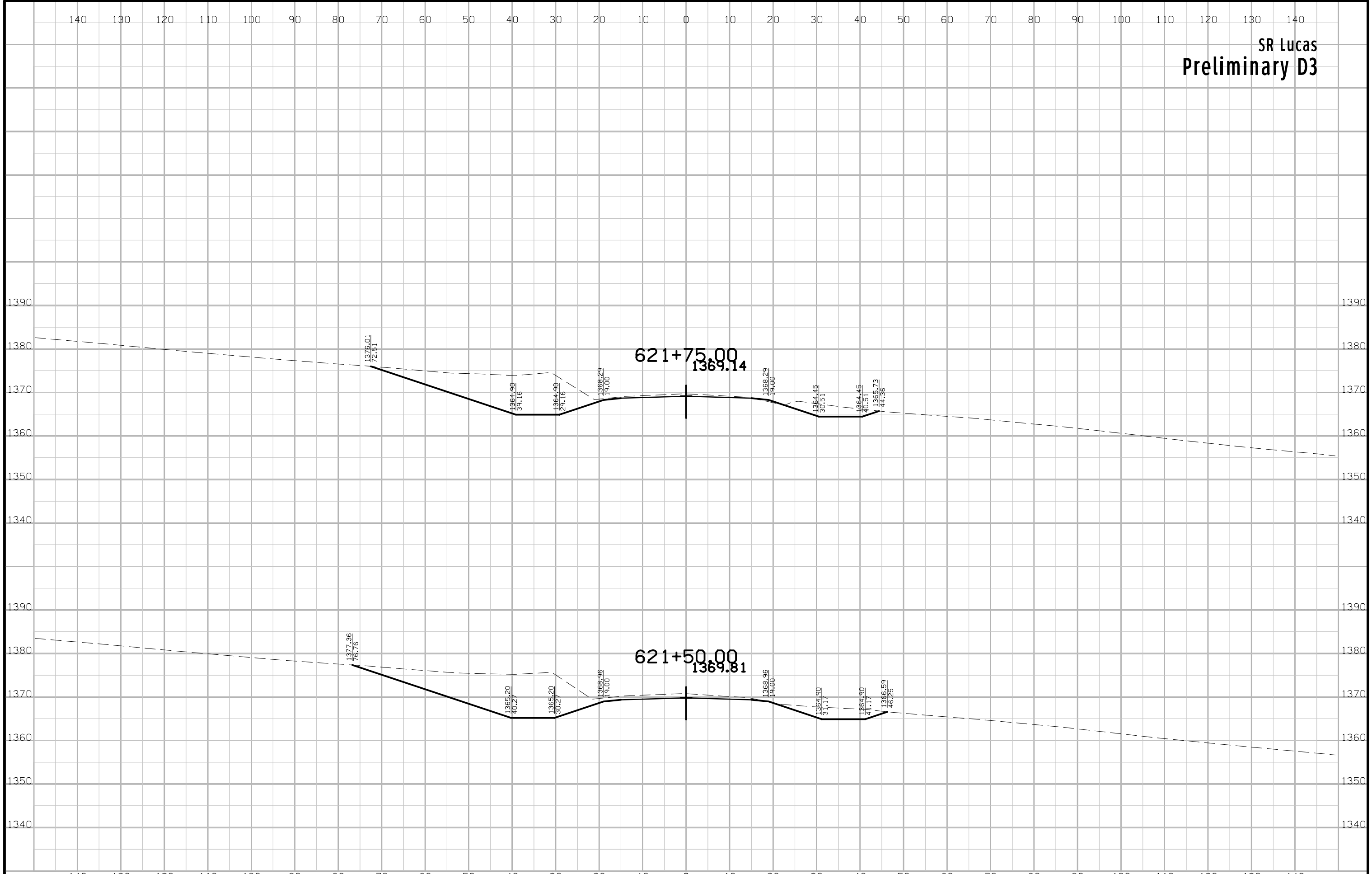


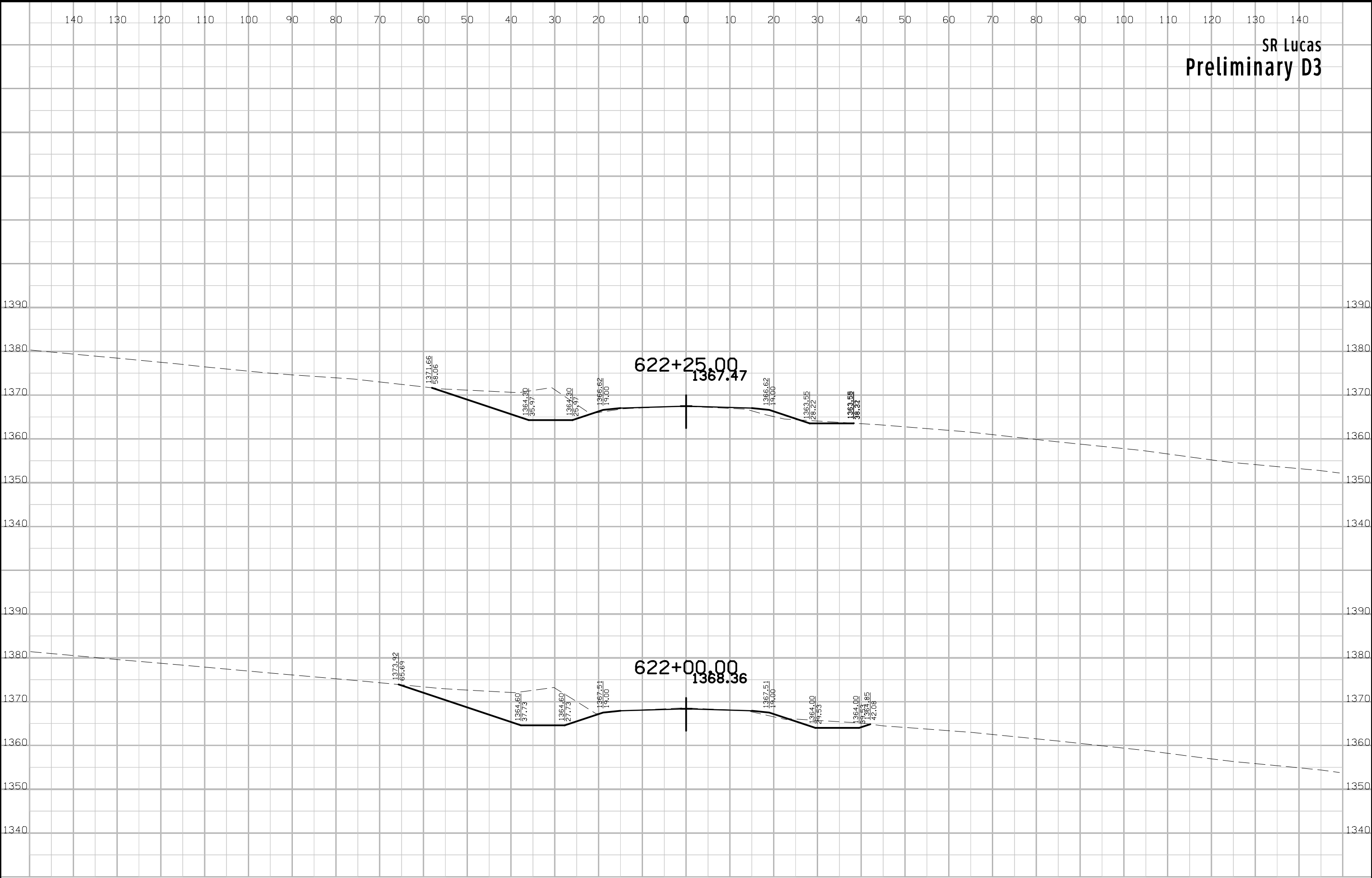
SR Lucas
Preliminary D3



SR Lucas
Preliminary D3



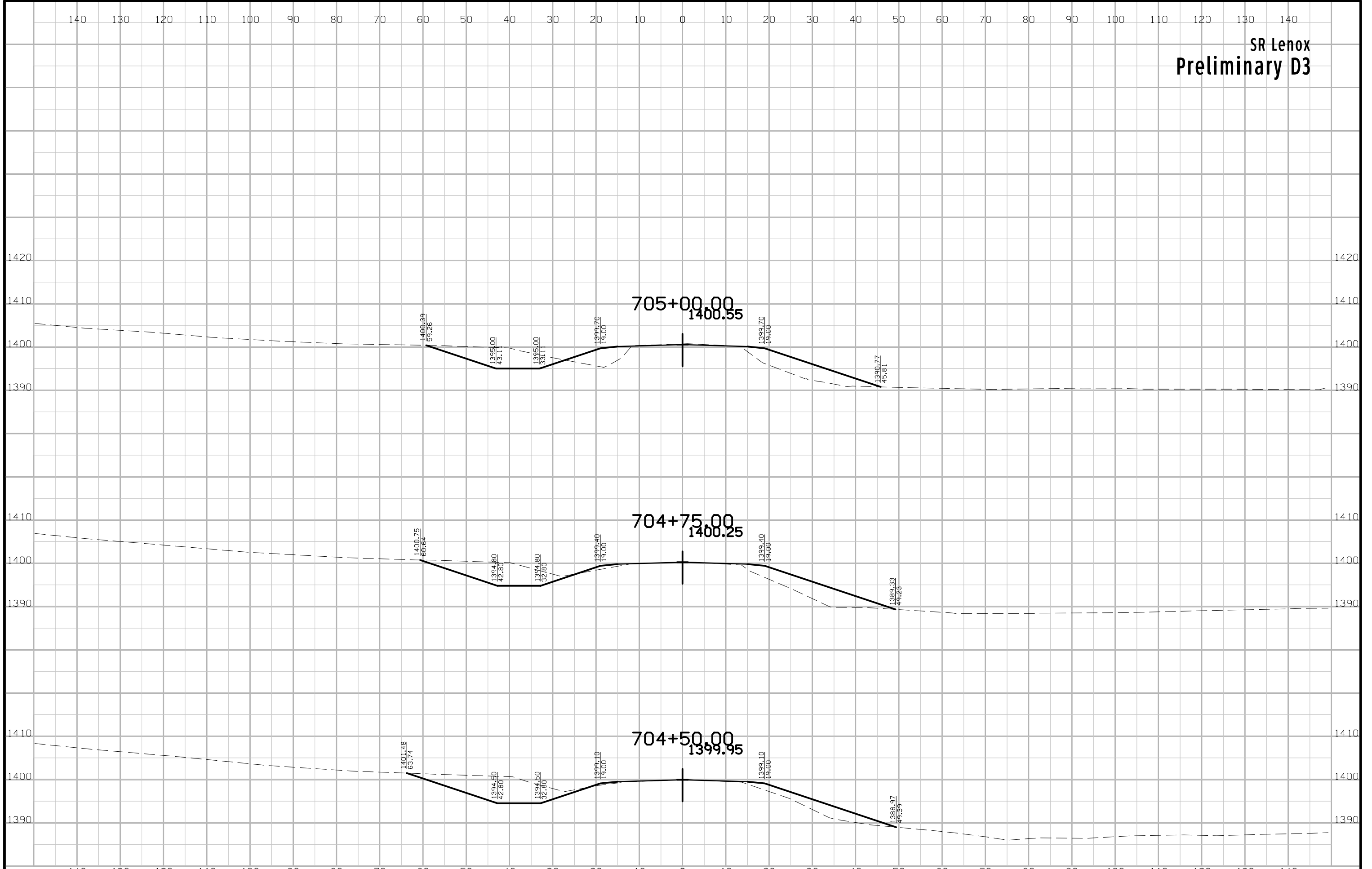




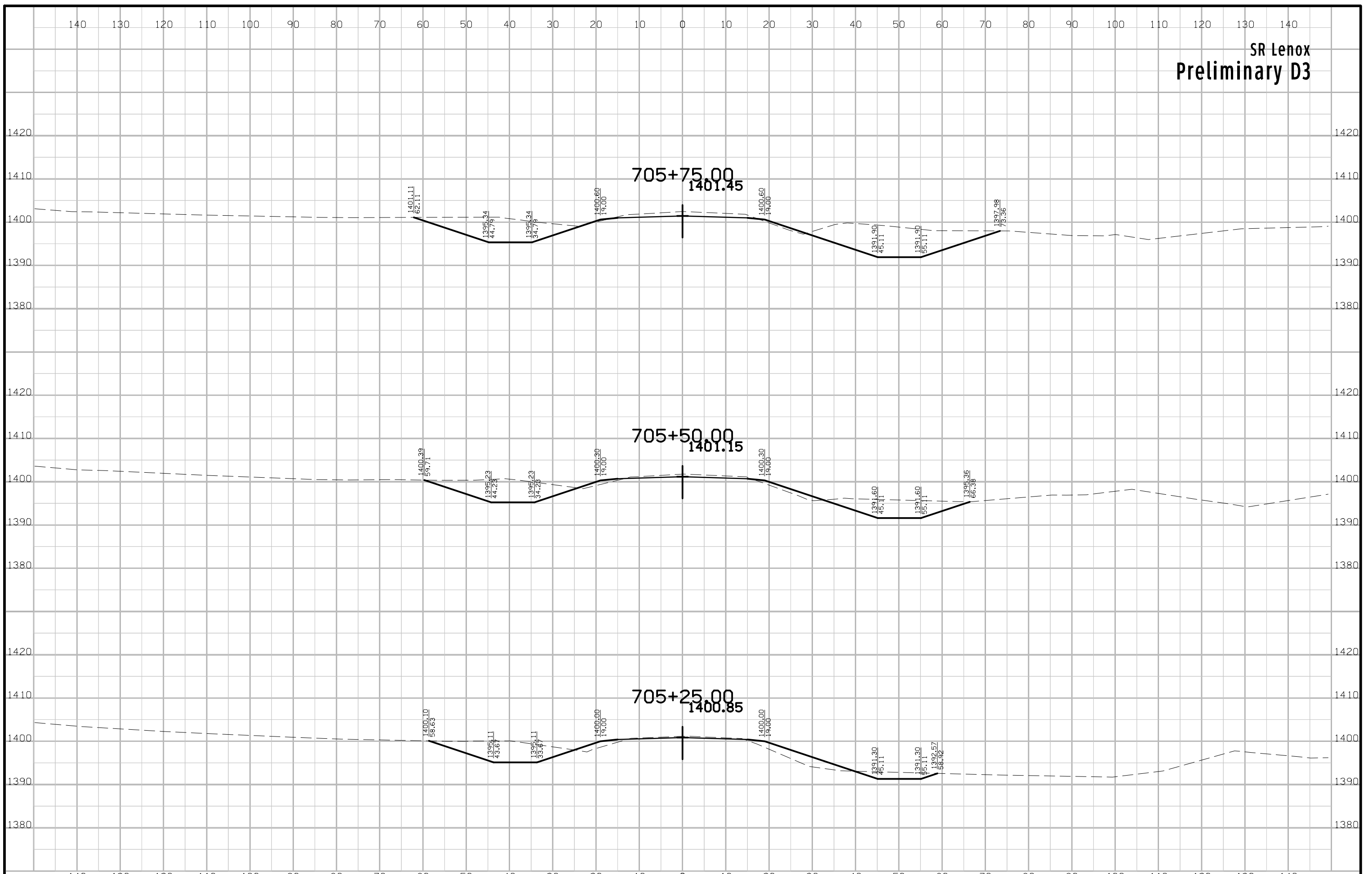
SR Lucas
Preliminary D3



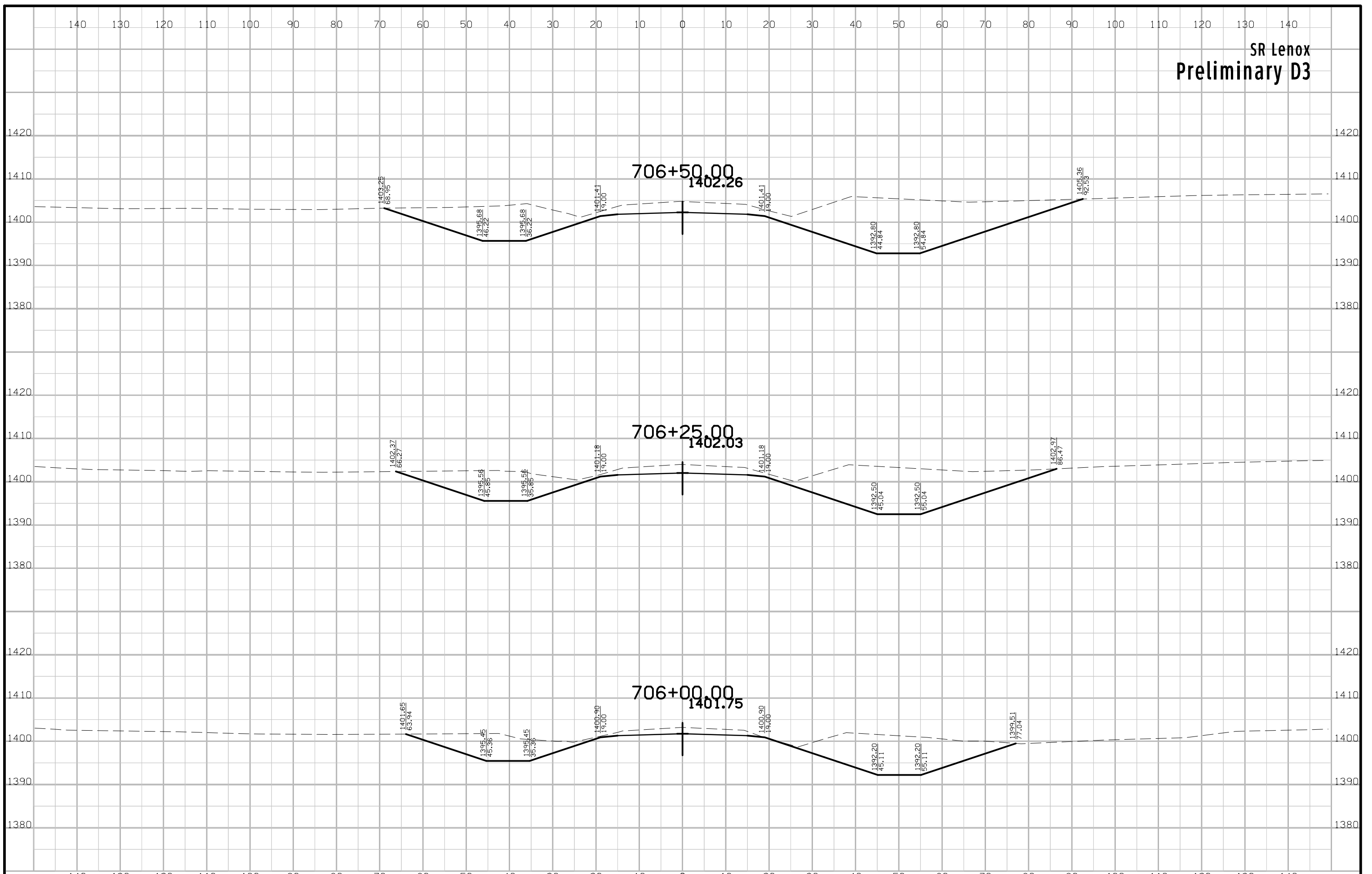
SR Lenox
Preliminary D3



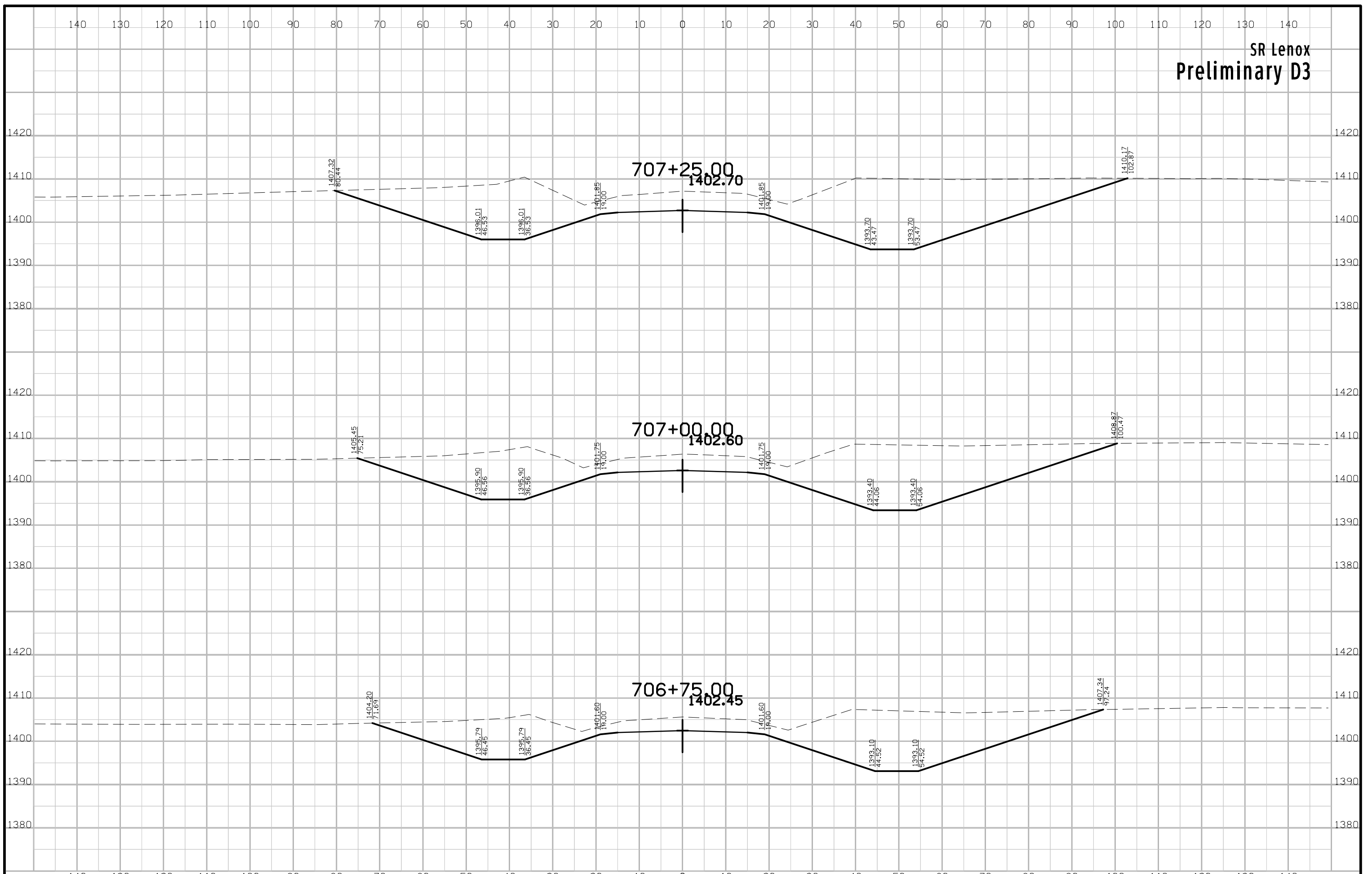
SR Lenox
Preliminary D3



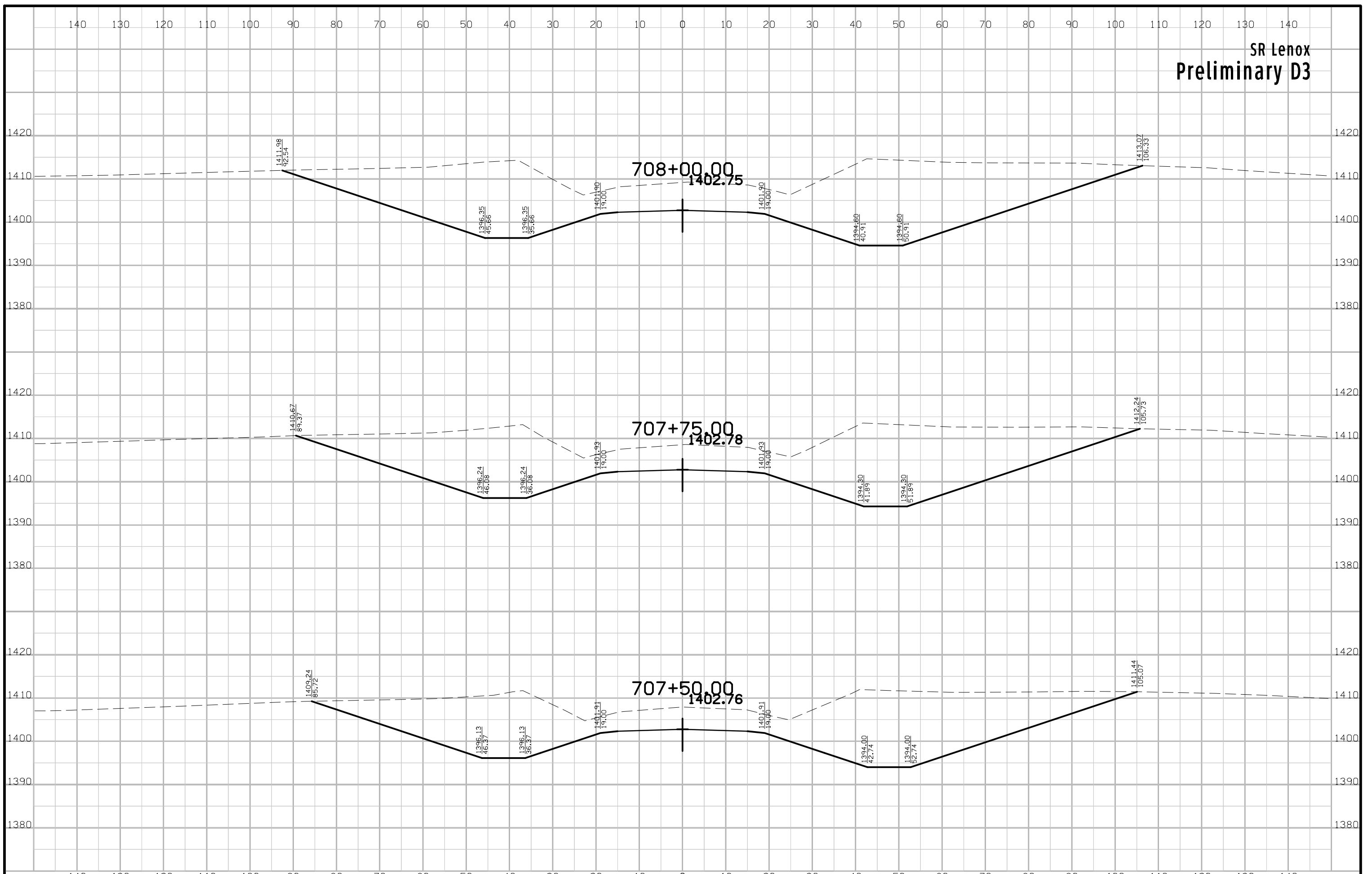
SR Lenox
Preliminary D3



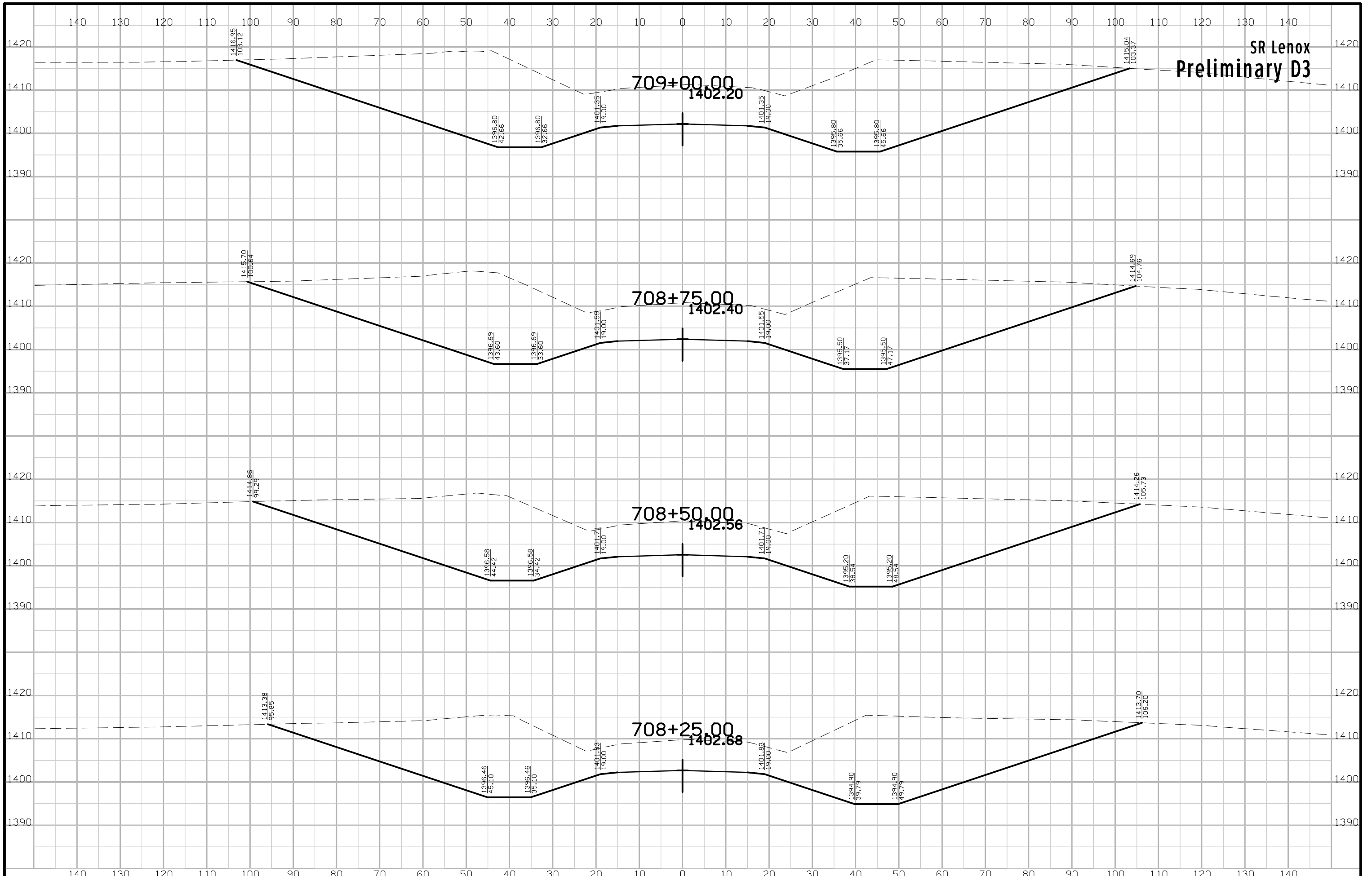
SR Lenox
Preliminary D3



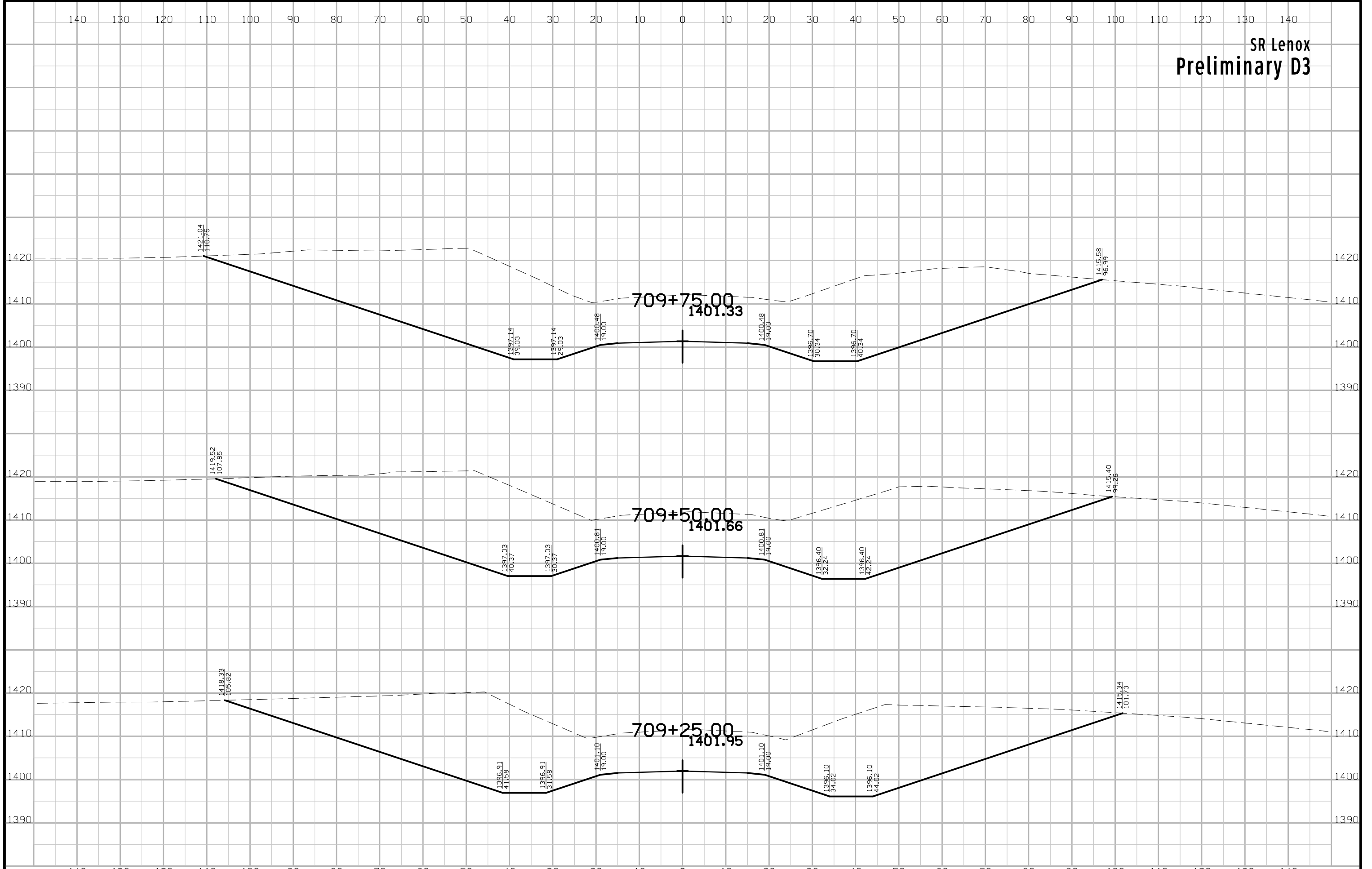
SR Lenox
Preliminary D3



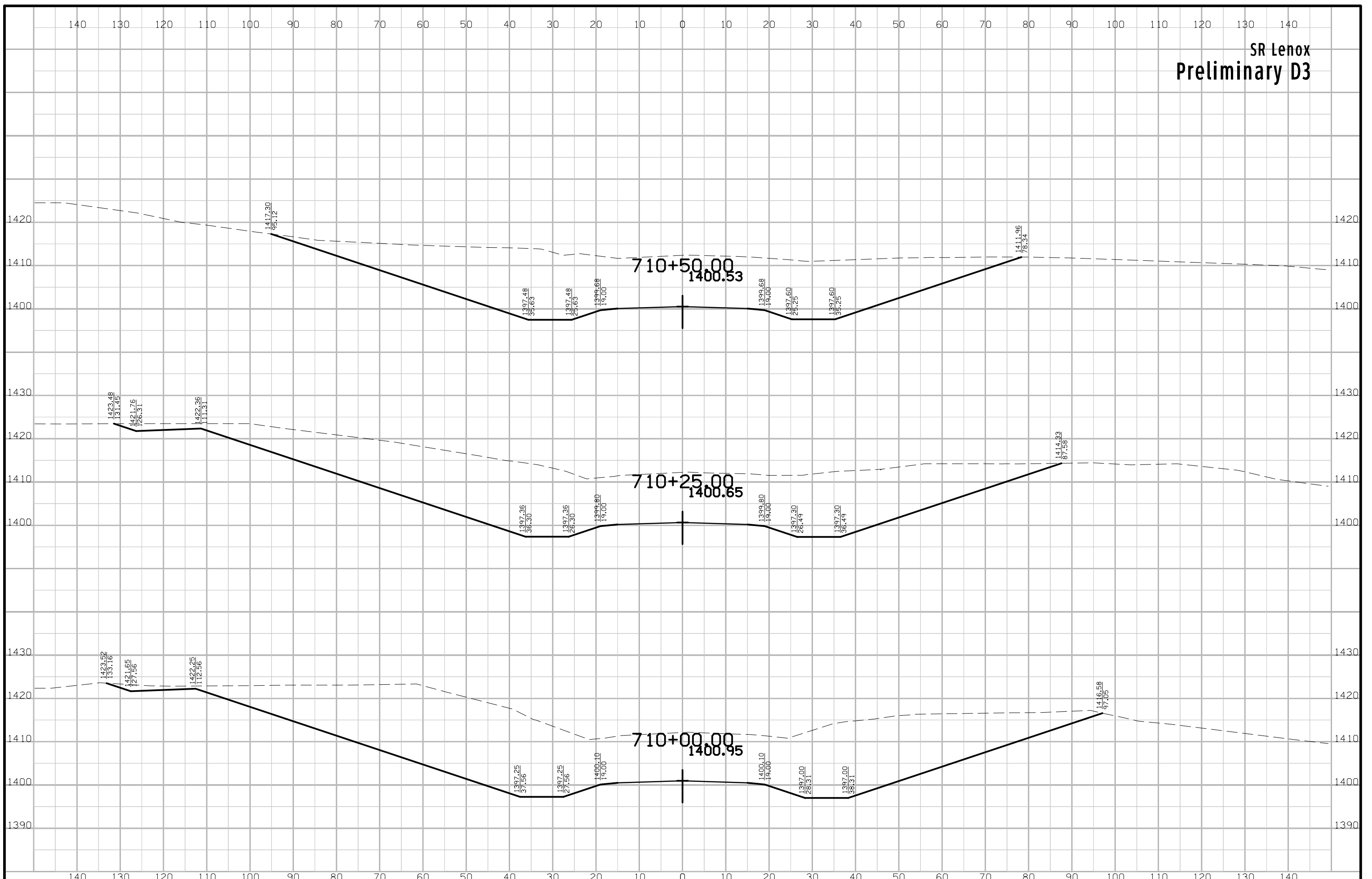
SR Lenox
Preliminary D3



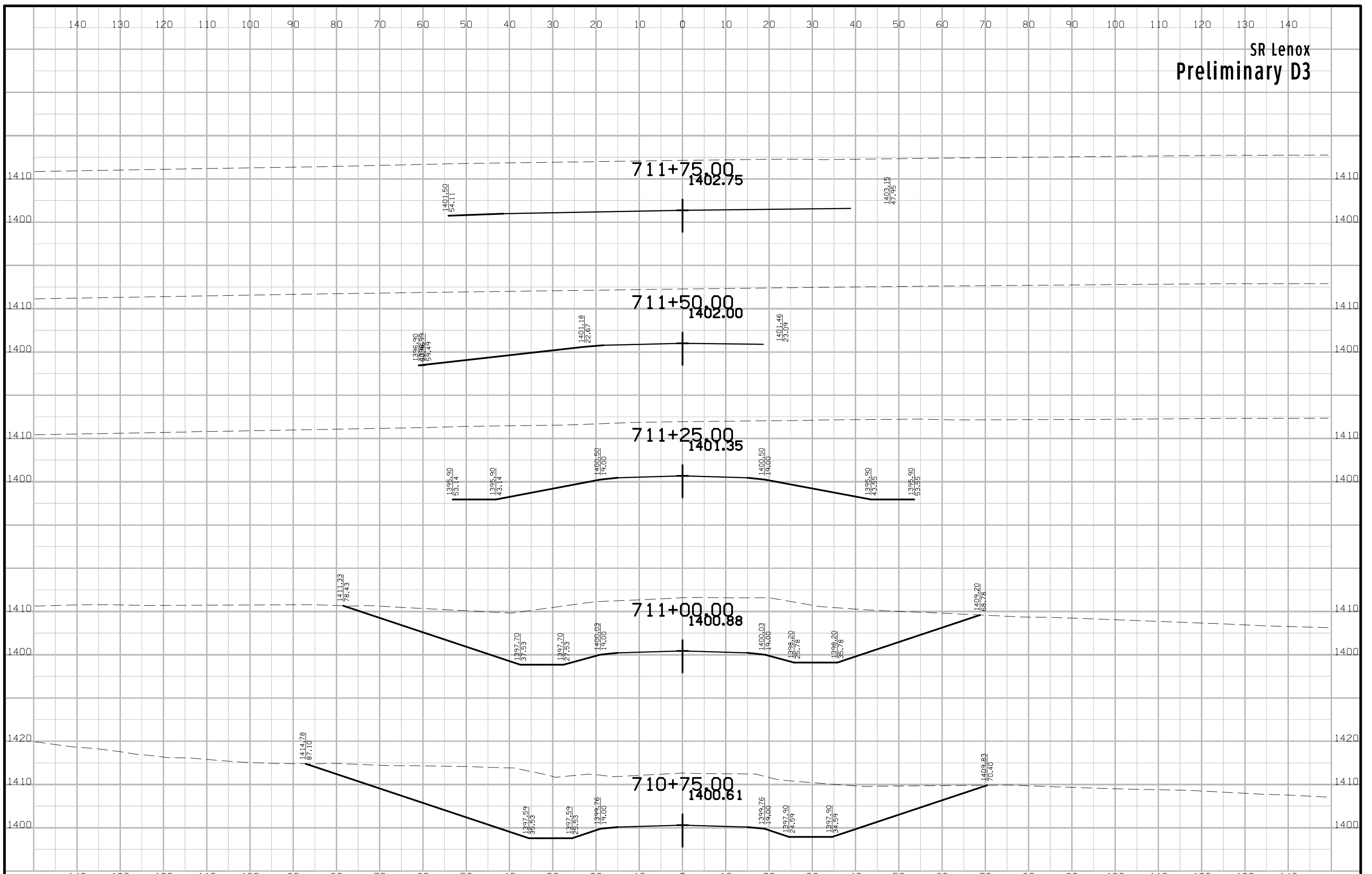
SR Lenox
Preliminary D3



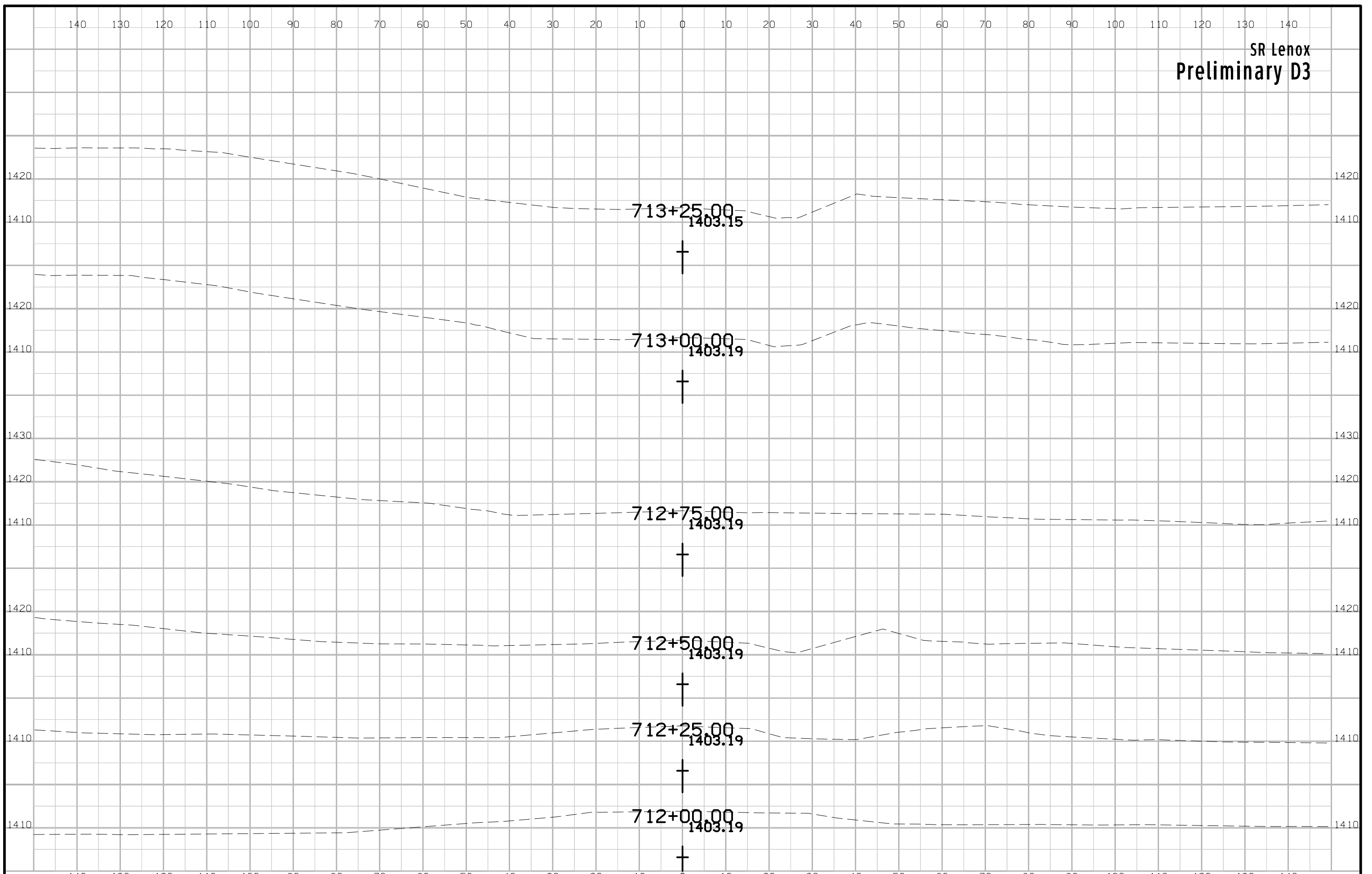
SR Lenox
Preliminary D3



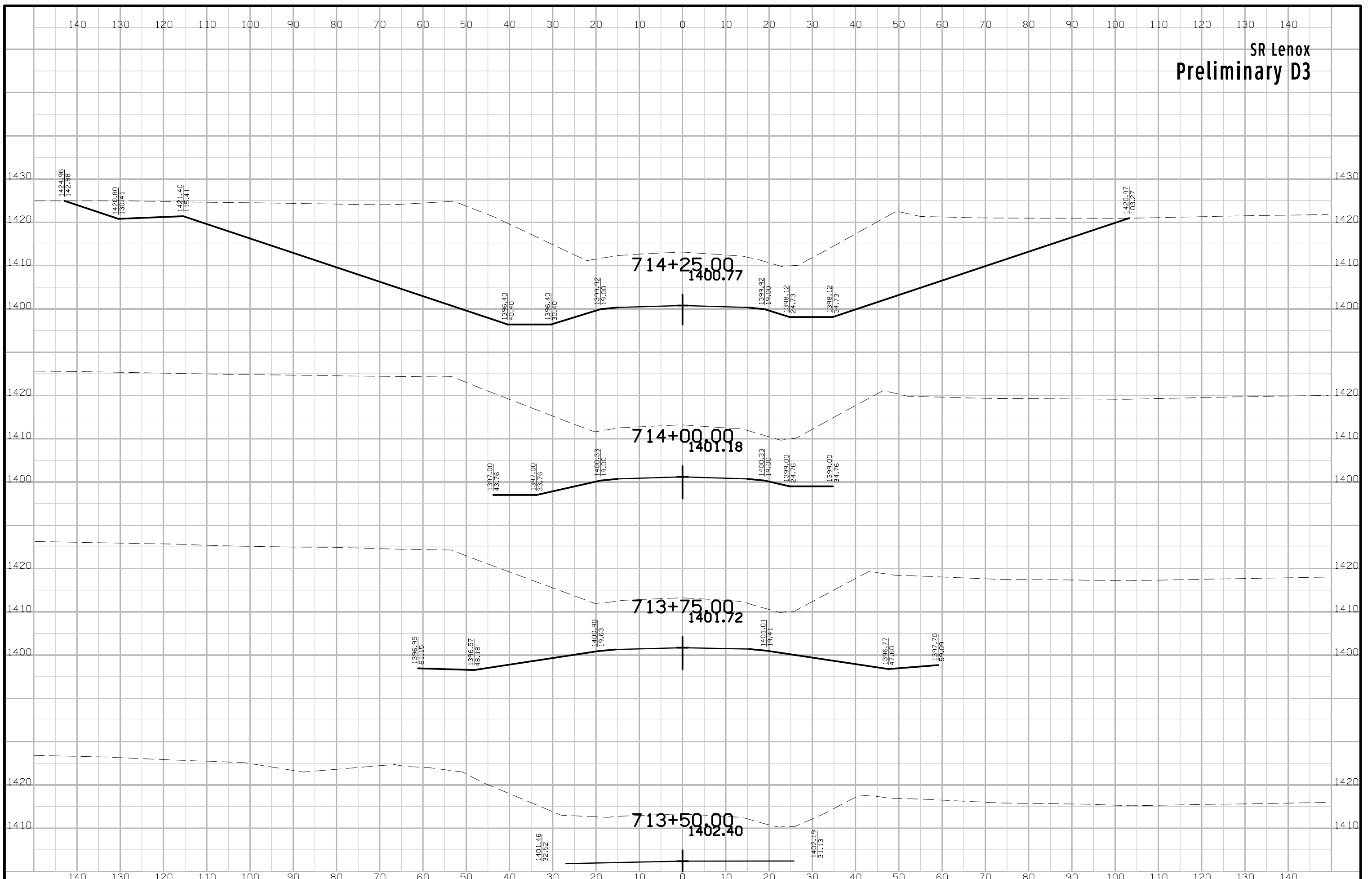
SR Lenox
Preliminary D3



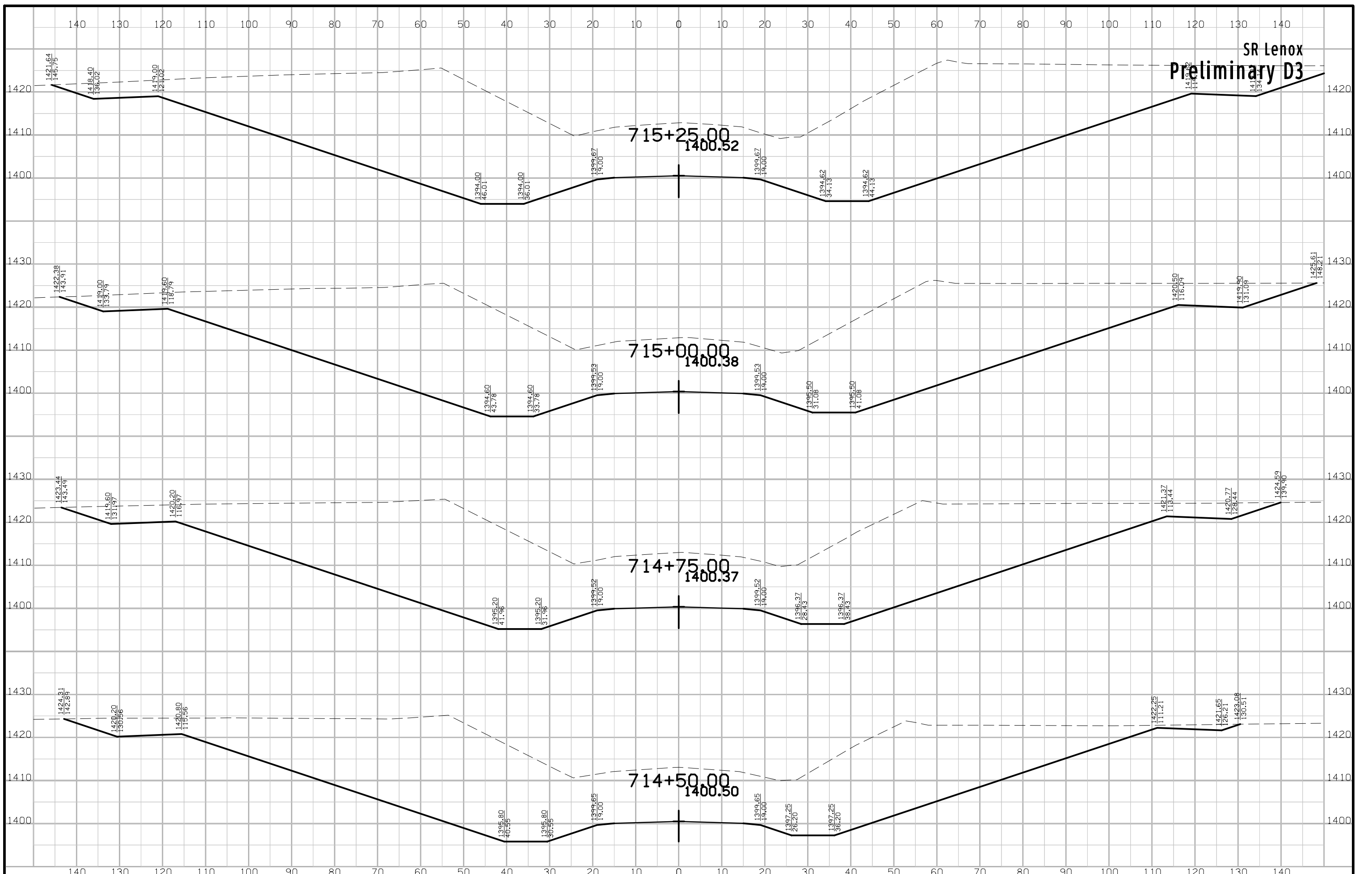
SR Lenox
Preliminary D3



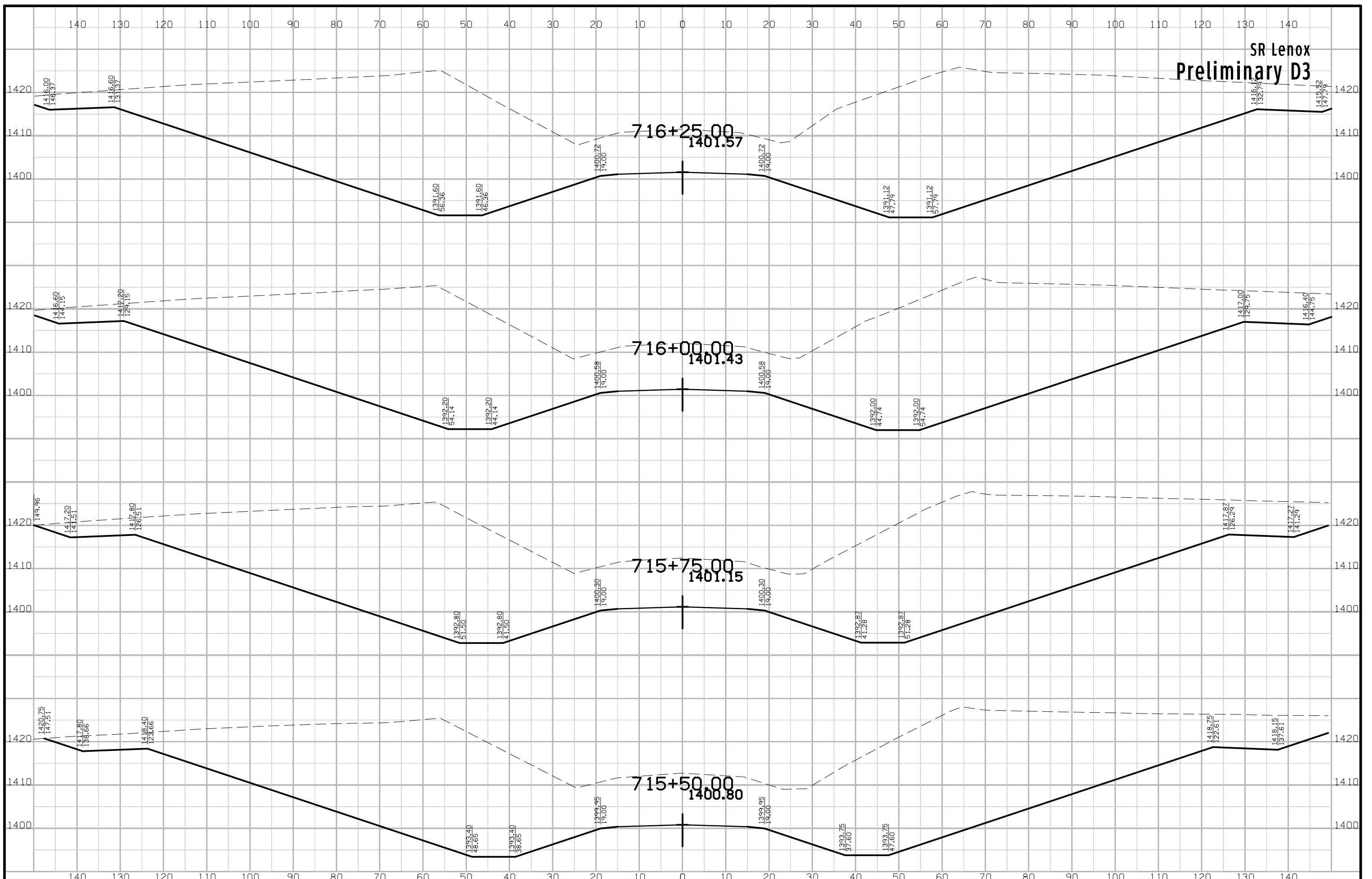
SR Lenox
Preliminary D3



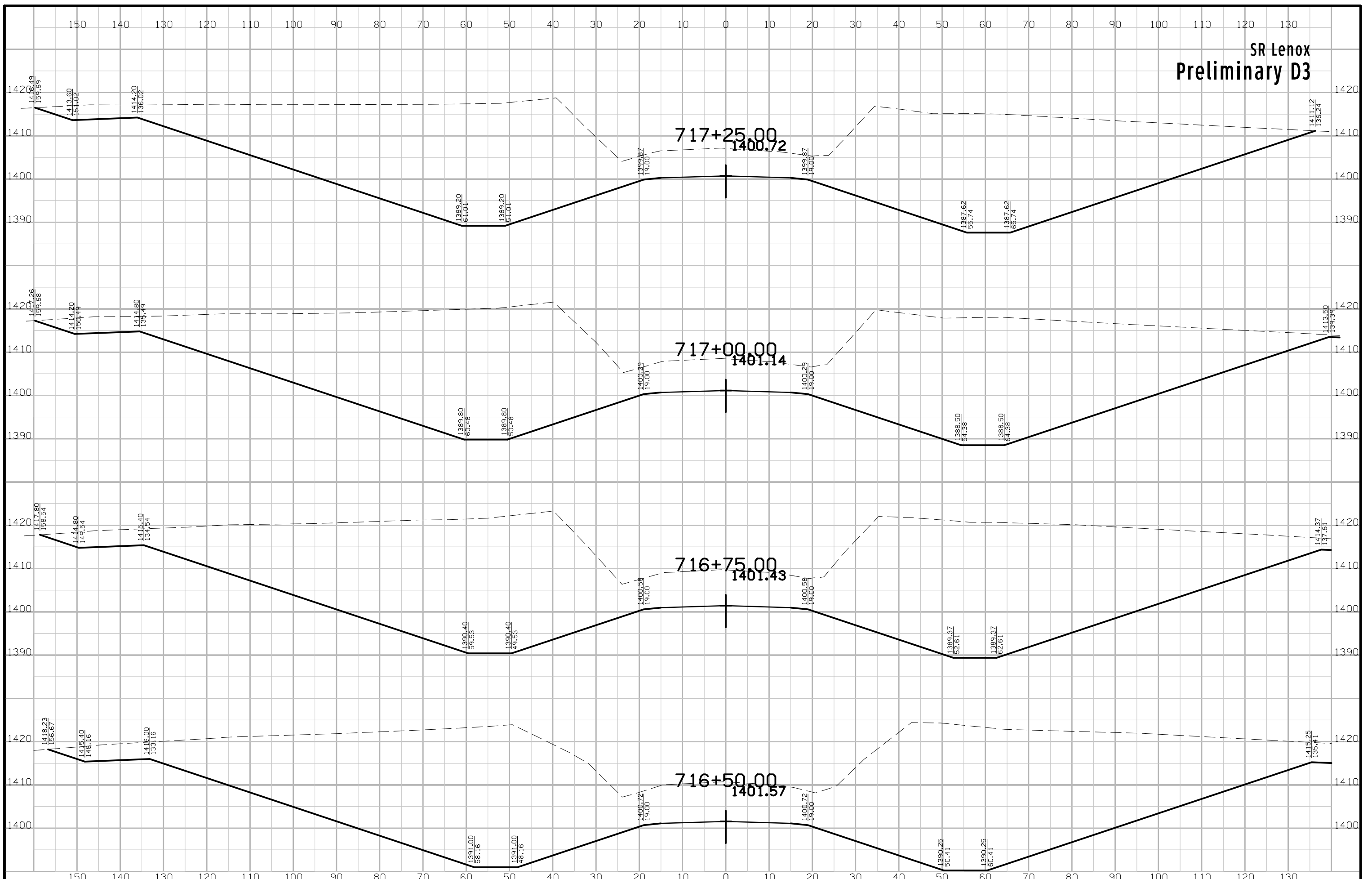
SR Lenox
Preliminary D3



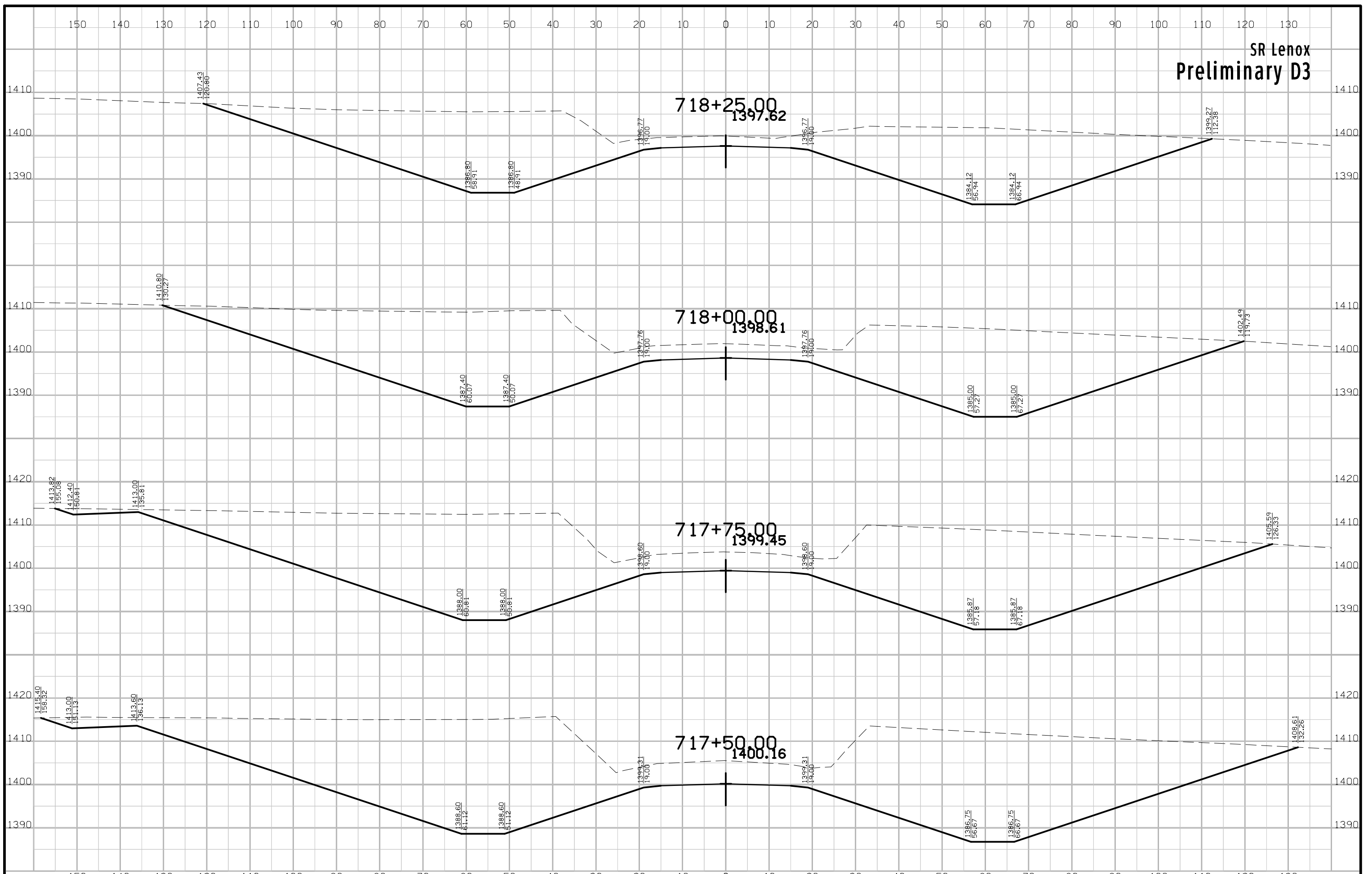
SR Lenox
Preliminary D3



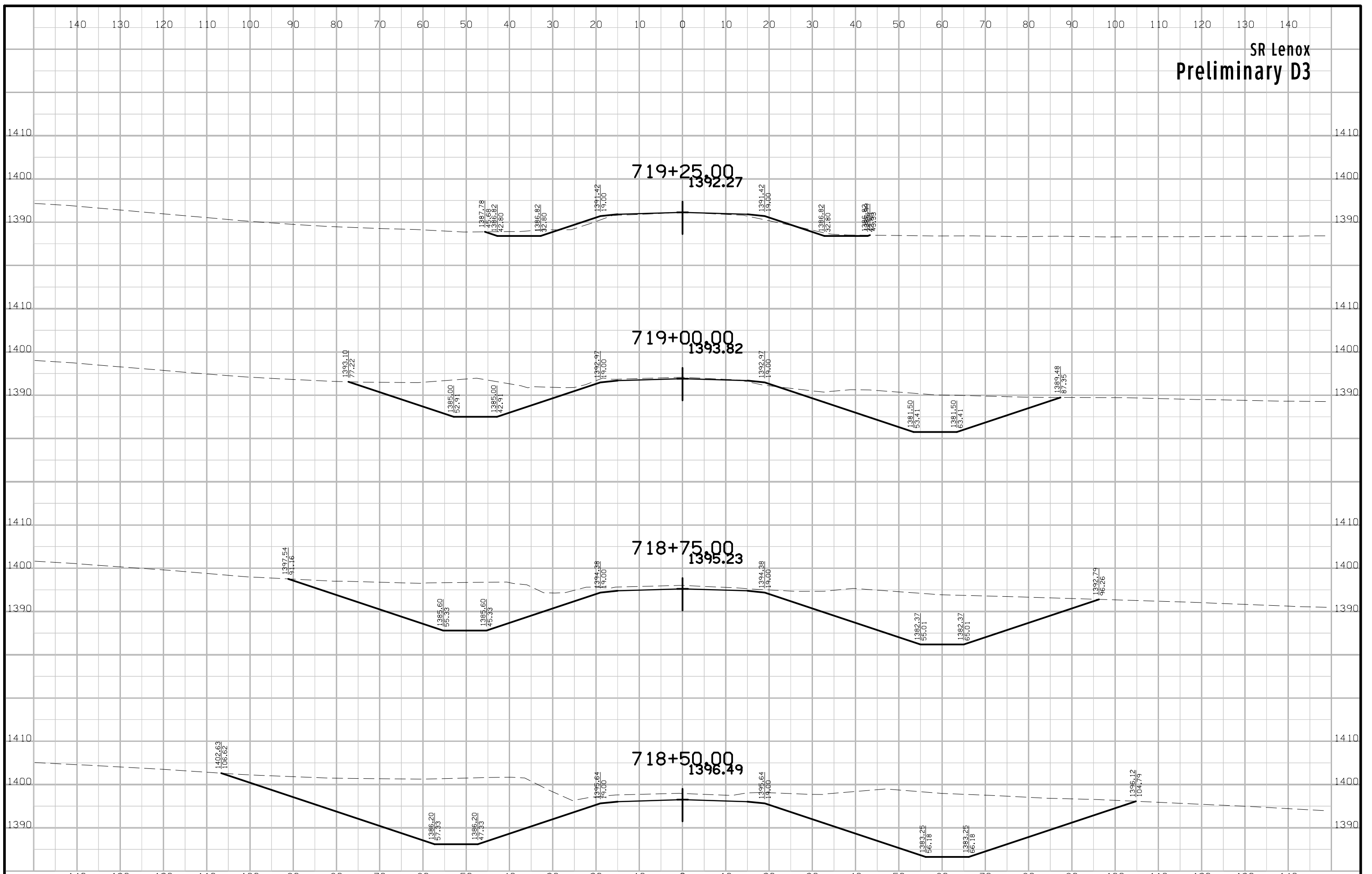
SR Lenox
Preliminary D3



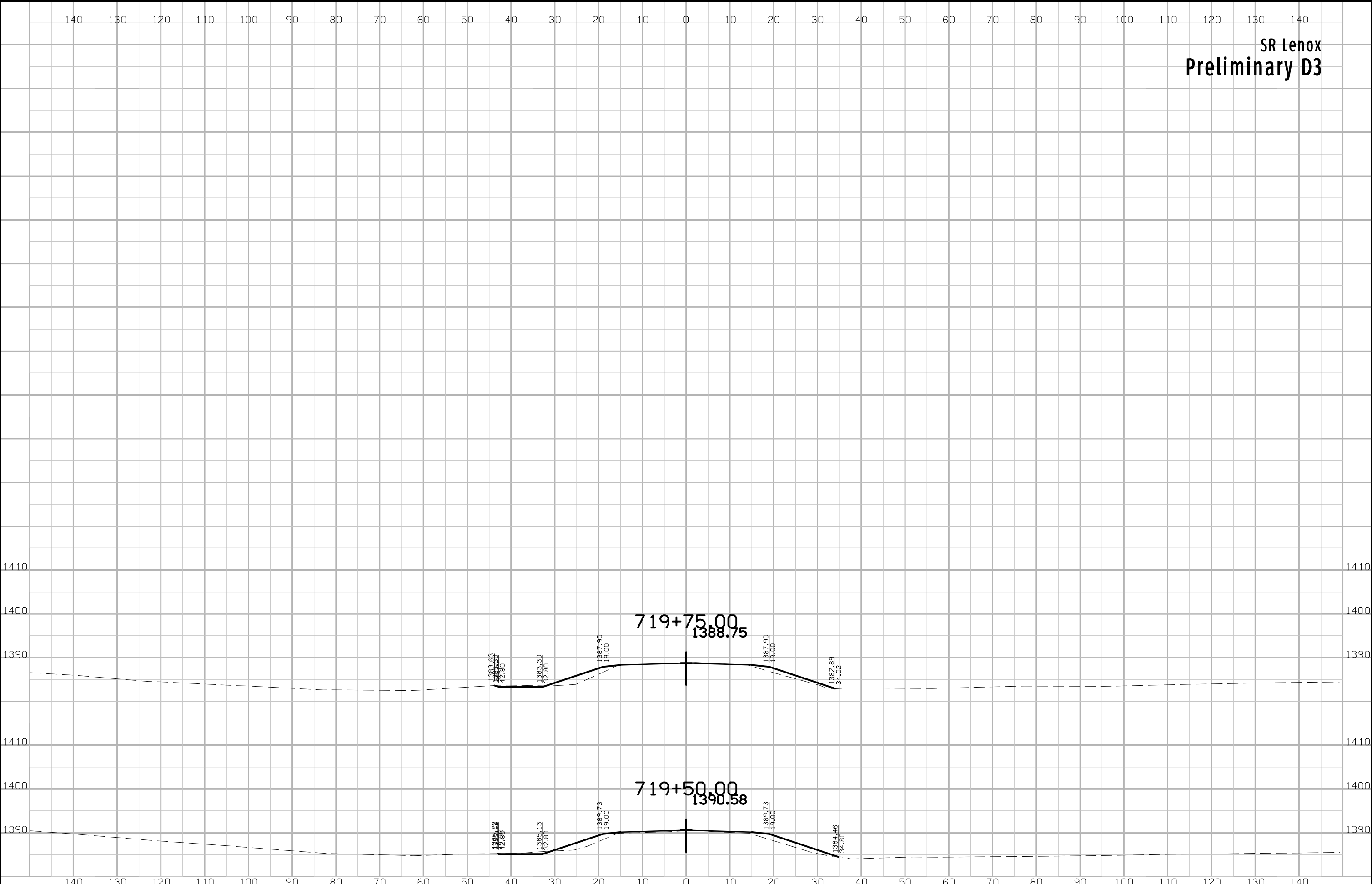
SR Lenox
Preliminary D3



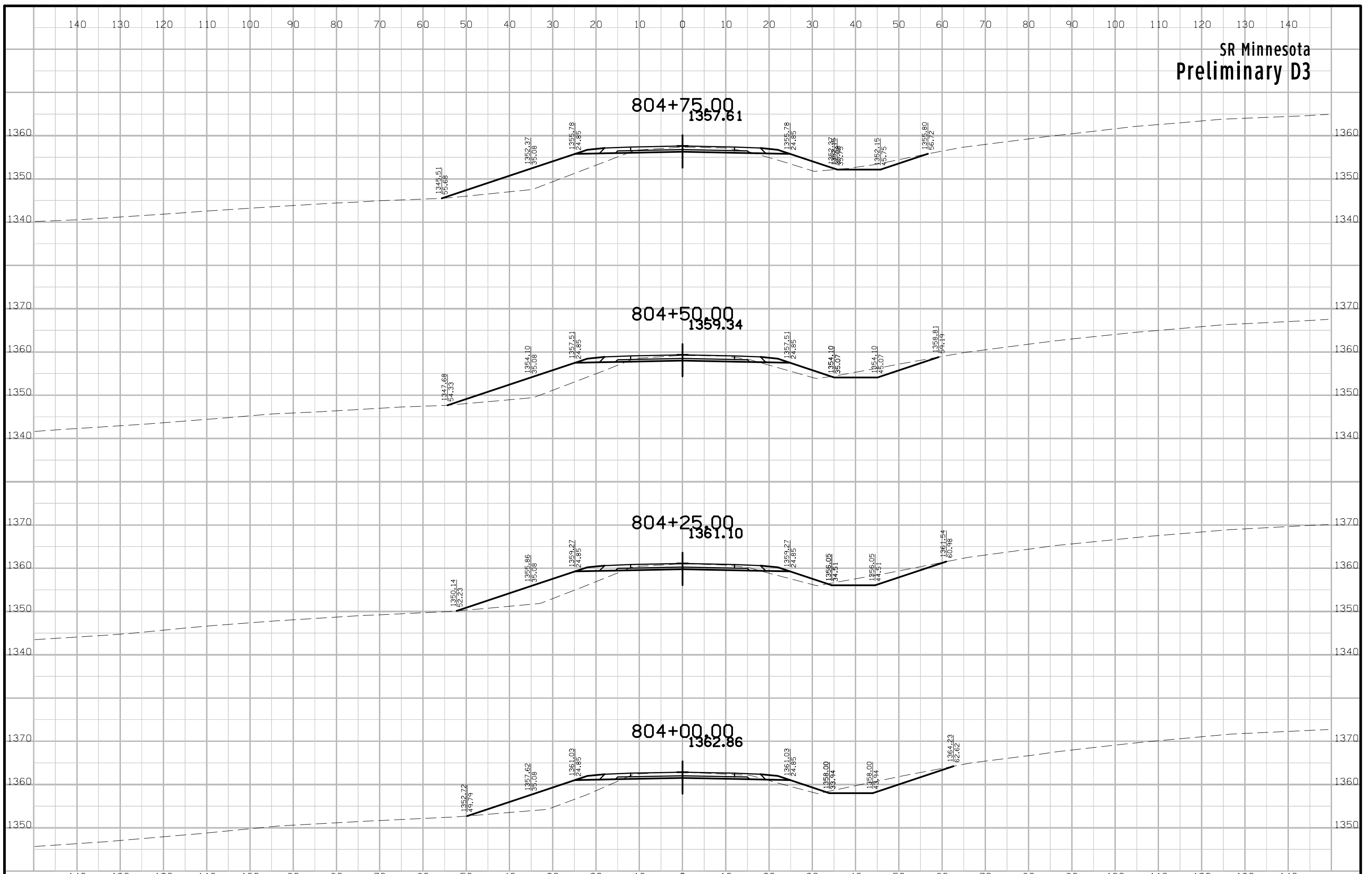
SR Lenox
Preliminary D3



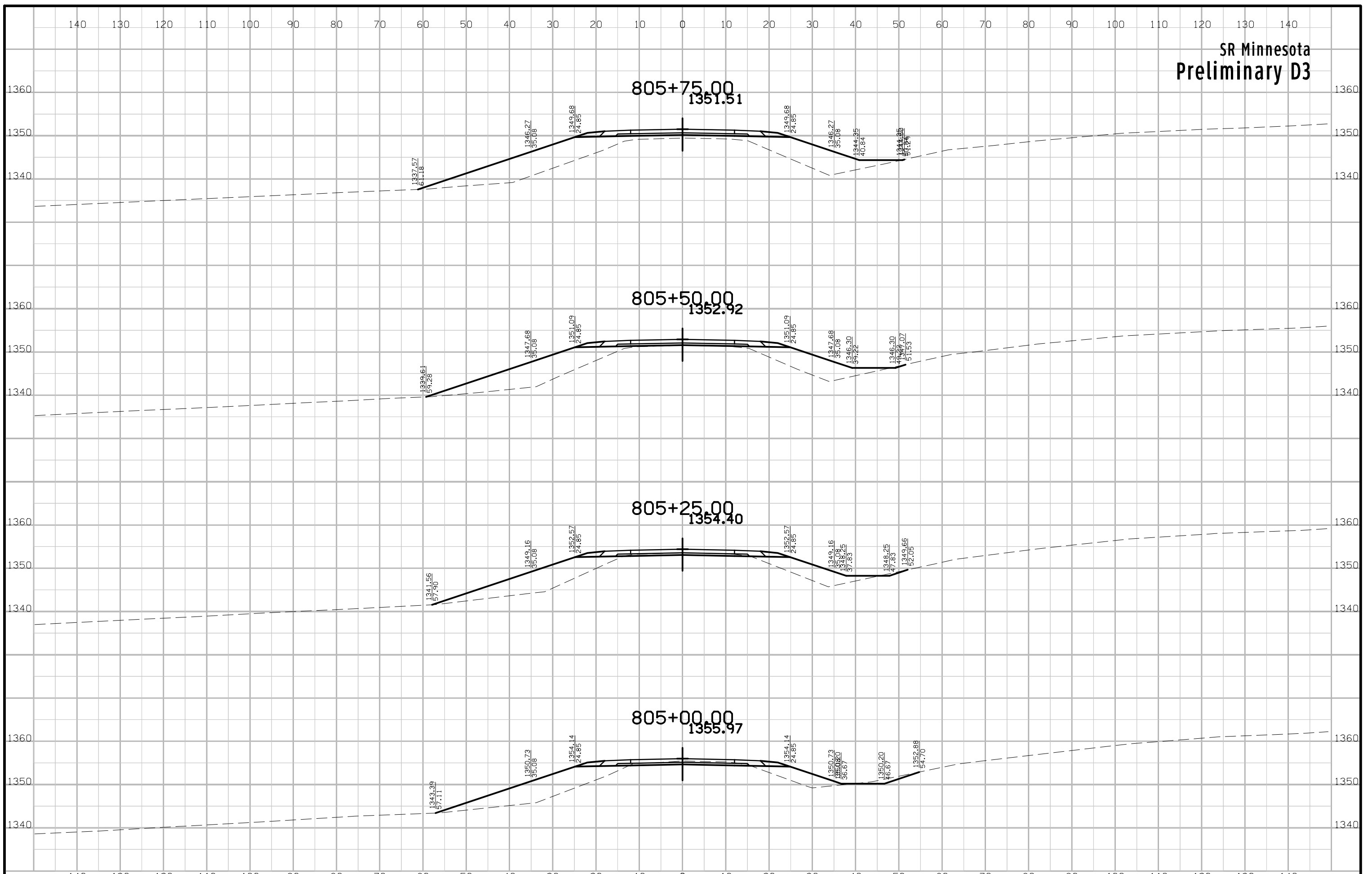
SR Lenox
Preliminary D3



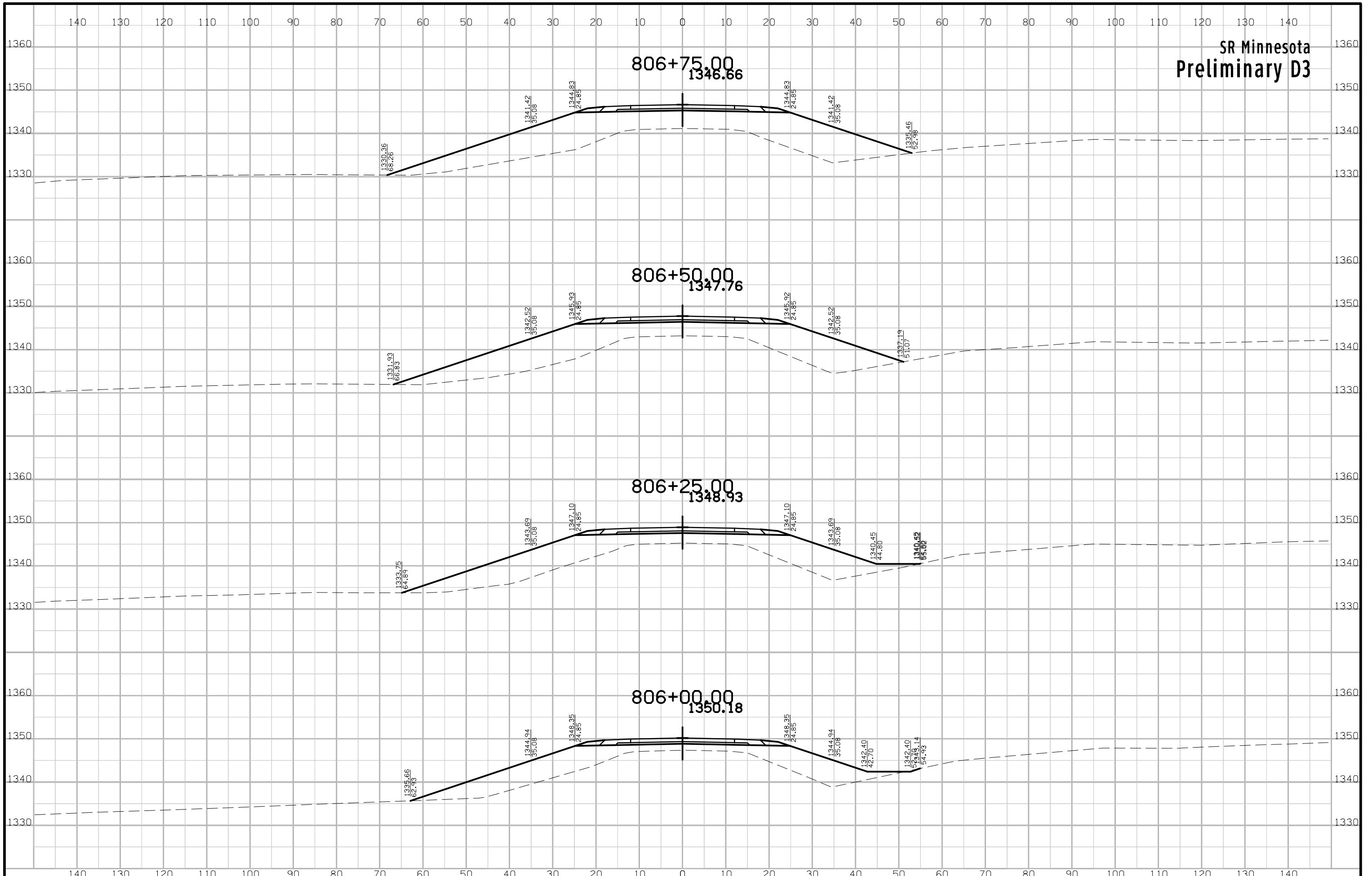
SR Minnesota
Preliminary D3



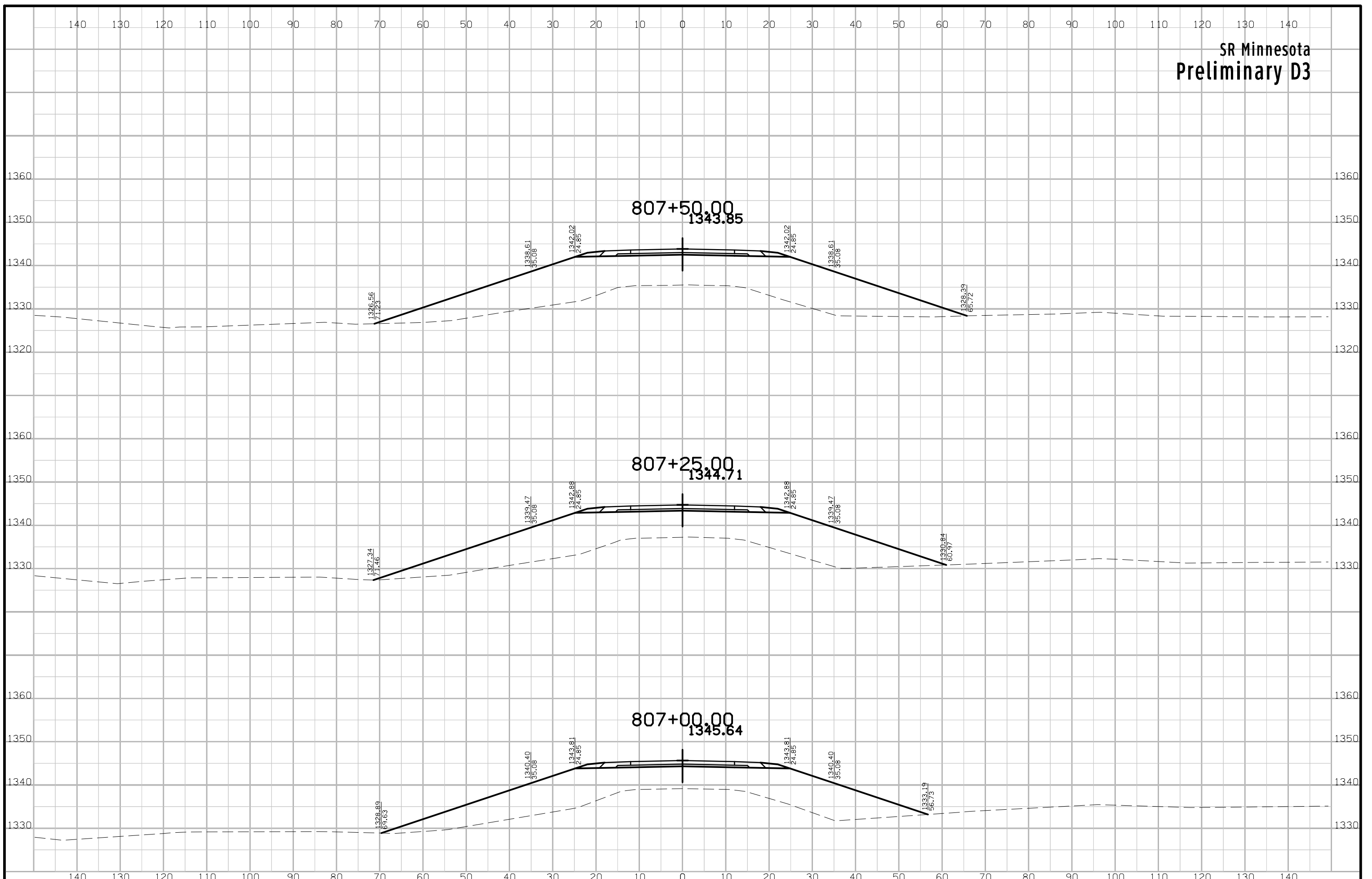
SR Minnesota
Preliminary D3



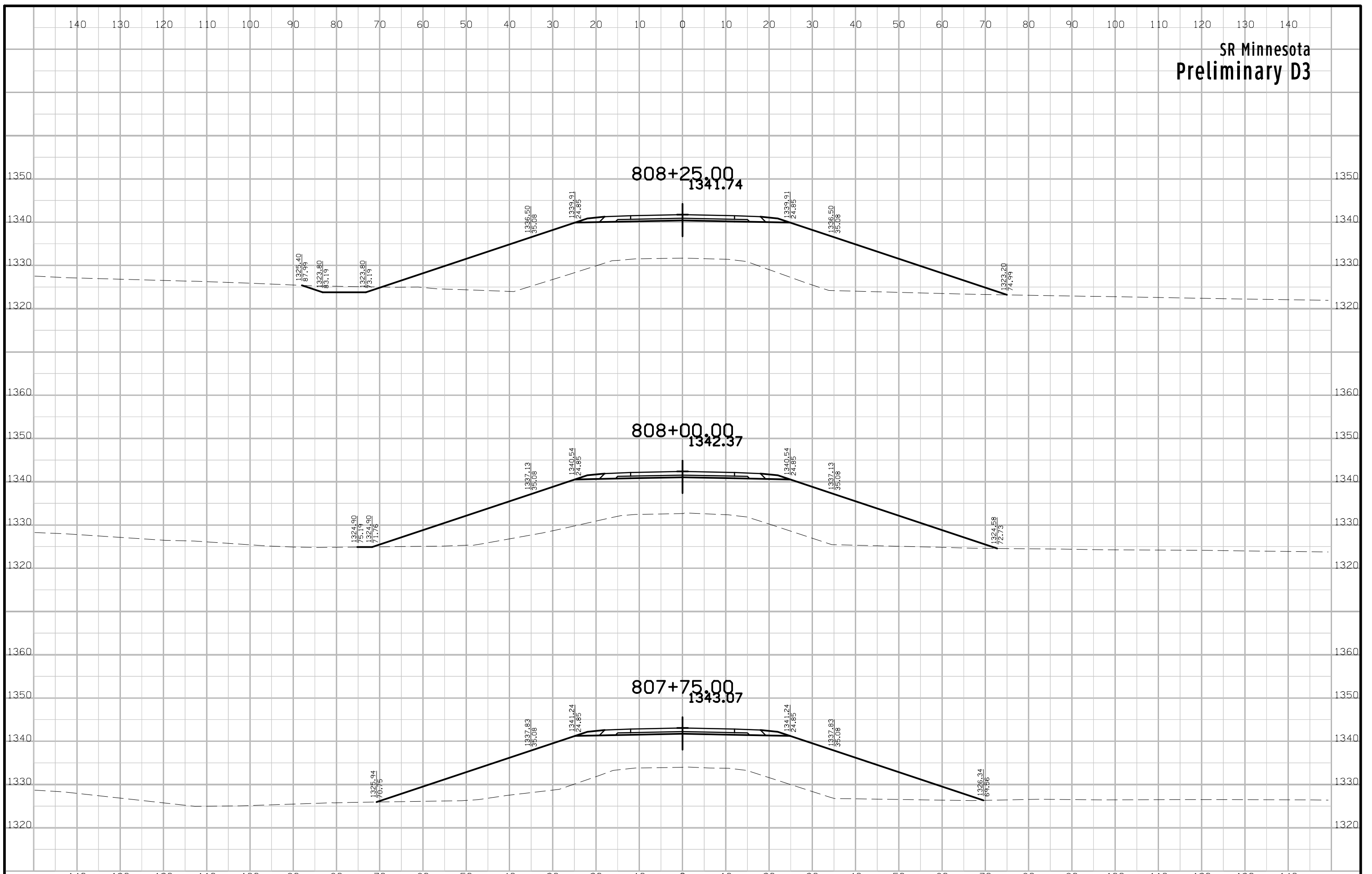
SR Minnesota
Preliminary D3



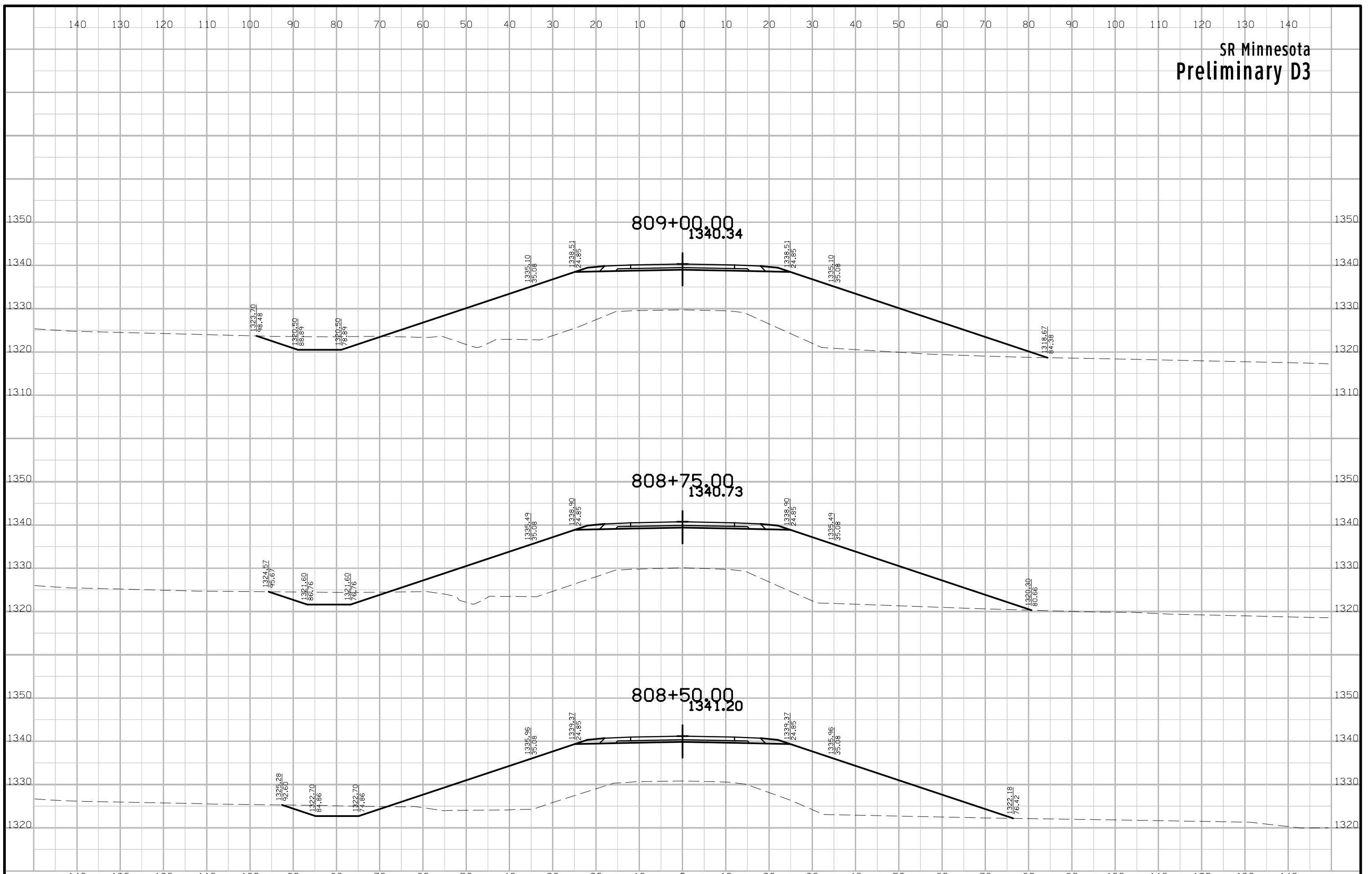
SR Minnesota
Preliminary D3



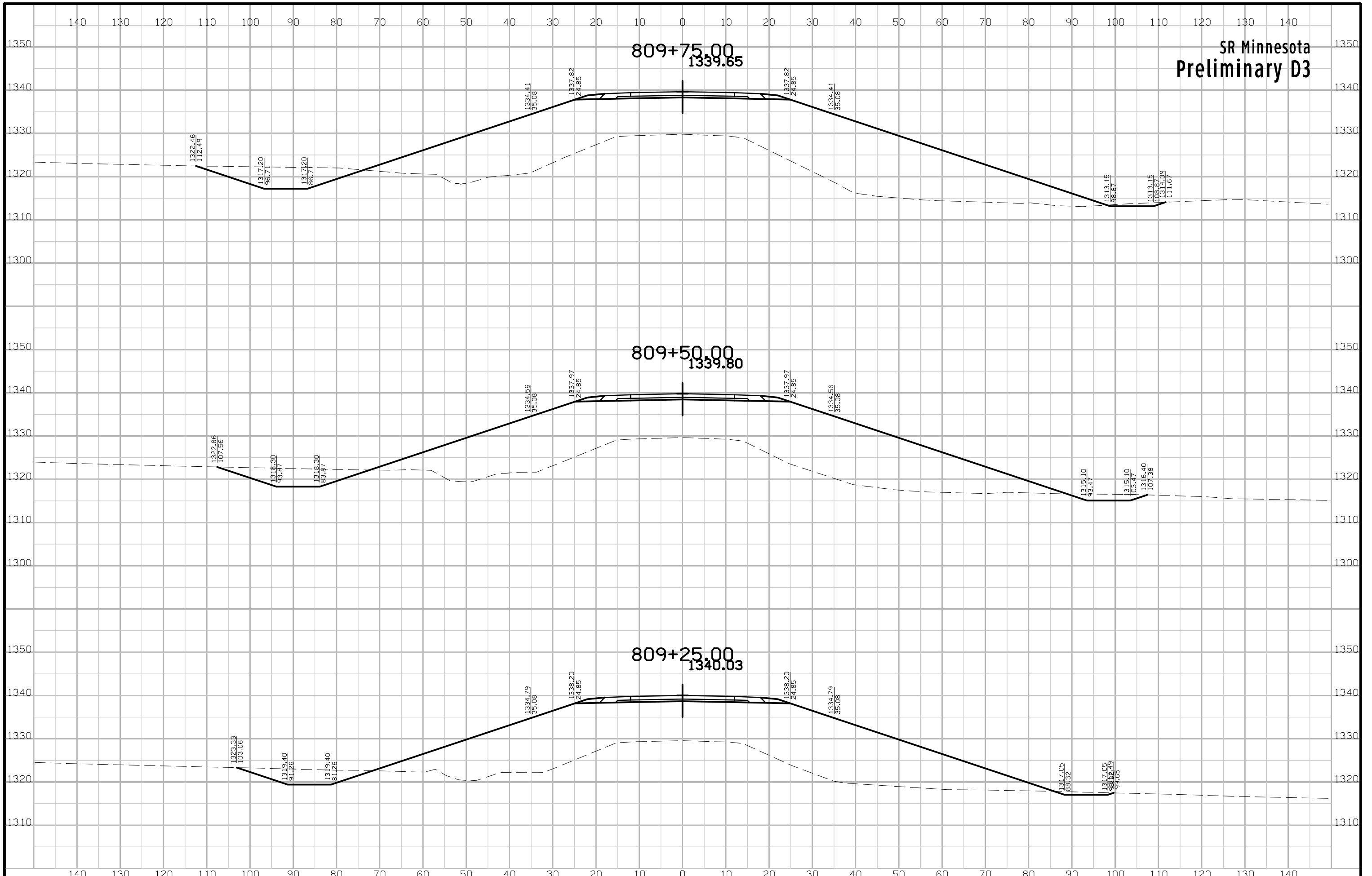
SR Minnesota
Preliminary D3



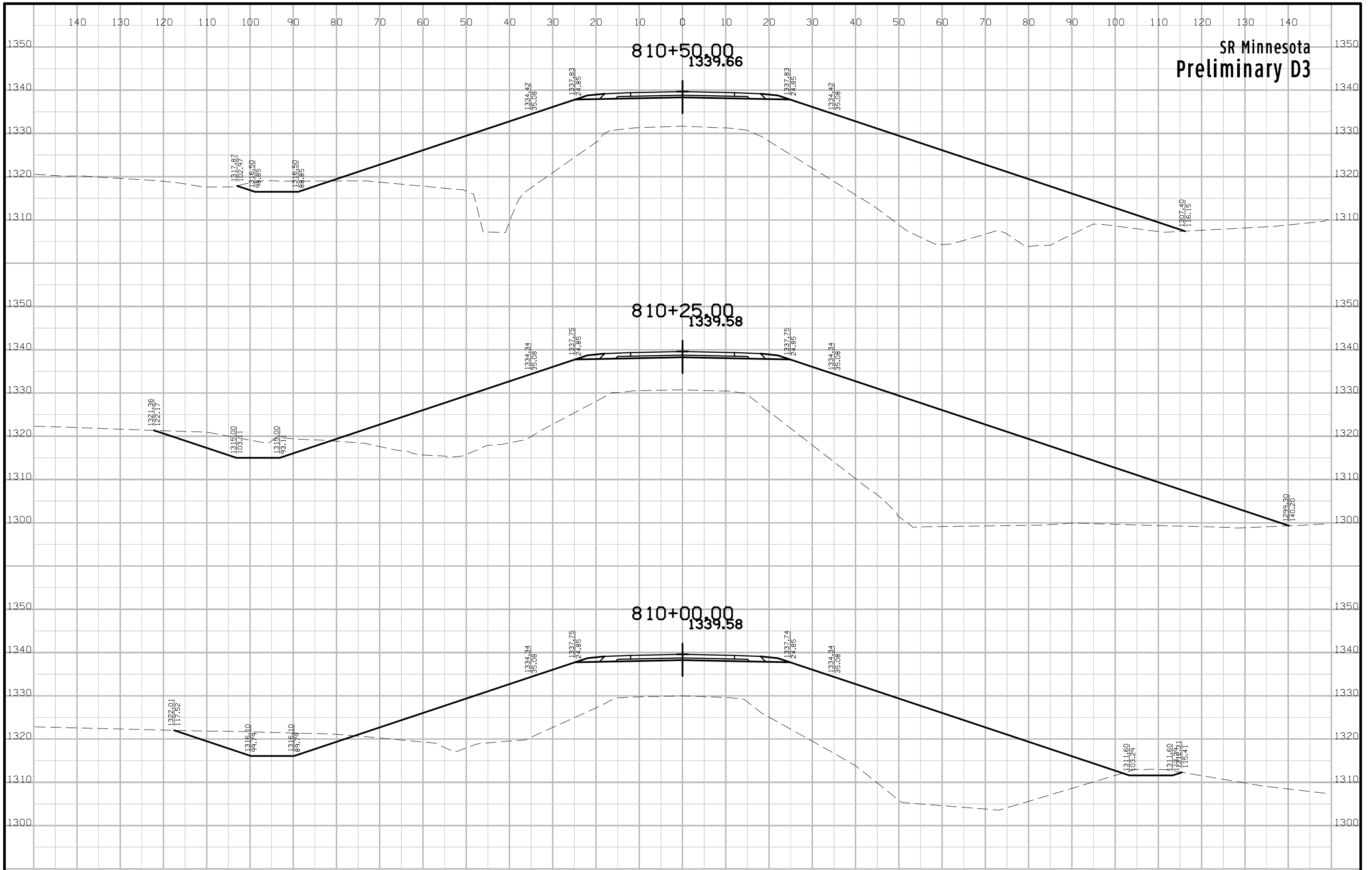
SR Minnesota
Preliminary D3



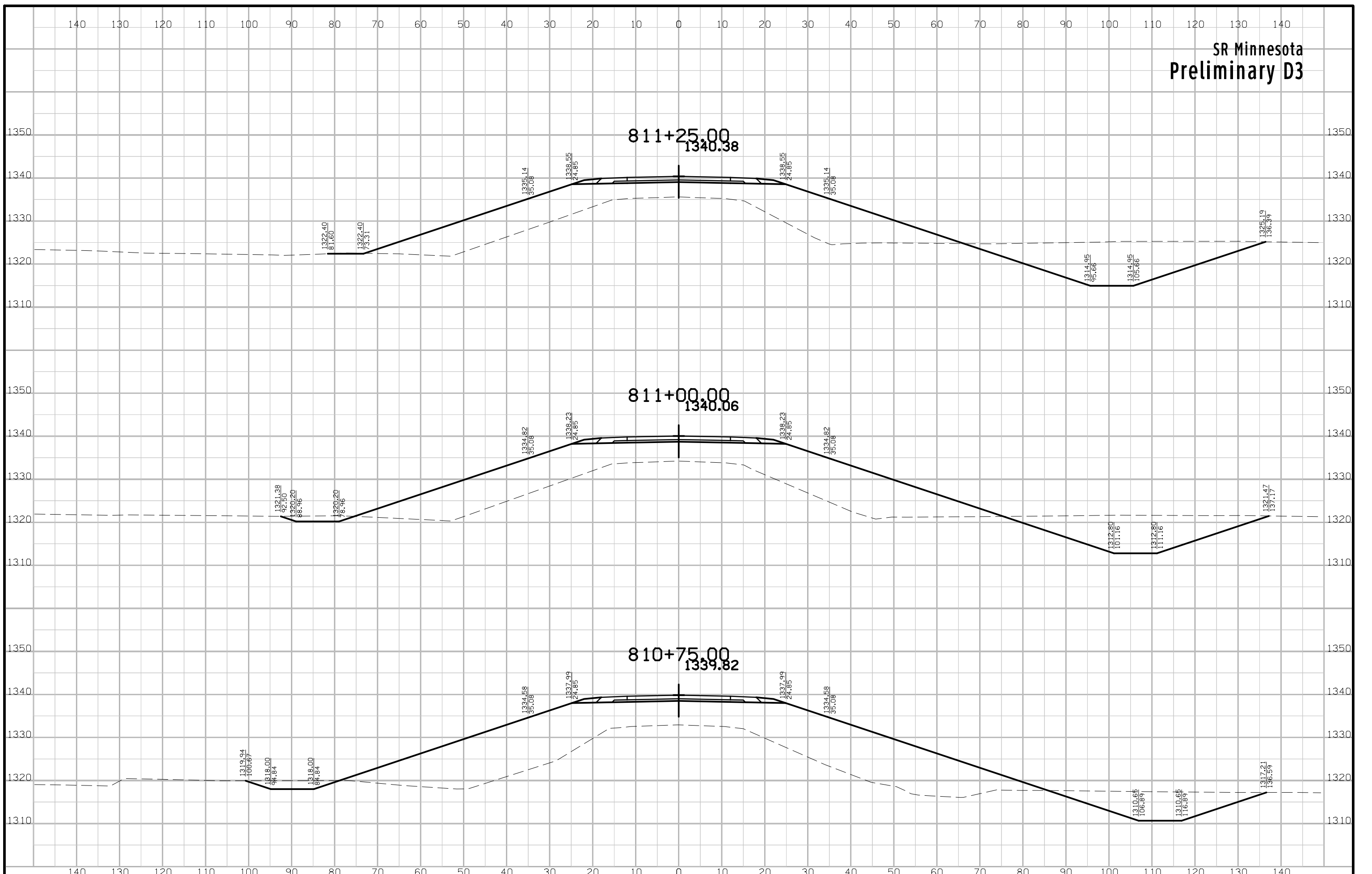
SR Minnesota
Preliminary D3



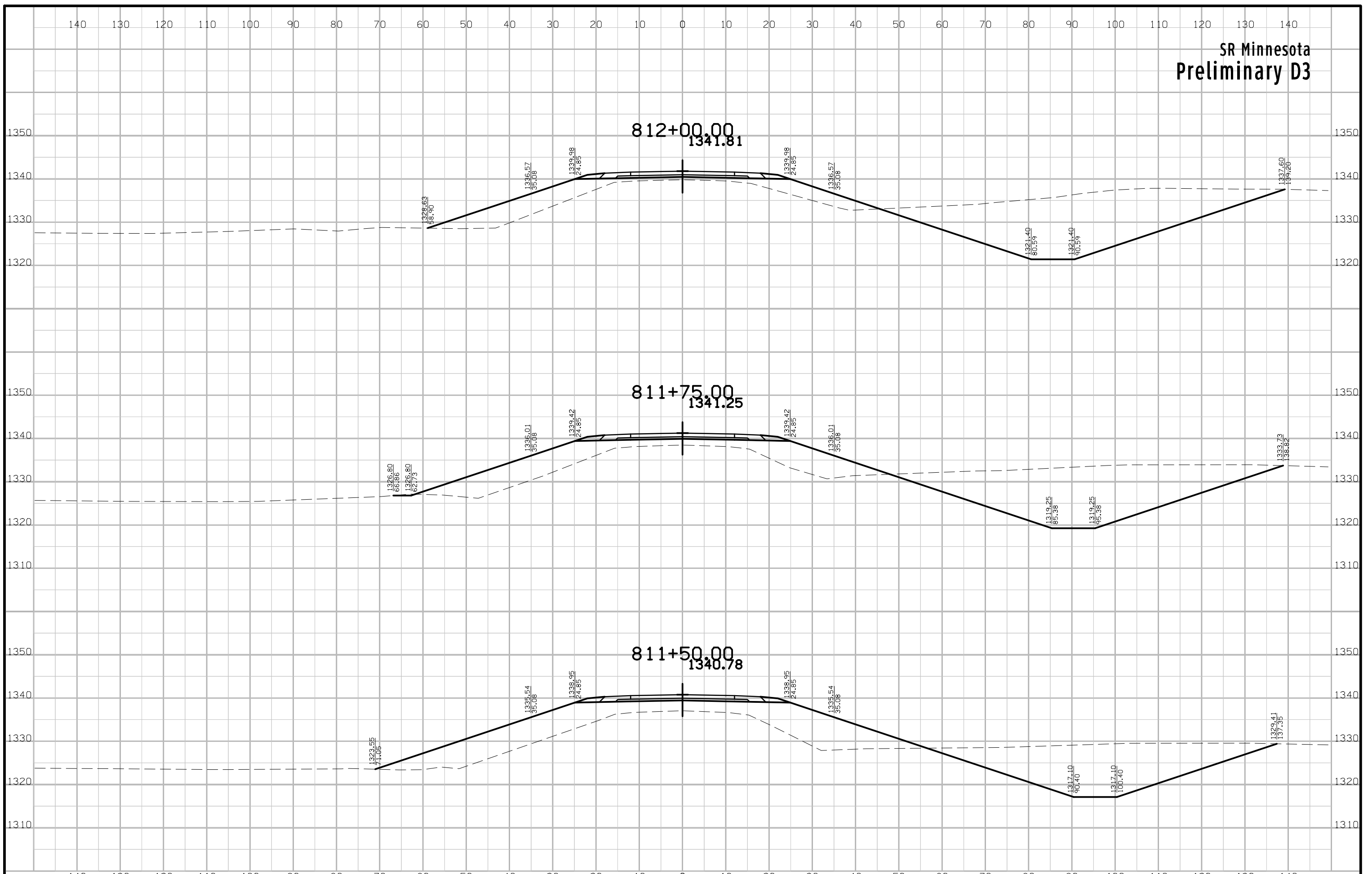
SR Minnesota
Preliminary D3

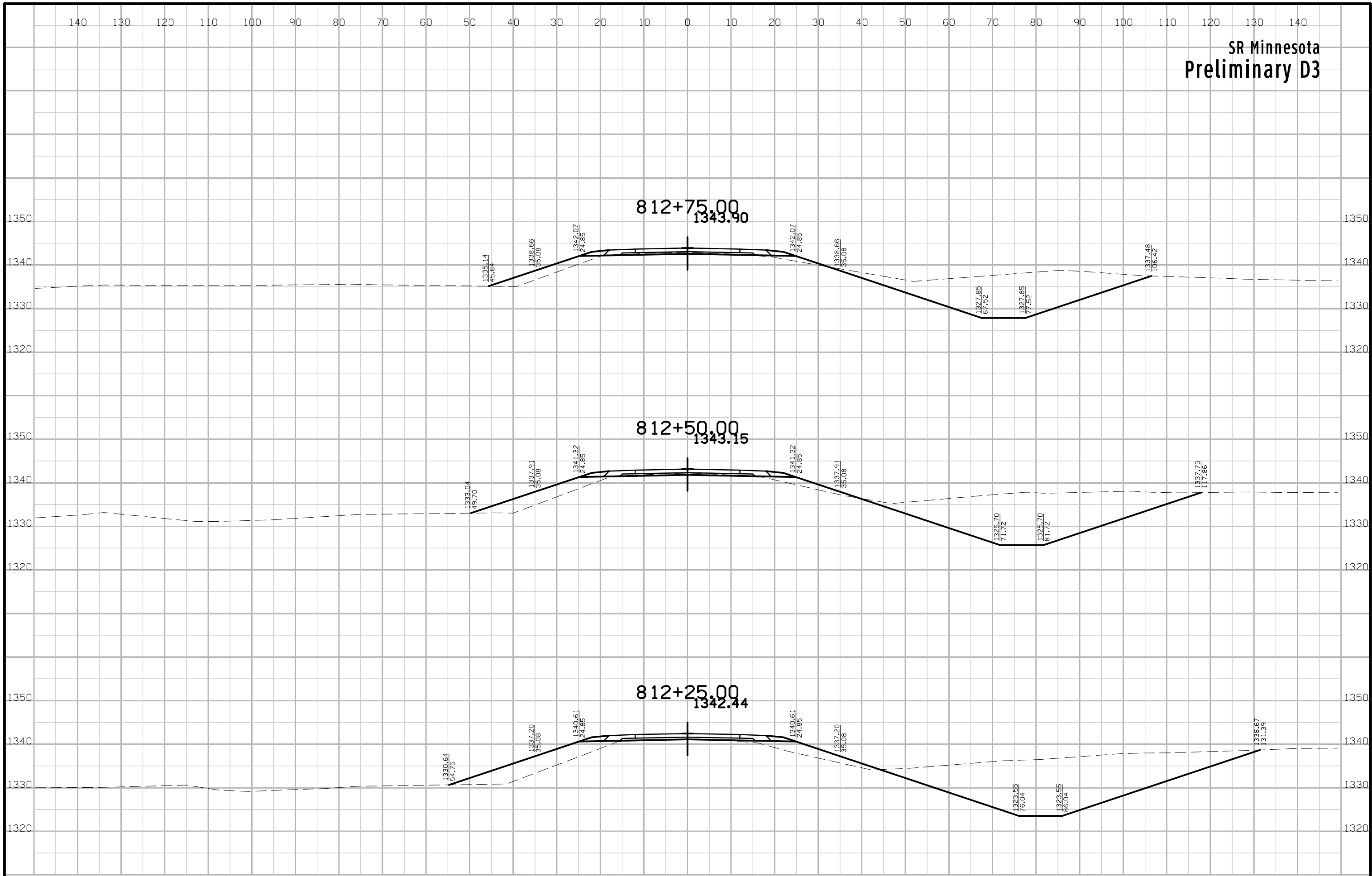


SR Minnesota
Preliminary D3

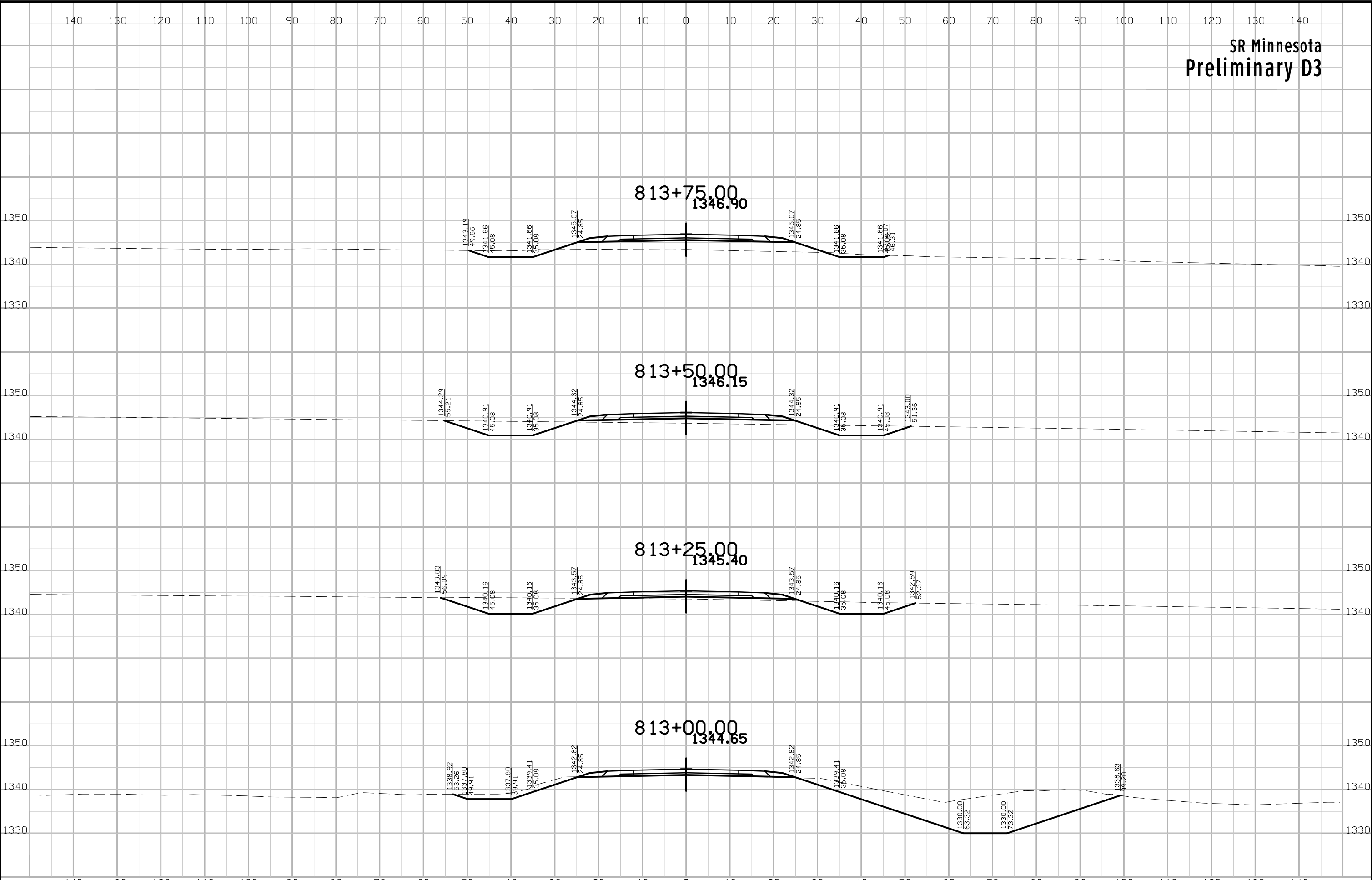


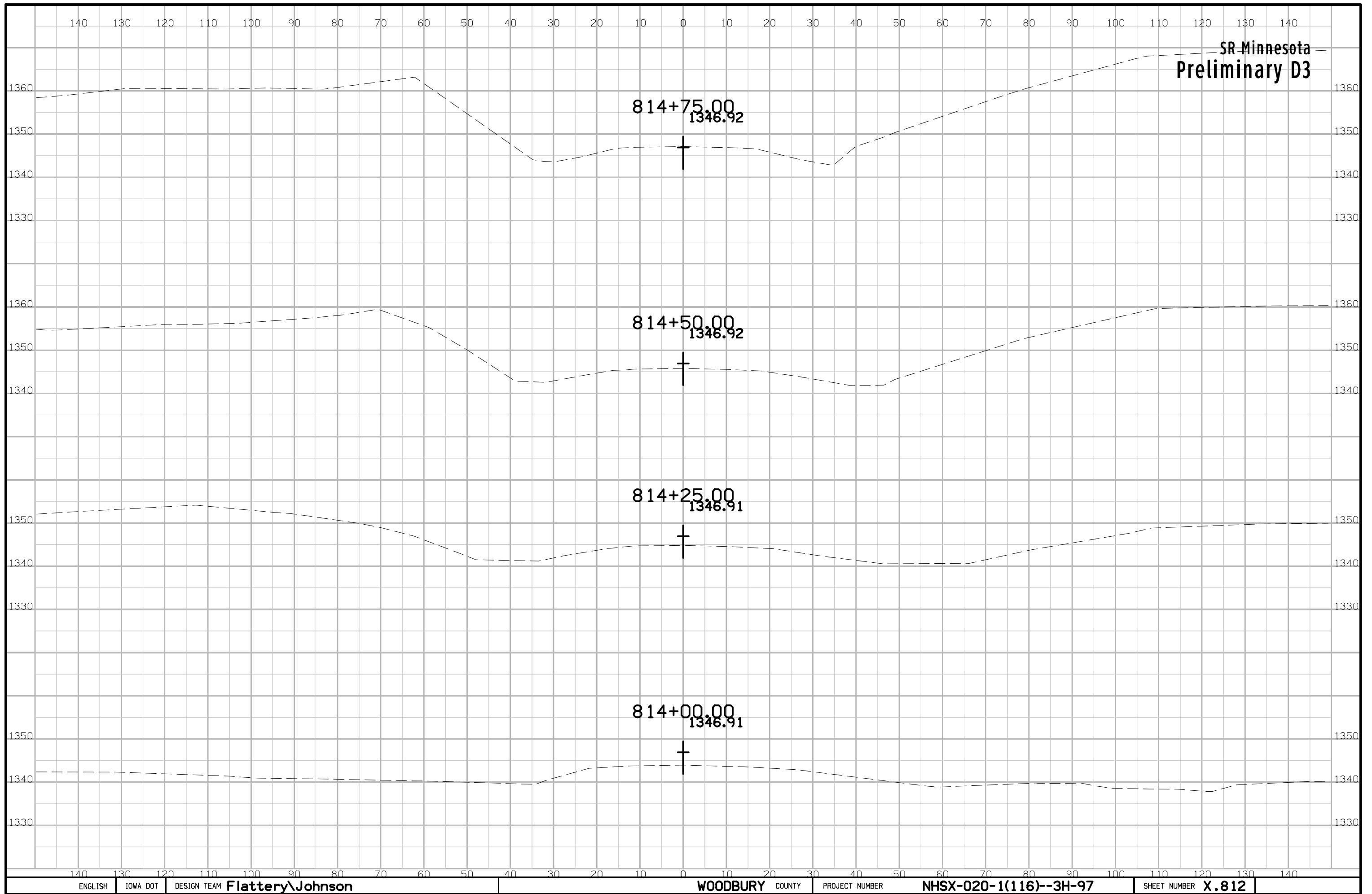
SR Minnesota
Preliminary D3



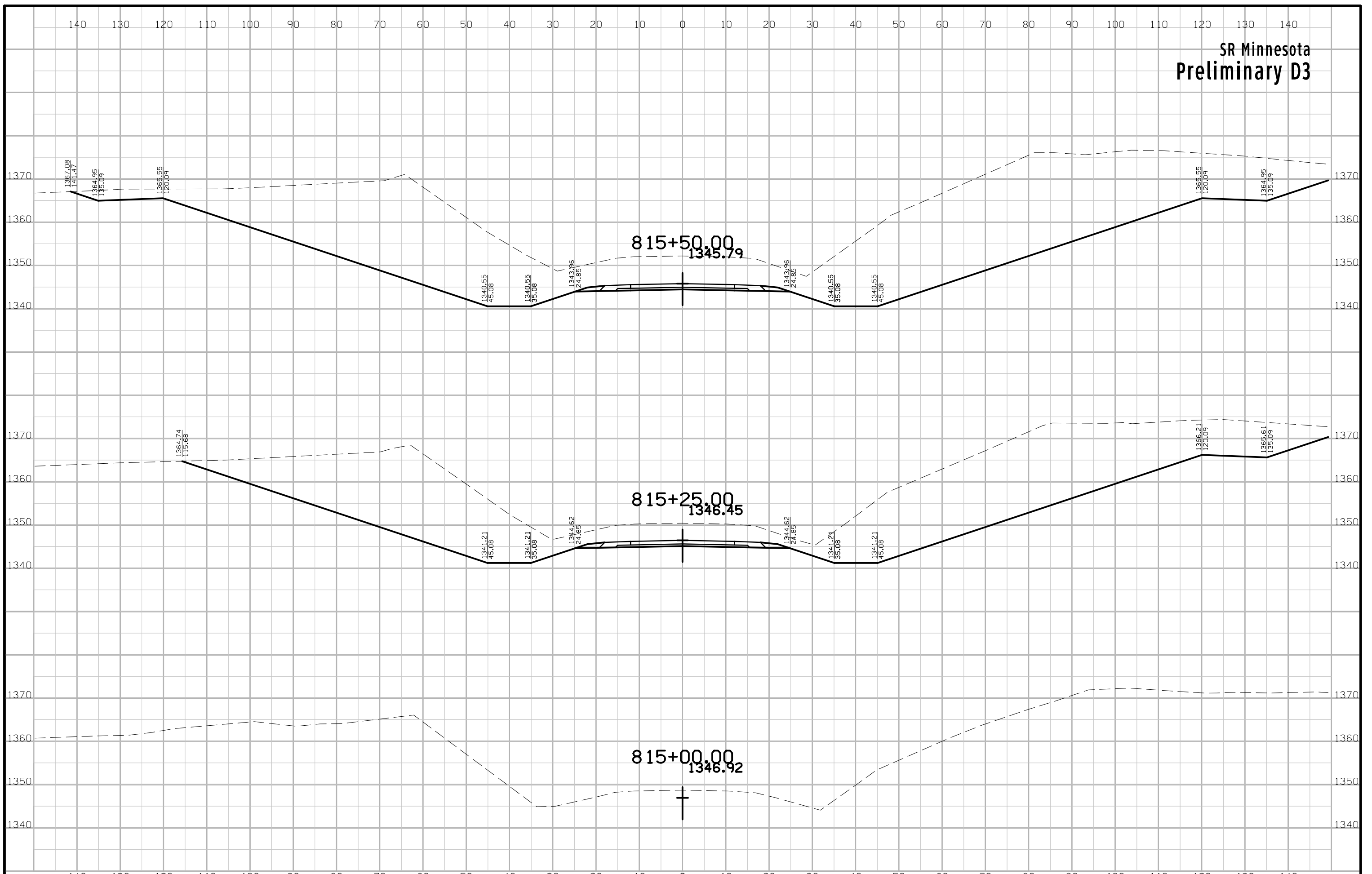


SR Minnesota
Preliminary D3

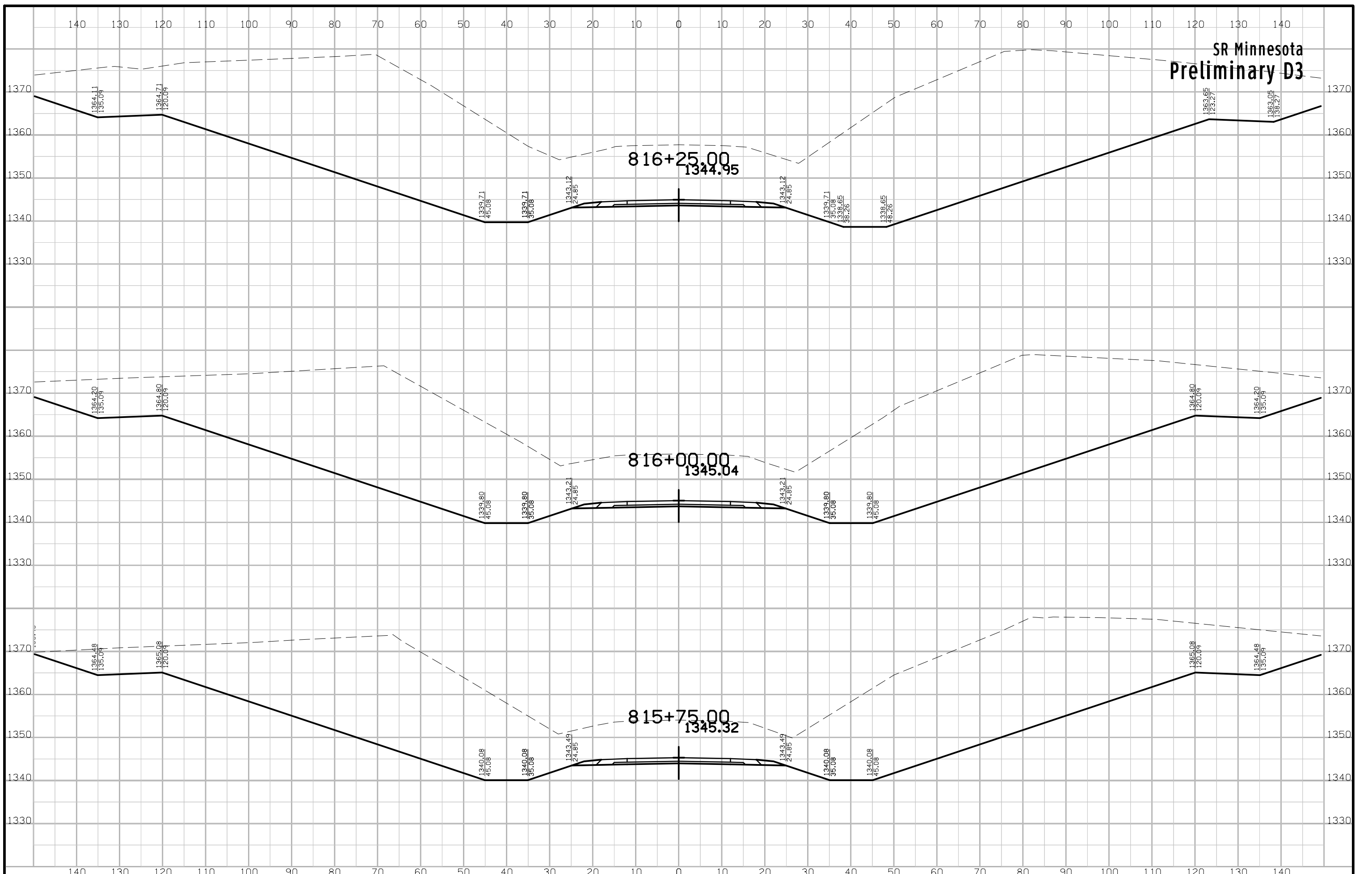




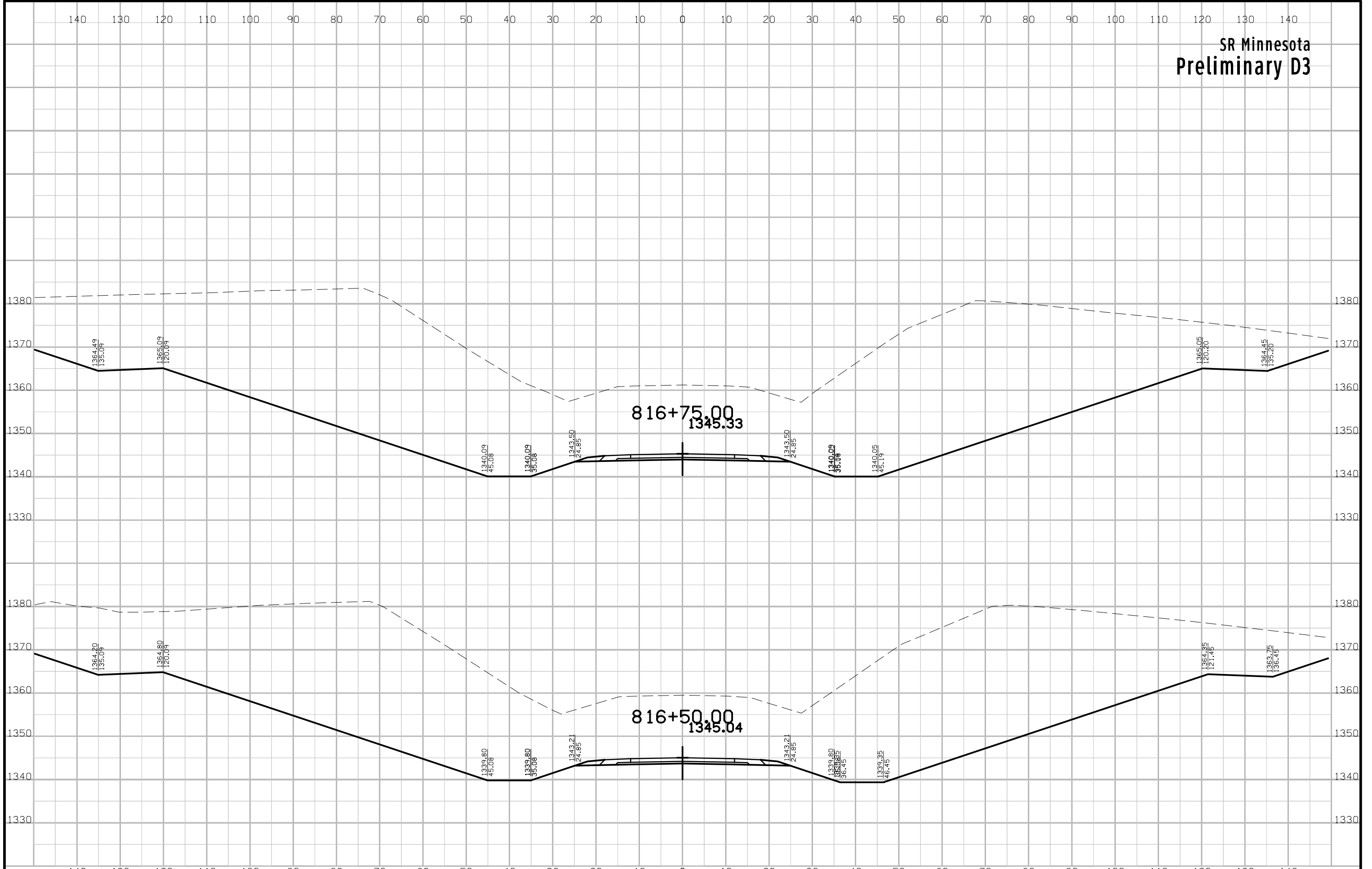
SR Minnesota
Preliminary D3



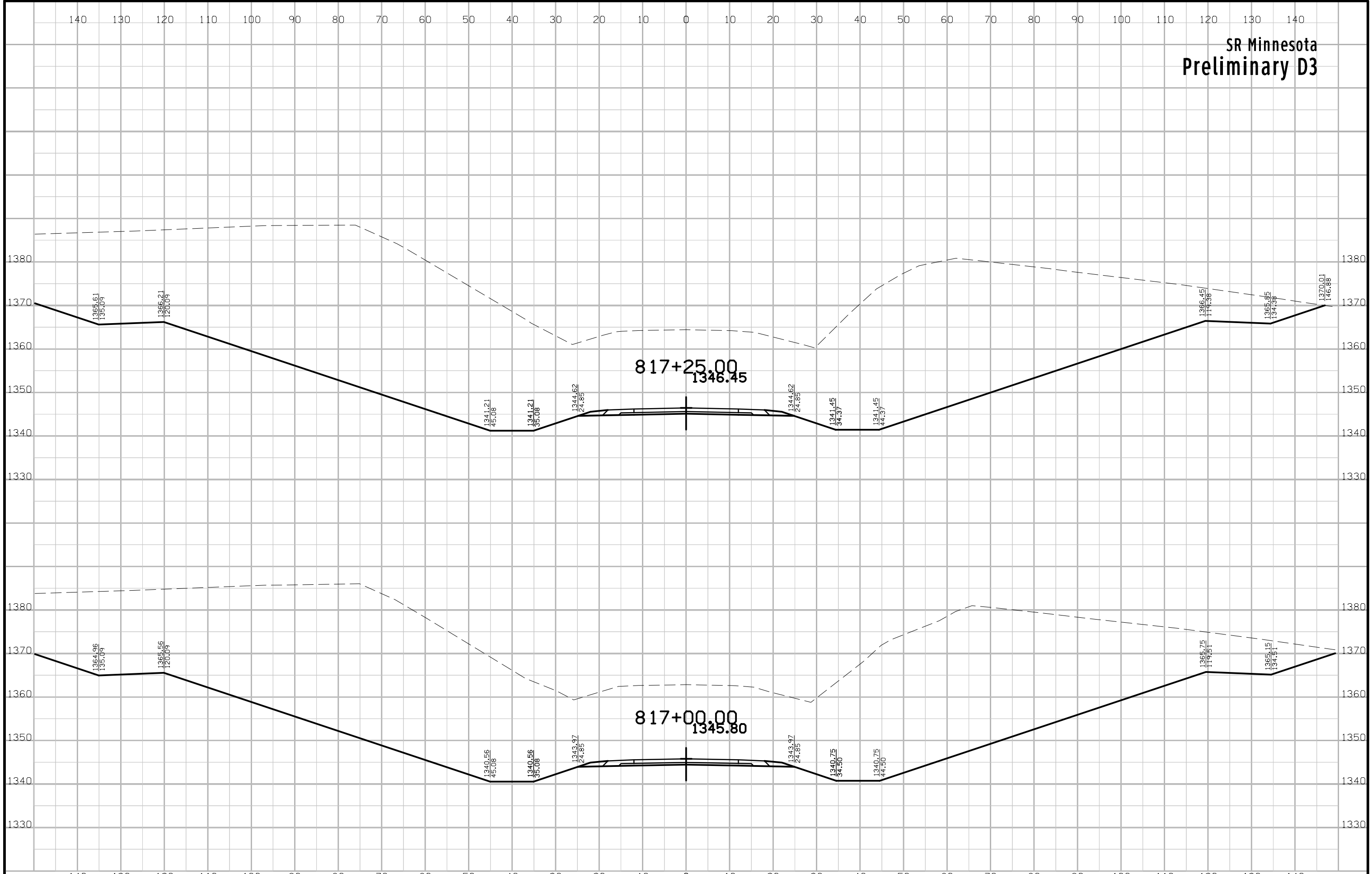
SR Minnesota
Preliminary D3



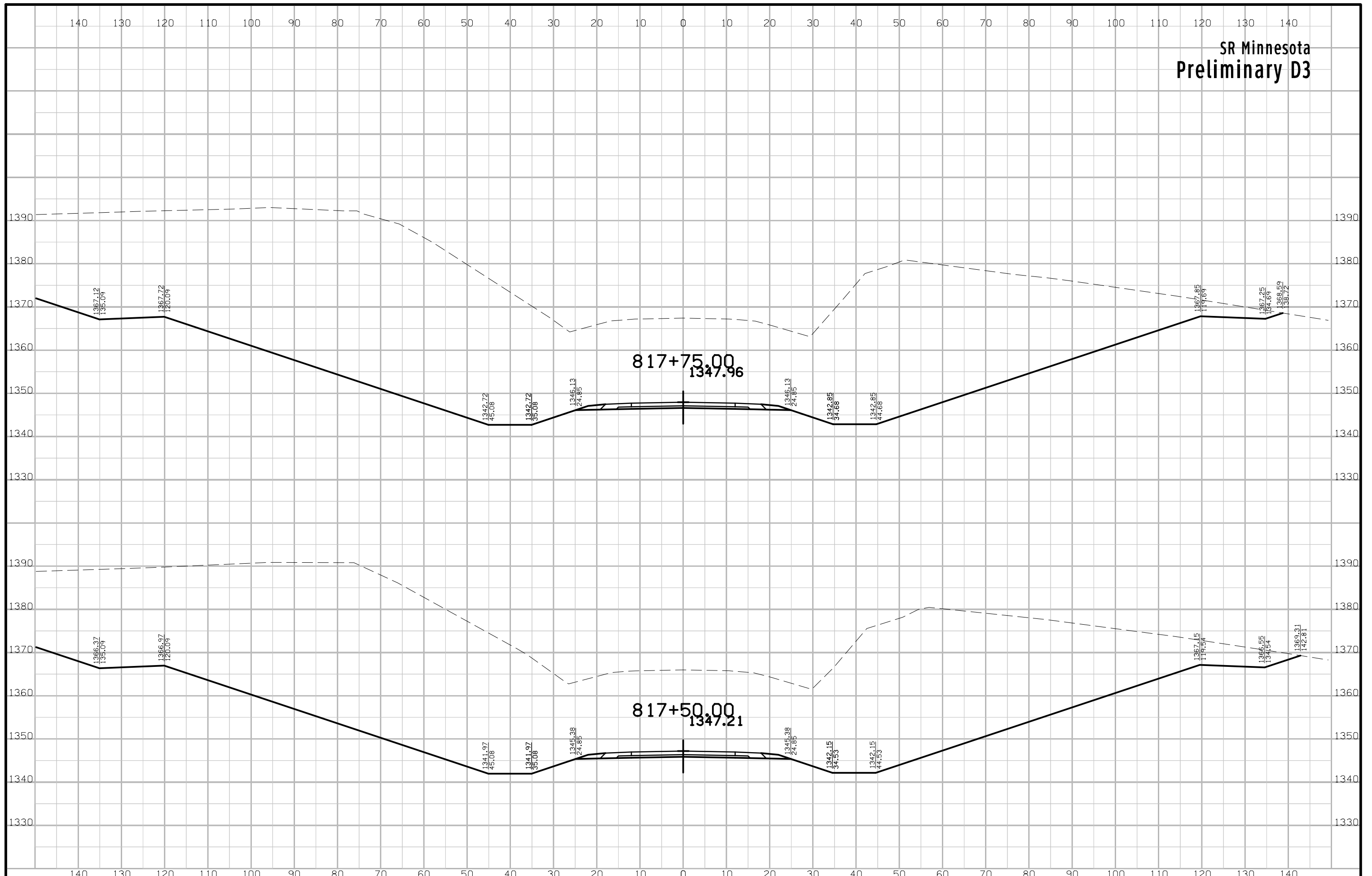
SR Minnesota
Preliminary D3



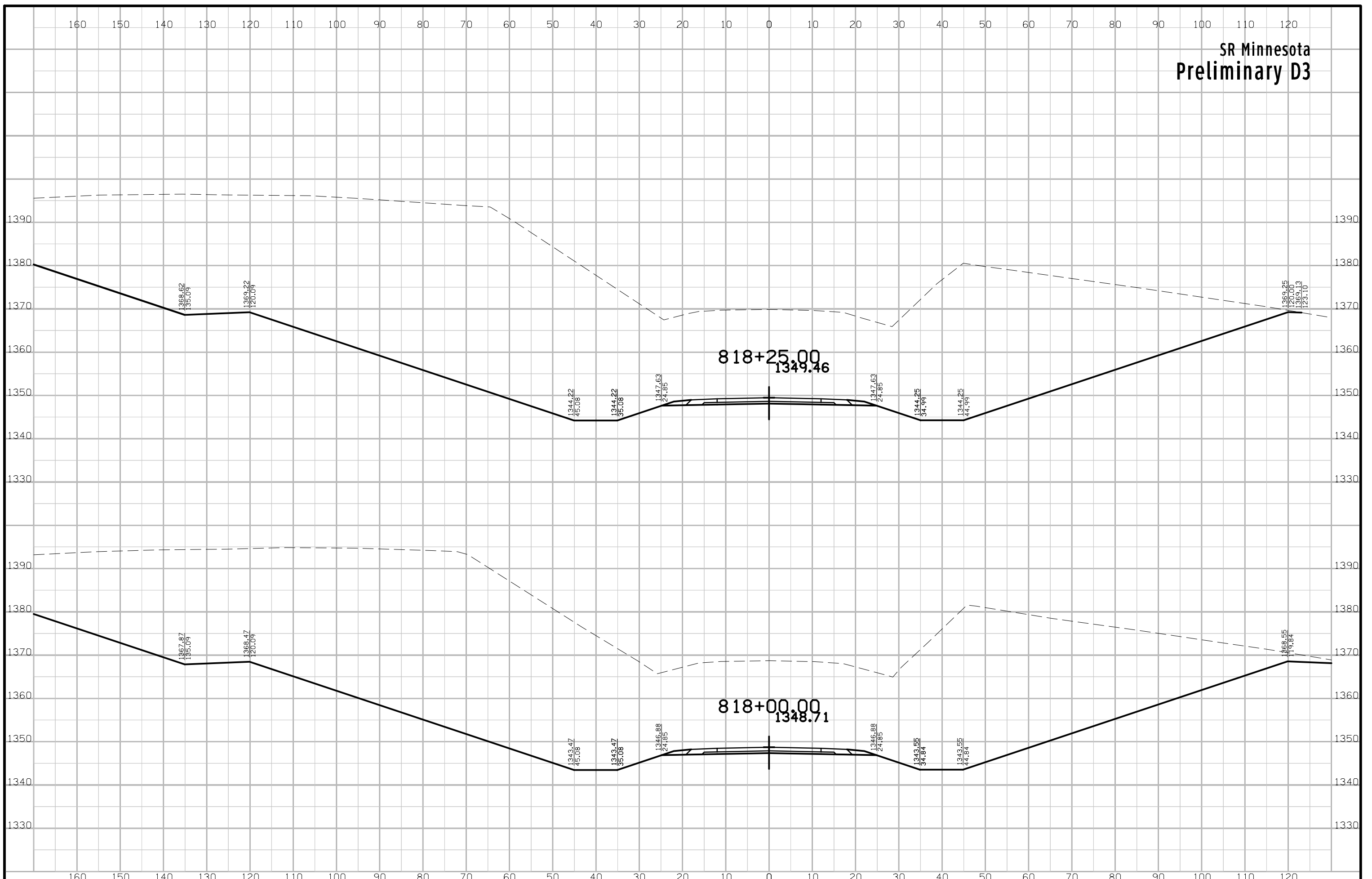
SR Minnesota
Preliminary D3



SR Minnesota
Preliminary D3



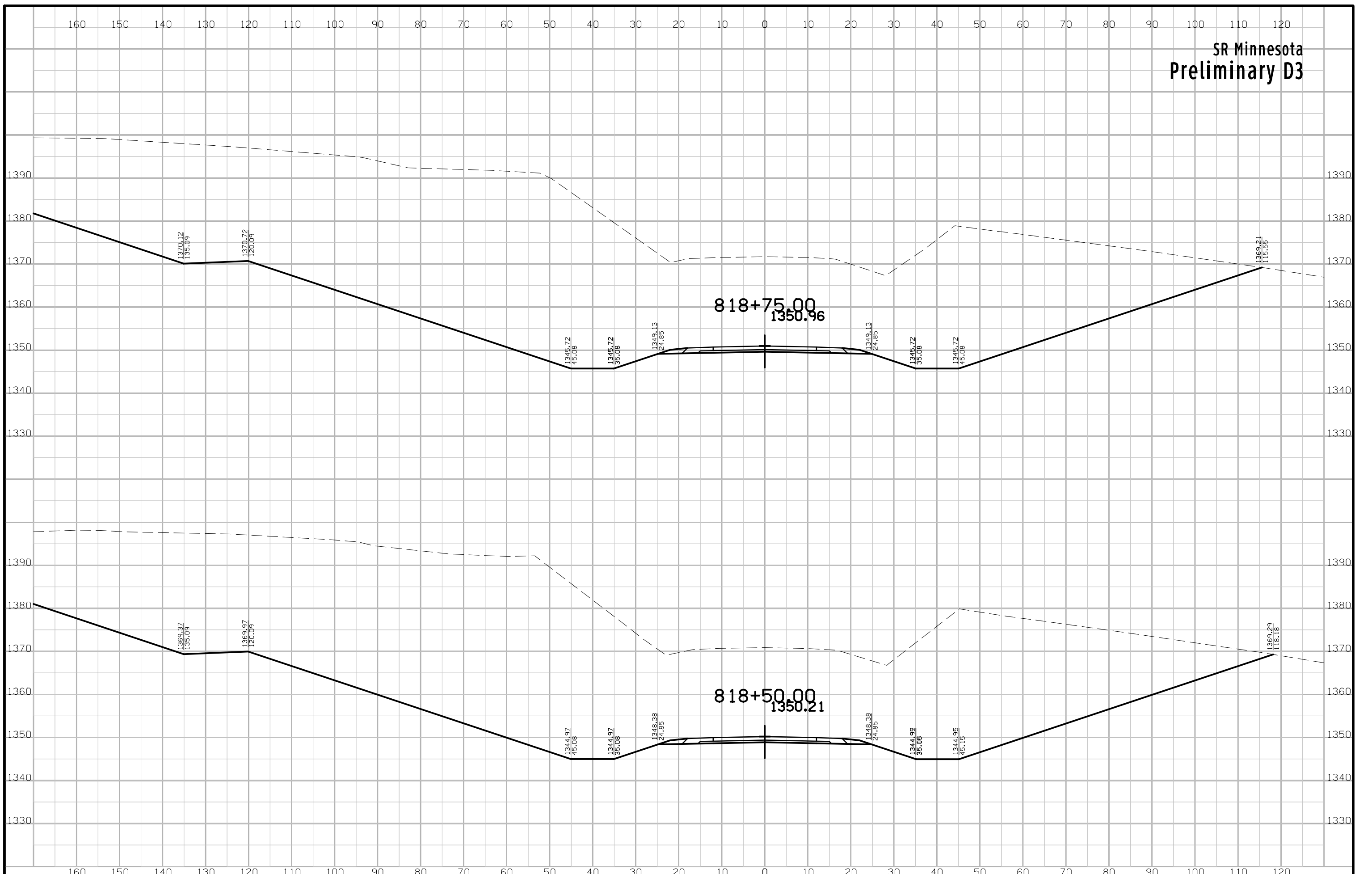
SR Minnesota
Preliminary D3



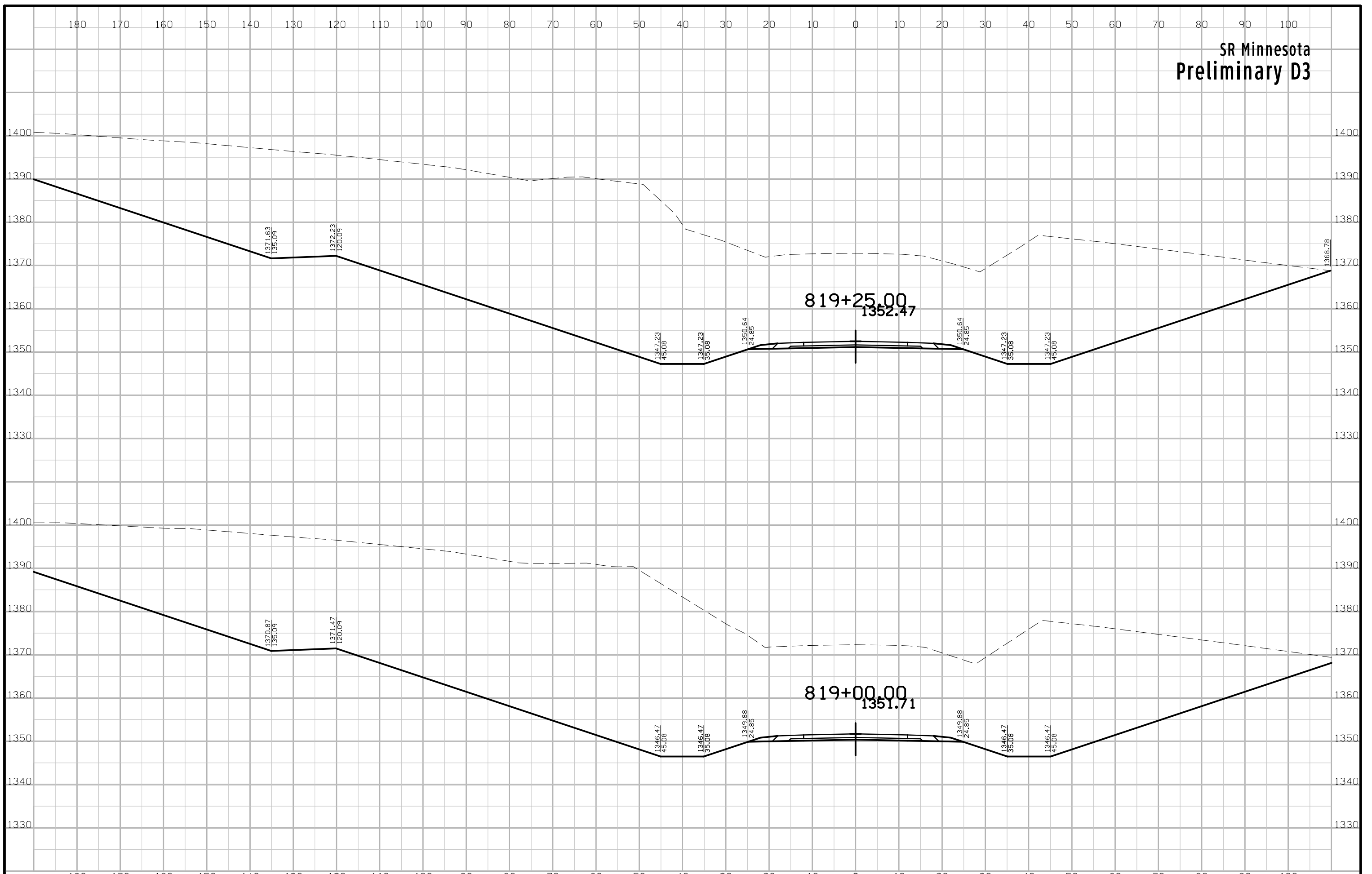
818+25.00
1349.46

818+00.00
1348.71

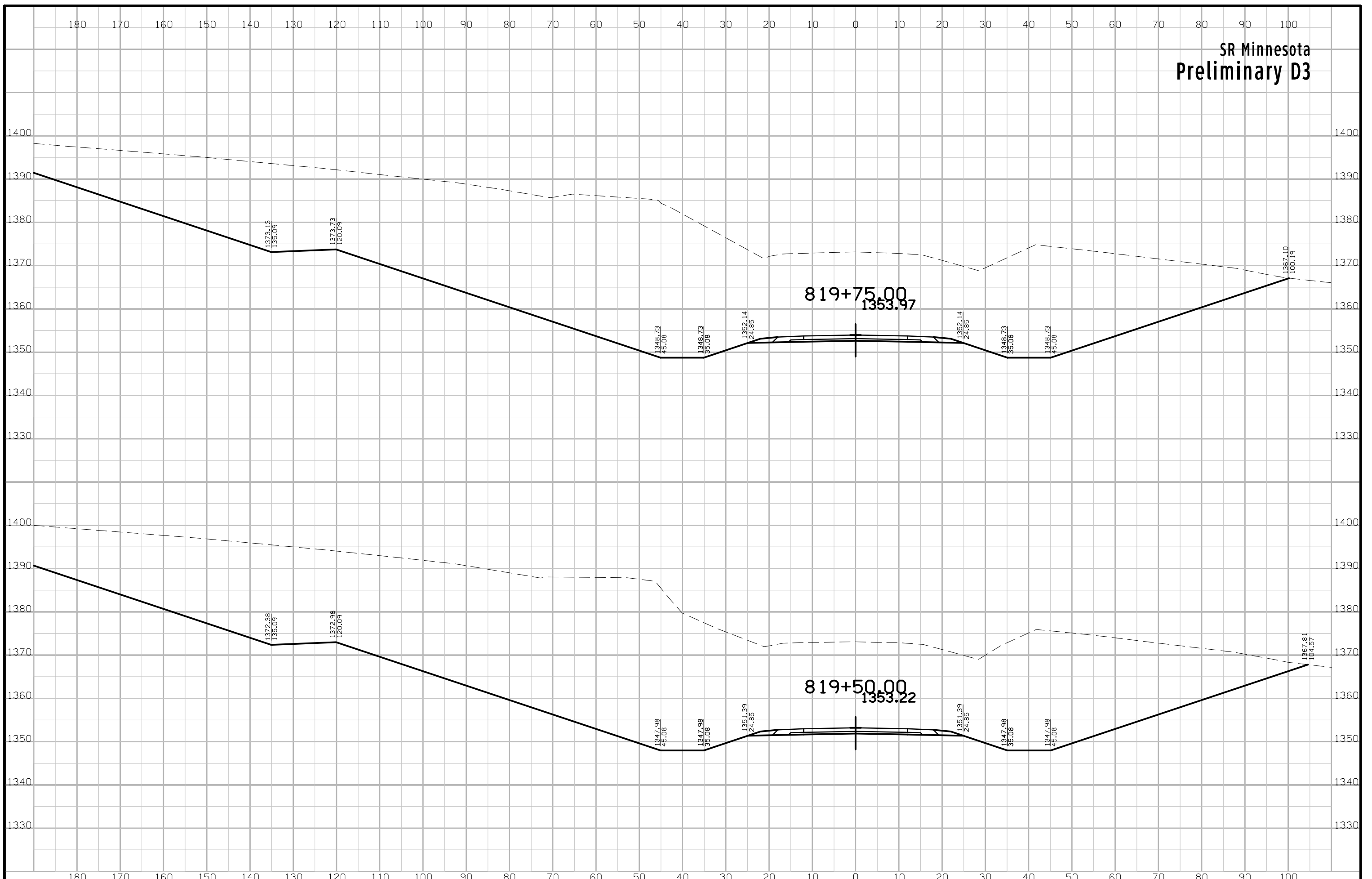
SR Minnesota
Preliminary D3



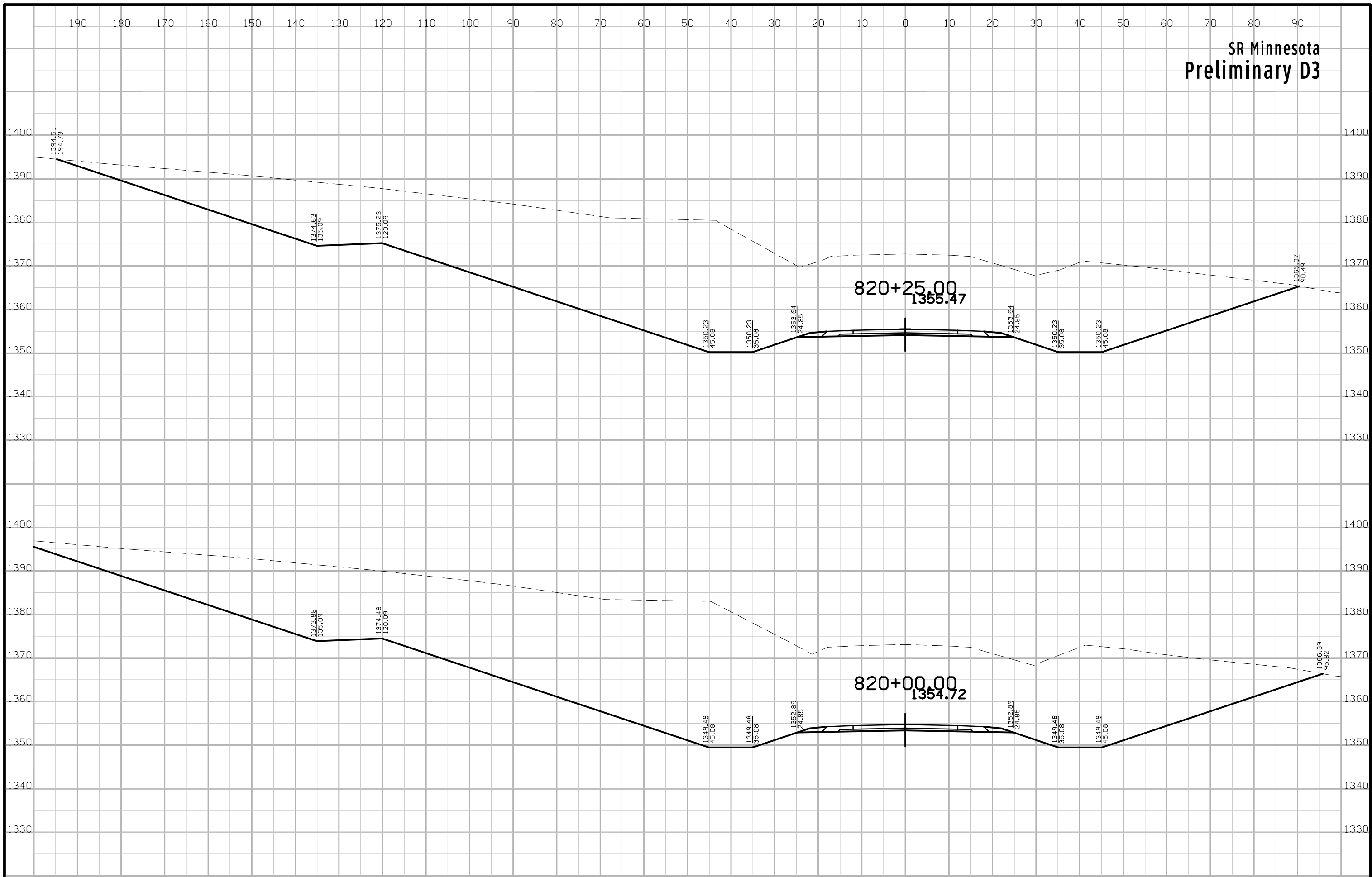
SR Minnesota
Preliminary D3



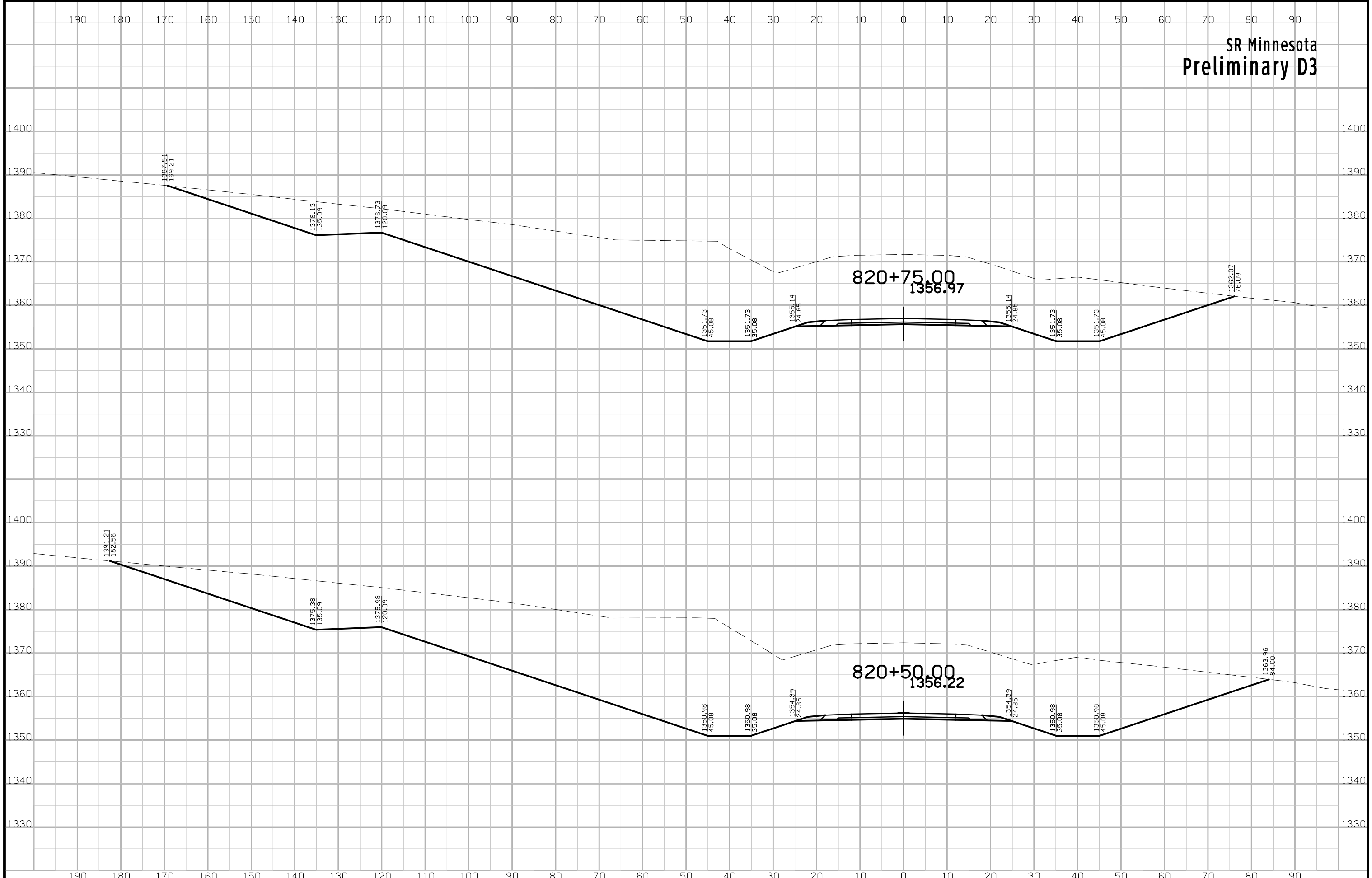
SR Minnesota
Preliminary D3



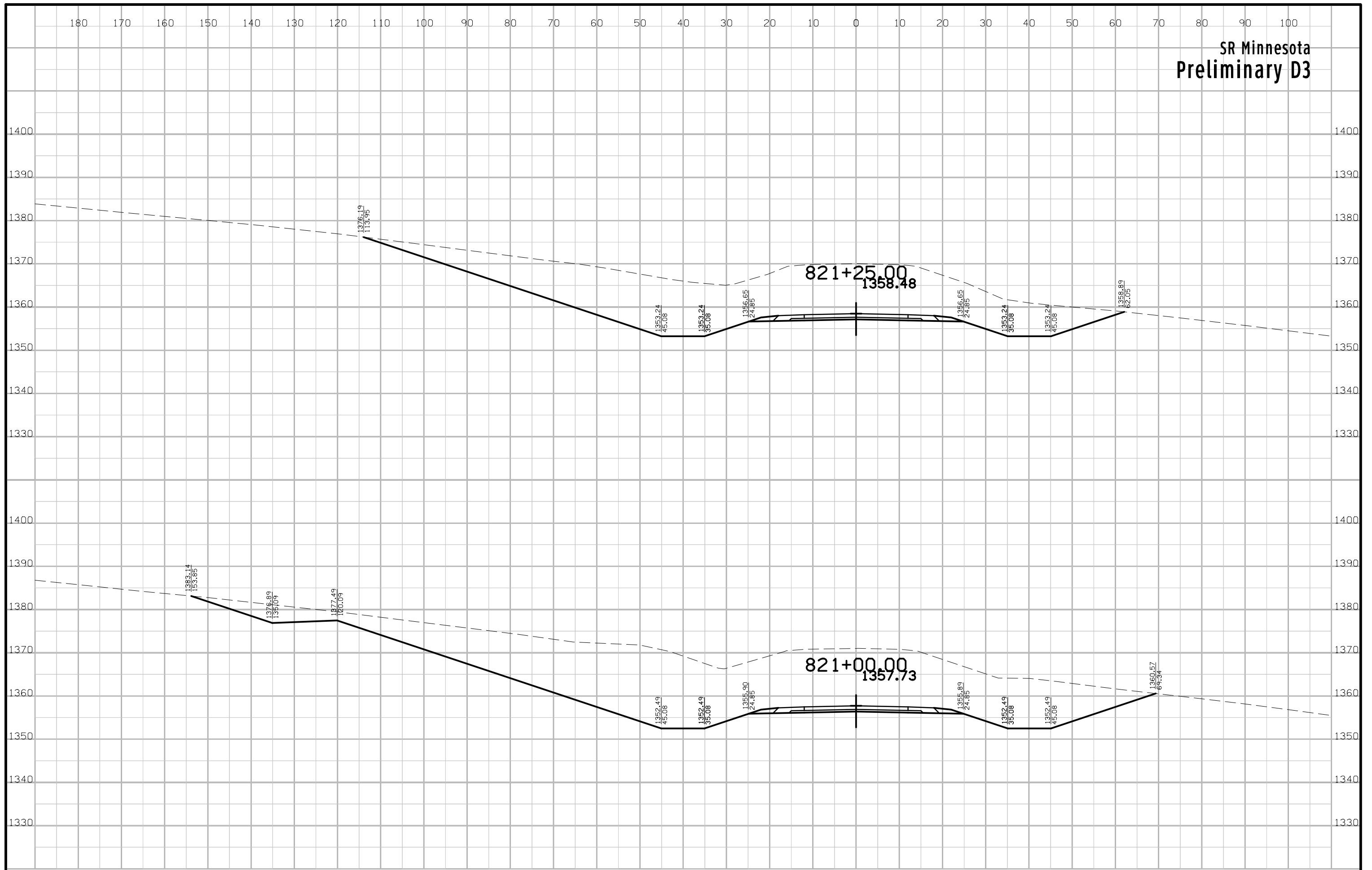
SR Minnesota
Preliminary D3



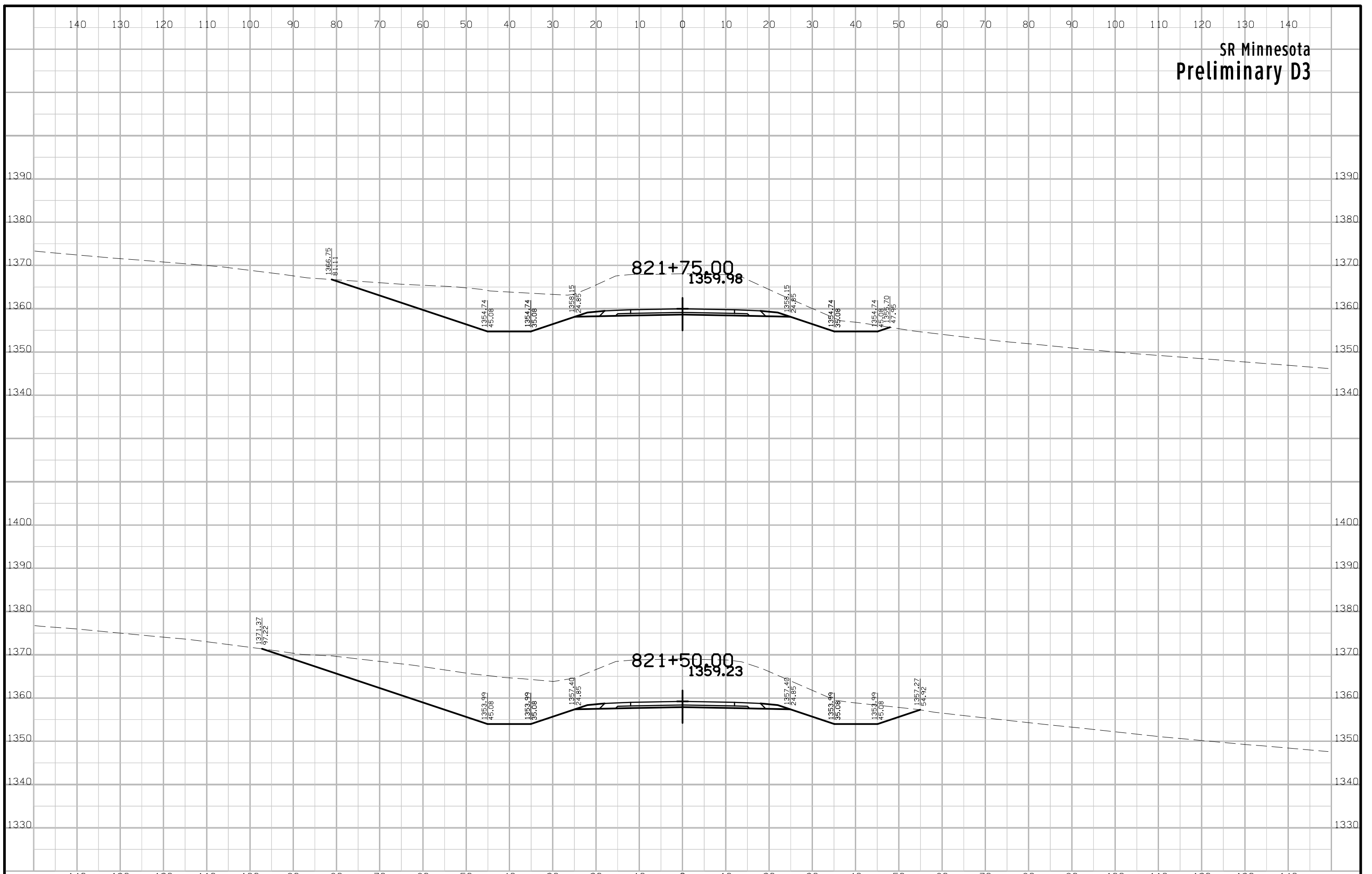
SR Minnesota
Preliminary D3



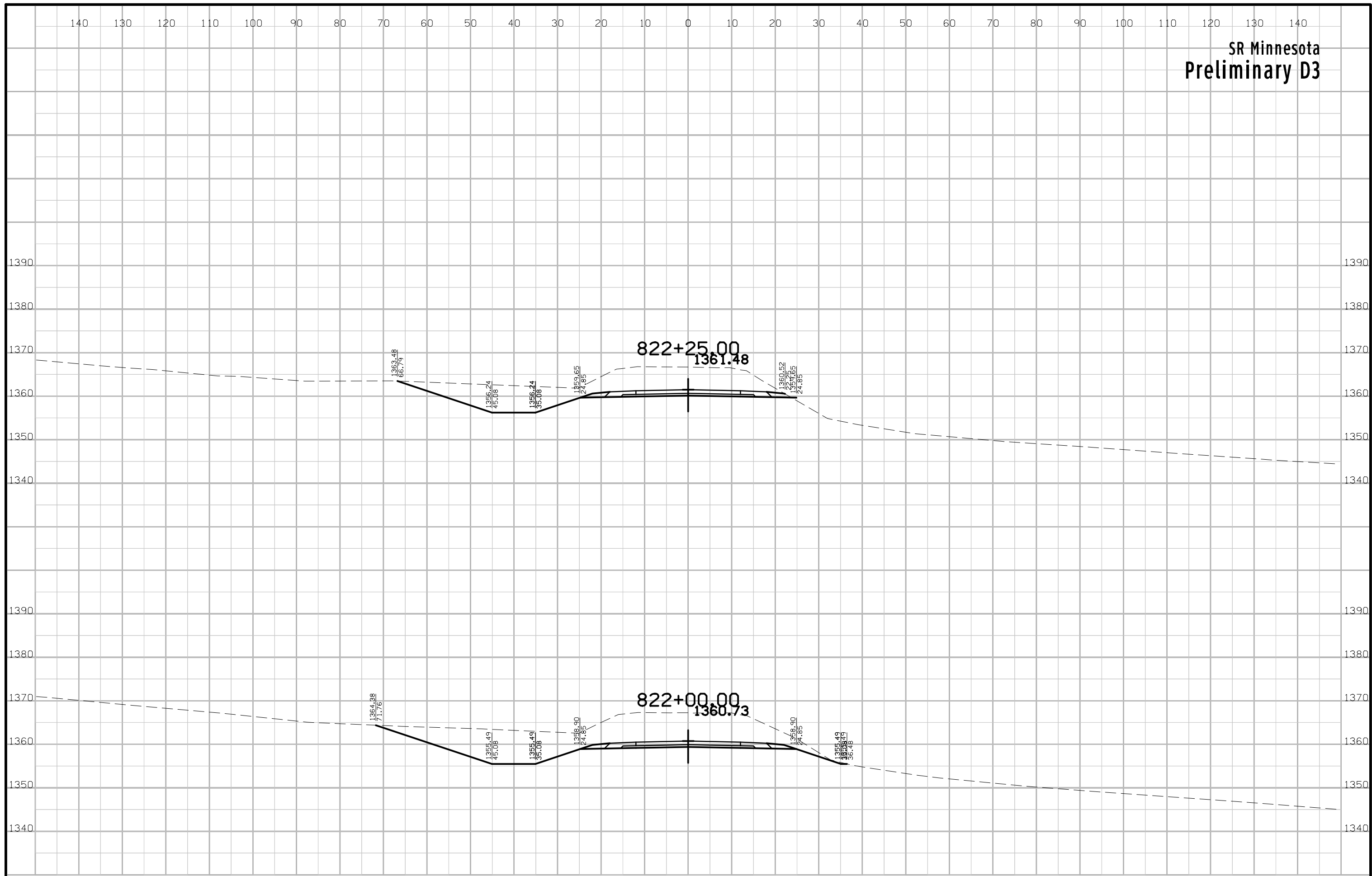
SR Minnesota
Preliminary D3



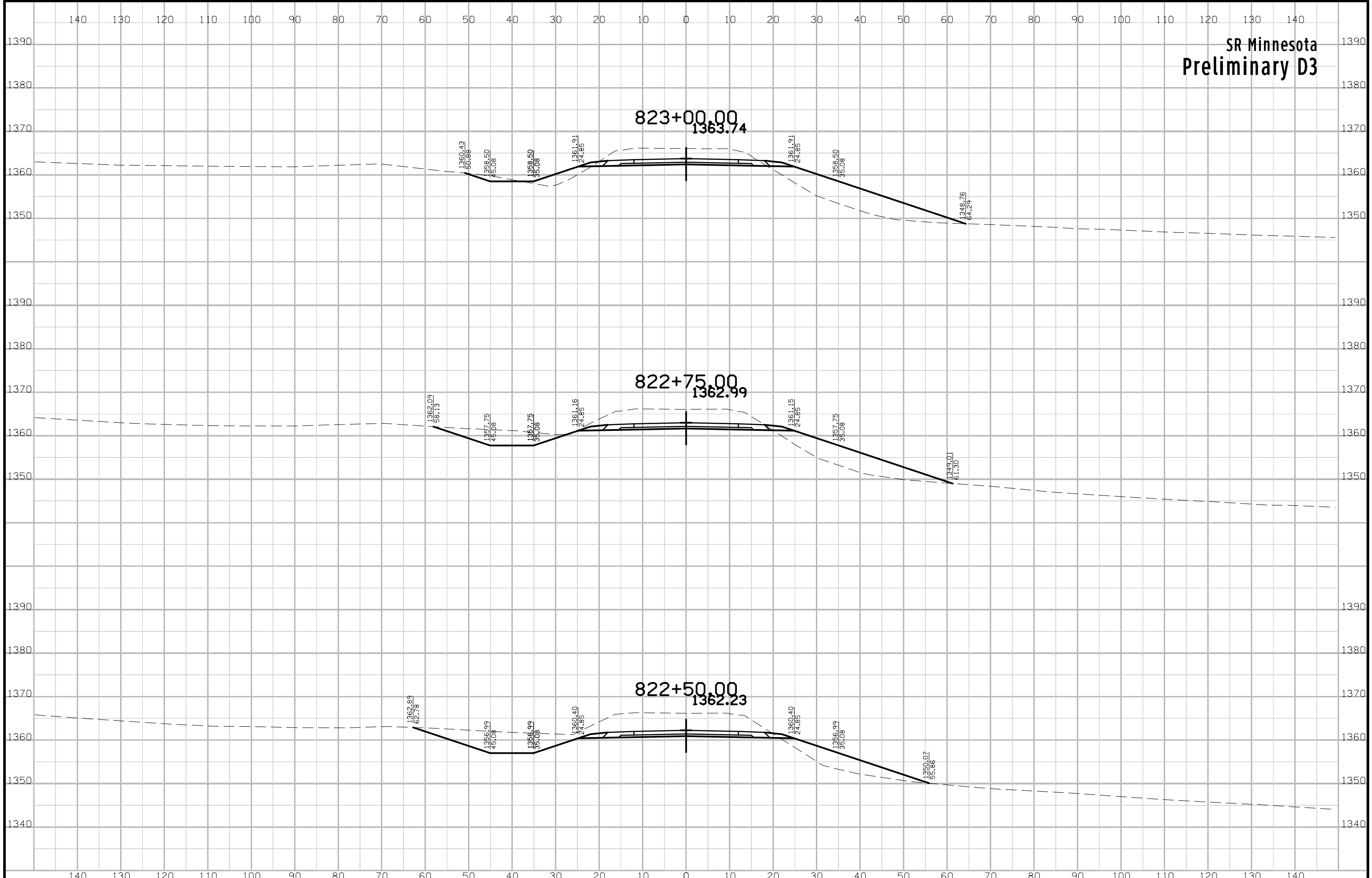
SR Minnesota
Preliminary D3



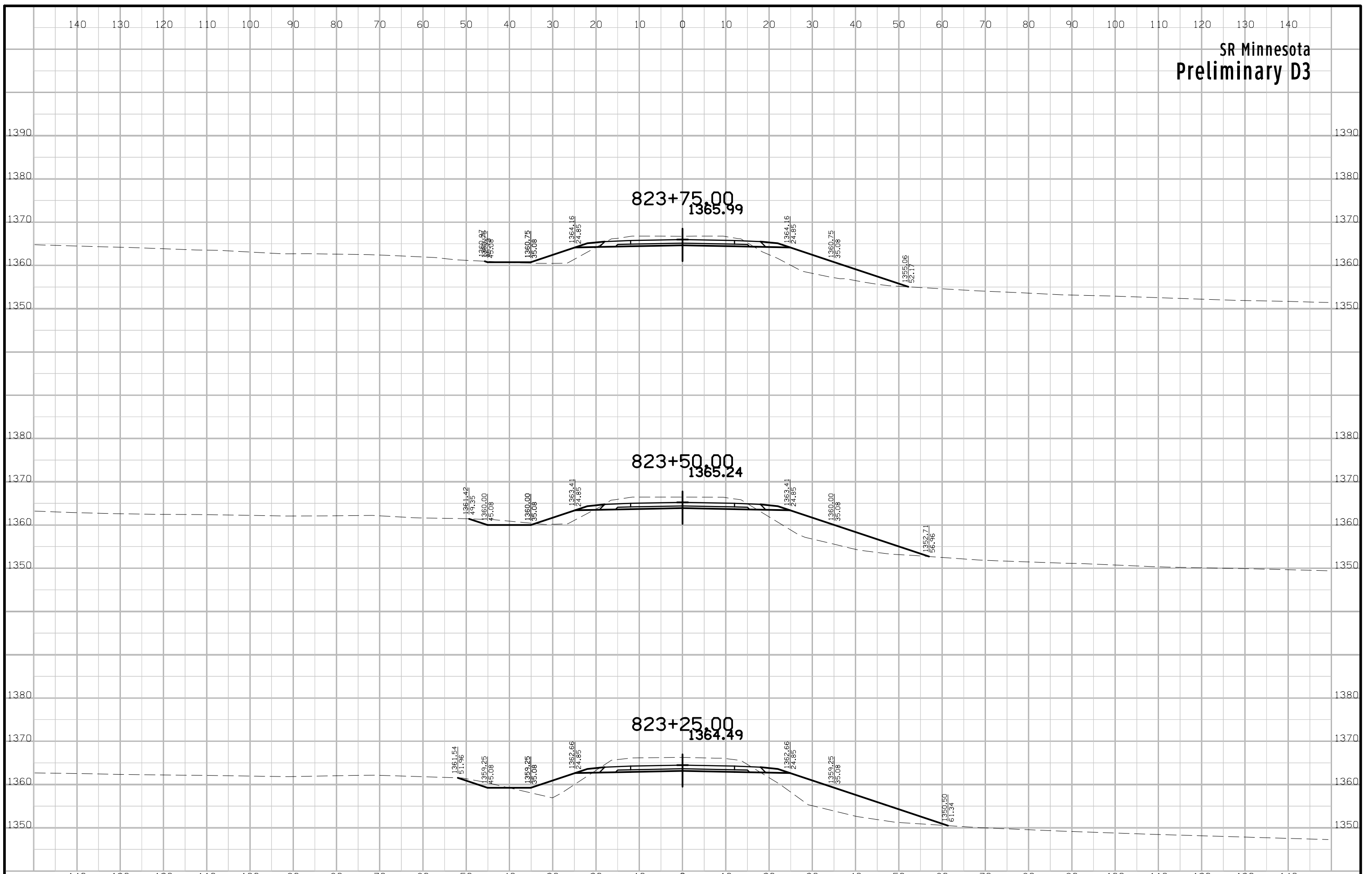
SR Minnesota
Preliminary D3



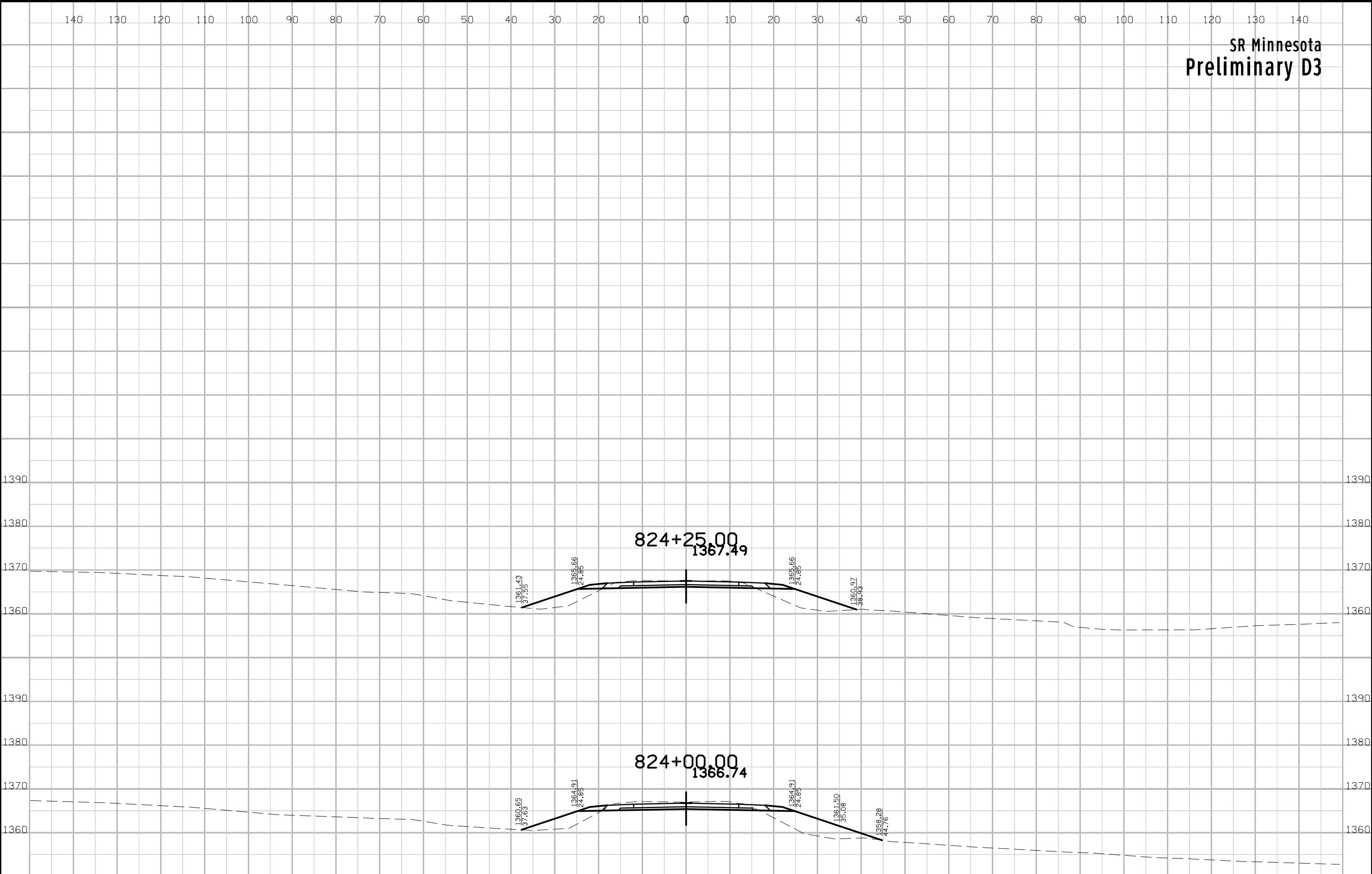
SR Minnesota
Preliminary D3



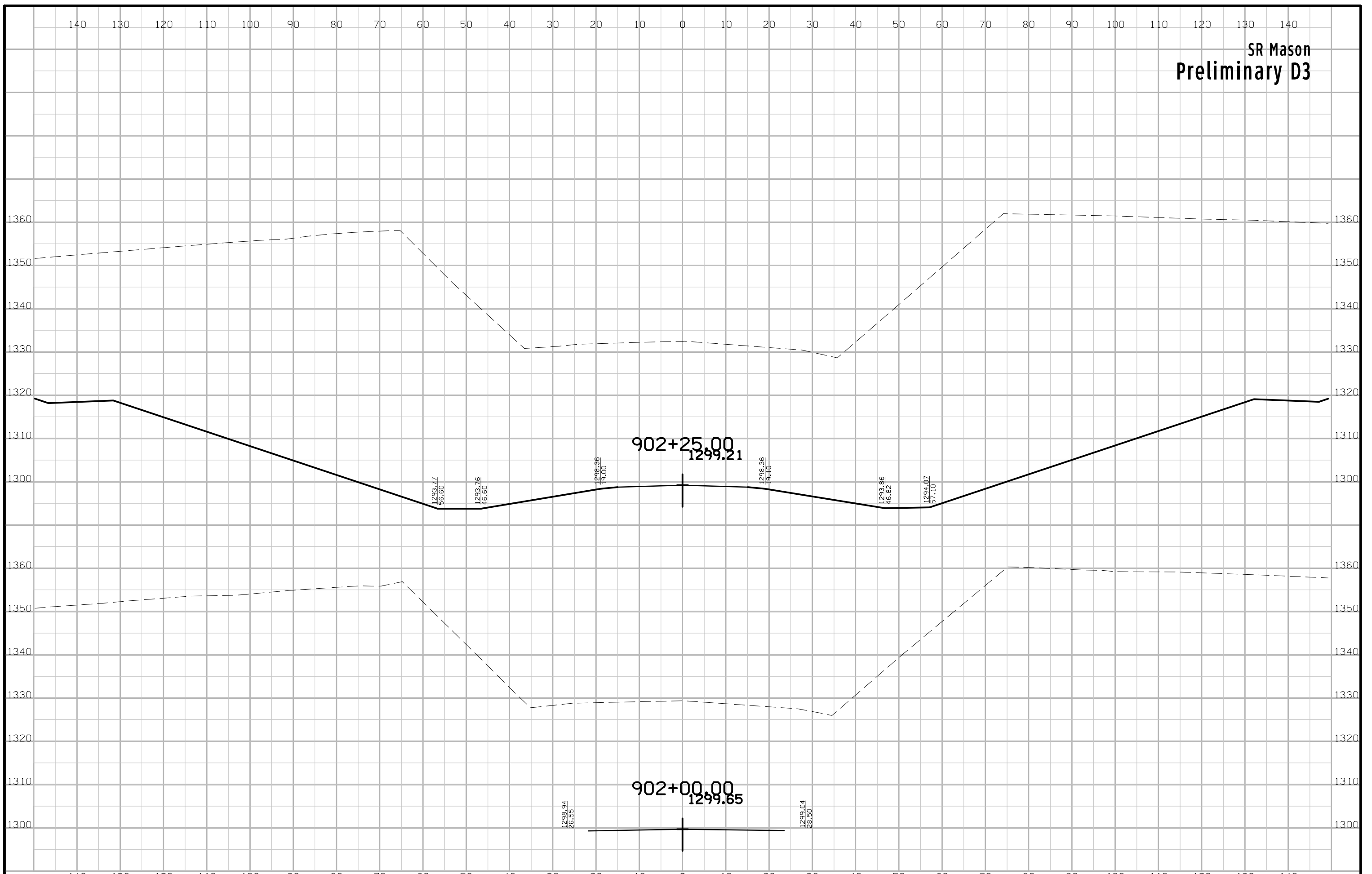
SR Minnesota
Preliminary D3



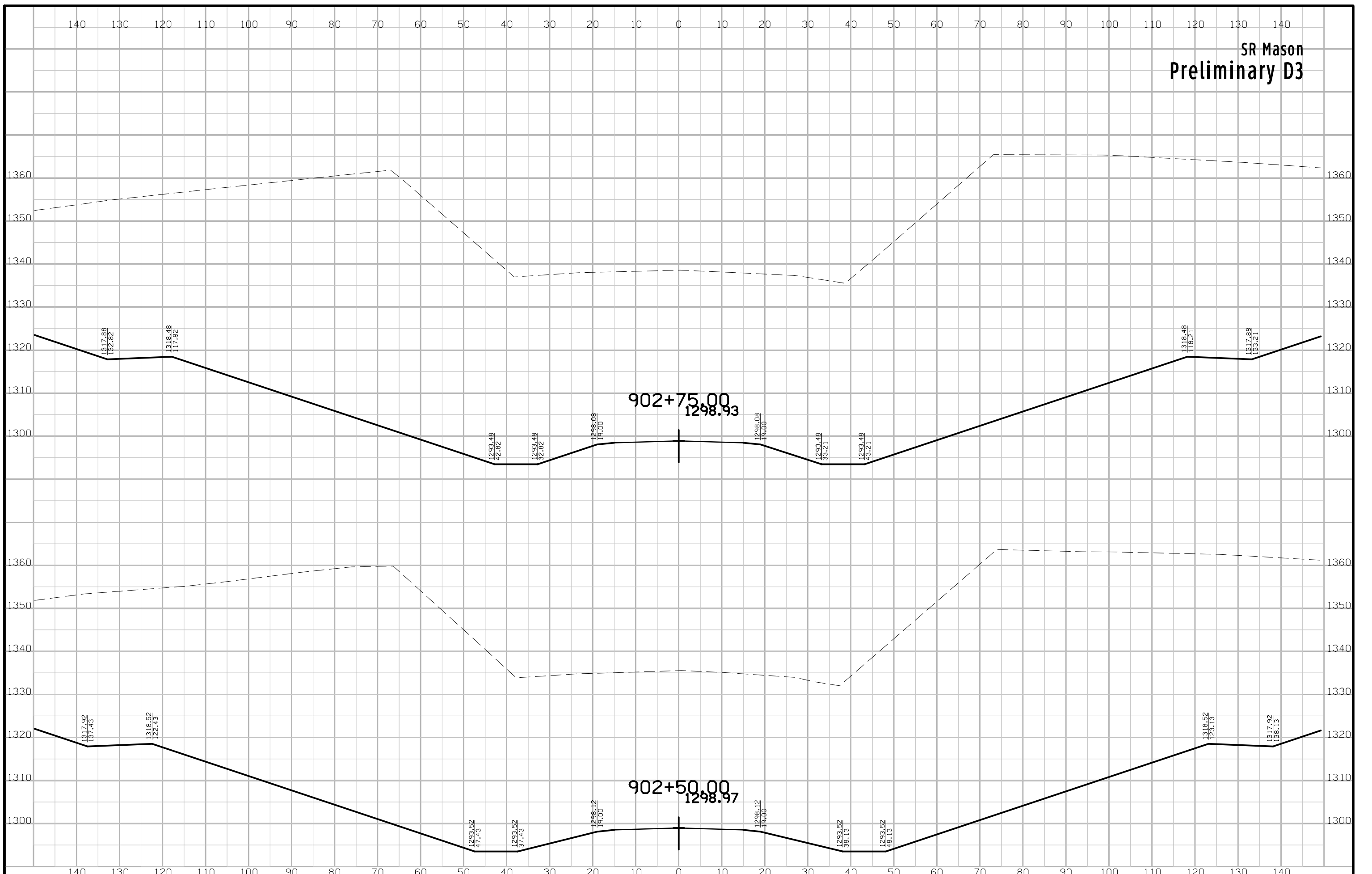
SR Minnesota
Preliminary D3



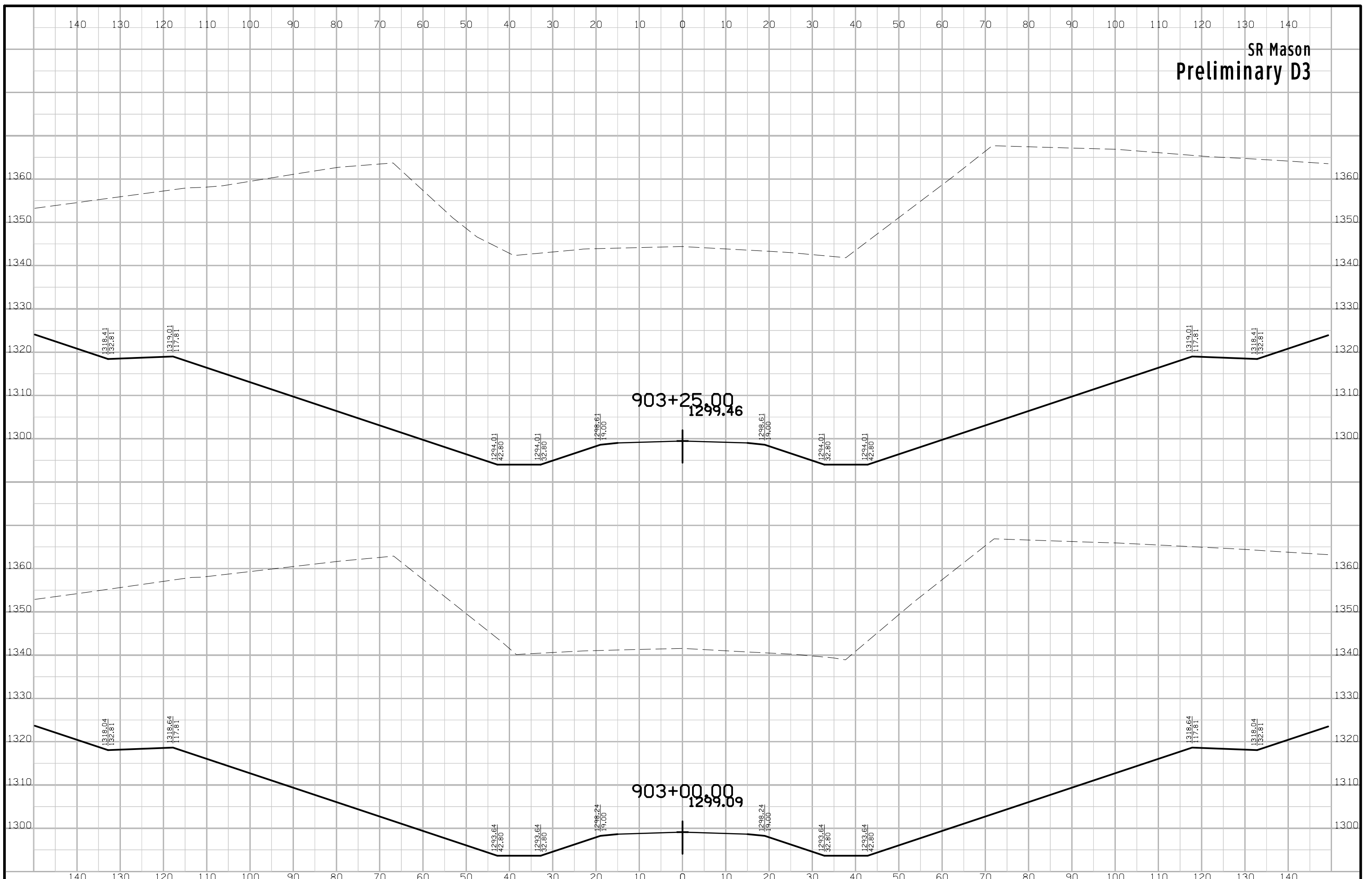
SR Mason
Preliminary D3



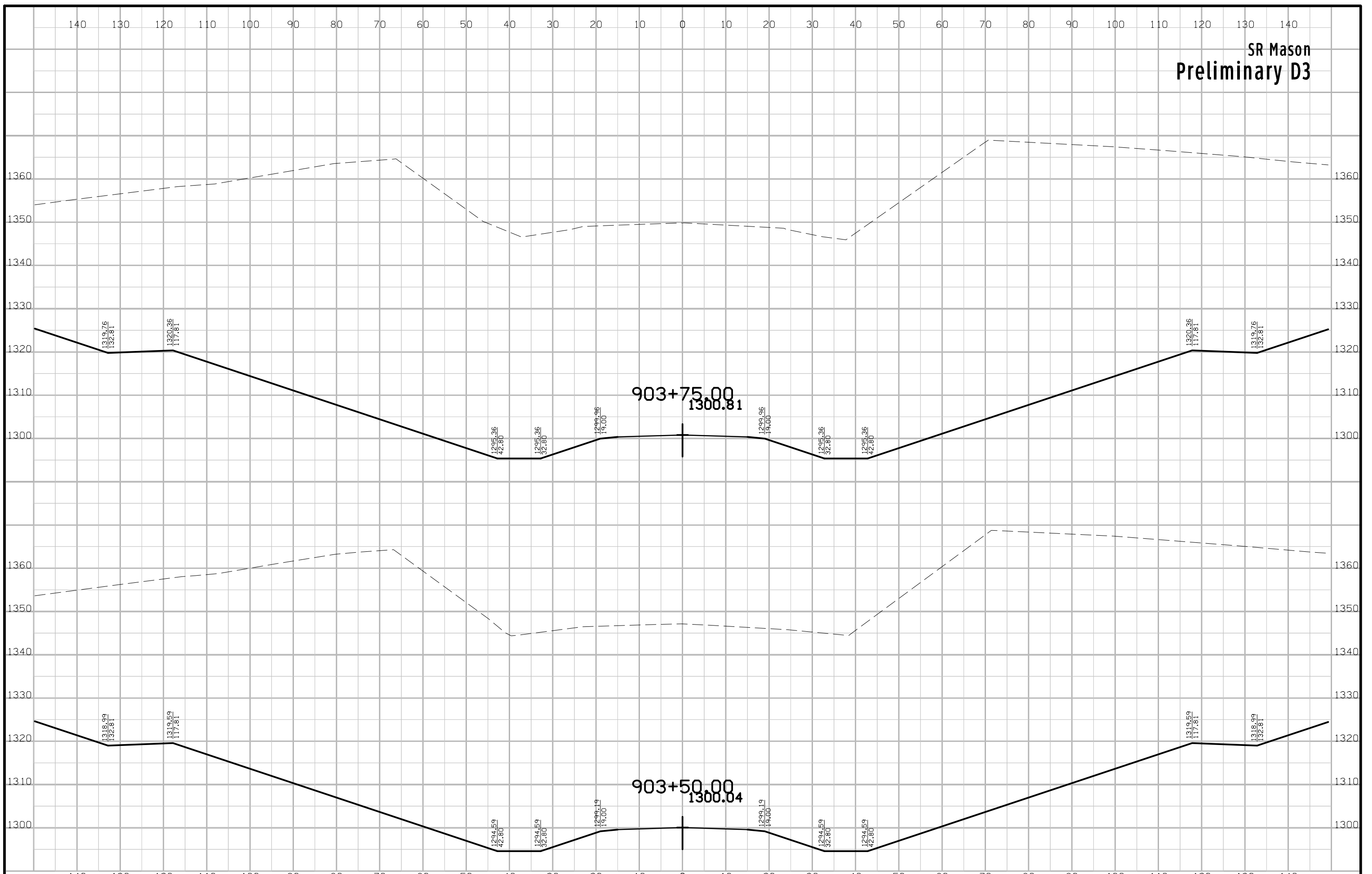
SR Mason
Preliminary D3



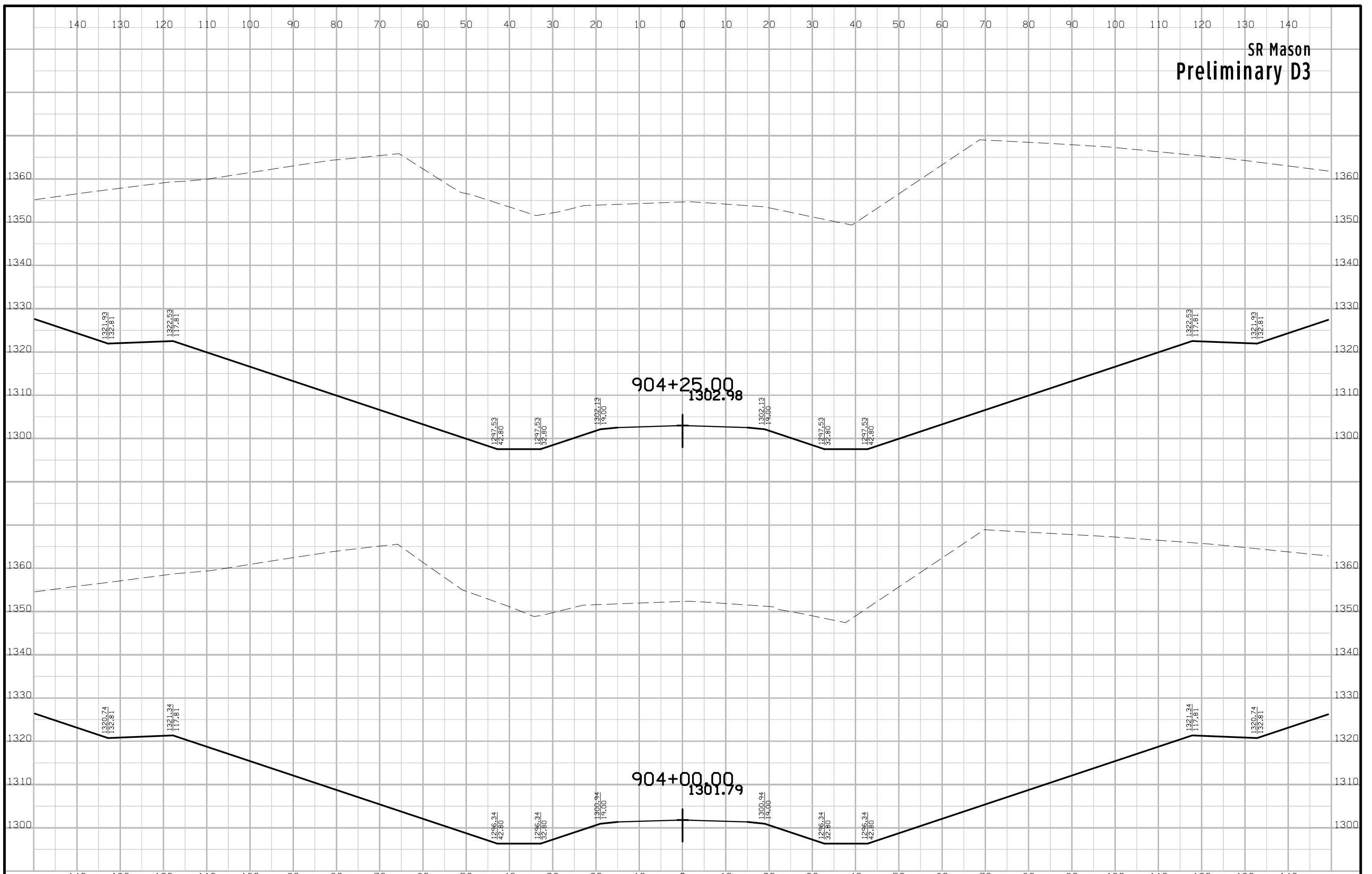
SR Mason
Preliminary D3



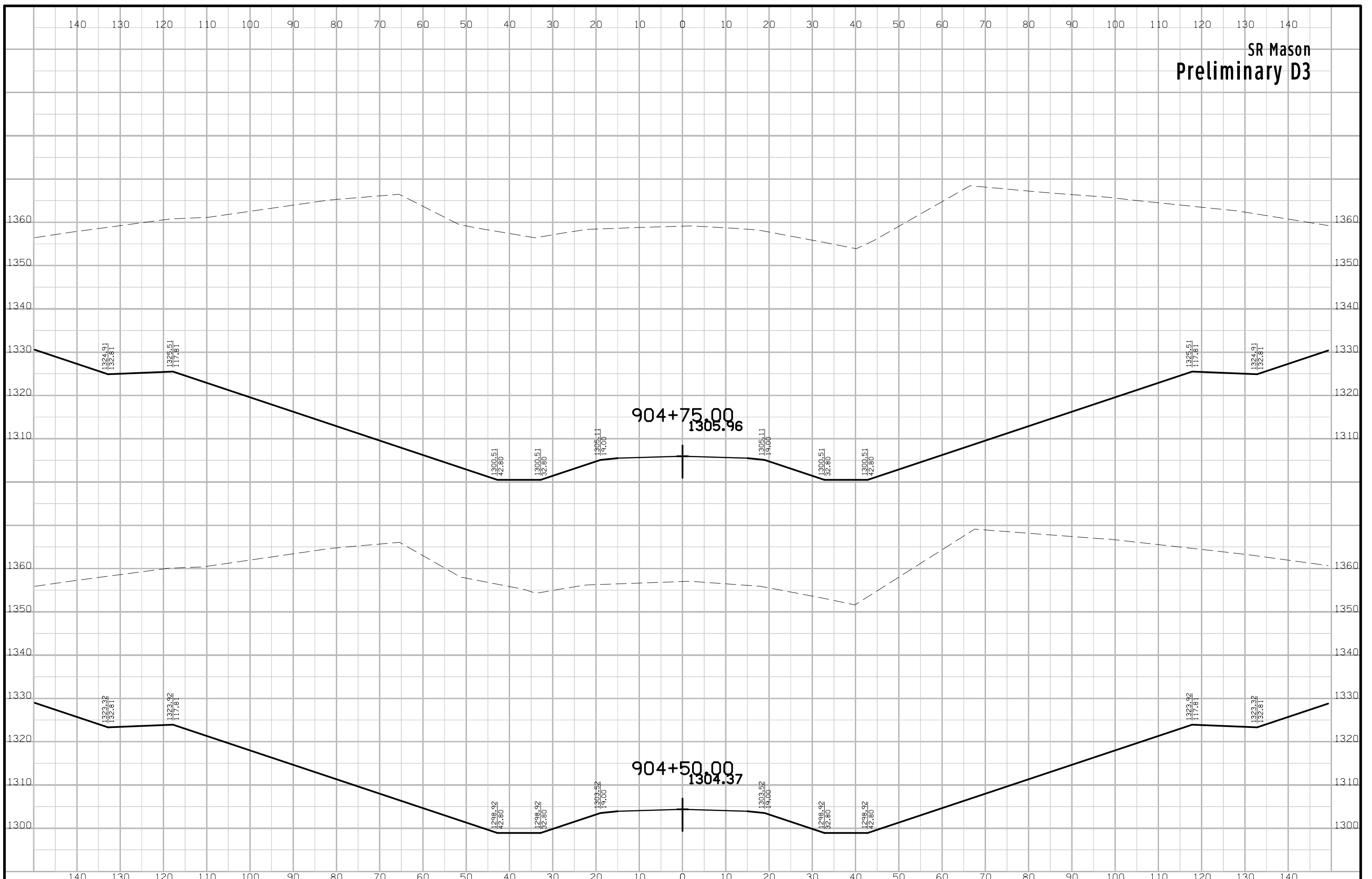
SR Mason
Preliminary D3



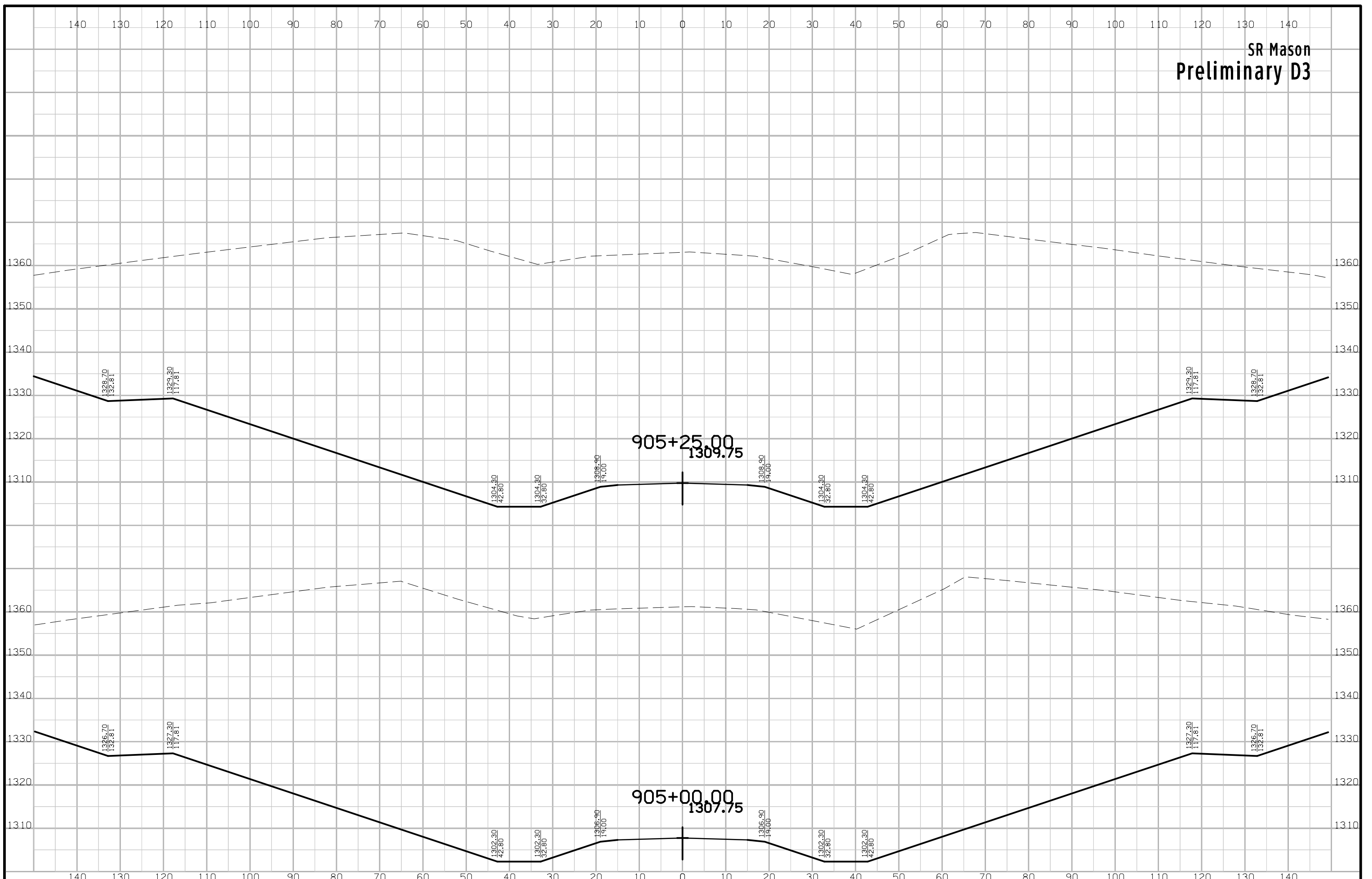
SR Mason
Preliminary D3



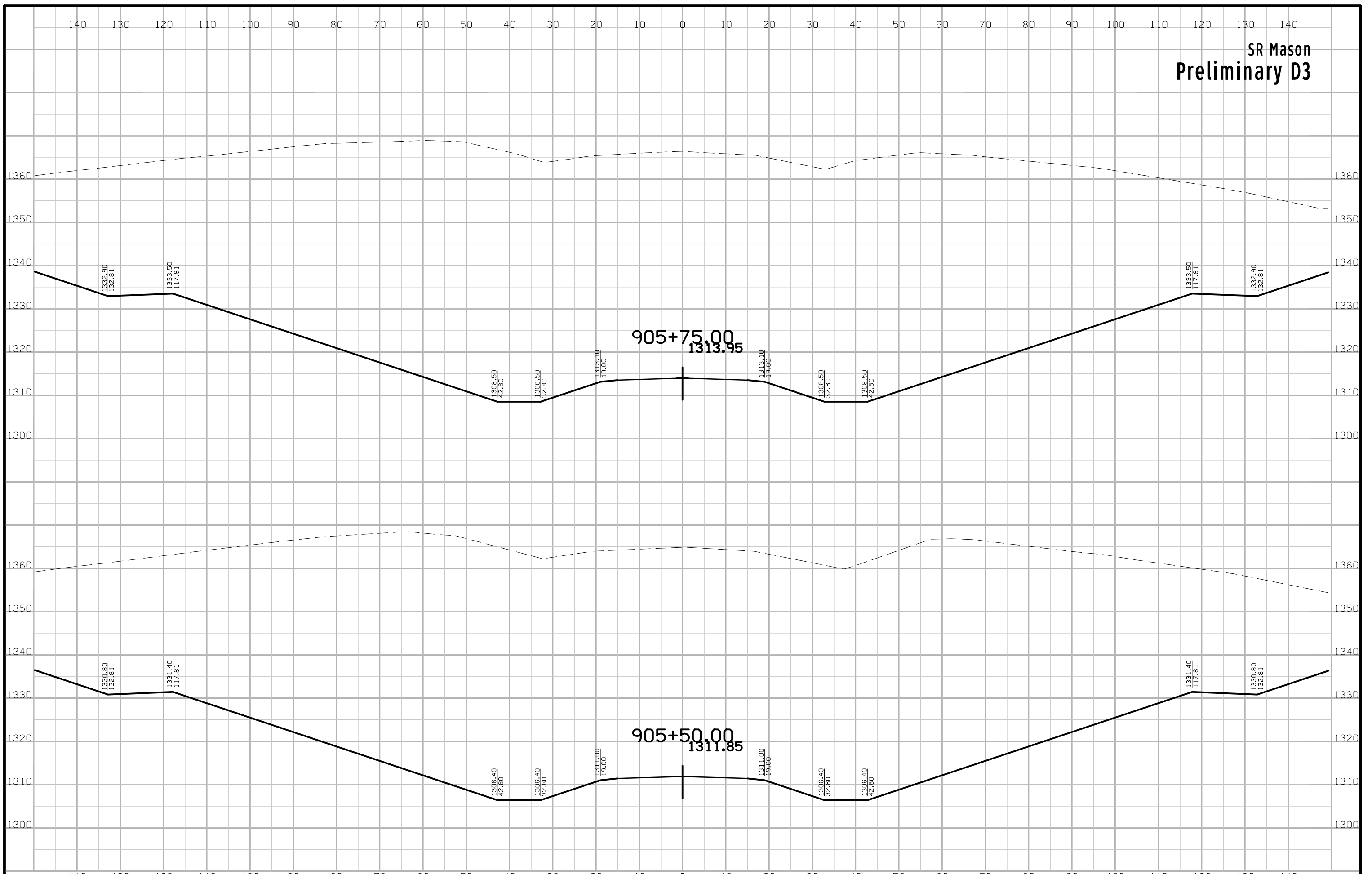
SR Mason
Preliminary D3



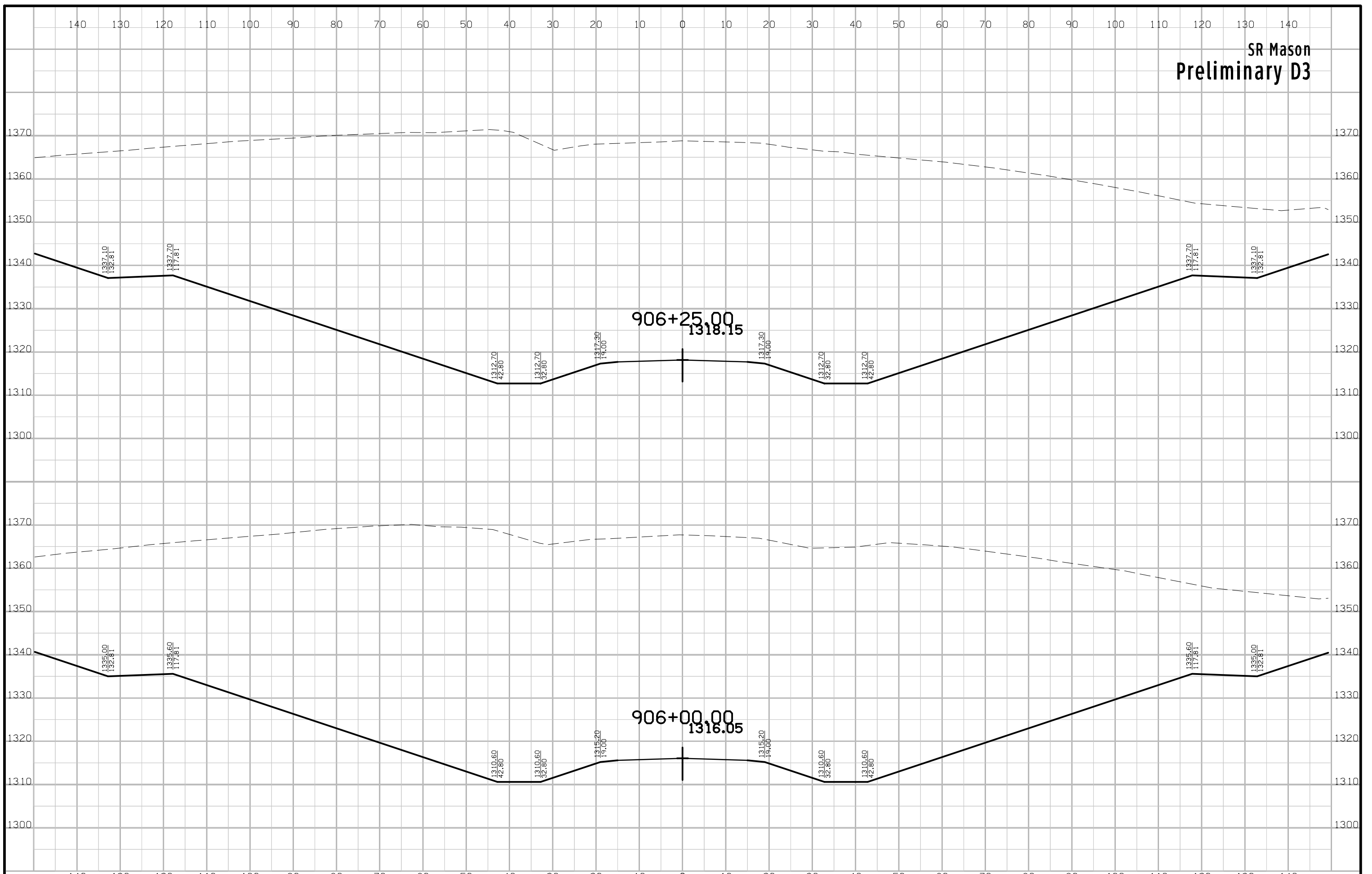
SR Mason
Preliminary D3



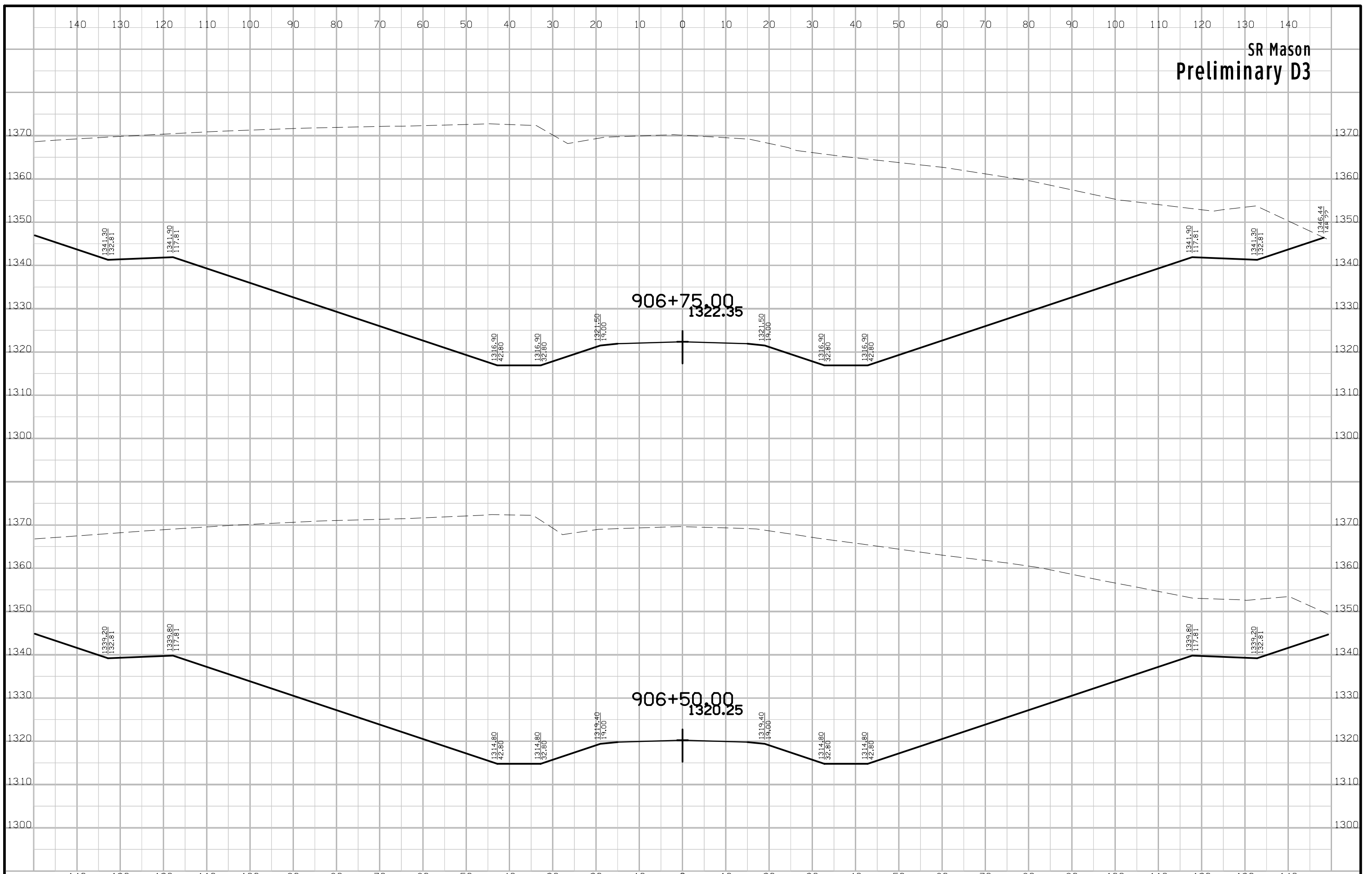
SR Mason
Preliminary D3



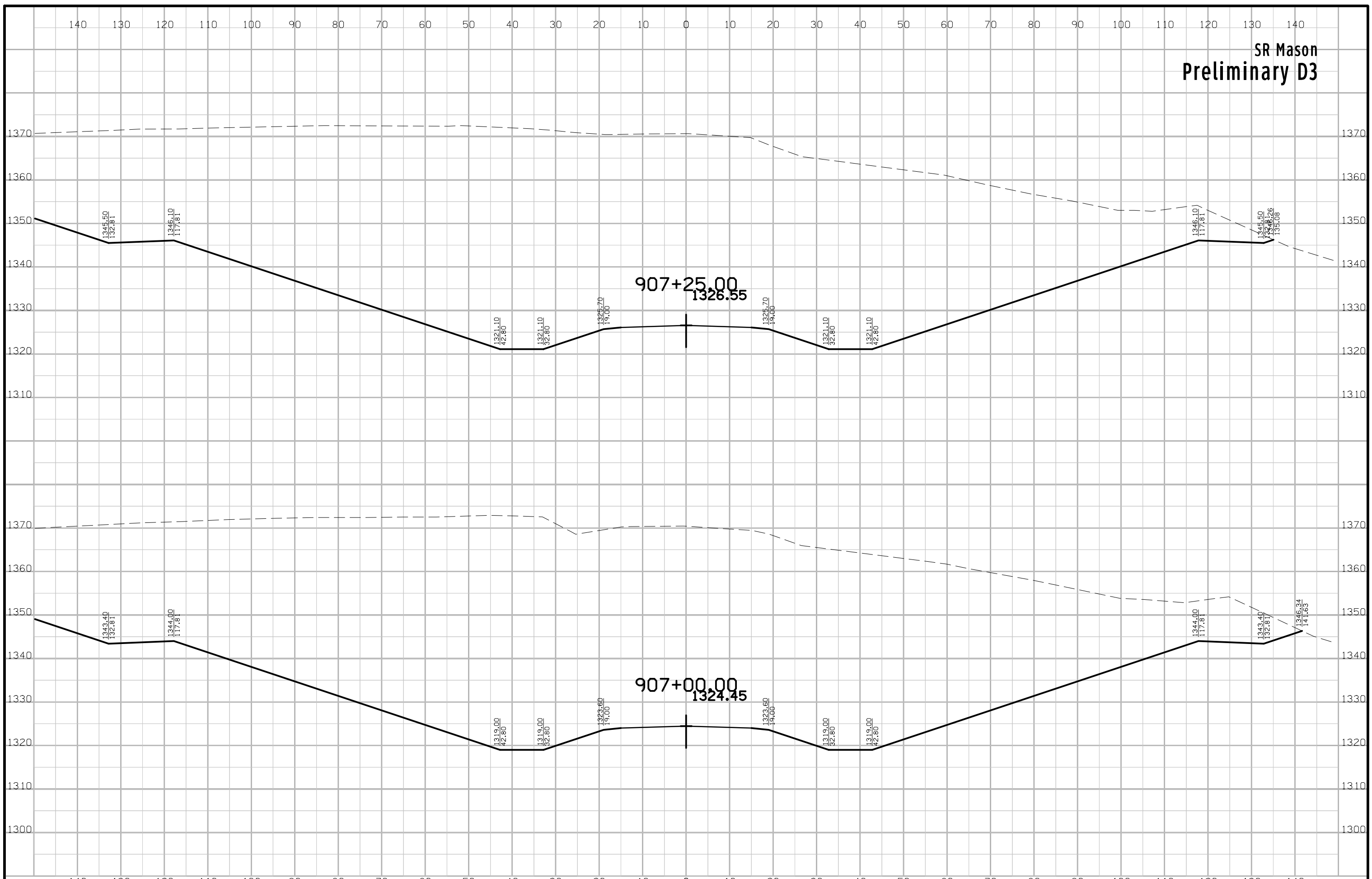
SR Mason
Preliminary D3



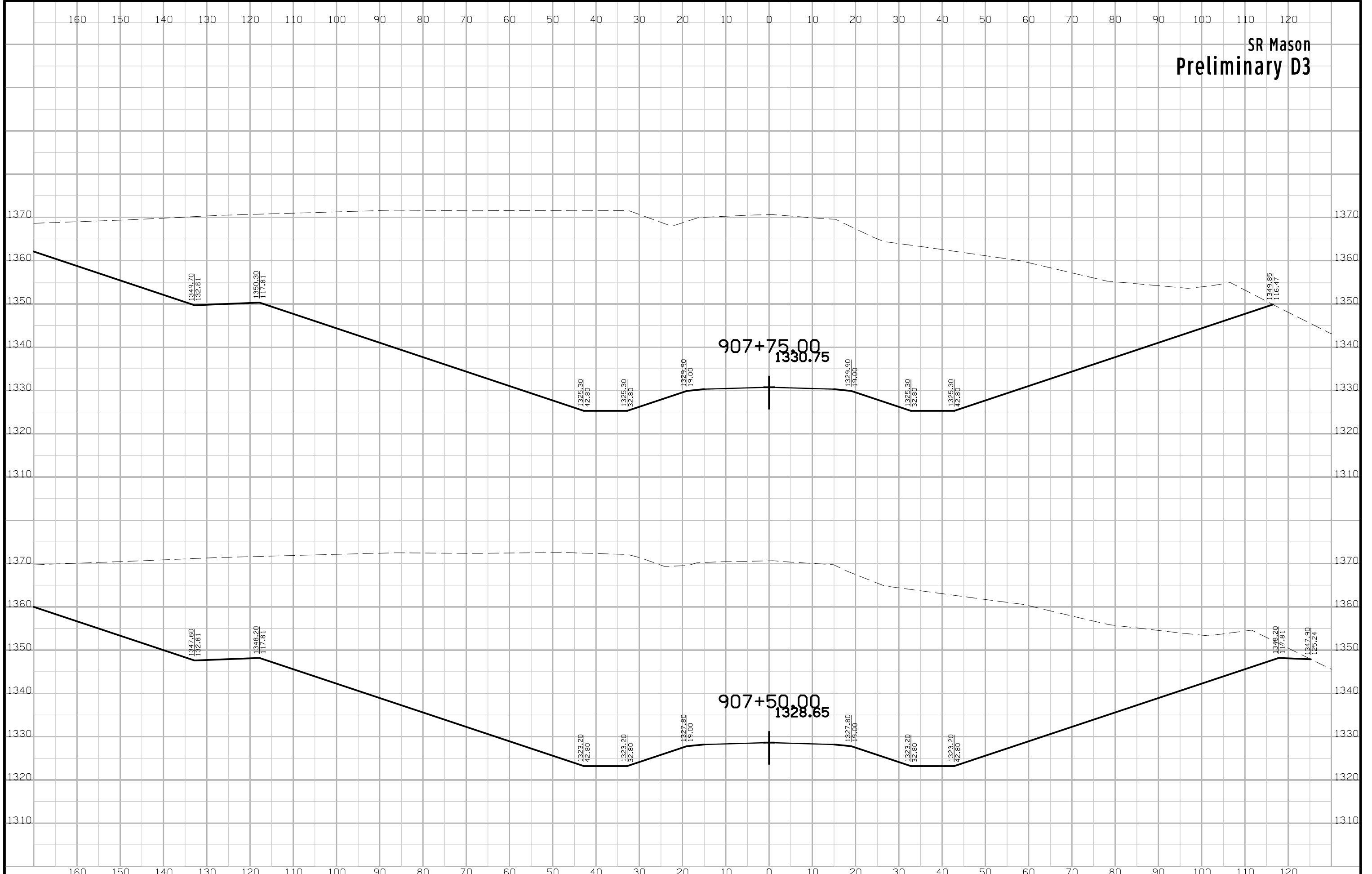
SR Mason
Preliminary D3



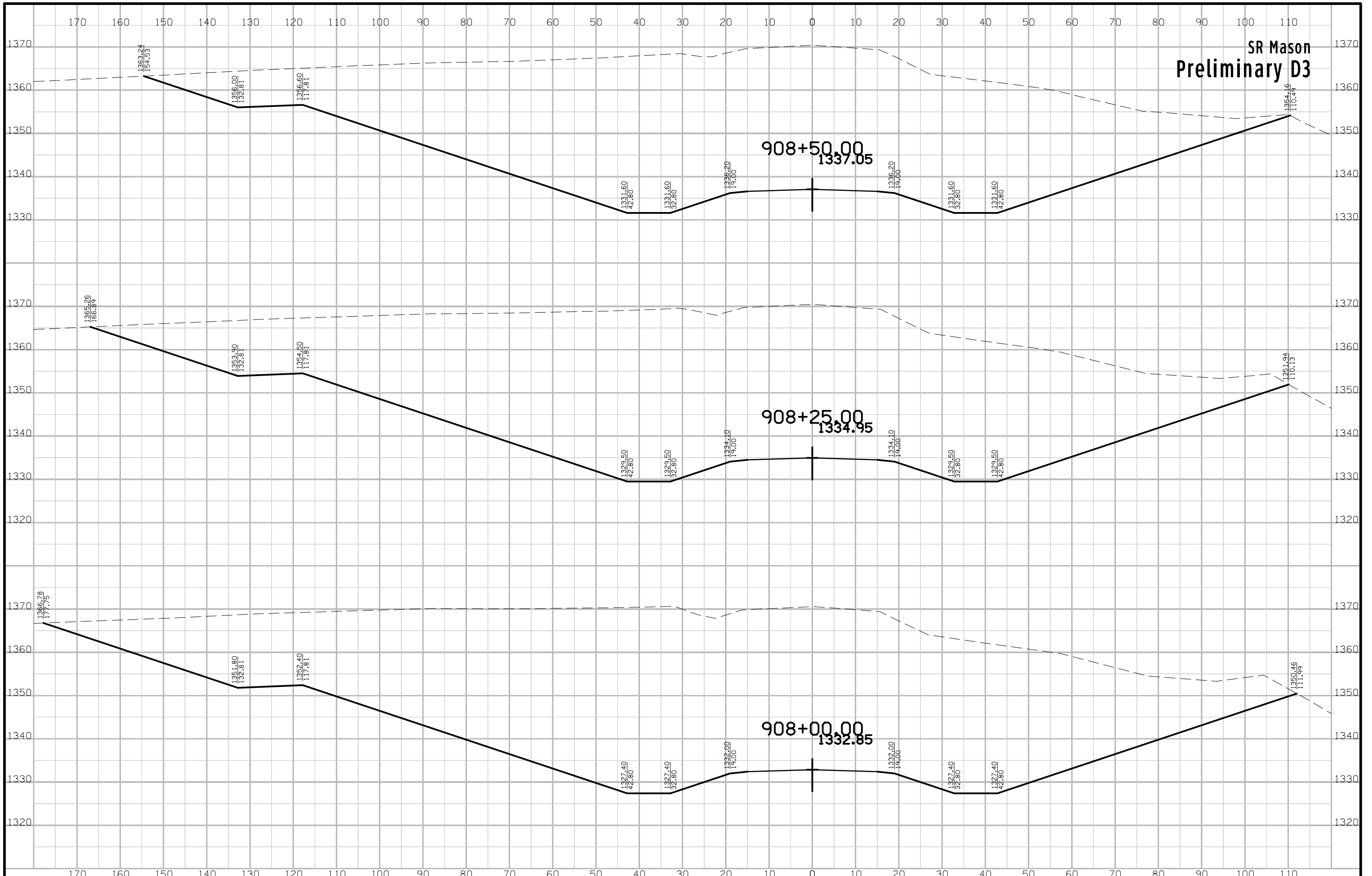
SR Mason
Preliminary D3



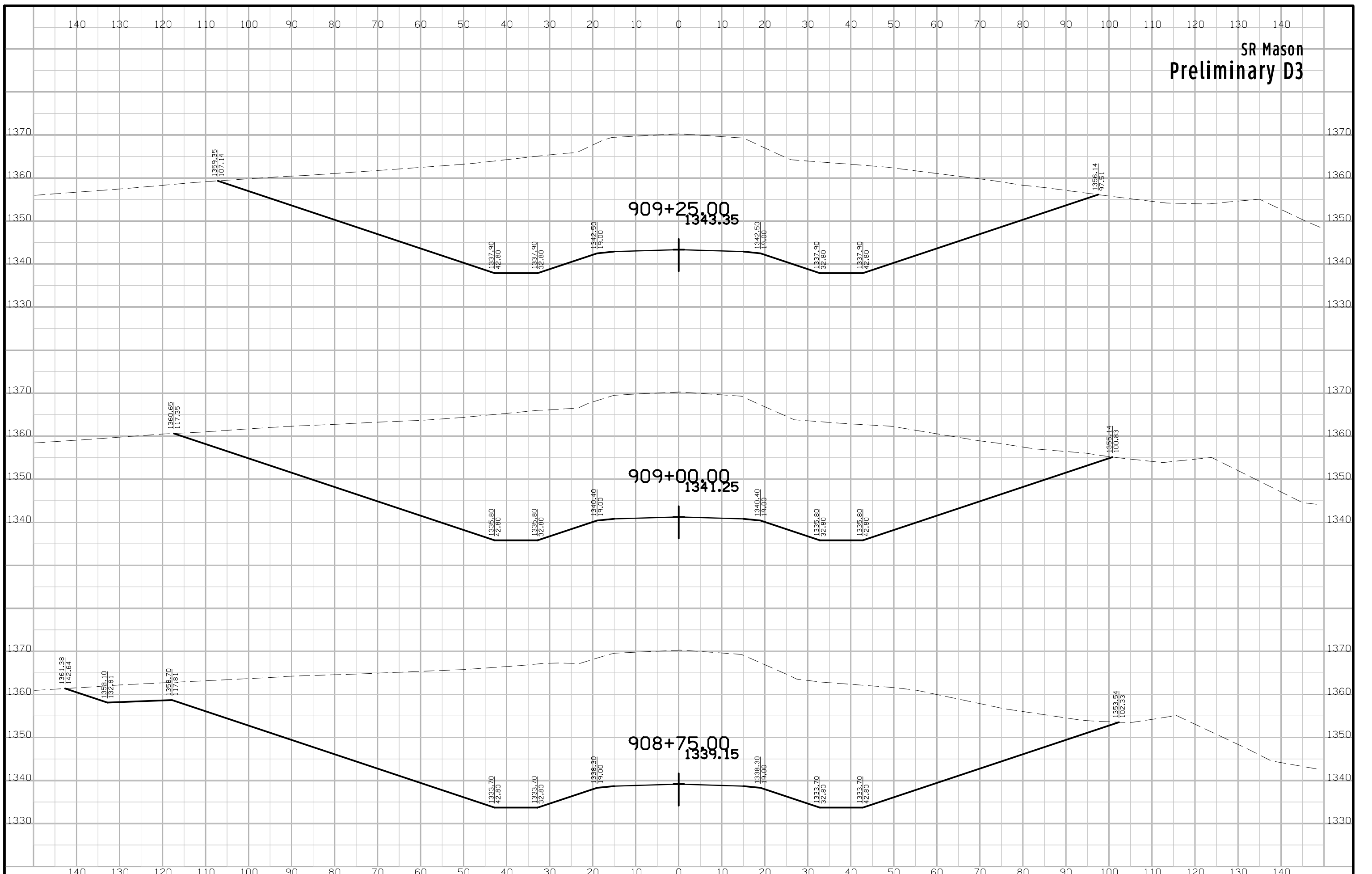
SR Mason
Preliminary D3



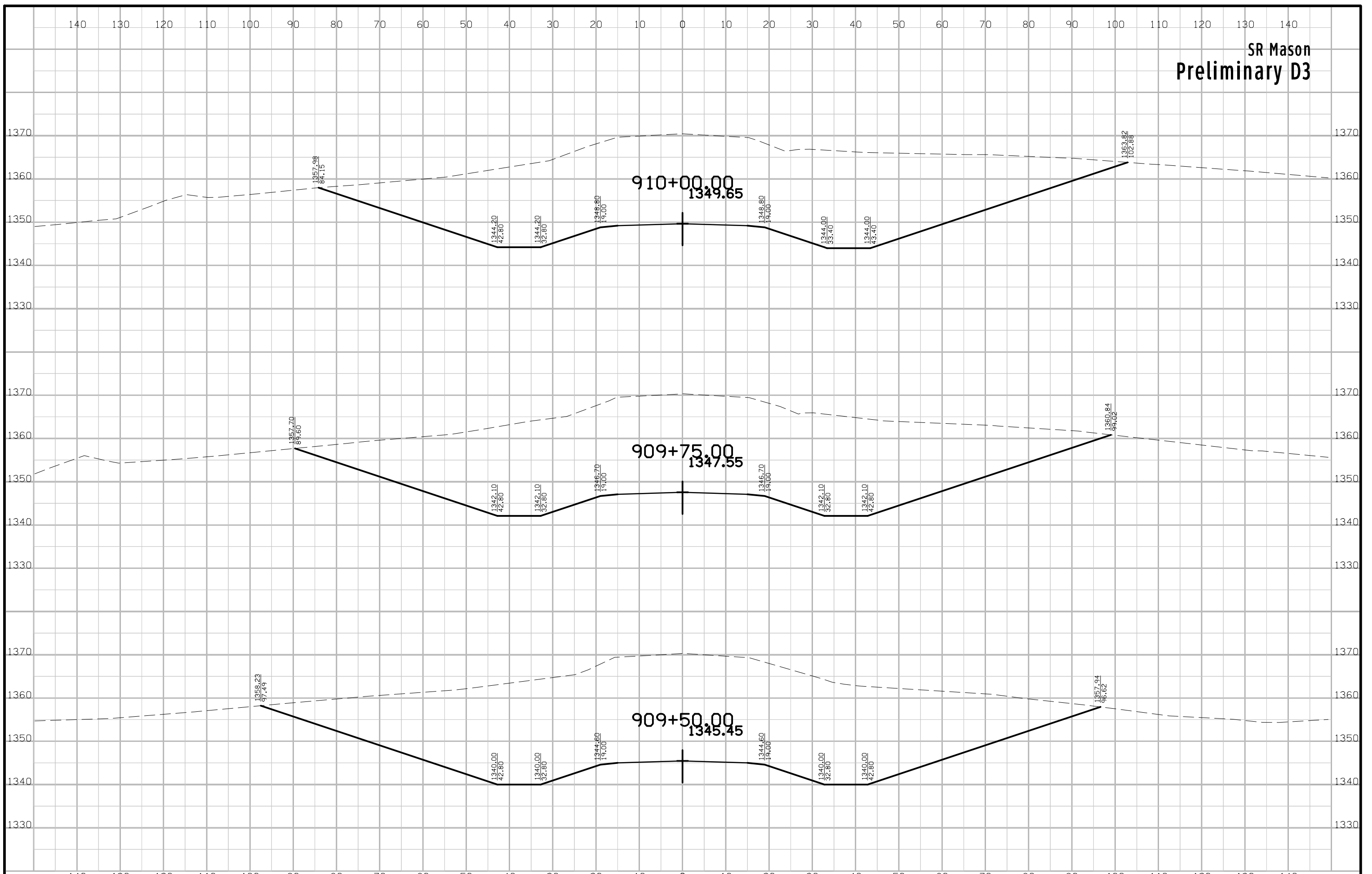
SR Mason
Preliminary D3

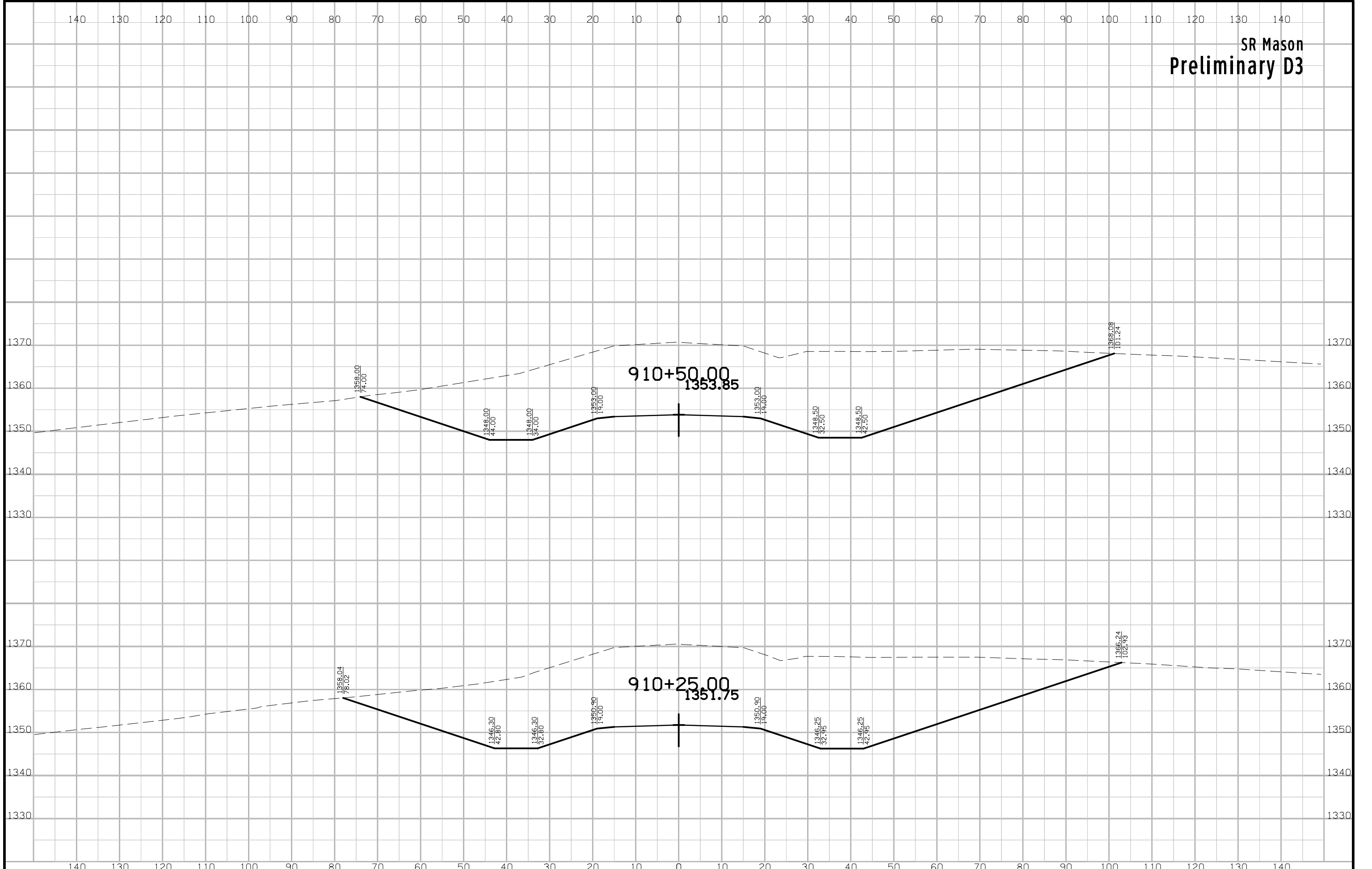


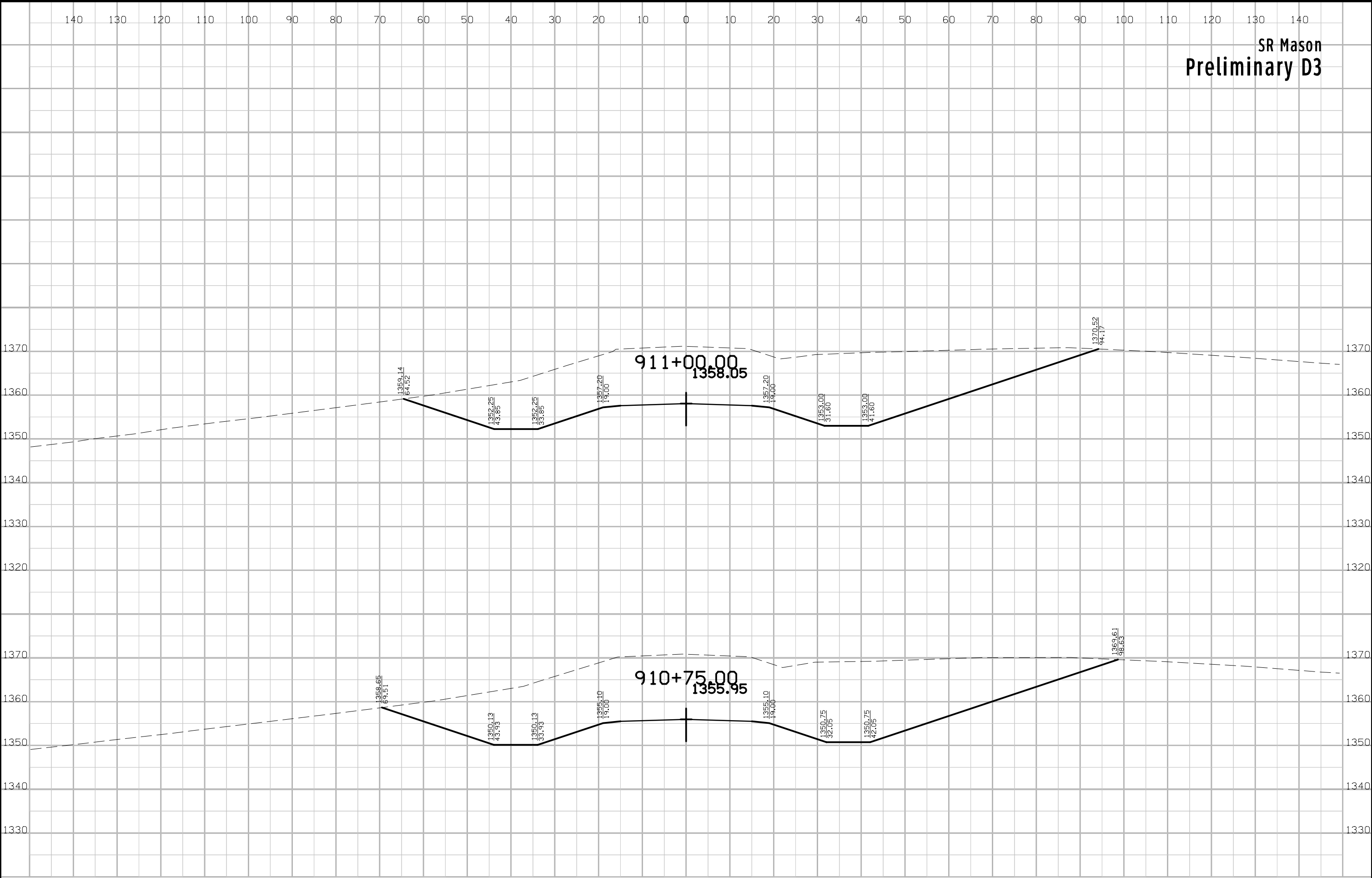
SR Mason
Preliminary D3



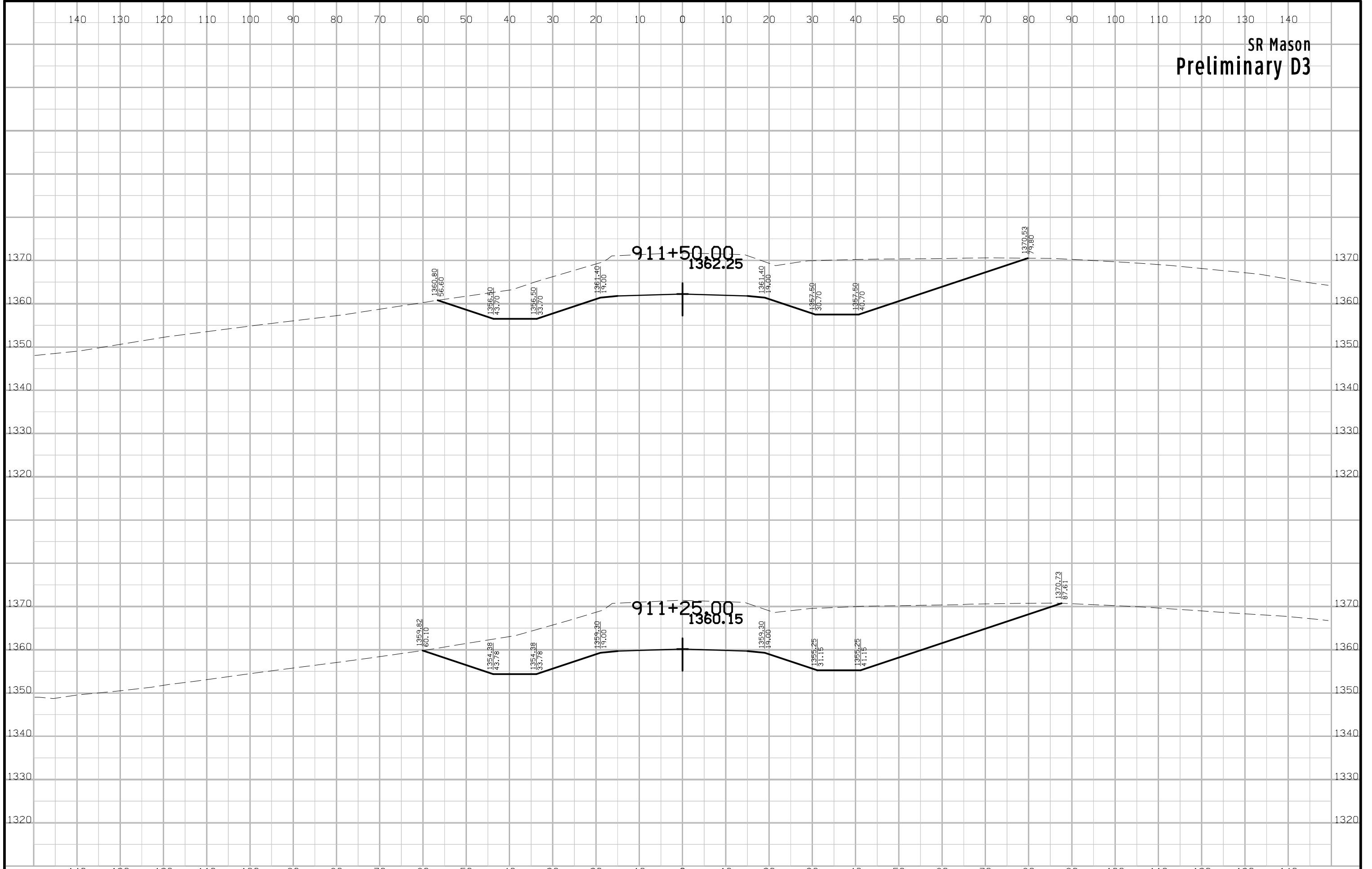
SR Mason
Preliminary D3



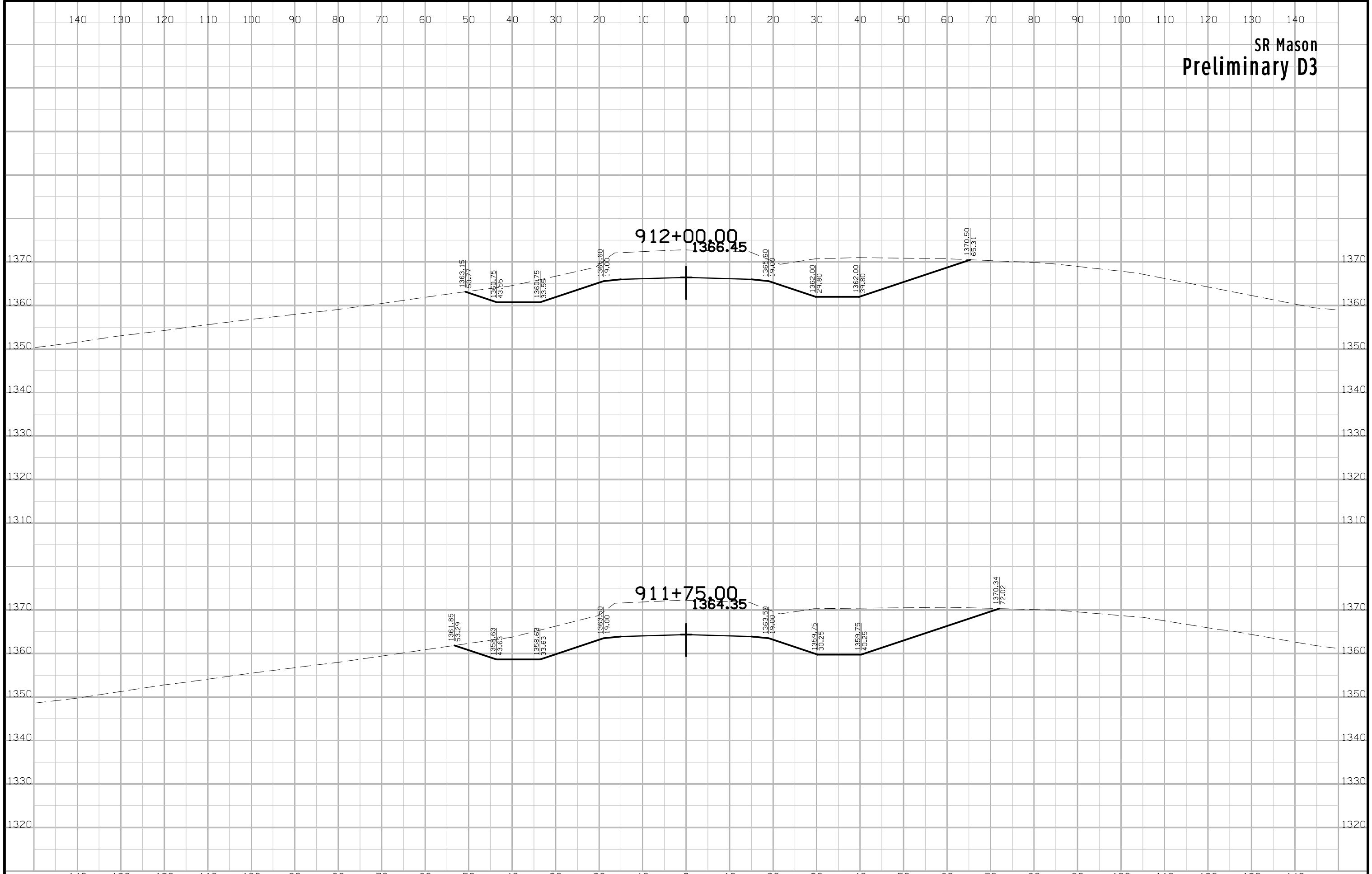




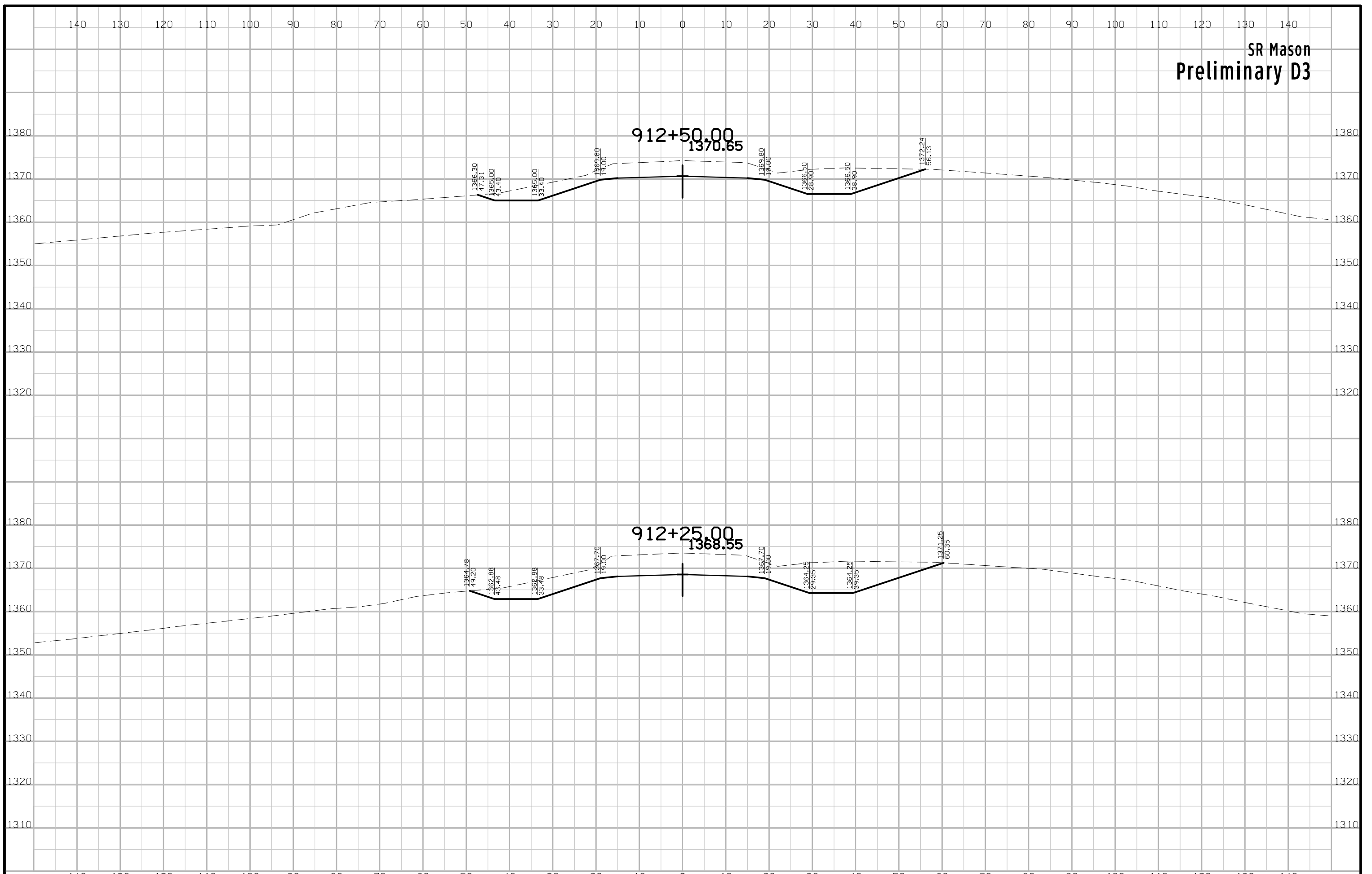
SR Mason
Preliminary D3

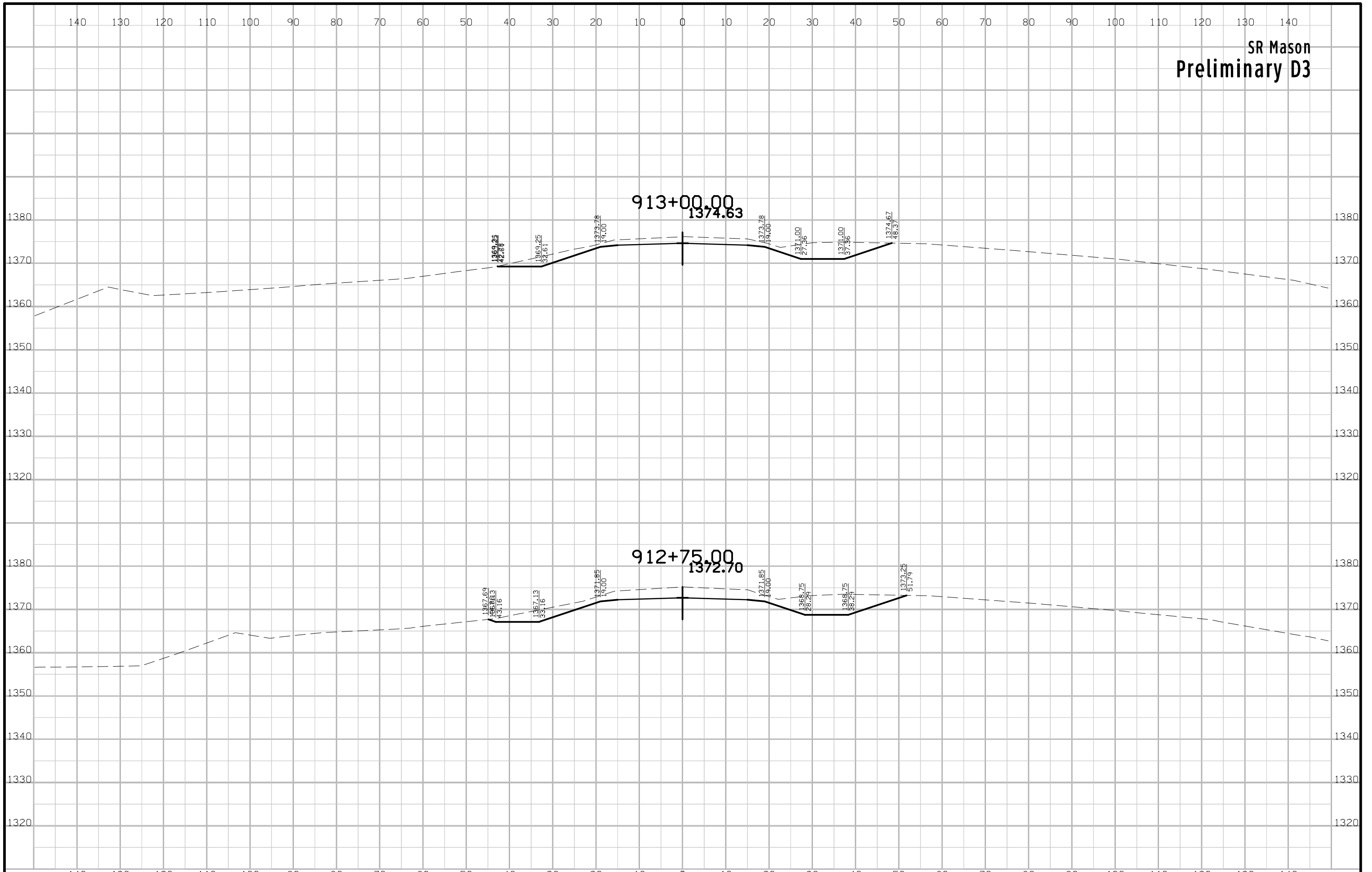


SR Mason
Preliminary D3

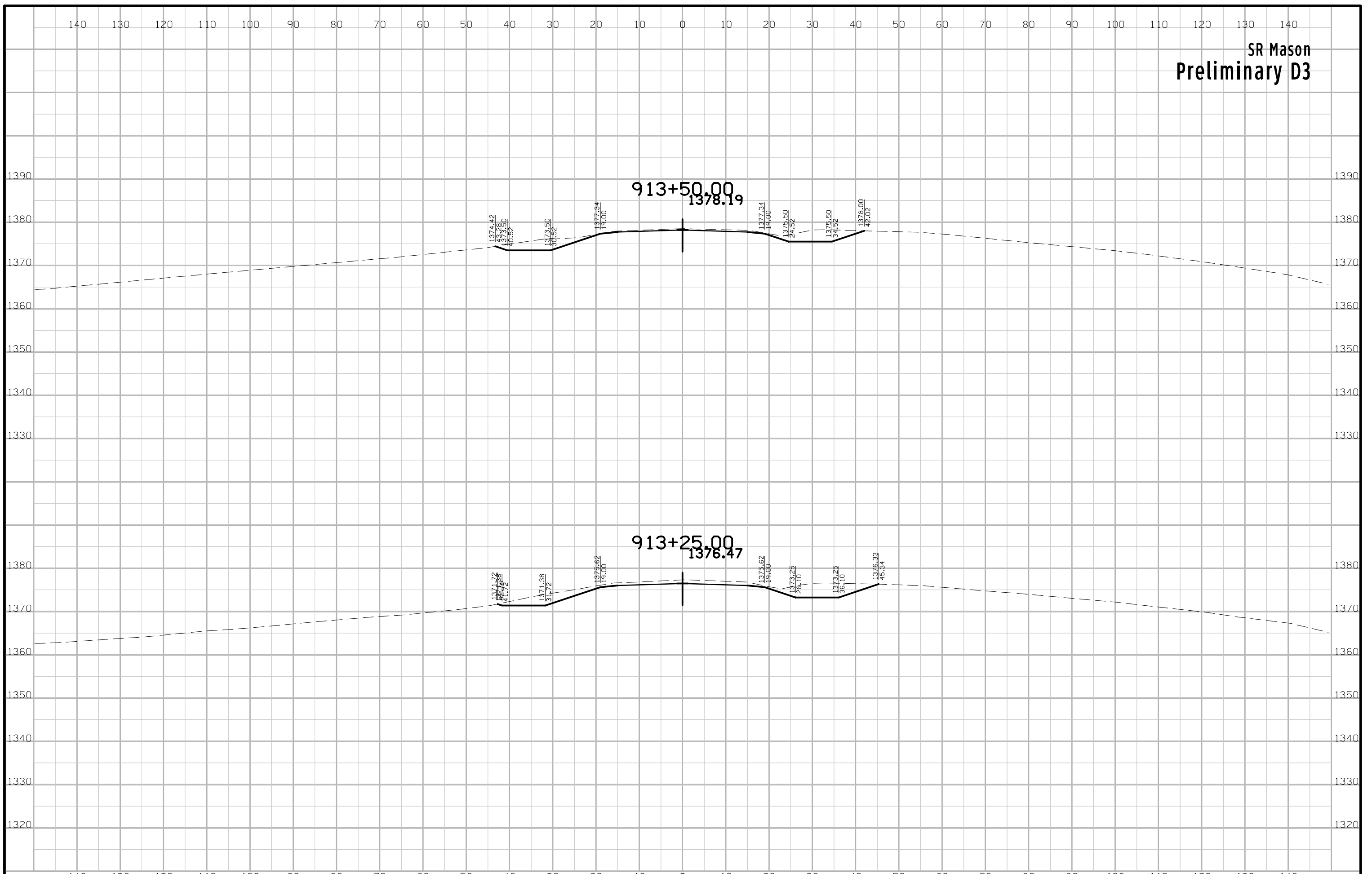


SR Mason
Preliminary D3

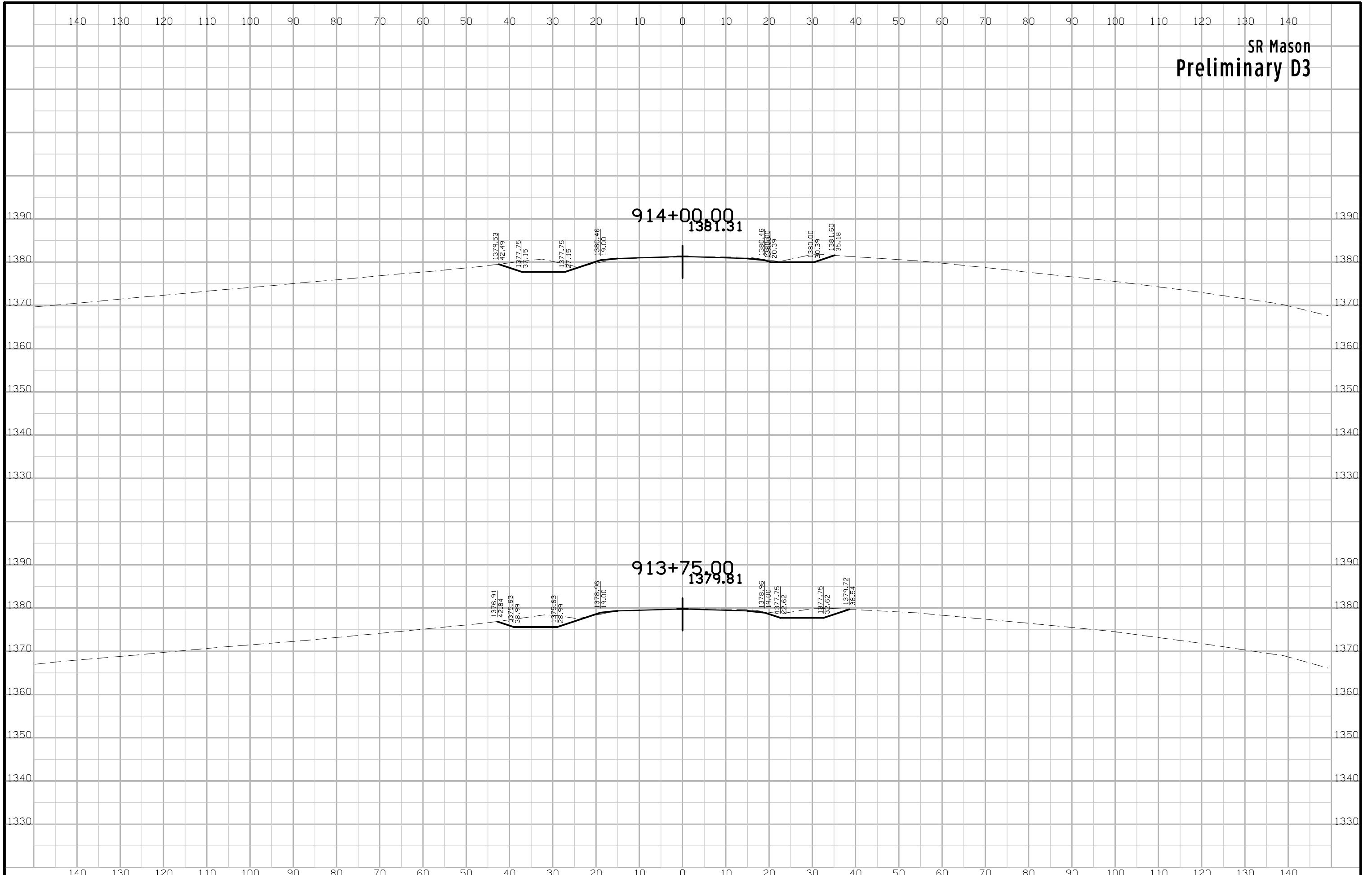




SR Mason
Preliminary D3



SR Mason
Preliminary D3



SR Mason
Preliminary D3

